

UNITED STATES ENVIRONMENTAL PROTECTION AGENCY WASHINGTON, D.C. 20460

MAY - 5 2017

OFFICE OF SOLID WASTE AND EMERGENCY RESPONSE

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MEMORANDUM

SUBJECT: Release of Standard Operating Procedure for an In Vitro Bioaccessibility Assay for Lead and Arsenic in Soil and Validation Assessment of the In Vitro Arsenic Bioaccessibility Assay for Predicting Relative Bioavailability of Arsenic in Soils and Soil-like Materials at Superfund Sites

Schatzi Fitz-James, Acting Director Dehata FROM: Assessment and Remediation Division Office of Superfund Remediation and Technology Innovation (OSRTI)

TO: Superfund National Program Managers, Regions 1-10

The purpose of this memorandum is to transmit the Technical Review Workgroup (TRW) for Metals and Asbestos technical documents entitled "Standard Operating Procedure for an In Vitro Bioaccessibility Assay for Lead and Arsenic in Soil" and "Validation Assessment of In Vitro Arsenic Bioaccessibility Assay for Predicting Relative Bioavailability of Arsenic in Soils and Soil-like Materials at Superfund Sites." The Standard Operating Procedure provides an update to EPA Method 1340 (Standard Operating Procedure for an In Vitro Bioaccessibility Assay for Lead in Soil, April 2012, EPA 9200.2-86) by including an assessment of arsenic bioaccessibility. The Validation Assessment Report presents the basis for the Agency's determination that the In Vitro Bioaccessibility Assay (IVBA) method has satisfied the validation and regulatory acceptance criteria for application of the method for arsenic.

EPA Method 1340 was first published as an SW-846 Method by EPA Office of Resource Conservation and Recovery in 2013 for the assessment of lead bioaccessibility as a method to calculate Relative Bioavailability (RBA) and is now regularly used at Superfund sites. Since then, the TRW has worked to incorporate the assessment of arsenic bioaccessibility into this same method. Arsenic and lead are commonly found together at Superfund sites and accurately measuring their RBA has a significant impact on the risk assessment and on the selection of soil cleanup levels. The addition of arsenic to this method allows the arsenic RBA to be measured rapidly and inexpensively. The method does not require the use or sacrifice of animals, and the reduced cost per sample allows risk assessors to obtain a more representative number of soil samples per exposure unit. Additionally, the incorporation of arsenic into the already existing method for lead means that laboratories already have experience performing the assay. These two documents can be accessed on the US EPA Superfund Website:

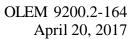
https://www.epa.gov/superfund/soil-bioavailability-superfund-sites-guidance#arsenic. Please contact Matt Lambert at lambert.matthew@epa.gov or 703-603-7174 if you have any questions or concerns.

Attachments:

- 1. "Standard Operating Procedure for an In Vitro Bioaccessibility Assay for Lead and Arsenic in Soil"
- 2. "Validation Assessment of In Vitro Arsenic Bioaccessibility Assay for Predicting Relative Bioavailability of Arsenic in Soils and Soil-like Materials at Superfund Sites."

cc:

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Standard Operating Procedure for an *In Vitro* Bioaccessibility Assay for Lead and Arsenic in Soil

1.0 SCOPE AND APPLICATION

1.1 The purpose of this standard operating procedure (SOP) is to define the proper analytical procedure for the validated in vitro bioaccessibility (IVBA) assay for lead and arsenic in soil (U.S. EPA, 2007b, 2017), to describe the typical working range and limits of the assay, quality assurance (QA), and to indicate potential interferences. The method described herein has been validated only for lead and arsenic in soil, not other contaminants or matrices (e.g., water, air, amended soils, dust, food, etc.) (U.S. EPA, 2007b, 2017).

1.2 The SOP described herein is typically applicable for the characterization of lead and arsenic bioaccessibility in contaminated soil. Users are cautioned that deviations in the method from the assay as described may impact the results and the validity of the method. Users are strongly encouraged to document and report any deviations, as well as any comparisons, with other methods and associated Quality Assurance (QA) requirements.

1.3 This document is intended to be used as a reference for developing site-specific Quality Assurance Project Plans (QAPPs) and Sampling and Analysis Plans (SAPs), but not intended to be used as a substitute for a site-specific QAPP or a detailed SAP or laboratory Standard Operating Procedure. The information contained in this method is provided by EPA as guidance for the analyst and the regulatory community to use in making judgments necessary to generate results that meet the data quality objectives for the intended application.

1.4 Mention of trade names or commercial products does not constitute endorsement or recommended use by U.S. EPA.

1.5 For additional information on method development, see method EPA SW-846-1340 (https://www.epa.gov/sites/production/files/2015-12/documents/1340.pdf) and general information on quality assurance and hazardous waste materials test methods (https://www.epa.gov/hw-sw846/quality-assurance-and-hazardous-waste-test-methods).

2.0 DEFINITIONS

2.1 Bioavailability (BA): The fraction of an ingested dose (i.e., *in vivo*) that crosses the gastrointestinal epithelium and becomes available for distribution to internal target tissues and organs.

2.2 Absolute bioavailability: Bioavailability expressed as a fraction (or percentage) of a dose.

2.3 Relative bioavailability (RBA): The ratio of the bioavailability of a metal in one exposure context (i.e., physical chemical matrix or physical chemical form of the metal) to that in another exposure context. For example, for this method, RBA is defined as the ratio of bioavailability of lead in soil to lead in water.

2.4 Bioaccessibility: An *in vitro* measure of the physiological solubility of the metal that may be available for absorption into the body.

2.5 Batch: A group of analytical and control/QC samples that are extracted simultaneously and is limited to 20 environmental samples in addition to the batch QC samples.

2.6 Phosphate-amended soil: Phosphate rich materials (e.g., fertilizers) applied to lead-contaminated soils.

2.7 Amended soil: *In-situ* remediation approach to sequester a soil contaminant for the purpose of reducing its bioavailability and transport.

2.8 In vitro: Outside the living body and in an artificial environment.

2.9 In vivo: In the living body of an animal.

3.0 BACKGROUND AND METHOD SUMMARY

3.1 Background

Reliable analysis of the potential health hazards from ingestion of lead and arsenic in the environment depends on accurate information on a number of key parameters, including (1) concentration of metal in environmental media (soil, dust, water, food, air, etc.), (2) intake rates of each medium, and (3) the rate and extent of absorption of lead or arsenic (i.e., "bioavailability") from each medium. Knowledge of bioavailability is important because the amount of lead or arsenic that actually enters the blood and body tissues from an ingested medium depends on the physical-chemical properties of both the contaminants and the medium. For example, lead in soil may exist, at least in part, as poorly water-soluble minerals, and may also exist inside particles of inert matrices such as rock or slag of variable size, shape, and association. These chemical and physical properties may tend to influence (usually decrease) the bioavailability of lead when ingested. Thus, equal ingested amounts of different forms of lead in different media may not be of equal health concern.

Since solubilization is usually required for absorption across membranes, poorly soluble forms of metals, with low bioaccessibility, may also have low bioavailability. In certain circumstances, if solubility is the major determinant of absorption at the portal of entry, bioaccessibility may be a predictor of bioavailability. Lead is an example of this, as is further discussed in U.S. EPA (2007b).

