# FINAL REPORT

Providing Additional Support for MNA by Including Quantitative Lines of Evidence for Abiotic Degradation and Co-metabolic Oxidation of Chlorinated Ethylenes

# ESTCP Project ER-201584



#### SEPTEMBER 2017

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## **FINAL REPORT**

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### ACRONYMS AND ABBREVIATIONS

AFB	Air Force Base
bgs	Below Ground Surface
BSM	Basal Salts Medium
<sup>14</sup> C	Radioactive Carbon 14
<sup>14</sup> C-CO <sub>2</sub>	Carbon Dioxide labelled with Carbon 14
<sup>14</sup> C-NSR	Nonstrippable Residue labelled with Carbon 14
<sup>14</sup> C-TCE	Trichloroethene labelled with Carbon 14
mCi	milli-curie (a unit of radioactivity)
CINN	<i>trans</i> -Cinnamonitrile
Ct	Cycle number at threshold (see Definitions)
d	Day
DAPI	4,6-Diamidino-2-phenylindole
cDCE	<i>cis</i> -1,2-Dichloroethene
tDCE	trans-1,2-Dichloroethene
1,1-DCE	1,1-Dichloroethene
DDI	Distilled Deionized water
DEM/VAL	Demonstration and Validation
DNA	Deoxyribonucleic Acid
DO	Dissolved Oxygen
DOD	Department of Defense
dpm	Disintegrations per minute
EAP	Enzyme Activity Probe
EISB	Enhanced <i>In Situ</i> Bioremediation
EPA	Environmental Protection Agency
ESTCP	Environmental Security Technology Certification Program
FID	Flame Ionization Detector
FSGW	Filter-Sterilized Groundwater
GC	Gas Chromatograph
GC/FID	Gas Chromatograph with a Flame Ionization Detector
GC/TCD	Gas Chromatograph with a Thermal Conductivity Detector
3HPA	3-Hydroxyphenylacetylene
IDW	Investigation Derived Wastes
IWL	Industrial Waste Lagoon at TEAD
LSC	Liquid Scintillation Cocktail

MBTs	Molecular Biological Tools
MCL	Maximum Contaminant Level
MCRD	Marine Corps Recruit Depot
mmoZ	qPCR Primer for Soluble Methane Monooxygenase Enzyme
MNA	Monitored Natural Attenuation
NAPL	Nonaqueous-Phase Liquid
NSR	Nonstrippable Residue
NYSDEC	New York State Department of Environmental Conservation
NYSDOH	New York State Department of Health
O&M	Operation & Maintenance
OIWL	Old Industrial Wastewater Lagoon at TEAD
PA	Phenylacetylene
PCE	Tetrachloroethene
PCR	Polymerase Chain Reaction
pH	potential of Hydrogen
PHE	qPCR Primer for Phenol Monooxygenase (Phenol Hydrolyase) Enzyme
PNNL	Pacific Northwest National Laboratory (DOE)
POET	Point Of Entry Treatment system
PVC	Poly(Vinyl Chloride)
qPCR	Quantitative Real-Time Polymerase Chain Reaction
RDEG	a qPCR Primer for Ring-Hydroxylating Toluene Monooxygenease Enzyme
RMO	a qPCR Primer for Ring-Hydroxylating Toluene Monooxygenease Enzyme
RPD	Relative Percent Difference
RPM	Remedial Project Manager
SMMO	qPCR Primer for Soluble Methane Monooxygenase Enzyme
T2,3-di	Toluene-2,3-dioxygenase Enzyme
T3-mono	Toluene-3-monooxygenase Enzyme
TEAD	Tooele Army Depot, Utah
1,1,1-TCA	1,1,1-Trichloroethane
TCAAP	Twin Cities Army Ammunition Plant
TCD	Thermal Conductivity Detector
TCE	Trichloroethene
TOL	qPCR Primer for Toluene/Xylene Side Chain Monooxygenase Enzyme
TOD	qPCR Primer for Toluene Dioxygenase Enzyme
USEPA	United States Environmental Protection Agency
VC	Vinyl Chloride
VOC	Volatile Organic Compound

### DEFINITIONS

- **Abiotic Oxidation:** Oxidative contaminant transformation without direct involvement of a biological system. Involves the abiotic oxidation of the organic compound of interest to carbon dioxide and other products. For example, He et al. (2009) show that the reaction of cDCE with magnetite results in the production of CO<sub>2</sub> and likely water and chloride. This is consistent with the work of Darlington et al. (2008). This reaction can occur under oxic or anoxic conditions.
- **Abiotic Reduction:** Reductive contaminant transformation without the direct involvement of a biological system. Involves the abiotic reduction of the organic compound of interest to a more reduced compound. For example, Butler and Hayes (1999) and Lee and Batchelor (2002 a, b and 2003) show that TCE is abiotically reduced to chloroacetylene and/or acetylene which is then oxidized to CO<sub>2</sub>, water, and chloride. Abiotic transformations of chlorinated organics can occur under oxic or anoxic conditions and can be significant at sites with iron-rich minerals, including iron sulfide, pyrite, fougerite, magnetite, and Fe(II)-containing phyllosilicates.
- <u>Aerobic Co-oxidation</u>: Oxygen-dependent oxidation reaction(s) leading to detoxification of chlorinated ethylenes. Involves the biologically-mediated oxidation of organic compounds to produce an enzyme that fortuitously degrades TCE and potentially PCE. This reaction predominantly occurs under oxic to hypoxic conditions.
- <u>Aerobic Oxidation:</u> Oxygen-dependent oxidation reaction(s) leading to detoxification. Involves the biologically-mediated oxidation of compounds of interest and occurs when oxygen in used as an electron acceptor and the organic compound is used as the electron donor. For example, during aerobic oxidation, vinyl chloride is oxidized to the nontoxic end-products carbon dioxide, water, and chloride. This reaction predominantly occurs under oxic conditions.
- **Anaerobic Oxidation:** Oxygen-independent oxidation reaction(s) leading to detoxification. Occurs only under anoxic conditions. Involves the biologically-mediated oxidation of compounds of interest and occurs when an electron acceptor other than oxygen is utilized as an electron sink, and the organic compound is used as the electron donor. For example, during anaerobic oxidation under iron-reducing conditions, vinyl chloride is oxidized to the nontoxic end-products carbon dioxide, water, and chloride.
- Attenuation: Complement of processes that reduce contaminant concentrations in groundwater. Attenuation processes are dominated by dispersion, sorption, biodegradation and abiotic degradation.
- <u>Attenuation Rate Constant:</u> The proportionality constant quantifying the rate of change in the concentration of a contaminant due to the combined processes of dispersion, sorption, and biotic and abiotic degradation.
- **Bioattenuation:** Complement of all biological processes that reduce contaminant concentrations in groundwater.

- <u>**C**t</u>: The cycle number in a PCR amplification where the fluorescence exceeds the threshold value (background level) and amplification of the DNA is detectable.
- **Degradation:** Degradation involves the breakage of C-C or C-Cl bonds and generates products of lower molecular weight.
- **Degradation Rate:** The rate of change in contaminant concentration due only to the degradation of organic compounds. This rate does not consider the effects of dispersion or sorption and thus quantifies only the rate at which the mass of the parent compound is being removed from the system.
- **Degradation Rate Constant:** The proportionality constant quantifying the rate of change in concentration or mass of a chemical compound over time resulting from the transformation of a contaminant into a degradation product. At the field scale, degradation rate constants are typically described by first-order kinetics.
- **Enzyme Activity Probe:** Enzyme activity probes (EAPs) are chemicals used to detect and quantify specific activities of microorganisms in environmental samples (e.g., soil, water, or sediment). EAPs are compounds that serve as alternative or surrogate substrates for the protein catalysts (enzymes) responsible for the metabolic activities of microorganisms. These surrogate compounds are transformed by target enzymes into distinct and readily detectable products.
- **Mass Magnetic Susceptibility:** The degree of magnetization of a material in response to an applied magnetic field. It is one measure of the magnetic properties of a material. The susceptibility indicates whether a material is attracted into or repelled out of a magnetic field. In most hydrogeologic settings, magnetic susceptibility is a measure of the amount of magnetic present in the system. Magnetic susceptibility sondes measure the volume magnetic susceptibility. The mass magnetic susceptibility of the subsurface material is calculated by dividing the volume magnetic susceptibility by the bulk density of the material being analyzed (kg/m<sup>3</sup>).
- **Monitored Natural Attenuation (MNA):** The reliance on natural attenuation processes (within the context of a carefully controlled and monitored site cleanup approach) to achieve site-specific remedial objectives within a time frame that is reasonable compared to other methods. In order for MNA to be considered a viable remediation alternative, regulatory agencies often require evidence of degradation. In the past this degradation has largely been consider to be of strictly biological origin. It is now known that abiotic degradation can contribute to contaminant detoxification.
- **<u>Reductive Dechlorination (Hydrogenolysis)</u>:** Replacement of a halogen substituent with hydrogen with the concomitant addition of electrons to the organic molecule. For chlorinated aliphatic hydrocarbons, this process results in the degradation of organic compounds by chemical reduction with release of inorganic chloride ions.
- **<u>Relative Percent Difference:</u>** An expression of the difference between two numbers calculated as the difference expressed as a percent of the average of the two numbers.

- **Sonde:** A Sonde (*Sonde* is French for *probe*) is a water quality monitoring instrument, that may be stationary or may move up and down a water column, measuring water attributes including magnetic susceptibility, temperature, conductivity, salinity, dissolved oxygen, pH, turbidity, and depth.
- **Volume Magnetic Susceptibility:** Volume magnetic susceptibility is a property of space. The volume magnetic susceptibility is the ratio of the magnetization (the magnetic dipole moment per unit volume) measured in amperes per meter divided by the magnetic field strength, measured in amperes per meter. The units for volume magnetic susceptibility cancel out.

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### **EXECUTIVE SUMMARY**

#### **OBJECTIVES**

The overarching objectives of the work described herein were to:

- (1) Provide a method to readily and inexpensively acquire the magnetic susceptibility data required to evaluate the abiotic degradation of TCE by magnetite in aquifer materials using existing non-metallic groundwater monitoring wells.
- (2) Provide a method to readily and inexpensively acquire the data required to evaluate and quantify the rate constant for aerobic biological co-oxidation of TCE.