In vitro bioaccessibility (IVBA%) =
$$\frac{C_{ext} \cdot V_{ext} \cdot 100}{Soil_{conc} \cdot Soil_{mass}}$$

where:

 C_{ext} = *in vitro* extractable contaminant (i.e., lead or arsenic) in the in vitro extract (mg/L) V_{ext} = extraction solution volume (L) $Soil_{conc}$ = contaminant concentration (i.e., lead or arsenic) in the soil sample being assayed (mg/kg) $Soil_{mass}$ = mass of soil sample being assayed (kg)

The *in vitro* bioaccessibility assay described in this SOP provides a rapid and relatively inexpensive alternative to *in vivo* assays for predicting RBA of lead and arsenic in soils and soil-like materials (i.e., sediments, mining materials). The method, which measures the extent of metal solubilization in an extraction solvent that resembles gastric fluid, is based on the concept that solubilization of metals in gastrointestinal fluid is likely to be an important determinant of bioavailability *in vivo*. The IVBA is used to estimate the *in vivo* RBA. Measurements of IVBA using this assay have been shown to be a reliable predictor of *in vivo* RBA of lead and arsenic in a wide range of soil types and phases from a variety of different sites (U.S. EPA, 2007b, 2017).

3.2 Rationale for Method

Most previous *in vitro* test systems have employed more complex fluid intended to simulate gastric fluid. For example, Medlin (1997) used a fluid that contained pepsin and a mixture of citric, malic, lactic, acetic, and hydrochloric acids. When the bioaccessibility of a series of test substances were compared using 0.4M glycine buffer (pH 1.5) with and without the inclusion of the enzyme and metabolic acids, no significant difference was observed. This indicates that the simplified buffer employed in the procedure is appropriate, even though it lacks some constituents known to be present in gastric fluid.

The dissolution of a contaminant from a test material into the extraction fluid depends on a number of variables including extraction fluid composition, temperature, pH, time, agitation, and solid/fluid ratio. Additional discussion of these procedures is available in U.S. EPA (2007b) and Drexler and Brattin (2007). The following is a discussion of the reasons why the particular variables were established as they were for this IVBA method along with a few caveats:

<u>Temperature</u>. A temperature of 37°C is used because this is approximately the temperature of gastric fluid *in vivo* in humans.

<u>pH.</u> The human gastric pH values tend to range from 1 to 4 during fasting (see U.S. EPA, 2007b, Appendix A). A pH of 1.5 was selected because the highest amounts of lead and arsenic are extracted at pH 1.5, compared with higher pHs (Brattin et al., 2013; U.S. EPA, 2007b).

<u>Extraction Time.</u> The time that ingested material is present in the stomach (i.e., stomachemptying time) is about 1 hour for a child, particularly when a fasted state is assumed (see U.S. EPA, 2007a, Appendix A). Thus, an extraction time of 1 hour should be used. It was found that allowing the bottles to stand at room temperature for up to 4 hours after rotation at 37° C caused no significant variation (<10%) in lead concentration (U.S. EPA, 2007b).

<u>Agitation.</u> If the test material is allowed to accumulate at the bottom of the extraction apparatus, the effective surface area of contact between extraction fluid and the test material may be reduced, which may influence the extent of contaminant solubilization. Depending on which theory of dissolution is relevant (Nernst and Brunner, 1904 or Dankwerts, 1951), agitation will greatly affect either the diffusion layer thickness or the rate of production of fresh surface. Previous workers have noted problems associated with both stirring and argon bubbling methods (Medlin, 1997). Although no systematic comparison of agitation methods was performed, an end-over-end method of agitation is recommended.

<u>Soil/Fluid Ratio and Mass of Test Material.</u> A solid-to-fluid ratio of 1/100 (mass per unit volume) should be used to reduce the effects of metal dissolution when lower ratios (1/5 and 1/25) are used. Tests using NIST Standard Reference Material (SRM) 2710 showed no significant variation (within \pm 1% of control means) in the fraction of lead extracted with soil masses as low as 0.2 g per 100 mL (U.S. EPA, 2007b). However, use of low masses of test material could introduce variability due to small scale heterogeneity in the sample and/or to weighing errors. Therefore, the final method employs 1.0 g of test material in 100 mL of extraction fluid.

In special cases, the mass of test material may need to be <1.0 g to avoid the potential for saturation of the extraction solution. Tests performed using lead acetate, lead oxide, and lead carbonate indicate that if the bulk concentration of a test material containing these relatively soluble forms of lead exceed approximately 50,000 ppm, the extraction fluid becomes saturated at 37°C and, upon cooling to room temperature and below, lead chloride crystals will precipitate. To prevent precipitation this from occurring, the concentration of lead in the test material should not exceed 50,000 ppm, or the mass of the test material should be reduced to 0.50 ± 0.01 g (U.S. EPA, 2007b). The IVBA extraction has been conducted on soils with arsenic concentrations up to 13,000 ppm (Juhasz et al., 2007). However, studies to determine if the extraction fluid becomes saturated at soil arsenic concentrations >13,000 ppm have not been conducted.

3.3 Summary of Method

After drying and sieving to $150 \,\mu\text{m}$, 1 g of soil sample is rotated with 100 mL (0.1 L) of 0.4 M glycine buffered extraction fluid (pH 1.50) at 37°C for 1 hour. The supernatant is separated from the sample by filtration and analyzed for lead and/or arsenic by an appropriate analytical method (e.g., Method 6010 and Method 6020).

4.0 INTERFERENCES

4.1 Solvents, reagents, glassware, and other sample processing hardware may yield artifacts and/or interferences during sample analysis. All of these materials must be demonstrated to be free from interferences under the conditions of the analysis by analyzing method blanks. Specific selection of reagents may be necessary.

4.2 While the predictive relationship between IVBA and RBA for lead and arsenic has been shown to be applicable to the variety of soil types, anthropogenic sources (e.g., mining operations, orchards), and elemental forms (U.S. EPA, 2007b, 2017), the bioavailability of contaminated soil is influenced by a variety of site-specific considerations and there are limitations when applying both the *in vivo* and *in vitro* assays (U.S. EPA, 2007b). As such, it is essential to identify IVBA samples containing unusual and/or untested forms of either lead or arsenic as potential sources of uncertainty. These samples will help to inform future research to better understand limits on applicability of the methods outlined in this SOP.

4.3 Excess phosphate in the sample medium may result in interference for the measurement of lead. IVBA results for phosphate-treated soils have not been shown to correlate with extraction results from juvenile swine *in vivo* assays (Scheckel et al., 2013). As a result, the methodology discussed in this SOP is not suited for lead in phosphate-amended soils. The role of phosphate on arsenic IVBA and RBA is not clear; however, phosphate amendments should be avoided in arsenic contaminated soils to avoid unintended transport. The impact of other soil amendments (i.e., iron-based or organic [compost] amendments) have not been fully examined to determine if they influence IVBA results relative to *in vivo* data.

4.4 It is not recommended to analyze lead IVBA for soils exceeding a total lead concentration of 50,000 ppm in order to avoid saturation of the extraction fluid, and because risk management decisions are not likely to be improved by analyzing IVBA for soil with concentrations of lead above this level.

4.5 The IVBA extraction for arsenic has been conducted on soils with arsenic concentrations up to 13,000 ppm (Juhasz et al., 2007). However, users should be cautioned that studies to determine if the extraction fluid becomes saturated at soil arsenic concentrations >13,000 ppm have not been conducted.

4.6 Additional information on interferences and potential problems are discussed further in Section 11.

5.0 SAFETY

This method does not address all safety issues associated with its use. The laboratory is responsible for maintaining a safe work environment and a current awareness file of Occupational Safety and Health Administration (OSHA) regulations regarding the safe handling of the

chemicals specified in this method. A reference file of material safety data sheets (MSDSs) should be available to all personnel involved in these analyses.

6.0 EQUIPMENT AND SUPPLIES

This method recommends the use of a water bath (Section 6.1) or an incubated air chamber (Section 6.2).

A statistical comparison (t-test) was made between the NIST SRM data for lead derived from IVBA extractions that were performed by laboratories employing air (incubator type) as the temperature controlling $(37 \pm 2^{\circ}C)$ medium, versus water (aquarium type water bath). The comparison showed that, for this set of results, there was no statistical difference between the two (2) techniques of controlling the temperature of sample bottles during the extraction.

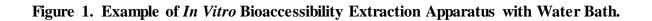
Additional testing to confirm these results was conducted by EPA's NERL and included four *in vitro* scenarios using NIST SRM 2710a (n = 27 for each scenario):

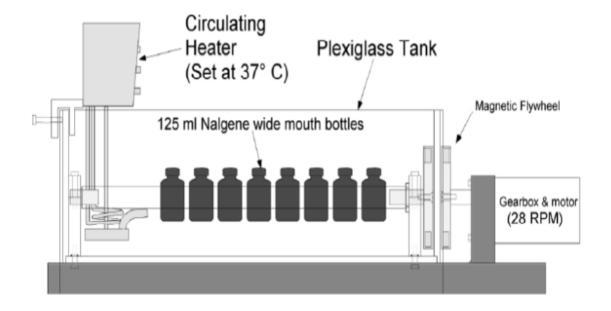
- 1. Water bath + preheated gastric solution
- 2. Water bath + room temperature gastric solution
- 3. Air incubator + preheated gastric solution
- 4. Air incubator + room temperature gastric solution

Results of the t-tests indicate that there was no statistically significant difference in observed mean Pb IVBA values for NIST 2710a SRM between scenarios 1 and 2; 1 and 3; and 2 and 3. The mean Pb IVBA value from scenario 4 (air temperature controlled, gastric solution not- preheated) was slightly lower. Therefore, the mean Pb IVBA value for scenario 4 was statistically different from the other three scenarios (Nelson et al., 2013).

6.1 Water Bath

If the water bath option is used, the specific extraction device is an electric motor (the same motor as is used in the toxicity characteristic leaching procedure (TCLP, Method 1311) driven flywheel, which drives a rotating block situated inside a temperature-controlled water bath (See Figure 1). The extraction device must be capable of holding a capped 125-mL wide-mouth high density polyethylene (HDPE) bottle. The water bath should be filled such that the extraction bottles are completely immersed. Temperature in the water bath should be maintained at $37 \pm 2^{\circ}$ C using an immersion circulator heater, and the water bath temperature should be monitored and recorded. The electric motor must be capable of 30 ± 2 rpm.





6.2 Incubated Air Chamber

If the air incubator option is used, the specific extraction device will rotate the extraction bottles within an incubated air chamber. It must be capable of rotating at 30 ± 2 rpm and designed to hold capped 125-mL wide-mouth HDPE bottles (see Figure 2 for an example of an extraction device in an incubated air chamber). The incubator must be capable of maintaining $37 \pm 2^{\circ}$ C. The temperature inside the incubator should be monitored and recorded.

Figure 2. Example of *In Vitro* Bioaccessibility Extraction Apparatus with Air Incubator.



6.3 HDPE bottles, 125 mL in size, equipped with airtight screw-cap seals should be used. Care should be taken to ensure that the bottles do not leak and to minimize contamination during the extraction procedure.

6.4 Automated temperature compensation (ATC) pH electrode – used for measuring the pH of the extraction fluid both prior to and after the experiment

7.0 REAGENTS AND STANDARDS

7.1 Reagent grade chemicals, at a minimum, should be used in all tests. Unless otherwise indicated, all reagents should conform to the specifications of the Committee on Analytical Reagents of the American Chemical Society (ACS), where such specifications are available. Other grades may be used, provided the reagent is of sufficiently high purity to permit its use without lessening the accuracy of the determination.

7.2 All reagents shall be free of lead and arsenic. For lead, the final extraction fluid shall be tested to confirm that lead concentrations are $<\frac{1}{4}$ (<one-fourth) of the project-required detection limit (PRDL) of 100 µg/L (i.e., less than 25 µg/L lead in the unprocessed reagent blank). For arsenic, the final extraction fluid shall be tested to confirm that arsenic

concentrations are $<\frac{1}{4}$ (<one-fourth) of the project-required detection limit (PRDL) of 100 µg/L (i.e., less than 25 µg/L arsenic in the unprocessed reagent blank).

7.3 Reagent water must be interference free. All references to water in this method refer to reagent water, unless otherwise specified.

7.4 Cleanliness of all materials used to prepare and/or store the extraction fluid and buffer is essential. All glassware and equipment used to prepare standards and reagents shall be properly cleaned, acid washed, and triple-rinsed with deionized water prior to use.

7.5 Extraction fluid – 0.4 M glycine (free base, reagent-grade glycine in deionized water), adjusted to a pH of 1.50 ± 0.05 at 37°C using trace metal-grade concentrated hydrochloric acid (HCl).

7.5.1 Prepare 2 liters (L) of extraction fluid in a volumetric flask (Class A) using American Society for Testing and Materials (ASTM) Type II deionized (DI) water. Record within two significant digits the weight of glycine using an analytical balance and measure 1.9 L of deionized water ± 1 mL in a pre-acid washed flask. Add 60.06 \pm 0.05 grams of glycine (free base) to a flask containing 1.9 L of deionized water. Glycine should be weighed using an analytical balance calibrated daily according to the manufacturer's instructions. Solution can be transferred to a wide-mouth HDPE bottle for ease of handling. Place the HDPE bottle containing the extraction fluid in a water bath at 37°C and heat until the extraction fluid reaches 37°C. Standardize the pH meter using an ATC pH electrode at 37°C or pH buffers maintained at 37°C in the water bath. Add trace metal-grade concentrated HCl (12.1 N) until the solution pH reaches 1.50 \pm 0.05. Bring the solution to a final volume of 2 L (0.4 M glycine).

7.5.2 If the extraction fluid is prepared in advance of the extraction, the extraction fluid must be heated to 37° C and the pH shall be adjusted to 1.5 using trace metal grade concentrated HCl prior to conducting the extraction batch.

8.0 SOIL SAMPLE PREPARATION, PRESERVATION, AND STORAGE

8.1 All test soils should be prepared by drying ($<40^{\circ}$ C) and sieving to $<150 \,\mu$ m. The $<150 \,\mu$ m size fraction was used because this particle size is representative of that which adheres to children's hands (U.S. EPA, 2016). Stainless steel sieves are recommended. Samples should be thoroughly mixed prior to use to ensure homogenization. Mixing and aliquoting of samples using a riffle splitter is recommended. Clean HDPE storage bottles are recommended.

8.2 To perform this assay, soil standards and test soils should be weighed using an analytical balance calibrated daily according to the manufacturer's instructions. Soil samples should be weighed to *four significant digits* (i.e., the nearest 0.0001 gram).

8.3 All samples should be archived after analysis and retained for further analysis for a period of six (6) months. No preservatives or special storage conditions are required.