#### **TECHNOLOGY DESCRIPTION**

Using mass magnetic susceptibility to predict abiotic degradation of chlorinated alkenes by magnetite in the aquifer matrix has been shown to be viable, but before the work presented in this report, such evaluation required that a core sample of the aquifer material be submitted for laboratory analysis. This report shows that an inexpensive downhole sonde (probe) can be used in existing 2- and 4-inch PVC groundwater monitoring wells to quantify magnetic susceptibility of aquifer material.

Bacteria that degrade natural organic matter in groundwater contain enzymes (oxygenases) that can aerobically degrade TCE through a process of biological co-oxidation. Bacteria that contain active oxygenase enzymes can be recognized using fluorescent Enzyme Activity Probes (EAP), and the bacteria can be counted under a microscope. There are primers that can be used in the Polymerase Chain Reaction (qPCR) to amplify DNA that codes for selected oxygenase enzymes. A qPCR assay can be used to determine the number of gene copies for these enzymes in a sample of groundwater. Aerobic cooxidation is a promising risk management strategy for large dilute plumes, but its application has been limited because the co-oxidation of TCE in the environment is difficult to quantify by simply measuring changes in the concentration of TCE in the field, and the numbers of bacteria in groundwater that have the oxygenase enzymes has not been directly correlated to field-scale rates of degradation.

Because determining field scale rates for co-oxidation of TCE using concentration data is problematic, a <sup>14</sup>C labelled TCE assay was developed to measure rate constants. The utility of EAPs and qPCR assays to evaluate co-oxidation of TCE was determined by comparing the rate constant developed using the <sup>14</sup>C-labelled TCE assay to the abundance of cells that react with EAPs or the abundance of gene copies for oxygenase enzymes.

#### **DEMONSTRATION RESULTS**

Values for volume magnetic susceptibility were determined in 26 PVC wells using a downhole sonde. The values were converted to mass magnetic susceptibility, and compared to values for mass magnetic susceptibility from laboratory analyses on samples from boreholes that were adjacent to the wells. There was good agreement between the two measurements.

Out of the 19 groundwater samples evaluated using the <sup>14</sup>C-TCE assay, TCE co-oxidation could be documented in 8 samples, with first order rate constants ranging from 0.00658 to 2.65 yr<sup>-1</sup>.

In a particular water sample, the abundance of gene copies of the most common oxygenase was similar to the abundance of cells reacting to the EAPs.

Some oxygenase enzymes were more abundant in groundwater from some wells and other enzymes were more abundant in other wells. Cooxidation of TCE could not be attributed to any one oxygenase enzyme. To further complicate interpretation of the abundance of DNA gene copies, not all the DNA in bacteria is actively transcribed to make enzymes at any one time. If the mRNA transcript for an enzyme is present in a sample, that is evidence that the gene is being transcribed.to make the active enzyme. The total abundance of active DNA gene copies was calculated as the sum of the individual gene copies of oxygenase enzymes for which the mRNA transcript was detected. There was a useful relationship between the total abundance of active DNA gene copies and the rate constants for TCE cooxidation. The 80% prediction interval of a regression of the rate constants on the total abundance of active DNA gene copies is only one order of magnitude wide.

### COSTS

The cost to determine volume magnetic susceptibility in one well using a down-hole sonde is approximately \$2,000. The cost of the <sup>14</sup>C assay of the rate constant of cooxidation of TCE is approximately \$476 per well. The cost of the EAP assay is approximately \$1,900 per well. The cost of the qPCR analyses is approximately \$835 per well.

#### **IMPLEMENTATION ISSUES**

Laboratory microcosm studies have shown that some aquifer sediments have appreciable values for mass magnetic susceptibility but no evidence for abiotic degradation of TCE. Values of mass magnetic susceptibility should only be used as a second line evidence to support a rate constant for TCE degradation that is extracted from site characterization data, as is illustrated in the decision logic of Lebrón et al. (2015). Mass magnetic susceptibility should not be used as primary line of evidence to extract a rate constant. Similarly, the abundance of cells that react to an EAP or the abundance of DNA amplified by a qPCR marker for an oxygenase enzyme should be used as a second line evidence to support a rate constant for TCE degradation that is extracted rate constant for TCE degradation that is extracted are constant. Similarly, the abundance of cells that react to an EAP or the abundance of DNA amplified by a qPCR marker for an oxygenase enzyme should be used as a second line evidence to support a rate constant for TCE degradation that is extracted from site characterization data. They should not be used as primary line of evidence to extract a rate constant.

Two other significant implementation issues are the cost of the enzyme activity probe (EAP) analyses and the fact that they can only be completed by the Pacific Northwest National Laboratory (PNNL) and the requirement that the <sup>14</sup>C-TCE assay be done in a certified and permitted laboratory. A third implementation issue has to do with the integrity of the PVC monitoring wells; specifically, 2-inch groundwater monitoring wells. If these wells are not sufficiently straight, or if the joints are not flush, then the magnetic susceptibility sonde cannot be lowered into the well, and it will not be possible to obtain mass magnetic susceptibility readings in such wells.

### **1.0 INTRODUCTION**

This section provides a general overview of the project. It is divided into several subsections.

#### 1.1 BACKGROUND

Monitored natural attenuation (MNA) and enhanced bioremediation have gained popularity as remediation approaches at sites contaminated with chlorinated solvents over the past 25 years. ESTCP Project Number ER-201129 developed a quantitative framework to aid in the selection of MNA or bioremediation approaches (biostimulation alone, or biostimulation combined with bioaugmentation) at sites contaminated with chlorinated ethylenes. Upon completion of ER-201129, two shortcomings regarding the current state of the science were identified, including:

- In some cases, the investigator may not want to expend the resources necessary to fully implement the decision framework developed for ER-201129. The most notable example occurs when the investigator has worked through the decision framework and will not be able to proceed without magnetic susceptibility data. Using mass magnetic susceptibility to predict abiotic degradation of chlorinated alkenes by magnetite in an aquifer matrix has been shown to be effective (ESTCP, 2015; He, 2009). However, before the work presented herein, this evaluation required that a core sample from a borehole be submitted for laboratory analysis. Obtaining core samples at many sites is unrealistic because the drilling program has been completed. Thus, general and widespread acceptance of the approach outlined in ER-201129 was limited. As detailed in this report, this project develops and validates a more affordable technique to measure magnetic susceptibility with a sonde (probe) that can be used in existing 2-inch or 4-inch inner-diameter non-metallic monitoring wells should increase the implementability and use of the decision framework developed for ER-201129, including BioPIC.
- Bacteria that degrade natural organic matter in groundwater contain enzymes (oxygenases) that can aerobically degrade trichloroethylene (TCE) through co-oxidation. These bacteria use oxygenase enzymes to degrade organic matter in groundwater. Trichloroethylene is fortuitously degraded by the same oxygenase enzymes that are produced during degradation of native organic matter. This degradation mechanism is promising for large dilute plumes, but its application has been limited because the numbers of bacteria in groundwater that have the oxygenase enzymes have not been directly correlated to degradation rates until now. This degradation pathway was not included in ER-201129 because it had not yet been quantified. This report quantifies the relationship between oxygenase enzymes and degradation rates.

A number of studies have demonstrated that remedial goals can be met with significantly reduced environmental impacts, capital investment, and operation and maintenance (O&M) costs by implementing MNA. The results of this project and the results presented in this report should increase the number of sites where MNA is implemented because it allows the Department of Defense (DOD) to better describe the mechanisms and processes that contribute to natural attenuation. This is because degradation by magnetite and aerobic cooxidation have largely been neglected when evaluating MNA in the past, which often has resulted in the misinterpretation of degradation mechanisms and thus, the efficacy of MNA.

For example, when abiotic degradation or aerobic co-oxidative degradation are the predominant degradation mechanisms, the investigator may falsely conclude that degradation has "stalled" at dichloroethylene (DCE), typically *cis*-1,2-DCE (*c*DCE). With the information presented in this report, the DOD and other responsible parties will be able to present State and Federal regulatory agencies with quantitative estimates of the contribution of abiotic degradation by magnetite and aerobic co-oxidation to the overall rate of natural attenuation at DOD sites contaminated with chlorinated ethylenes. An increase in the use of MNA will minimize detrimental environmental impacts, such as greenhouse gas emissions, at sites where unnecessary remediation previously would have taken place. This will reduce both capital and O&M costs to the DOD.

#### **1.2 OBJECTIVES OF THE DEMONSTRATION**

The overarching objectives of the work described herein are to:

- (1) Provide a method to readily and inexpensively acquire the magnetic susceptibility data required to evaluate the abiotic degradation of chlorinated ethylenes by magnetite in existing non-metallic groundwater monitoring wells.
- (2) Provide a method to readily and inexpensively acquire the data required to evaluate and quantify the aerobic co-oxidation of TCE.

Based on the data and information presented in this report, these objectives have been met. It is anticipated that this work will further promote the implementation of MNA where it previously was not implemented because of a lack of understanding of these important degradation processes, and the inability for them to be readily quantified at many sites.

#### **1.3 REGULATORY DRIVERS**

Presently, the maximum contaminant levels (MCLs) for the chlorinated ethylenes PCE, TCE, cDCE, and vinyl chloride (VC) are 5 micrograms per liter ( $\mu g/L$ ), 5  $\mu g/L$ , 70  $\mu g/L$ , and 2  $\mu g/L$ , respectively (http://water.epa.gov/drink/contaminants/index.cfm). At many sites, a risk-based assessment dictates cleanup goals, which often means that MCLs are not the regulatory driver. In any event, some type of remedial action is required at many DOD sites where chlorinated ethylenes are present. This project expands on the elucidation of degradation pathways outlined in ESTCP ER-201129 to allow DOD RPMs to choose the most efficacious remediation approach to meet remedial objectives.

### 2.0 TECHNOLOGY

This section provides an overview of the technology components demonstrated in this report.

### 2.1 TECHNOLOGY DESCRIPTION

The results presented in this report allow the efficacy of MNA to be evaluated more efficiently and accurately than it has been in the past using tools that had already been developed but had not been adequately tested for environmental applications. Specifically, the techniques described and quantified in this report benchmark abiotic degradation by magnetite and aerobic co-oxidation at sites contaminated with chlorinated ethylenes. Figure 2.1.1 is a process schematic showing integration of key components of the demonstration.