9.0 QUALITY ASSURANCE/QUALITY CONTROL

Each laboratory should maintain a formal QA program. The laboratory should also maintain records to document the quality of the data generated. Development of in-house QC limits for each method is encouraged. Use of instrument-specific QC limits is encouraged, provided such limits will generate data appropriate for use in the intended application. All data sheets and QC data should be maintained for reference or inspection. The information contained in this method is provided by EPA as guidance to be used by the analyst and the regulatory community in making judgments necessary to generate results that meet the DQOs for the intended application.

9.1 Initial demonstration of proficiency (IDP)

Each laboratory must demonstrate initial proficiency by generating data of acceptable precision and bias for target analytes in a clean matrix. It is recommended that the laboratory repeat the demonstration of proficiency whenever new staff members are trained or significant changes in instrumentation and/or procedures are made.

9.2 Quality assurance for the extraction procedure are as follows (summarized in Table 1 for lead and Table 2 for arsenic):

9.2.1 Reagent blank: Unprocessed (not run through the extraction procedure) extraction fluid should be analyzed for each new batch of extraction fluid. The reagent blank is considered within control limits if its result is less than the lower limit of quantitation (LLOQ). The corrective action for a blank hit above LLOQ should include preparing a new batch of extraction fluid and reprocessing any samples that were prepared with the failing reagent fluid. The reagent blank should be run at a frequency of 1 in 20 samples (minimum of one per batch).

9.2.2 Method blank: Extraction fluid only (i.e., no test soil) is carried through all steps of the method at a frequency of 1 in 20 samples (minimum of 1 per batch). The method blank is considered within control limits if its result is less than the LLOQ. The corrective action for a recovery above the LLOQ should include making a new extraction fluid and reprocessing any samples that were prepared with the failing method blank.

9.2.3 Laboratory Control Sample (LCS): A LCS consisting of a spiked blank should be run once per batch (minimum 1 in 20 samples). The LCS may be spiked with the same source as the calibration standards and needs to be carried through all steps of the rotation procedure. The extraction fluid should be spiked at either 10 mg/L lead or 10 mg/L arsenic. The control limits are 85–115% recovery. The corrective action for outliers should include an analyst review that all dilutions and spike concentrations were performed correctly. If no error is found, either re-extract the samples or flag and narrate the defect and possible bias in the data.

9.2.4 Matrix Spike (MS): A MS should be run once per batch (minimum 1 in 20 samples). The MS should be prepared after extraction and filtration of the supernatant. The matrix spike should be prepared at either 10 mg/L lead and/or 10 mg/L arsenic. The control limits are 75–125% recovery. The corrective action for outliers should include an analyst review that all dilutions and spike concentrations were performed correctly. If no error is found, either re-extract the samples or flag and narrate the defect and possible bias in the data.

9.2.5 Duplicate sample: A duplicate sample should be run once per batch (minimum 1 in 20 samples) and carried through all steps of the method. The relative percent difference (RPD) should be less than 20%. The corrective action for outliers should include either re-extraction of the samples or flagging the data.

9.2.6 Control soils for Lead: The National Institute of Standards and Testing (NIST) standard reference materials (SRMs) 2710a or 2711a (Montana Soil) can be used as control soils. The reference material shall be carried through all steps of the method and analyzed at a frequency of 1 in 20 samples (minimum of 1 per batch). The IVBA is calculated using the equation shown in Section 12.1.

9.2.6.1 NIST SRM 2710a: Analysis of the NIST SRM 2710a for lead should yield a mean IVBA result of 67.5%, with an acceptable range of 60.7-74.2%. The IVBA result in terms of mg/kg should be 3,440 mg/kg, with a range of 3,096–3,785 mg/kg (Shaw Environmental, Inc., 2011). For the lead concentration (Pb_{soil}) in the SRM, the median lead concentration presented in the Addendum to the NIST certificate for leachable concentrations determined using Method 3050 (5,100 mg/kg) should be used (NIST, 2009a).

9.2.6.2 NIST SRM 2711a: Analysis of the NIST SRM 2711a for lead should yield a mean IVBA result of 85.7%, with an acceptable IVBA range of 75.2–96.2%. The IVBA result in terms of mg/kg should be 1,114 mg/kg, with a range of 980–1,249 mg/kg (Shaw Environmental, Inc., 2011). For the lead concentration (Pb_{soil}) in the SRM, the median lead concentration presented in the Addendum to the NIST certificate for leachable concentrations determined using Method 3050 (1,300 mg/kg) should be used (NIST, 2009b).

9.2.7 Control soils for Arsenic

<u>Note</u>: NIST SRM 2711a is not an appropriate control soil for the IVBA assay for arsenic due to the low arsenic concentration.

9.2.7.1 NIST SRM 2710a: Analysis of the NIST SRM 2710a for arsenic should yield a mean IVBA result of 41.0%, with an acceptable IVBA range 32.9–49.1% (Appendix B). For the arsenic concentration (As_{soil}) in NIST 2710a, the median lead concentration presented in the Addendum to the

NIST certificate for leachable concentrations determined using Method 3050 (1,400 mg/kg) should be used (NIST, 2009a).

9.3 Lower limit of quantitation check standard

9.3.1 The laboratory should establish the LLOQ as the lowest point of quantitation which, in most cases, is the lowest concentration in the calibration curve. The LLOQ should be verified by the analysis of at least seven (7) replicate samples, which are spiked at the LLOQ and processed through all preparation and analysis steps of the method. The mean recovery and relative standard deviation of these samples provide an initial statement of precision and accuracy at the LLOQ. In most cases, the mean recovery should be $\pm 35\%$ of the true value and the RSD should be $\leq 20\%$. In-house limits may be calculated when sufficient data points exist. The monitoring of recovery data for the LLOQ check standard over time is useful for assessing precision and bias. Refer to a scientifically valid and published method (such as Chapter 9 of *Quality Assurance of Chemical Measurements* [Taylor, 1987] or the Report of the Federal Advisory Committee on Detection and Quantitation Approaches and Uses in Clean Water Act Programs [http://water.epa.gov/scitech/methods/cwa/det/index.cfm]) for calculating precision and bias for LLOQ.

9.3.2 Ongoing LLOQ verification, at a minimum, is carried out on a quarterly basis to validate quantitation capability at low analyte concentration levels. This verification may be accomplished either with clean control material (e.g., reagent water, method blanks, Ottawa sand, diatomaceous earth, etc.) or a representative sample matrix (free of target compounds). Optimally, the LLOQ should be less than or equal to the desired regulatory action levels based on the stated project-specific requirements.

Analysis	Frequency	Control Limits	Corrective Action
Reagent blank	once per batch (minimum 1 in 20 samples)	<25 µg/L lead	Make new extraction fluid and rerun all analyses.
Method blank	once per batch (minimum 1 in 20 samples)	<50 μg/L lead	Make new extraction fluid and rerun all analyses.
LCS (10 mg/L)	once per batch (minimum 1 in 20 samples)	85–115% recovery	Ensure dilutions and spike concentrations are correct. If no error is found, re-extract the samples or flag the data.
Matrix spike (10 mg/L)	once per batch (minimum 1 in 10 samples)	75–125% recovery	Ensure dilutions and spike concentrations are correct. If no error is found, re-extract the samples or flag the data.
Duplicate sample	once per batch (minimum 1 in 10 samples)	±20% RPD	Re-extract the samples or flag the data.
Control soil (NIST SRMs 2710a and 2711a)	once per batch (minimum 1 in 20 samples)	NIST 2710a mean 67.5% (acceptable range: 60.7–74.2%) NIST 2711a mean 85.7% (acceptable range: 75.2–96.2%)	Re-extract the samples or flag the data.