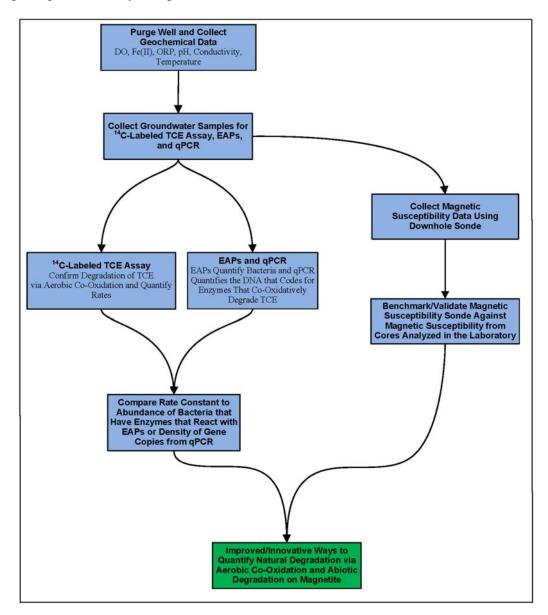


Figure 2.1.1. Process Schematic Showing Integration of Key Technology Components.

### 2.2 TECHNOLOGY DEVELOPMENT

This Section provides a detailed description of the technology development.

#### 2.2.1 Quantifying Abiotic Degradation by Magnetite Using a Magnetic Susceptibility Sonde

Borehole sondes and laboratory magnetic susceptibility meters measure the volume magnetic susceptibility of the aquifer material. Volume magnetic susceptibility is a property of space. The volume magnetic susceptibility is the ratio of the magnetization (the magnetic dipole moment per unit volume) measured in amperes per meter divided by the magnetic field strength, measured in amperes per meter. The units for volume magnetic susceptibility cancel out. The mass magnetic susceptibility of the subsurface material is calculated by dividing the volume magnetic susceptibility as measured by the sonde by the bulk density of the material being analyzed ( $kg/m^3$ ).

Magnetite is a natural component of many aquifers. Abiotic degradation of chlorinated ethylenes in aquifer materials containing magnetite can be an important mechanism for natural attenuation (Lee and Batchelor, 2002; Ferrey et al., 2004; Darlington, et al., 2008; He et al., 2009; Darlington, et al., 2013; He et al. 2015). In contrast to anaerobic biodegradation, abiotic degradation by magnetite does not go through a sequential reductive dechlorination (Lee and Batchelor, 2002; Darlington et al., 2013). That is, tetrachloroethylene (PCE) is not degraded to produce trichloroethylene (TCE), TCE is not degraded to cDCE, and cDCE is not degraded to produce vinyl chloride (VC). As a consequence, degradation of chlorinated ethylenes by magnetite does not produce compounds that are on the list of USEPA MCLs.

The measurement of the magnetic properties of the earth for geological mapping and for the direct detection of iron-rich ores has been used for many years. It is one of the most common geophysical survey techniques. Variations in the magnetic field reading are caused by variations in the local magnetic susceptibility and/or variations in the local remnant magnetism of geological materials.

Borehole logging of magnetic susceptibility has been used for mineral exploration for decades, being first developed for use in petroleum exploration (Broding et al., 1952). Because borehole magnetic susceptibility measurements are made using an alternating current induction technique, the downhole sonde used for this project is an instrument which responds only to very local variations in magnetic susceptibility. Such a device operates by generating a small alternating magnetic field, usually at an audio frequency, and measuring changes in the amplitude of this magnetic field caused by the presence of nearby magnetically-susceptible material (McNeill et al., 1996).

Relatively few magnetic minerals have geological significance, with magnetite (Fe<sub>3</sub>0<sub>4</sub>) being by far the most important (McNeill et al., 1996). Other magnetic minerals that may occasionally be significant include pyrrhotite (Fe<sub>7</sub>S<sub>8</sub>), ilmenite (Fe<sub>2</sub>Ti0<sub>3</sub>), and a form of hematite known as maghemite ( $\gamma$ Fe<sub>2</sub>O<sub>3</sub>) (Grant and West, 1965). Under ordinary circumstances the magnetic susceptibility of soil and sediment is dominated by magnetite (Dearing, 1999, page 39; He et al., 2009, pages 77-78). There is an important exception. Greigite (Fe<sub>3</sub>S<sub>4</sub>) can form in sediments with adequate sources of sulfide and iron (Roberts, 2015). The magnetic susceptibility of greigite can be as high 2.0E-04 m<sup>3</sup>/kg (Decker et al., 2000), which brings it in the same range as magnetite. In sulfate-reducing aquifers (i.e., strongly reducing/anoxic), it is possible that greigite will produce magnetic susceptibility that can be confused for magnetite. However, in such aquifer systems, anaerobic biological reductive dechlorination will likely be the predominant degradation mechanism.

Magnetite is extremely resistant to weathering, which makes it useful for environmental engineering applications. Most rocks contain magnetite, in an amount which varies from very small fractions of a percent to several percent, and even tens of percent in some iron ore deposits (McNeill et al., 1996). Rocks containing magnetite weather to form detrital magnetite which is found in sediments such as those that make up the shallow subsurface in which solute plumes of chlorinated ethylenes are found.

The magnetic susceptibility of aquifer sediment can be characterized with good sensitivity and at low cost. There is a direct correlation between the quantity of magnetic materials in aquifer sediments and their magnetic susceptibility (Figure 2.2.1; Lindsley et al., 1966; Balsley and Buddington, 1958; Werner, 1945; Canfield and Berner, 1987; Horneman et al., 2004). The relationship is linear over a range in values of two orders magnitude. However, there is significant variation from one sample to the next. The 95% prediction interval on the quantity of magnetic materials varies by a factor of 3.4 from the regression line.

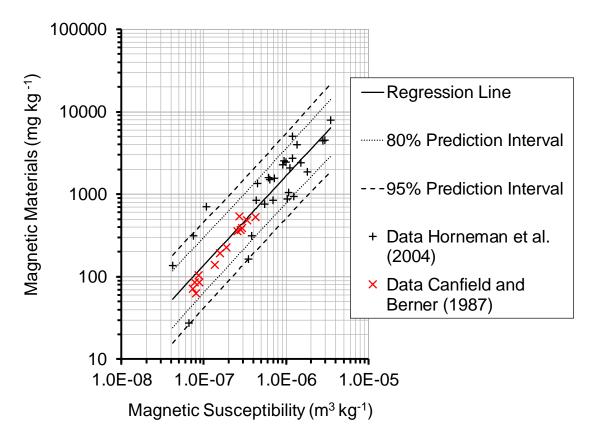


Figure 2.2.1. Relationship between the Mass Magnetic Susceptibility of a Sediment and the Content of Magnetic Minerals.

Redrawn for Figure 6.5 of He et al. (2009).

Mass magnetic susceptibility is a useful surrogate for the quantity of magnetite in aquifer material. This is particularly true because it is not possible to directly measure magnetite at concentrations less than 10000 mg kg<sup>-1</sup> and most aquifer materials contain less than 10000 mg kg<sup>-1</sup> of magnetic materials (He et al., 2009).

Using mass magnetic susceptibility to predict abiotic degradation of chlorinated alkenes by magnetite in the aquifer matrix has been shown to be viable, but before the work presented in this report, such evaluation required that a borehole core sample be submitted for laboratory analysis. Unfortunately, obtaining core samples at many sites is problematic because the majority of DOD and other hazardous waste sites have largely been characterized and no additional boreholes/groundwater monitoring wells are planned. Because the abiotic degradation by magnetite has only recently been discovered (Lee and Batchelor, 2002; Ferrey et al., 2004; Darlington, et al., 2008; Darlington, et al., 2013; He et al., 2009; He et al. 2015), most previous site characterization efforts did not include collection of borehole core samples for magnetic susceptibility analysis. Thus, the ability to quantify abiotic degradation by magnetite was limited before this project. In this report, an affordable technique is developed and validated that measures magnetic susceptibility with a sonde (probe) that can be easily deployed into existing two- or four-inch non-metallic groundwater monitoring wells. This project determined that there is a relationship between magnetic susceptibility determined using a relatively inexpensive downhole magnetic susceptibility sonde and the magnetic susceptibility of an aquifer determined through laboratory analyses of aquifer matrix samples collected from borehole core samples. If properly utilized, the downhole magnetic susceptibility sonde has the ability to save the DOD significant amounts of money in unnecessary drilling costs while still allowing abiotic degradation mechanisms facilitating MNA to be quantified.

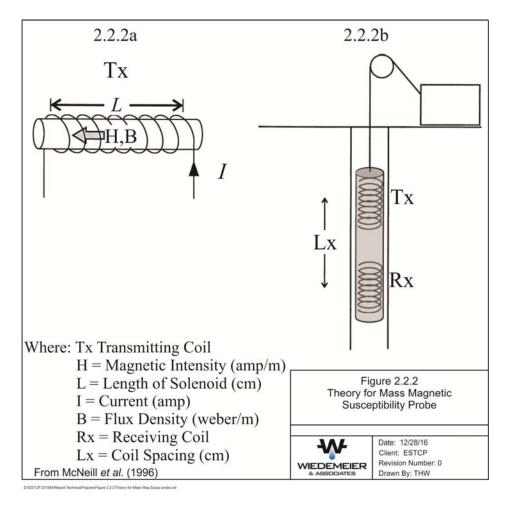


Figure 2.2.2. Theory for Mass Magnetic Susceptibility Probe

Borehole sondes such as those used for magnetic susceptibility are based on electromagnetic induction. This principle is illustrated in Figure 2.2.2. A small transmitter coil (Tx) is energized with an alternating current at an audio frequency. Figure 2.2.2a shows a long (with respect to its diameter) solenoidal coil through which flows a current. Inside the coil, at a large distance from the ends, the magnetic field is uniform, with magnetic intensity H.

$$H=NI/L \tag{2.1}$$

where H = Magnetic Intensity (amp/m); N = Number of Turns; I = Current (amp); and L = Length of Solenoid (m).

This coil (Tx; Figure 2.2a) generates an alternating magnetic field which is sensed by a nearby receiver coil (Rx; Figure 2.2b). The receiver coil together with a capacitor bank and oscillator circuit produce an alternating magnetic field in the vicinity of the coil (McNeill et al., 1996). Any magnetic material which is bought within the influence of this field will bring about a reduction in the natural resonant frequency of the oscillator circuit (McNeill et al., 1996). The magnetic susceptibility of the materials immediately around the borehole is proportional to the reduction in the natural resonant frequency. This is measured by a meter/data logger attached to the sonde.

In the general case where the ground exhibits finite magnetic susceptibility and electrical conductivity, the measured magnetic field is a complicated function of the ground permeability, electrical conductivity, the operating frequency of the instrument and the intercoil spacing (McNeill et al., 1996). However, at sufficiently low frequencies, such that the low induction number approximation is fulfilled (McNeill, 1980), the response simplifies substantially. In this case, the response from the ground electrical conductivity appears essentially in the quadrature phase component of the received magnetic field while the response from the magnetic susceptibility appears in the in-phase component. Two caveats must be considered in connection with this statement (McNeill et al., 1996). The first is that, where the particles of magnetite are small enough so that they are essentially single domain, it can be shown (Mullins and Tite, 1973) that the contribution from magnetic susceptibility also has a small quadrature phase component, which, since only the in-phase component will be measured to obtain the magnetic susceptibility, is not of concern here. The second caveat is that, for moderate to large electrical conductivities, such as those associated with oil deposits and the deep subsurface, the conductivity response also contains a small in-phase response (Doll, 1949). Since it is this component that is measured, electrical conductivity must also be measured in areas with large electrical conductivities in order to correct the in-phase reading, particularly when measuring small magnetic susceptibilities (McNeill et al., 1996). Thus, unless the medium is known to be characterized by low electrical conductivities, which is the case for most shallow hydrogeologic systems, it is necessary to use a conductivity sonde to obtain conductivity data with which to correct the susceptibility data. This correction is generally small (McNeill et al., 1996) and because of the relatively low conductivities associated with shallow groundwater, was neglected. As shown by the results presented herein, this appears to be a valid assumption.

The inductive magnetic susceptibility borehole sonde that was used for this demonstration employs the general configuration shown in Figure 2.2.2. Figure 2.2.3 shows the general implementation of the theory described in the schematic diagram presented in Figure 2.2.2.

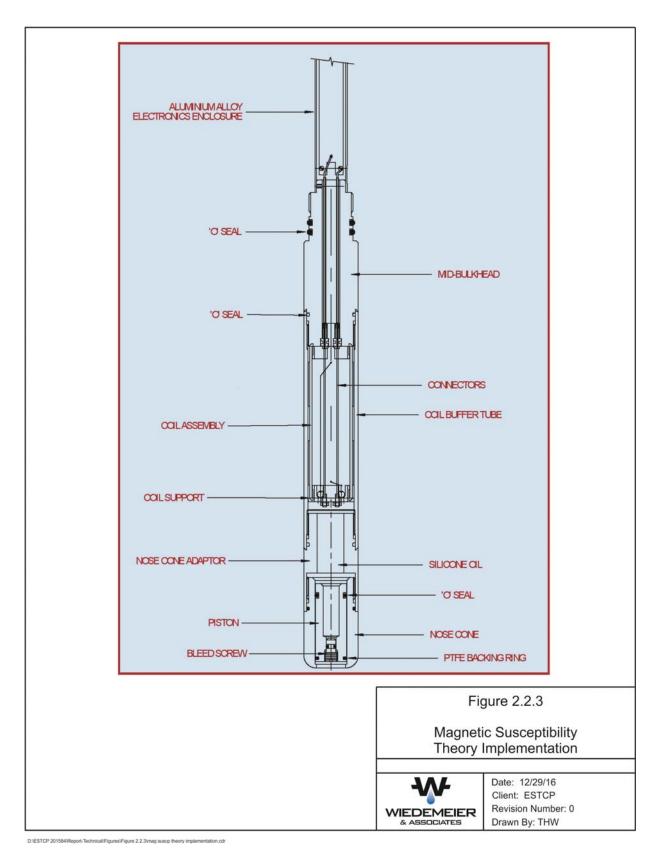


Figure 2.2.3. Magnetic Susceptibility Theory Implementation

#### 2.2.2 Quantifying Aerobic Co-Oxidation of Trichloroetyhlene

Bacteria that degrade natural organic matter in groundwater contain enzymes (oxygenases) that can aerobically degrade TCE through a process of co-oxidation. This degradation mechanism is promising for large dilute plumes, but its application has been limited because the numbers of bacteria in groundwater that have the oxygenase enzymes has not been directly correlated to field-scale rates of degradation. Because determining field scale rates for co-oxidation of TCE using concentration data is problematic, a <sup>14</sup>C labelled TCE assay was developed to help quantify degradation rates. To allow the use of this assay at other sites, a protocol for collecting and analyzing samples using the <sup>14</sup>C labelled TCE assay is provided in Appendix F.

The utility of enzyme activity probes (EAPs) and the quantitative real-time polymerase chain reaction (qPCR) assays was evaluated by comparing the rate constant for aerobic biodegradation to the abundance of cells that react with EAPs or the abundance of gene copies for oxygenase enzymes. To allow the use of EAPs at other sites, an abbreviated protocol for collecting and analyzing EAP samples is provided in Appendix E.

### 2.2.2.1 <sup>14</sup>C-TCE Assay

Co-oxidation of TCE in the environment is difficult to quantify by simply measuring changes in the concentration of TCE in the field. The monitoring approach used for this study included an assay employing <sup>14</sup>C-labeled TCE. Groundwater samples collected in the field were shipped on ice via an overnight carrier to Clemson University. Upon receipt, the groundwater was warmed to room temperature, and highly purified <sup>14</sup>C-labeled TCE was added to the collection bottles. At regular intervals (ranging from a few hours to several days), the fate of the <sup>14</sup>C-labeled TCE was ascertained by quantifying the disappearance of <sup>14</sup>C-labeled TCE and the accumulation of <sup>14</sup>C-labeled products, including <sup>14</sup>CO<sub>2</sub> and soluble <sup>14</sup>C-labeled compounds such as formate, glycolate, and oxalate. The high precision of these measurements due to the strong signal emanating from <sup>14</sup>C made it possible to estimate pseudo-first order rate coefficients for TCE degradation over a relatively short time frame.

The use of <sup>14</sup>C-labeled compounds to determine the fate of a parent compound, the rate of degradation, and the identity of the products formed has been in practice for decades. This includes the fate of <sup>14</sup>C-labeled TCE and other chlorinated organic contaminants. The Freedman laboratory has extensive experience in the use of <sup>14</sup>C-labeled compounds (e.g., Darlington et al., 2008, 2013; Fullerton et al., 2013; Shan et al. 2010). One complication with using <sup>14</sup>C-labeled TCE is the presence of impurities. Typically, vendors provide <sup>14</sup>C-labeled TCE that is 95-98% radio-chemically pure. The presence of impurities presents a problem when trying to quantify TCE degradation, especially over relatively short time intervals. One way to avoid this problem is to further purify the <sup>14</sup>C-labeled TCE before adding it to microcosms. The Freedman laboratory has accomplished this in previous studies by passing a stock solution of <sup>14</sup>C-labeled TCE through a gas chromatographic column and then injecting the eluent from the column into a microcosm when TCE elutes. This has achieved an appreciable improvement in purity of the solution. For the current project, additional purification was evaluated by placing a second gas chromatograph (GC) column in series with the first. However, two columns in series turned out not to provide any additional improvement in purity, so a single column was used. Results for the comparison between one and two columns in series is presented in section 3.1.2.

The <sup>14</sup>C assay is one of three types of measurements that were used in this study to document the occurrence of in situ co-oxidation of TCE. The first order rate coefficients from the <sup>14</sup>C assays were correlated with EAP and qPCR data. As shown in this report, these three types of measurements provide a more complete picture of in situ transformation than any one of the measurements by itself.

#### 2.2.2.2 Enzyme Activity Probes

Several methods are available to assess the in-situ activity of microbes in the subsurface. However, these methods can be time consuming and frequently provide overestimates of the actual rates of activity (Phelps et al., 1994). The recent design of a suite of EAPs has permitted the determination of specific aerobic cometabolism of chlorinated ethylenes, most notably TCE. EAPs that serve as alternate substrates for TCE cometabolizing enzymes have been developed for four separate aromatic oxygenases (Keener et al., 1998; 2001; Miller et al., 2002; Clingenpeel et al., 2005), and for the soluble methane monooxygenase (SMMO; Miller et al., 2002) (Figure 2.2.4).

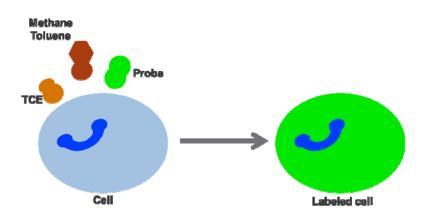
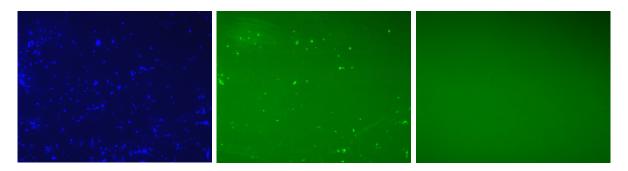


Figure 2.2.4. Schematic of Enzyme Activity Probes Showing Primary Substrates (methane/toluene), Co-metabolic Substrate (TCE) and EAP (Probe).

Once EAP is oxidized by co-metabolic enzyme, a fluorescent byproduct is generated, producing fluorescent cells. Other substrates that support TCE oxidation include: benzene; ammonia; phenol; naphthalene and propane.

These non-fluorescent probes are transformed by the enzymes into a quantifiable fluorescent signal upon transformation, thus providing direct evidence of cometabolic enzyme activity. Enzyme probes have been evaluated at a number of DOE and DOD sites over the last eight years (Lee et al., 2005; Lee et al., 2008; Wymore et al., 2007). Based on these analyses of contaminated groundwater, with TCE concentrations ranging from less than 100  $\mu$ g/L to over 10,000  $\mu$ g/L, it appears that enzyme probes provide a direct estimate of aerobic cometabolic enzyme activity for subsurface populations. As shown by this work, EAPs can provide valuable information regarding the presence and activity of in situ microbial enzyme systems important for aerobic cometabolism for plume-wide assessment of intrinsic assessment of degradation. Total bacteria present were determined by staining with DAPI (4,6-Diamidino-2-phenylindole), and these numbers are compared to bacteria fluorescing upon addition of EAP (Figure 2.2.5).



## Figure 2.2.5. The Micrograph on the Left Represents the Total Number of Microbial Cells (DAPI-stained); the Center Micrograph Represents the Cells that Transformed the Probe into a Fluorescent Product.