 Table 1. Recommended Control Limits for Quality Control Samples: Lead

RPD, Relative percent difference

Analysis	Frequency	Control Limits	Corrective Action
Reagent blank	once per batch (minimum 1 in 20 samples)	<25 µg/L arsenic	Make new extraction fluid and rerun all analyses.
Method blank	once per batch (minimum 1 in 20 samples)	<50 μg/L arsenic	Make new extraction fluid and rerun all analyses.
LCS (10 mg/L)	once per batch (minimum 1 in 20 samples)	85–115 % recovery	Ensure dilutions and spike concentrations are correct. If no error is found, re-extract the samples or flag the data.
Matrix spike (10 mg/L)	once per batch (minimum 1 in 10 samples)	75–125% recovery	Ensure dilutions and spike concentrations are correct. If no error is found, re-extract the samples or flag the data.
Duplicate sample	once per batch (minimum 1 in 10 samples)	±20% RPD	Re-extract the samples or flag the data.
Control soil (NIST 2710a)	once per batch (minimum 1 in 20 samples)	NIST 2710a mean 41.0% (acceptable range: 32.9–49.1%)	Re-extract the samples or flag the data.

Table 2. Recommended Control Limits for Quality Control Samples: Arsenic

RPD, Relative percent difference

10.0 CALIBRATION AND STANDARDIZATION

10.1 An automated temperature compensation (ATC) pH electrode shall be used for measuring the pH of the extraction fluid prior and post experiment. Each instrument/ electrode system must be calibrated at a minimum of two points that bracket the expected pH (1.5) of the samples and are approximately two pH units or more apart. Repeat adjustments on successive portions of the two buffer solutions until readings are within 0.05 pH units of the buffer solution value as indicated in SW-846 method 9045D for Soil and Waste pH (<u>http://www.epa.gov/osw/hazard/testmethods/sw846/pdfs/9045d.pdf</u>). The pH meter should be calibrated and checked with standard solutions within the calibration range (e.g., pH = 1 and 2) according to the manufacturer's instructions. After calibration, the meter is ready to analyze samples.

10.2 Thermometers capable of measuring $37 \pm 2^{\circ}C$ are needed.

10.3 The analytical balance should be calibrated daily in accordance with the manufacturer's instructions.

10.4 Pipettes should be calibrated in accordance with the manufacturer's instructions and the laboratory QA plan.

11.0 PROCEDURE

11.1 The extraction fluid for this procedure is 0.4 M glycine (free base, reagent grade glycine in deionized water), adjusted to a pH of 1.50 ± 0.05 at $37 \pm 2^{\circ}$ C using trace metal grade concentrated hydrochloric acid (HCl). See Section 7.5 for extraction fluid preparation details.

11.2 Pre-heat the TCLP extractor water bath OR incubator (See Section 6.0) to 37°C. Record the temperature at the beginning and end of each extraction batch (an example of an extraction data recording form is provided in Appendix A).

11.3 Soil samples should be thoroughly mixed immediately prior to removing aliquots for extraction to ensure homogenization (i.e., rotate sample bottles using X, Y, Z motion).

11.4 The extraction procedure is begun by placing 1.00 ± 0.05 g of sieved test material (<150 µm; U.S. EPA, 2016) into a 125-mL wide-mouth HDPE bottle. **Record weight of soil to** *four significant digits* (i.e., the nearest 0.0001 gram). Care should be taken to ensure that static electricity does not cause soil particles to adhere to the lip or outside threads of the bottle; if necessary, an antistatic brush should be used to eliminate static electricity prior to adding the test substrate.

11.5 Measure 100 ± 0.5 mL of the $37 \pm 2^{\circ}$ C buffered extraction fluid (0.4 M glycine, pH 1.5), using a graduated cylinder or automated dispenser, and transfer extraction fluid to the 125-mL wide-mouth HDPE bottle.

11.6 The bottle should be tightly sealed and then shaken or inverted to ensure that there is no leakage and that no soil is caked on the bottom of the bottle.

11.7 Fill the extractor (TCLP extractor OR rotating extractor inside of a pre-heated incubator, see Section 6.0 for details) with 125-mL bottles containing test materials or Quality Control samples (see Section 7.0). Record start time of rotation.

<u>NOTE</u>: Care should be taken to prevent contamination of the samples during rotation (e.g., getting bath water in the threads around the cap and possibly into the sample when the cap is removed). Precautions that laboratories may consider include but are not limited to: the type of bottle that is used, sealing the samples in plastic freezer bags with air expelled before installing in the water bath extractor, and/or sealing the bottles with tape or Parafilm[®].

11.8 Samples are extracted by rotating the samples at 30 ± 2 rpm for 1 hour.

11.9 After 1 hour, the bottles should be removed from the rotator, dried, and placed upright on the bench top to allow the soil to settle to the bottom.

11.10 A 40-mL sample of supernatant fluid is then removed directly from the extraction bottle into a disposable syringe. After withdrawal of the sample into the syringe, a Luer-Lok attachment fitted with a 0.45- μ m cellulose acetate disk filter (25 mm diameter) is

attached, and the 15 mL aliquot of fluid is filtered through the attachment to remove any particulate matter into a pre-acid washed polypropylene centrifuge tube or other appropriate sample vial for analysis.

11.11 Record the time that the extract is filtered (i.e., extraction is stopped). If the total time elapsed for the extraction and filtration process exceeds 90 minutes, the test must be repeated (i.e., Steps 11.1-11.10).

11.12 Measure and record the pH of fluid remaining in the extraction bottle. If the fluid pH is not within ± 0.5 pH units of the starting pH, the test must be discarded and the sample re-analyzed. In some cases (mainly slag soils), the test material can increase the pH of the extraction buffer, and this could influence the results of the bioaccessibility measurement. To guard against this, the pH of the fluid should be measured at the end of the extraction step (just after a sample was withdrawn for filtration and analysis). If the pH is not within 0.5 pH units of the starting pH (1.5), the sample should be re-analyzed. If the second test also results in an increase in pH of >0.5 units, it is reasonable to conclude that the test material is buffering the solution. In these cases, the test should be repeated using manual pH adjustment during the extraction process, stopping the extraction at 5, 10, 15, and 30 minutes and manually adjusting the pH down to pH 1.5 at each interval by drop-wise addition of HCl.

11.13 Store filtered sample(s) in a refrigerator at $4 \pm 2^{\circ}$ C until they are analyzed. This filtered sample of extraction fluid is then analyzed for lead and/or arsenic by ICP-AES or ICP-MS (U.S. EPA Method 6010C or Method 6020A). For lead, the method detection limit (MDL) in extraction fluid should be approximately 20 µg/L for Method 6010 and 0.1–0.3 µg/L for Method 6020 (U.S. EPA, 2012a, b). For arsenic, the MDL in extraction fluid should be approximately 20–40 µg/L for Method 6010 and 1–5 µg/L for Method 6020.

<u>NOTE</u>: In some cases, high dissolved solids (e.g., Fe oxides) in the extracts may cause nebulizer performance issues by inductively coupled plasma-optical emission spectrometry (ICP-OES) or inductively coupled plasma-mass spectrometry (ICP-MS). If this is encountered, dilution of the extracts tenfold is recommended before analysis. Correct for any dilutions in the calculations. Alternately, a high solids nebulizer may be useful. Graphite furnace atomic absorption spectrophotometry (GFAA) should be avoided due to the high levels of HCl in the extracts.