The right micrograph shows a negative response with the probe.

#### 2.2.3 Quantitative PCR (qPCR) for Oxygenase and Dioxygenase Genes

In general, qPCR provides an opportunity to identify specific microorganisms or even specific genes in a microbial community in order to assess the potential for that community to carry out a desired biotransformation process. Aerobic cometabolism of TCE is a fortuitous reaction catalyzed by diverse monooxygenases and dioxygenases with somewhat broad substrate ranges (Frascari et al., 2015). Because of the phylogenetic diversity of these enzymes (and the genes that code for them), it is impossible to develop a single nucleic acid-based biomarker for TCE-However, many of these enzymes do share structural cometabolizing microorganisms. similarities that are reflected in conserved stretches of their encoding DNA sequences, against which broadly-specific, degenerate PCR primers have been constructed. From environmental studies performed with these primers, it is known that there is abundant diversity in the recovered sequences (Baldwin et al., 2003; Nebe et al., 2009). Application of qPCR at contaminated sites provides quantification of a diverse range of known organisms and genes that are relevant to aerobic cometabolism. To date, qPCR is the only method that can identify the broad diversity of oxygenase genes and/or organisms known to possess those genes. In particular, qPCR allows for the assessment of genes and/or organisms relevant for aerobic cometabolism of chlorinated solvents. The qPCR results can be related back to the EAP results to provide a comprehensive assessment of changes in number and activity of genes along the midline of a contaminant plume or over spatial and/or temporal scales.

#### 2.2.4 Relationship between EAP and qPCR Targets

The enzyme probe data relates to the qPCR data as shown in the table below (Table 2.2.1). Some of the targets for the qPCR analyses do not directly correspond to EAP analyses and are completed in order to target other oxygenase enzymes which are known to also cometabolize contaminants such as chlorinated solvents. While there are dozens of known enzymes, some are more commonly found in environmental systems and/or are potential targets for remediation strategies such as bioaugmentation or biostimulation (propane, methane, benzene etc.). Table 2.2.1 provides a list of all of the qPCR targets considered for the current demonstration and completed herein.

## Table 2.2.1. Relationship between the EAP, the Oxygenase(s)/ Pathway and the qPCR Methods Completed Within.

Probe	Pathway	qPCR
3-hydroxyphenylacetylene	toluene-2-monooxygenase toluene-3-monooxygenase	RMO, PHE
	toluene-2,3-dioxygenase	TOD
	toluene-2,3-dioxygenase	TOD
phenylacetylene	toluene-3-monooxygenase toluene-2-monooxygenase	RMO, PHE
3-ethyylbenzoate	toluene-side-chain-monooxygenase	TOL
trans-cinnamonitrile	toluene-2,3-dioxygenase	TOD
coumarin, naphthalene	Soluble methane monooxygenase	mmoX, pmoA

#### 2.3 ADVANTAGES AND LIMITATIONS OF THE TECHNOLOGY

The advantages and limitations of the technology described in this report are described below. The authors are not aware of any alternative technologies.

#### Advantages:

The advantages of the methods described in this report include:

- The results presented in this report allow elucidation and quantification of degradation mechanisms that in the past could not be readily quantified using only existing monitoring wells. For example, in the past, soil samples were required to quantify magnetic susceptibility in an aquifer matrix. The use of a downhole magnetic susceptibility sonde circumvents this limitation. Also, as opposed to collecting discrete soil/sediment samples which are discontinuous along the length of the borehole, the use of a downhole sonde allows continuous readings along the length of the entire borehole in which a PVC monitoring well has been installed. This increases the level of detail for magnetic susceptibility measurements across the contaminated aquifer, thus allowing better characterization. The use of a downhole sonde also significantly reduces costs at those sites where exploratory site characterization has largely been completed and there are no plans for a drilling rig to be mobilized to the site in the future.
- Outside of the <sup>14</sup>C assay described in Appendix F, there is no technically viable approach to directly measure a rate constant for the natural biological cooxidation of TCE in groundwater. Aerobic co-oxidation of TCE by oxygenase enzymes yields products such as CO<sub>2</sub>, CO, formate, glycolate, and oxalate. These products are also formed during biodegradation of non-chlorinated and naturally occurring organic matter, and therefore prior to the work presented in this report, it was not possible to distinguish their source.

Furthermore, when the concentration of TCE in the environment is low relative to background organic matter, the concentration of biodegradation products formed from TCE co-oxidation may be very low by comparison. Use of <sup>14</sup>C-labeled TCE overcomes this problem, since all of the carbon-based products formed will also be labeled. Even trace levels of products are measurable, because of the extremely strong "signal" from <sup>14</sup>C.

- Use of <sup>14</sup>C-labeled TCE makes it possible to quantify the rate of TCE transformation with significantly greater precision than simply measuring the disappearance of TCE.
- The assay used for this project only utilized groundwater. It is shown in this report that rates of TCE co-oxidation are quantifiable without having to employ core samples in the assay. The sensitivity of the assay permits determination of transformation rates without the presence of core material.
- Although use of <sup>14</sup>C material can only be performed in laboratories permitted to use radioactive material, <sup>14</sup>C poses much lower hazards in comparison to other radioisotopes that are commonly used, e.g., for medical applications.
- EAP is a direct measurement of bacteria with active oxygenase enzymes, so few biases are associated with application of the technology. EAP is currently the only technology available to probe activity of oxygenases responsible for co-metabolism of TCE.
- qPCR is a proven and commercially available technology for determining the presence of bacteria carrying copies of oxygenase genes responsible for co-metabolism of TCE.

#### **Possible Limitations:**

The possible limitations of the work presented herein are:

- The magnetic susceptibility sonde cannot be used in stainless steel wells. Wells larger than 4 inches in diameter may be problematic for collecting accurate magnetic susceptibility data because of the size of the borehole required for such wells. However, larger sondes, with a larger radius of influence, are available.
- As mentioned above, <sup>14</sup>C assays can only be performed in laboratories that are permitted to use radioactive material. Furthermore, the cost for <sup>14</sup>C-labeled TCE is considerable (~\$11,000 per mCi), mainly because it is no longer available as a stock compound and must therefore be custom synthesized. If the assay is adopted for more frequent use, suppliers may opt to once again provide <sup>14</sup>C-labeled TCE as a stock item, which will decrease the cost.
- The <sup>14</sup>C assay is not yet commercialized. It is hypothesized that the successful demonstration of the protocol presented in this report will provide considerable motivation for private companies to offer the service. An analogous situation was the use of compound specific isotope analyses (CSIA). At one time, use of this technology for groundwater samples was limited to a select few academic laboratories. As the value of the approach became apparent, commercial laboratories stepped in to meet the growing demand. We anticipate that a similar outcome will develop for the <sup>14</sup>C assay proposed in this study.

- EAP at the current level of development are only a qualitative predictor of aerobic bioremediation, since probe response was never adequately calibrated to the actual rate of contaminant biodegradation in groundwater at field sites. EAP analytical services are currently only available through PNNL.
- qPCR can be affected by biases associated with DNA extraction, as well as issues associated with efficiency of DNA amplification.

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#### 3.0 PERFORMANCE OBJECTIVES

Tables 3.1.1 and 3.2.1 summarize the performance objectives, success criteria and data requirements for the demonstration. Subsequent sub-sections provide additional details regarding each performance objective. All performance objectives were met for this project.

#### 3.1 QUALITATIVE PERFORMANCE OBJECTIVES

This section discusses the qualitative performance objectives for this project, which are summarized in Table 3.1.1.

#### 3.1.1 Easy to Use Procedure for Collecting Magnetic Susceptibility Data

For magnetic susceptibility data to be useful there must be an inexpensive way to collect these data from existing monitoring wells. This is because most sites are past the borehole core data collection phase.

#### 3.1.1.1 Data Requirements

The primary data requirement for this performance objective was field implementation of the magnetic susceptibility sonde at various depths and in various conditions. Specifically, the field testing of existing, readily-available technology to quantify magnetic susceptibility in existing PVC monitoring wells using a magnetic susceptibility sonde to determine ease of use.

#### 3.1.1.2 Success Criteria

This qualitative performance objective is considered to be met because users are now able to easily obtain accurate magnetic susceptibility data in existing PVC monitoring wells using a commercially-available downhole magnetic susceptibility sonde.

#### 3.1.2 Develop an Assay Based on <sup>14</sup>C-TCE That Will Allow Determination of TCE Co-Oxidation Rates in Groundwater Samples

#### 3.1.2.1 Data Requirements

Development of the <sup>14</sup>C assay included an evaluation of a new method for purifying <sup>14</sup>C-TCE. The intent was to reach a higher level of purity than has previously been accomplished and thereby minimize interference from background contamination. The original method involved purification of the <sup>14</sup>C-TCE stock solution by an aliquot (50  $\mu$ L) through a GC column and injecting the gas flow into a serum bottle as the <sup>14</sup>C-TCE eluted, presumptively separated from any contaminants. A second method was evaluated that involved placing the first column in series with a second column. The details of each arrangement are described below.

The 160 mL glass serum bottles to which the purified TCE was added contained 100 mL of groundwater, filter sterilized groundwater (FSGW), or distilled deionized (DDI) water. The bottles were sealed with Teflon-faced grey butyl rubber septa and crimp caps. Before injecting the <sup>14</sup>C-TCE, approximately 50 mL of headspace was withdrawn from each bottle using a 100-mL gas-tight syringe (SGE Analytical Science, removable Luer Lock) to ensure the bottles were not over-pressurized. After the headspace withdrawal, the bottles were immediately inverted to reduce gas diffusion through the punctured Teflon-faced septa.

Objective(s)	Data Requirements	Success Criteria	Results				
Develop an approach for measuring magnetic susceptibility in non- metallic groundwater monitoring wells that provides data of useful quality.	uring magnetic ptibility in non- lic groundwater oring wells thatsusceptibility from sondes in monitoring wells that can be compared to measurements of magnetic susceptibility on core		This performance metric was met. Users have access to a commercially-available downhole sonde that has been validated to provide data of useful quality.				
Develop an assay based on <sup>14</sup> C-TCE that will allow for determination of TCE co-oxidation rates in groundwater samples.	n <sup>14</sup> C-TCE that willof accumulation of <sup>14</sup> Clow for determinationlabel in transformationTCE co-oxidationproducts of TCE intes in groundwatergroundwater samples		This performance metric was met for 8 out 19 groundwater samples that were evaluated. Out of the 19 groundwater samples evaluated, statistically significant rates of TCE co- oxidation were observed in 8 samples.				
Combined application of qPCR and EAP will show the presence of bacteria with active enzymes in groundwater.	Data on the abundance of bacteria in groundwater reacting to the EAP or that contain DNA that is amplified by the qPCR primers for oxygenase enzymes.	EAP and qPCR can be configured and implemented to provide sufficient sensitivity for application to diverse aerobic aquifers.	EAP and qPCR analyses were applied to 19 groundwater samples, meeting performance metrics by showing presence and activity of TCE cometabolizing bacteria at numerous sites.				
Compare consumption rates of <sup>14</sup> C-TCE to number of bacteria with active enzymes	Rate constants for cooxidation of TCE in water samples as determined by the <sup>14</sup> C-TCE assay and data on the abundance of bacteria reacting to the EAP or that contain DNA that is amplified by the qPCR primers.	In every well tested, a statistically significant rate constant and an abundance above the quantitation limit of bacteria reacting to one or more EAP or DNA that is amplified by one or more qPCR primer.	Cooxidation of TCE was only detected in 8 water samples where the rate constants for cooxidation were $> 0.01$ per year. The abundance of bacteria with active enzymes can only be used to evaluate sites where the rate constants are $> 0.01$ per year.				

<b>Table 3.1.1.</b>	Qualitative	Performance	<b>Objectives.</b>
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The original method employed a stainless-steel column packed with 1% SP-1000 on 60/80 Carbopack-B (8 ft x 1/8 in x 2.1 mm, Supelco, Inc.) (Darlington et al., 2008). The end of the column was connected to a four-port valve in the GC oven. The valve was positioned so that the flow exited the oven through stainless-steel tubing (1.59 mm) rather than going to a detector. The end of the tubing from the GC oven had a threaded Luer Lock fitting for attachment of a sterile needle, through which serum bottles were injected at a predetermined residence time to trap TCE as it eluted from the column. The carrier gas in the column was high purity N<sub>2</sub> (Airgas<sup>®</sup>) at a flow rate of 33.5  $\pm$  0.5 mL/min. The temperature program was 60 °C for 2 min, increase at 20°C per min to 150°C, increase at 10°C to 200°C and hold for 28.5 min.

Under these conditions, the elution time for TCE was 9.6 to 11.1 min. The GC program was continued after TCE eluted to minimize any possibility that contaminants in the stock solution might accumulate on the column.

For the second method, another stainless-steel column packed with 10% SP-1000 on 80/100 SUPELCOPORT (Supelco) was connected to the 4-port valve after the first column and before the stainless-steel tubing (1.59 mm). Addition of a second column significantly decreased the flow rate of the entire system. Thus, an isothermal temperature program at 200°C with a 20-min hold time was used to decrease the time interval that TCE eluted through both columns. At a carrier gas flow rate of  $10.3\pm0.2$  mL/min, the time interval for TCE to elute was 9.9 to 11.5 min.

Two sets of triplicate serum bottles containing 100 mL of DDI water were used to compare the two methods for adding <sup>14</sup>C-TCE. After adding the <sup>14</sup>C-TCE, a 3-mL aqueous sample was removed and processed as follows: it was added to a 20-mL glass vial; the pH was raised above 10 added by adding a drop of 8 M NaOH; it was sparged with N<sub>2</sub> for 30 min (550±50 mL/min); 15 mL of liquid scintillation cocktail was added; and the <sup>14</sup>C activity was quantified using a liquid scintillation counter. The average disintegrations per minute (dpm) in the 3 mL samples was 23.7±3.8 for the single column and 26.6±2.7 for the dual column approach; the difference is not statistically significantly (p = 0.35) (Appendix D). Consequently, the singly column method of purification was used for the <sup>14</sup>C assay. As noted in subsequent sections, this level of purification was adequate to permit detection of a half-life as long as 105 years.

#### 3.1.2.2 Success Criteria

 $\neq$ Őe success of the purification step is based on the level of impurities remaining at the start of the assay. The success of the assay is based on whether or not rates of <sup>14</sup>C-TCE transformation in samples from the field are discernable from rates in controls containing sterile DDI water.

The <sup>14</sup>C assay provides a tool to determine if TCE is undergoing transformation and if so, at what rate. Because of the specialized nature of the assay, it must be performed in a laboratory that is licensed to use <sup>14</sup>C labeled material. Nevertheless, the outcome of the assay is easily understandable to most end users, in the form of pseudo-first order rate coefficients. Based on the authors' experience teaching many university classes and giving professional training courses, the default metric to describe rates of biodegradation in groundwater are pseudo first-order rate constants. Scientists come to the courses and training familiar with first-order rate constants. Site managers are well acquainted with use of models to predict the rate of contaminant degradation based on first order transformation processes. The <sup>14</sup>C assay provides information in a familiar format that is needed to assess natural rates of attenuation.

#### 3.1.3 Methods for Identifying Presence and Activity of Co-Metabolic Bacteria for TCE Oxidation

Aerobic co-metabolism of chlorinated ethylenes such as TCE requires the presence of bacteria with oxygenases implicated in co-metabolism. Combined application of qPCR and EAP shows the presence of active enzymes in groundwater from the site.

#### 3.1.3.1 Data Requirements

Data on the abundance of bacteria in groundwater reacting to the EAP or that contain DNA that is amplified by the qPCR primers for oxygenase enzymes. Groundwater samples were collected and analyzed by qPCR and EAP to determine if microbial populations were detectable in site groundwater, thus demonstrating the potential for biodegradation.

#### 3.1.3.2 Success Criteria

EAP and qPCR can be configured and implemented to provide sufficient sensitivity for application to diverse aerobic aquifers. EAP and qPCR analyses were applied to 19 groundwater samples, meeting performance metrics by showing presence and activity of TCE cometabolizing bacteria at numerous sites.

### 3.1.4 Demonstrate Baseline Method for Linking TCE Transformation Rates to Numbers of Bacteria with Co-oxidation Enzymes

The baseline method uses data on the abundance of bacteria that react to an EAP or the amount of DNA that is amplified by a primer for an oxygenase enzyme to estimate or predict a plausible rate constant for TCE cooxidation. The method is calibrated by a comparsion to the data provided from the wells that are sampled in the survey. Under ideal conditions, it will be possible to extract a statistically significant rate constant from the data from each well, and it should be possible to measure the abundance of one or more EAPs and one or more primers in water from each well.

#### 3.1.4.1 Data Requirements

The data requirements are rate constants for <sup>14</sup>C-TCE cooxidation by bacteria in the groundwater samples and data on the abundance of bacteria that react to the EAPs and data on the abundance qPCR primers for oxygenase enzymes associated with bacteria that are known to cooxidize TCE.

#### 3.1.4.2 Success Criteria

The criteria for success in the survey of wells used to calibrate the baseline method are as follows. A rate constant for TCE cooxidation will be determined that is greater than zero at 95% confidence. In each particular water sample, the abundance of bacteria responding to at least one of the EAP assays is above the quantitation limit and the abundance of DNA amplified by at least one qPCR assay is above the quantitation limit.

#### **3.2 QUANTITATIVE PERFORMANCE OBJECTIVES**

This section discusses the qualitative performance objectives for this project, which are summarized in Table 3.2.1.

Objective(s)	Data Requirement(s)	Success Criteria *	Results
Quantify relationship between magnetic susceptibility from a direct-reading downhole sonde and that from laboratory analyses on samples from boreholes into which PVC monitoring wells were installed.	Magnetic susceptibility data from laboratory analyses of core samples from boreholes into which PVC wells were installed. A readily available magnetic susceptibility sonde (probe) was lowered into these same wells (Section 4), and real-time magnetic susceptibility data were collected.	The correlation between magnetic susceptibility determined using the sonde and that from laboratory analyses of core samples were determined. The Pearson's correlation coefficient, r, was be calculated. If r is greater than 0.75, then the criteria for this performance objective has been met.	The plot of mass magnetic susceptibility from the sonde versus that determined from lab analyses of core samples yields r = 0.94 and $R^2 = 0.88$ . Thus, this performance objective is met and the downhole sonde is considered to be a good tool for collecting representative magnetic susceptibility data from existing PVC wells.
Determine first order rate constants of TCE co- oxidation using a $^{14}$ C- TCE assay. Rate constants were determined by measuring the rate of accumulation of $^{14}$ C label in transformation products in water samples.	Data on the rate of accumulation of <sup>14</sup> C label in TCE transformation products as provided by the <sup>14</sup> C-TCE assay. Rate constants were determined in groundwater samples taken from 19 wells at five sites. There were four wells at each of four sites and three wells at one site.	Objective is met if the rates of <sup>14</sup> C product accumulation from <sup>14</sup> C-TCE in groundwater samples are statistically significant in comparison to controls containing filter sterilized groundwater at 95% confidence.	This performance metric was met in 8 of 19 water samples. Out of the 19 groundwater samples evaluated, statistically significant rates of TCE co-oxidation were observed in 8, with first order rates ranging from 0.00658 to 2.65 yr <sup>-1</sup> .
Quantify numbers of oxygenase genes present in groundwater community with qPCR analysis, and numbers of bacteria with active oxygenase enzymes can be quantified using EAP analysis.	Quantify activity of oxygenase genes based on EAP and surrogate qPCR measurements. Quantify activity measured for positive control organisms, negative controls, matrix spikes and blanks to determine specificity of EAP and qPCR. Quantify activity in replicate samples from same well.	EAP and qPCR techniques provide reproducible data when comparing groundwater replicates (<30% RPD). Blanks have no background fluorescence. Positive controls show active enzymes. Matrix spikes provide 70 to 130% recovery of positive control organism. Control assays perform as expected.	This performance metric was achieved. EAP and qPCR provided reproducible data between replicates. Controls such as blanks, matrix spikes, and positive controls demonstrated expected results that fell within established criteria. In general, qPCR results corresponded to the EAP results for the PHE and RMO primer sets, but not for the TOD and TOL primer sets. Gene targets for sMMO were only detected significant levels (>103 cells/ml) at three of the 19 wells tested.
Demonstrate ability to determine TCE transformation rates by numbers of bacteria with active co-oxidation enzymes determined by EAP and qPCR	Rate constants for cooxidation of TCE in water samples as determined by the <sup>14</sup> C-TCE assay and data on the abundance of bacteria reacting to the EAP or that contain DNA that is amplified by the qPCR primers	The slope of a regression of the common logarithm of the rate constant for TCE cooxidaiton on the common logarithm of the abundance of EAP or qPCR markers will be greater than zero at 95% confidence.	The slope was greater than zero at 95% confidence for the CINN EAP and for the PHE, RMO, and MMO qPCR markers. The the prediction interval of the regression was used to develop a screening approach to evaluate whether TCE cooxidation might be useful for MNA at a site.