<u>NOTE</u>: In some cases, the amount of lead present in the sample will begin to saturate the extraction fluid, and the extraction response will cease to be linear. If the concentration of lead in the extract exceeds approximately 500 mg/L (depending on the sample matrix and mineralogy), this upper limit may have been reached. It is not recommended to analyze IVBA for soils exceeding a total lead concentration of 50,000 ppm in order to avoid saturation of the extraction fluid, and because risk management decisions are not likely to be improved by analyzing IVBA for soil with concentrations of lead above this level.

11.14. Examples of an extraction record, gastric extraction fluid preparation record, and an example batch format and IVBA calculation are provided in Appendix A (Tables A1–A3).

11.15. Once received by the laboratory, all samples and extracts should be checked-in, verified, and maintained under standard chain-of-custody (e.g., U.S. EPA, 2012c).

12.0 DATA ANALYSIS AND CALCULATIONS

A split of each solid material (sieved to $<150 \mu$ m) that has been subjected to this extraction procedure should be analyzed for total lead and/or total arsenic concentration using analytical procedures taken from the U.S. EPA SW-846 (U.S. EPA, 2012d) or a non-destructive method such as Instrumental Neutron Activation Analysis. If SW-846 methods are used, the solid material should be acid digested according to SW-846 Method 3050B (December 1996 revision) or 3051A (microwave-assisted digestion, February 2007 revision), and the digestate analyzed for lead and/or arsenic concentrations determined by ICP-AES analysis (Method 6010C, February 2007 revision) or ICP-MS (Method 6020A, February 2007 revision). Note that although SW-846 Method 3050B states a hot plate is acceptable as a heating source, a hot plate should not be used; the heating source should be a block digestor.

12.1 *In vitro* bioaccessibility (IVBA) is calculated and expressed on a percentage basis using the following equation:

In vitro bioaccessibility =
$$\frac{C_{ext} \cdot V_{ext} \cdot 100}{Soil_{conc} \cdot Soil_{mass}}$$

where:

 $C_{ext} = in \ vitro \ extractable \ contaminant \ (i.e., lead/arsenic) in the in vitro$ extract (mg/L) $V_{ext} = extraction \ solution \ volume \ (L)$

Soil_{conc} = contaminant concentration (i.e., lead/arsenic) in the soil sample being assayed (mg/kg)

Soil_{mass} = mass of soil sample being assayed (kg)

12.2 In order for an *in vitro* bioaccessibility test system to be useful in predicting the *in vivo* RBA of a test material, it is necessary to empirically establish that a strong correlation exists between the *in vivo* and the *in vitro* results across many different samples. The currently preferred models for predicting RBA from IVBA for lead (U.S. EPA, 2007b) and arsenic (Diamond et al., 2016; U.S. EPA, 2017) are:

 $RBA_{lead}(\%) = 0.88 \bullet IVBA(\%) - 0.028 (R^2 = 0.92)$ $RBA_{arsenic}(\%) = 0.79 \bullet IVBA(\%) + 3.0 (R^2 = 0.87)$

where RBA and IVBA are expressed as percentages (not fractions). It is important to recognize that use of this equation to calculate RBA from a given IVBA measurement will yield the "typical" RBA value expected for a test material with that IVBA, and the true RBA may be somewhat different (either higher or lower).

12.3 If dilutions were performed, apply the appropriate corrections to the sample values.

13.0 METHOD PERFORMANCE

13.1 Method Performance for Lead. NIST SRMs 2710a and 2711a should be used as control soils for lead. The soil standard will be analyzed at a frequency of 1 in 20 samples (minimum 1 per batch). The NIST SRMs 2710a and 2711a are available from the National Institute of Standards and Technology, Standard Reference Materials Program (http://www.nist.gov/srm/). Acceptable performances of soil standards for lead are shown in Table 3. The calculations for percent Pb IVBA is shown in Section 12.1.

	Mean mg/kg	Acceptable mg/kg	Mean IVBA Result	Acceptable IVBA
Soil Standard	Result	Range	(%)	Range (%)
NIST 2710a	3,440	3,096–3,785	67.5	60.7-74.2
NIST 2711a	1.114	980-1.249	85.7	75.2-96.2

Table 3. Method Performance for Lead

13.2 Method Performance for Arsenic. NIST SRM 2710a should be used as a control soil for arsenic. The soil standard will be analyzed at a frequency of 1 in 20 samples (minimum 1 per batch). The NIST SRM 2710a is available from the National Institute of Standards and Technology, Standard Reference Materials Program (<u>http://www.nist.gov/srm/</u>). Acceptable performances of soil standards for arsenic are shown in Table 4. The calculation for percent As IVBA is shown in Section 12.1.

Soil Standard	Mean mg/kg Result	Acceptable mg/kg Range	Mean IVBA Result (%)	Acceptable IVBA Range (%)
NIST 2710a	1400	1300-1600	41.0	32.9-49.1

14.0 POLLUTION PREVENTION

14.1 Pollution prevention encompasses any technique that reduces or eliminates the quantity or toxicity of waste at the point of generation. Numerous opportunities for pollution prevention exist in laboratory operations. The EPA has established a preferred hierarchy of environmental management techniques that places pollution prevention as the management option of first choice (SW-846). Whenever feasible, laboratory personnel should use pollution prevention techniques to address their waste generation. When wastes cannot be feasibly reduced at the source, the Agency recommends recycling as the next best option.

14.2 For information about pollution prevention that may be applicable to laboratories and research institutions consult *Less is Better: Laboratory Chemical Management for Waste Reduction* available from the American Chemical Society's Department of Government Relations and Science Policy, 1155 16th Street, NW, Washington, DC 20036, http://www.acs.org.

15.0 WASTE MANAGEMENT

The Environmental Protection Agency requires that laboratory waste management practices are consistent with all applicable rules and regulations. The Agency urges laboratories to protect the air, water, and land by minimizing and controlling all releases from hoods and bench operations, complying with the letter and spirit of any sewer discharge permits and regulations, and by complying with all solid and hazardous waste regulations, particularly the hazardous waste identification rules and land disposal restrictions. For further information on waste management, consult The Waste Management Manual for Laboratory Personnel, available from the American Chemical Society's Department of Government Relations and Science Policy, 1155 16th Street, NW, Washington, DC 20036, (202) 872-4477.

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APPENDIX A

IVBA Extraction Forms and Calculation

Table A-1. Example Extraction Record

Date:									
Sample ID:									
BATCH No:									
Extraction Flu		•	· •						
Spike solution Lead and/or As					ndord odd	nd to V m	I artea ati	an colutio	
(100 mL total v				. (A IIIL OI Sta	indard adde		L extractio	on solutio	lis
	· ·	mple Prepa	1 ,			Extracti	on		
Sample ID	Bottle No.	Volume (mL)	Sample mass (g)	Agitation Time (min)	Initial pH	Final pH	Start Temp (C)	End Temp (C)	Total Time ^a (min)
Acceptable Range		100 ± 0.5	1.00 ± 0.01	60 ± 5	1.50 ± 0.5	1.50 ± 0.5	37 ± 2	37 ± 2	≤90
Method Blank	1								
LCS	2								
Control Soil	3								
Sample ID	4								
Sample ID	5								
Sample ID	6								
Sample ID	7								
Sample ID	8								
Sample ID	9								
Sample ID	10								
Sample ID	11								
Sample ID	12								
Regent blank	13								
Reagent blank i ^a Time between			•	o process.					

Sample Batch No: Date Prepared:									
Component		Fluid Pro	eparation	Actual					
•	Lot ID	1L	2L	Quantity	Comments				
Deionized water	ASTM Type II	0.95 L (approximate)	1.90 L (approximate)						
Glycine	Sigma Lot No.	$30.04\pm0.05g$	$60.08\pm0.05g$						
HCl (12.1N; Tr. Metal)	Fisher Optima	(approximate)	(approximate)						
Final Volume		1.0 L (class A)	2.0 L (class A)						
pH at 37°C		1.50 ± 0.05	1.50 ± 0.05						

Table A-2.	Gastric Extraction	Fluid	Preparation
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Table A3. Example Batch Format and IVBA Calculation

Date:		Sample ID:										
Batch N	lo.											
		ID: Glycine & HO	Cl, pH 1.5									
SRM II												
		ncentration: 10 m			1.1.4. V	τ	1	(100			1	. ??)
Lead Sp	piking Sol	ution vendor, Lo	t No. (X mL of st	1		L extractio	n solutions	(100 mL	total volum	e) labele	d as spikes	s)
Batch	Bottle			Soil	Soil	Valera	Volume	ICD (DL)		%	A	SD of
Batch #	No.	Туре	Sample ID	weight (grams)	weight (kg)	Volume (mL)	(L)	ICP (Pb) (mg/L)	(mg/kg)	70 IVBA	Avg % IVBA	SD 01 IVBA%
Insert	1	Method Blank	Method blank	n/a	n/a	100	0.1		00	n/a		
No.	2	LCS	LCS	n/a	n/a	100	0.1			n/a		
	3	Control soil	SRM 2710a	1.0019	0.00100	100	0.1	34.24	5100	67		
	4	Sample	Sample1 a	1.0016	0.00100	100	0.1	32.24	5100	63		
	5	Sample	Sample1 b	1.0006	0.00100	100	0.1	33.24	5100	65	64.1	1.4
	6	Matrix spike	Sample + spike	0.9985	0.00100	100	0.1					
	7	Sample	Sample2 a	1.0029	0.00100	100	0.1				Avg of	
	8	Sample	Sample2 b	1.0022	0.00100	100	0.1				Dups	SD
	9	Matrix spike	Sample + spike	1.0028	0.00100	100	0.1					
	10	Sample	Sample3 a	1.0004	0.00100	100	0.1				Avg of	
	11	Sample	Sample3 b	1.0029	0.00100	100	0.1				Dups	ups SD
	12	Matrix spike	Sample + spike	0.9972	0.00100	101	0.1		n/a	n/a		
	13	Reagent blank	unprocessed sample	n/a	n/a	100	0.1		n/a	n/a		

% IVBA = <u>(Concentration in IVBA extract mg/L) (0.1 L)</u> • 100 (Concentration in solid mg/kg) (weight of sample kg)

APPENDIX B

Provisional Reference Values for Arsenic IVBA of NIST 2710A Standard Reference Material

Consensus values for In Vitro Bioaccessibility (IVBA) of arsenic in soil reference materials (RM) are needed to support the Standard Operating Procedures (SOP) for determination of arsenic IVBA in soil. EPA is currently conducting multi-laboratory evaluations of arsenic IVBA for NIST 2710A and USGS Flat Creek RMs and has conducted similar evaluations of lead IVBA for these RMs. Until the arsenic IVBA evaluations are completed, EPA recommends using the provisional reference values for NIST 2710A in Table B-1. Although the provisional reference values are based on data from only two laboratories, the estimated prediction interval ($\pm 20\%$) is in the range observed for lead IVBA reference values (Table B-2). The data on which the arsenic IVBA reference values are based are provided in Tables B-3 (summary) and B-4 (individual replicates).

Laboratory	Reference Material	Laboratory Analysis	Total Soil Arsenic Method	Units	Number of Replicates	Lower 99% Prediction Limit	Mean	Upper 99% Prediction Limit	PI as Percent of Mean
All Labs ^a	NIST2710A	Arsenic IVBA	NIST Certificate ^b	%	131	32.9	41.0	49.1	± 19.8

Table B-1. Recommended Provisional Reference Value for Arsenic IVBA% of NIST 2710A

^aData provided by Karen Bradham (EPA PRD NERL) and John Drexler (University of Colorado). ^bNIST certificate median soil arsenic concentration: 1400 mg/kg.

Table B-2. Reference Values for Lead IVBA% of Standard Reference Materials

Laboratory	Reference Material	Laboratory Analysis	Total Soil Lead Method	Units	Number of Replicates	Lower 99% Prediction Limit	Mean	Upper 99% Prediction Limit	PI as Percent of Mean
QATS Round Robin	NIST2710A	Lead IVBA	NIST Certificate	%	35	60.7	67.5	74.2	±10
QATS Round Robin	NIST2711A	Lead IVBA	NIST Certificate	%	35	75.2	85.7	96.2	±12.3
QATS Round Robin	Flat Creek	Lead IVBA	EPA 3051A	%	30, 35 ^a	56.0	71.0	86.0	±21.1

^aBased on n=35 estimates of total Pb (mg/kg) and 30 estimates of IVBA Pb (mg/kg).

Laboratory ^a	Reference Material	Laboratory Analysis	Total Soil Arsenic Method	Units	Number of Replicates	Lower 99% Prediction Limit	Mean	Upper 99% Prediction Limit	PI as Percent of Mean
EPA NERL	NIST2710A	Arsenic IVBA	NIST Certificate	%	117	33.1	40.8	48.4	± 18.8
U Colorado	NIST2710A	Arsenic IVBA	NIST Certificate	%	14	30.7	43.0	55.2	±28.5
All Labs	NIST2710A	Arsenic IVBA	NIST Certificate	%	131	32.9	41.0	49.1	±19.8

Table B-3. Values for Arsenic IVBA% of NIST 2710A Based Data from Individual Laboratories and Combined Data

^aData provided by Karen Bradham (EPA PRD NERL) and John Drexler (University of Colorado).

Replicate	Laboratory ^a	Soil Mass (g)	Extracted As (mg/L)	Total Soil As ^b (mg/kg)	As IVBA (%)
1	EPA NERL	1.00	5.59	1400	39.9
2	EPA NERL	1.00	5.56	1400	39.6
3	EPA NERL	1.00	5.33	1400	38.0
4	EPA NERL	1.00	5.14	1400	36.7
5	EPA NERL	1.00	6.40	1400	45.6
6	EPA NERL	1.00	6.40	1400	45.6
7	EPA NERL	1.00	5.98	1400	42.7
8	EPA NERL	1.00	6.15	1400	43.9
9	EPA NERL	1.00	5.46	1400	38.9
10	EPA NERL	1.00	5.82	1400	41.4
11	EPA NERL	1.00	6.39	1400	45.5
12	EPA NERL	1.00	5.25	1400	37.5
13	EPA NERL	1.00	5.26	1400	37.6
14	EPA NERL	1.00	5.19	1400	37.1
15	EPA NERL	1.00	5.54	1400	39.5
16	EPA NERL	1.00	5.43	1400	38.8
17	EPA NERL	1.00	5.52	1400	39.3
18	EPA NERL	1.00	5.20	1400	37.0
19	EPA NERL	1.00	5.08	1400	36.3
20	EPA NERL	1.00	5.19	1400	37.0
21	EPA NERL	1.00	5.24	1400	37.4
22	EPA NERL	1.00	6.01	1400	42.9
23	EPA NERL	1.00	5.57	1400	39.7
24	EPA NERL	1.00	5.58	1400	39.6
25	EPA NERL	1.00	5.66	1400	40.4
26	EPA NERL	1.00	5.25	1400	37.4
27	EPA NERL	1.00	5.25	1400	37.5
28	EPA NERL	1.00	5.51	1400	39.4
29	EPA NERL	1.00	4.89	1400	35.0
30	EPA NERL	1.00	5.61	1400	40.0
31	EPA NERL	1.00	5.36	1400	38.2
32	EPA NERL	1.01	5.94	1400	42.1
33	EPA NERL	1.00	5.86	1400	41.8
34	EPA NERL	1.00	5.84	1400	41.6
35	EPA NERL	1.00	4.83	1400	34.4
36	EPA NERL	1.00	5.12	1400	36.5