#### Table 3.2.1. Quantitative Performance Objectives

#### **3.2.1** Evaluate the Accuracy of Data for Mass Magnetic Susceptibility

#### 3.2.1.1 Data Requirements

To verify the validity of the data collected using the magnetic susceptibility sonde, a commercially-available sonde was deployed in wells where soil samples were collected from soil borings prior to well installation and analyzed for mass magnetic susceptibility in an analytical laboratory. The data collected using the downhole sonde were then compared to these previously-collected soil data and the relationship between the magnetic susceptibility data from the laboratory and the magnetic susceptibility measurements made using the sonde were determined.

#### 3.2.1.2 Success Criteria

The correlation between mass magnetic susceptibility determined using the sonde and mass magnetic susceptibility data collected using laboratory analysis of soil/sediment data was determined. Specifically, the Pearson's correlation coefficient, r, was calculated from a plot of mass magnetic susceptibility obtained from the sonde versus that obtained from laboratory analyses of core samples. The success criteria for this quantitative performance objective is a Pearson's correlation coefficient, r, between the core means and the sonde means of greater than 0.75. As discussed in Section 5.7, for the work presented in this report, r = 0.94, and the coefficient of determination,  $R^2 = 0.88$ . Thus, the magnetic susceptibility sonde provides a good tool for collecting representative data from existing non-metallic (PVC) monitoring wells.

#### **3.2.2** Determine First-Order Rates of TCE Co-Oxidation Using a <sup>14</sup>C-TCE Assay

#### 3.2.2.1 Data Requirements

Development of the <sup>14</sup>C assay included evaluation of a new method for purifying <sup>14</sup>C-TCE. The intent was to reach a higher level of purity than has previously been accomplished and thereby minimize interference from background contamination.

The <sup>14</sup>C assay was tested with a sample of surface water that was locally sourced, from theTwin Lakes Recreation Area on Lake Hartwell near Pendleton, SC. The site is ~10 min driving distance from the Freedman laboratory, in order to minimize changes during transport. Measurements of <sup>14</sup>C degradation products began immediately after adding <sup>14</sup>C-TCE to microcosms containing water from a seep discharges into an area with a high level of organic debris. The rate of accumulation of <sup>14</sup>C products was used to determine the pseudo-first order rate of TCE transformation, by fitting the data to a mass balance model for <sup>14</sup>C in the microcosms.

Additional tests to evaluate the efficacy of the <sup>14</sup>C assay were performed with a propanotrophic enrichment culture. This culture served as a positive control, since propanotrophs are known to be capably of biodegrading TCE via cometabolism.

Groundwater samples were immediately placed on ice after collection. The intent of doing so was to slow the rate of microbial activity until <sup>14</sup>C-TCE could be added in the laboratory. The effect of storage conditions on the outcome of the <sup>14</sup>C assay was evaluated using the propanotrophic culture. A 0.25% dilution was selected based on the results from the experimental described below. Three conditions were used to test the effects of temperature, each in triplicate: 1) ambient room temperature; 2) storage on ice for 24 h, then warmed for 2.5 h; and 3) storage on ice for 24 h, then warmed for 2.4 h; the latter most closely resembles how the groundwater samples were handled.

<sup>14</sup>C-TCE was added using the single column method, following the respective temperature treatments. The bottles were monitored for accumulation of <sup>14</sup>C products for 40 days.

#### 3.2.2.2 Success Criteria

#### Impurities in the <sup>14</sup>C-TCE Stock Solution

The initial goal for demonstrating the success of the purification step was to reduce the presence of <sup>14</sup>C impurities (i.e., <sup>14</sup>C not attributable to TCE) to less than 0.01% of the total <sup>14</sup>C activity. As indicated in section 2.2.2.1, the intent was to achieve this goal using two GC columns in series to purify the <sup>14</sup>C-TCE stock solution prior to adding it to the serum bottles. However, preliminary testing indicated that a single column was just as effective, so that approach was used when testing the DDI water and groundwater samples.

The level of impurities added to serum bottles was determined by comparing the dpm present in water samples after sparging, with and without <sup>14</sup>C-TCE added. For DDI water, the average dpm in 3 mL samples was 25.6±2.4, compared to 11.8±1.2 in samples of DDI water that did not receive <sup>14</sup>C-TCE. For groundwater samples, the average dpm in 3 mL was 29.5±6.4, compared to 12.0±0.9 in samples of DDI water that did not receive <sup>14</sup>C-TCE. The differences in dpm between the 3 mL samples with and without <sup>14</sup>C-TCE added (17.5 and 13.9, respectively) were presumably due to contaminants. For the groundwater samples, this amounted to 0.07% of the total dpm added to the serum bottles. For the DDI water, the residual level of dpm present amounted to 0.05% of the total dpm added to the serum bottles. From this perspective, the purification goal was not met. However, the goal was predicated on a shorter incubation time (~2 days) than what was ultimately adopted (up to 46 days). The longer incubation time affords a greater opportunity to detect a statistically significant rate of product accumulation above the controls, even with a background of impurities that is above 0.01%. As the results show, the lowest net rate quantified (0.00658 yr<sup>-1</sup>) translates to a half-life of 105 years, which indicates the assay is sufficiently sensitive. On this basis, the level of purification achieved is considered successful.

It should also be noted that the level of impurities reported above may not actually be impurities. The assessment of impurities involved adding the <sup>14</sup>C-TCE to the DDI water controls and then waiting approximately one hour before removing the 3 mL samples. It is quite possible that the higher level of <sup>14</sup>C products in these bottles was actually a consequence of decay, rather than impurities. Regardless, even if the activity reported was decay, the assay was still sensitive enough to detect low rates of TCE co-oxidation.

One of the concerns with the residual level of <sup>14</sup>C remaining after sparging was the possibility that 30 min of sparging was not sufficient to completely remove all of the TCE. This was evaluated by comparing residual levels of <sup>14</sup>C in samples that were sparged for 30 min versus 60 min. Triplicate serum bottles were prepared with DDI water and <sup>14</sup>C-TCE was added to each. After allowing the TCE to equilibrate between the headspace and liquid phases, duplicate 3 mL samples were removed from each bottle; one was sparged for 30 min and the other for 60 min. There was no statistically significant difference in the residual level of <sup>14</sup>C (p = 0.58) (Appendix D), indicating that TCE was not likely responsible for the residual levels reported above.

#### Preliminary Evaluation of the <sup>14</sup>C Assay Using Locally Sourced Water

As indicated above, a preliminary evaluation of the assay was performed with locally sourced water. Samples from a seep area were added to serum bottles and immediately capped in the field. Upon arrival at Clemson University, <sup>14</sup>C-TCE was added. Triplicate DDI water controls were prepared at the same time. There was a statistically significant rate of <sup>14</sup>C product accumulation in the bottles with surface water and in the DDI water controls (Appendix D). The first order rates were  $5.00 \times 10^{-2} \pm 3.56 \times 10^{-2}$  yr<sup>-1</sup> for the surface water samples and  $2.63 \times 10^{-2} \pm 1.29 \times 10^{-2}$  yr<sup>-1</sup> for the DDI water controls. Accumulation of <sup>14</sup>C products in the DDI water controls was likely a consequence of autoradiolysis of the <sup>14</sup>C-TCE. A Student's *t*-test indicated the first order rates are statistically different; consequently, a net rate of  $2.37 \times 10^{-2} \pm 1.67 \times 10^{-2}$  yr<sup>-1</sup> was calculated, which gives a half-life of 29 yr (95% confidence interval = 17-99 yr). These results confirm that the assay is capable of detecting co-oxidation rates that are useful for evaluating natural attenuation.

#### Experimental Controls

To determine rate constants for co-oxidation of TCE, it was necessary to demonstrate that the accumulation of <sup>14</sup>C products from <sup>14</sup>C-TCE was due to biotic activity and not a background level of reaction with the water. Initialy, DDI water served as the negative control. For each of the five sites, triplicate DDI water controls were prepared and monitored alongside the serum bottles containing groundwater. Subsequently, filter-sterilized groundwater (FSGW) was used for this purpose. When enough groundwater was available, FSGW controls were prepared for each well. A 47-mm nylon membrane filter disk with 2  $\mu$ m pores (Whatman<sup>TM</sup>) was used for this purpose. When not enough groundwater was available for a particular well to prepare FSGW controls, a control from the closest well was used. Use of the FSGW controls made it possible to improve the sensitivity of the assay, allowing for detection of TCE co-oxidation at rates even lower than those measured in the preliminary samples from Twin Lakes. Apparently, FSGW controls control for the assay. Overall, the rate of <sup>14</sup>C-TCE and therefore FSGW serves as a more representative control for the assay. Overall, the rate of <sup>14</sup>C-product accumulation in FSGW controls was 38% lower than in DDI water controls.

A mixed propanotrophic culture (ENV487), known to co-metabolize TCE, was used as a positive control for validating the assay. The mixed culture was obtained courtesy of Dr. Robert Stefan at Chicago Bridge and Iron, Inc. It was grown on propane gas and pure oxygen in basal salt medium (BSM) to a density of ~  $5.3 \times 10^{10}$  cell/mL, as previously described (Rodríguez, 2016). Following consumption of repeated additions of propane and oxygen, dilutions (25%, 2.5%, 0.25%, and 0.025%) were prepared with BSM in 160 mL serum bottles and <sup>14</sup>C-TCE was added. Accumulation of <sup>14</sup>C products is shown in Figure 3.2.1. Even in the most dilute treatment, the rate of product accumulation was significantly greater than in the BSM control with no cells present, in which there was no significant accumulation of products. The pseudo first-order rate constant and associated 95% confidence interval (CI) for the 0.01% dilution was  $1.71 \times 10^{-1} \pm 5.60 \times 10^{-2}$  yr<sup>-1</sup>, which gives a half-life of 4.1 years (95% CI = 3.1 to 6.0 yr). As shown below, this rate is similar to the rates determined for several of the groundwater samples. Additional testing is needed to determine how low a rate of TCE co-oxidation can be detected with the propanotrophic culture.