Table B-4. NIST 2710A Arsenic IVBA Replicate Data Used in Calculation of Provisional Reference Values

Replicate	Laboratory ^a	Soil Mass (g)	Extracted As (mg/L)	Total Soil As ^b (mg/kg)	As IVBA (%)
37	EPA NERL	1.00	5.29	1400	37.7
38	EPA NERL	1.00	5.88	1400	41.9
39	EPA NERL	1.00	5.69	1400	40.6
40	EPA NERL	1.00	5.88	1400	41.8
40	EPA NERL	1.00	5.70	1400	40.6
42	EPA NERL	1.00	5.44	1400	38.8
43	EPA NERL	1.00	5.35	1400	38.2
44	EPA NERL	1.00	5.38	1400	38.3
45	EPA NERL	1.00	5.37	1400	38.3
46	EPA NERL	1.00	5.42	1400	38.7
40	EPA NERL	1.00	5.30	1400	37.9
48	EPA NERL	1.00	5.10	1400	36.3
49	EPA NERL	1.00	6.00	1400	42.7
50	EPA NERL	1.00	5.21	1400	37.1
51	EPA NERL EPA NERL	1.00	5.19	1400	37.0
52	EPA NERL	1.00	6.29	1400	44.8
53	EPA NERL EPA NERL	1.00	5.92	1400	44.8
55	EPA NERL EPA NERL	1.00	5.64	1400	42.1
55	EPA NERL EPA NERL	1.00	5.60	1400	39.9
56					
50	EPA NERL	1.00	5.73	1400	40.8
	EPA NERL	1.00	5.90	1400	42.0
58	EPA NERL	1.00	5.59	1400	39.9
59	EPA NERL	1.00	5.55	1400	39.5
60	EPA NERL	1.00	5.73	1400	40.7
61	EPA NERL	1.00	5.95	1400	42.4
62	EPA NERL	1.00	5.83	1400	41.6
63	EPA NERL	1.00	5.63	1400	40.2
64	EPA NERL	1.00	5.64	1400	40.2
65	EPA NERL	1.00	6.18	1400	44.1
66	EPA NERL	1.00	5.70	1400	40.6
67	EPA NERL	1.00	5.39	1400	38.3
68	EPA NERL	1.00	5.85	1400	41.6
69	EPA NERL	1.00	6.14	1400	43.7
70	EPA NERL	1.00	6.05	1400	43.1
71	EPA NERL	1.00	6.53	1400	46.6
72	EPA NERL	1.00	6.13	1400	43.7

Table B-4. NIST 2710A Arsenic IVBA Replicate Data Used in Calculation of Provisional Reference Values

Replicate	Laboratory ^a	Soil Mass (g)	Extracted As (mg/L)	Total Soil As ^b (mg/kg)	As IVBA (%)
73	EPA NERL	1.00	6.35	1400	45.3
74	EPA NERL	1.00	6.21	1400	44.2
75	EPA NERL	1.00	5.24	1400	37.3
76	EPA NERL	1.00	5.60	1400	40.0
77	EPA NERL	1.00	6.05	1400	43.1
78	EPA NERL	1.00	5.99	1400	42.6
79	EPA NERL	1.00	5.45	1400	38.9
80	EPA NERL	1.00	5.73	1400	40.8
81	EPA NERL	1.00	5.79	1400	41.2
82	EPA NERL	1.00	5.55	1400	39.5
83	EPA NERL	1.01	6.09	1400	43.1
84	EPA NERL	1.00	5.68	1400	40.4
85	EPA NERL	1.00	5.28	1400	37.6
86	EPA NERL	1.00	5.26	1400	37.5
87	EPA NERL	1.00	5.50	1400	39.2
88	EPA NERL	1.01	5.67	1400	40.2
89	EPA NERL	1.00	5.36	1400	38.2
90	EPA NERL	1.01	5.70	1400	40.5
91	EPA NERL	1.00	5.68	1400	40.4
92	EPA NERL	1.01	5.48	1400	38.8
93	EPA NERL	1.01	5.35	1400	37.9
94	EPA NERL	1.00	5.62	1400	40.0
95	EPA NERL	1.00	5.63	1400	40.1
96	EPA NERL	1.01	5.94	1400	42.0
97	EPA NERL	1.00	6.57	1400	46.9
98	EPA NERL	1.00	5.77	1400	41.2
99	EPA NERL	1.00	6.14	1400	43.8
100	EPA NERL	1.00	6.50	1400	46.5
101	EPA NERL	1.01	6.36	1400	44.9
102	EPA NERL	1.01	6.14	1400	43.5
103	EPA NERL	1.01	6.62	1400	46.7
104	EPA NERL	1.01	6.21	1400	44.0
105	EPA NERL	1.01	6.70	1400	47.5
106	EPA NERL	1.00	6.45	1400	46.1
107	EPA NERL	1.00	5.73	1400	40.8
108	EPA NERL	1.01	5.87	1400	41.7

Table B-4. NIST 2710A Arsenic IVBA Replicate Data Used in Calculation of Provisional Reference Values

Replicate	Laboratory ^a	Soil Mass (g)	Extracted As (mg/L)	Total Soil As ^b (mg/kg)	As IVBA (%)
109	EPA NERL	1.01	5.98	1400	42.5
110	EPA NERL	1.00	6.04	1400	43.0
111	EPA NERL	1.00	5.42	1400	38.6
112	EPA NERL	1.00	5.49	1400	39.1
113	EPA NERL	1.01	6.15	1400	43.6
114	EPA NERL	1.01	6.63	1400	46.9
115	EPA NERL	1.01	5.93	1400	42.0
116	EPA NERL	1.01	6.14	1400	43.5
117	EPA NERL	1.00	6.44	1400	45.9
118	U. Colorado	1.00	5.10	1400	36.3
119	U. Colorado	1.02	5.22	1400	36.7
120	U. Colorado	1.01	5.69	1400	40.3
121	U. Colorado	1.01	6.55	1400	46.5
122	U. Colorado	1.00	6.69	1400	47.7
123	U. Colorado	1.00	6.34	1400	45.1
124	U. Colorado	1.00	6.75	1400	48.2
125	U. Colorado	1.00	6.45	1400	46.1
126	U. Colorado	1.00	6.34	1400	45.2
127	U. Colorado	1.01	6.46	1400	45.8
128	U. Colorado	1.02	5.79	1400	40.4
129	U. Colorado	1.01	5.69	1400	40.3
130	U. Colorado	1.00	5.68	1400	40.4
131	U. Colorado	1.01	6.02	1400	42.4

Table B-4. NIST 2710A Arsenic IVBA Replicate Data Used in Calculation of Provisional Reference Values

^aData provided by Karen Bradham *(EPA ORD NERL) and John Drexler, University of Colorado. ^bNIST certificate median soil arsenic concentration.