It is noteworthy that there was no statistically significant increase in <sup>14</sup>C products in the BSM control. This suggests that the BSM contains compounds that reduce the effects of radical production from autoradiolysis of <sup>14</sup>C-TCE. The compounds responsible may include the bicarbonate buffer and the nitroloacetic acid used to chelate the trace metals. In contrast, all of the DDI water controls and FSGW controls exhibited statistically significant rates of <sup>14</sup>C product accumulation; this made it necessary to check if the first order rate in the groundwater samples was statistically greater than in the controls. In eight of the wells tested, this was observed, so a net rate was calculated by subtracting out the rate of product accumulation in the FSGW controls. In the remaining well samples, the rate of product accumulation was not statistically greater than in the FSGW controls.

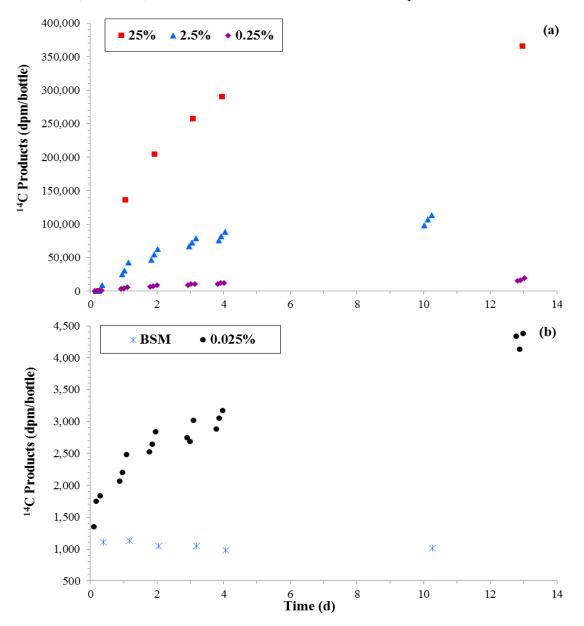


Figure 3.2.1. Accumulation of <sup>14</sup>C Products from <sup>14</sup>C-TCE Added to Various Dilutions of a Propanotrophic Enrichment Culture¶(a) 25%, 2.5%, 0.25%; and (b) 0.025% and the BSM Control with No Cells.

The data shown were fit to a mass balance model to determine first order rates of TCE co-oxidation.

#### Effect of Storage Conditions

The effect of storage conditions on the rate of  ${}^{14}$ C product accumulation are shown in Figure 3.2.2. Rates were very similar for the control treatment that was never cooled down to 4 °C (blue circles) and the treatment that was held at 4 °C for 2.5 h before being warmed to room temperature (red squares). The treatment that was held at 4 °C for 24 h before being warmed to room temperature (black triangles) behaved differently; this was most pronounced after day 4, as the accumulation rate slowed noticeably. However, when only the first 5 days of data were considered, there were no statistically significant differences among the first order rate coefficients. These results suggest that the conditions under which the groundwater samples were handled (i.e., shipment and storage on ice overnight, followed by warming to room temperature overnight) may have decreased the reaction rate. Consequently, the rates reported in this study are likely conservative. It is difficult to envision a different approach to handling the samples, since they need to be shipped to a laboratory to perform the <sup>14</sup>C-TCE assay. Additional studies on the effect of storage conditions using groundwater samples is warranted.

Based on the results presented in this report, the <sup>14</sup>C assay provides a tool to determine if TCE is undergoing transformation and, at what rate. Because of the specialized nature of the assay, it must be performed in a laboratory that is licensed to use <sup>14</sup>C labeled material. Nevertheless, the outcome of the assay is easily understandable to most end users, in the form of first order rate coefficients. Site managers are well acquainted with use of models to predict the rate of contaminant degradation based on first order transformation processes. The <sup>14</sup>C assay provides information in a familiar format that is needed to assess natural rates of attenuation.

#### 3.2.3 Quantification of Bacteria with Active Enzymes Associated with TCE Co-Metabolism

Numbers of oxygenase gene copies present in the groundwater community can be quantified with qPCR analysis, and numbers of bacteria with active oxygenase enzymes can be quantified using EAP analysis.

#### 3.2.3.1 Data Requirements

Collect and analyze groundwater samples to quantify activity of oxygenase genes based on EAP and surrogate qPCR measurements. Quantify activity measured for positive control organisms, negative controls, matrix spikes and blanks to determine specificity of EAP and qPCR. Quantify activity in replicate samples from the same groundwater monitoring well.

#### 3.2.3.2 Success Criteria

EAP and qPCR techniques provide reproducible data when comparing groundwater replicates (<30% RPD). Blanks have no background fluorescence. Positive controls show active enzymes. Matrix spikes provide 70 to 130% recovery of positive control organism. Control assays perform as expected demonstrating specificity and activity of qPCR primers and EAP probes.

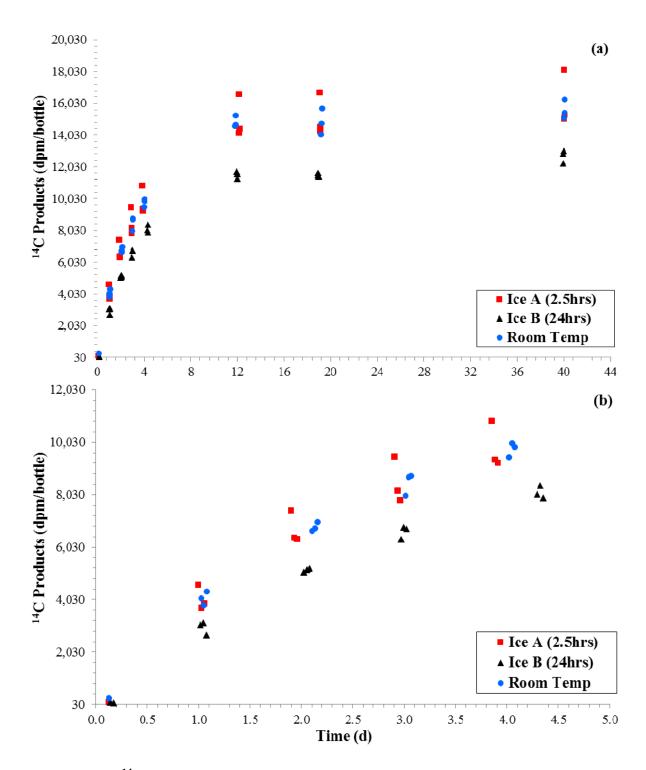


Figure 3.2.2. <sup>14</sup>C Product Accumulation in a 0.25% Propanotrophic Enrichment Culture Subjected to Different Storage and Warming Conditions Followed by Incubation with <sup>14</sup>C-TCE for (a) 40 Days and (b) the Same Bottles Showing Only the First 4 days.

*Ice A represents storing bottles on at 4 °C for 24 hrs, then warming to room temperature for 2.5 hrs. Ice B represents storage on ice for 24 hrs, then warming for 24 hrs.* <sup>14</sup>C-TCE was added immediately to the room temperature bottles.

## **3.2.4** Demonstrate Ability to Predict TCE Co-Oxidation Rates by Quantifying Number of Bacteria With Active Co-oxidation Enzymes

Linear regression will be used to evaluate the relationship between the rate constant for TCE cooxidation and abundance of bacteria that react with individual EAP or the abundance of DNA that is amplified by qPCR primers for selected oxygenase enzymes. The rate constants and the abundance data vary over several orders of magnitude. Linear regression assumes that the variance of the y data follows a normal distribution. To make the variance in the rate constants fit a normal distribution, the regression was performed usisng the logarithm of the rate constant and the logarithm of the abundance of the reactive cells or abundance of the DNA amplified by the primer.

#### 3.2.4.1 Data Requirements

The data requirements are rate constants for <sup>14</sup>C-TCE cooxidation by bacteria in the groundwater samples and data on the abundance of bacteria that react to the EAPs and data on the abundance of qPCR primers for oxygenase enzymes associated with bacteria that are known to cooxidize TCE.

#### 3.2.4.2 Success Criteria

For the purposes of the baseline method, a particular EAP or qPCR primer will be usedful to predict the rate constant for TCE cooxidation in the groundwater plume when the slope of the regression of the common logarithm of the rate constant on the common logarithm of the abundance of the EAP or qPCR marker is greater than zero at 95% confidence. If an EAP or qPCR primer is useful, the prediction interval on the rate constant will be used to evaluate whether the rate constant is might be useful for MNA at a particular site.

#### 4.0 SITE DESCRIPTIONS

This section provides a concise summary of the demonstration site(s) and includes site information that is relevant to the technology. In addition, it summarizes the work done at each site during the field effort.

#### 4.1 OVERVIEW

The following five (5) sites were selected for analysis under this program because there is an existing database for either the magnetic susceptibility of core samples from the site, or because there are existing data on the numbers of bacteria in groundwater that have enzymes that might degrade TCE, or both. In addition to the sites listed here, one other site was used for the magnetic susceptibility analysis, but no samples were collected for the <sup>14</sup>C assay or the EAP/qPCR analyses. Specifically, monitoring well U2-043 at OU-2 at Hill AFB was analyzed for mass magnetic susceptibility by collecting borehole core samples on December 7<sup>th</sup> and 8<sup>th</sup> 2015. Because the sampling team was so close to this Operable Unit during sampling at Hill AFB, OU-10, groundwater monitoring well U2-043 was sampled with the downhole sonde upon completion of sampling at OU-10. The sonde and borehole core laboratory analytical data from monitoring well U2-043 are included in the statistical analyses completed in this report.

Table 4.1.1 contains the well completion information for those wells sampled during this effort. Table 4.1.2 presents the laboratory magnetic susceptibility results for borehole core samples and grab samples for 10-20 silica sand.

#### Table 4.1.1. Well Completion Information for Those Wells Sampled During this Effort.

Well I.D.	Date	Easting	Northing	Ground Surface Elevation (feet msl)	Well Diameter (Inches)	Borehole Diameter (Inches)	W ell Material	Stick Up (feet)	Riser/Top of Casing Elevation (feet msl)	Depth to Top of Screen (feet bgs)	Depth to Base of Screen (feet bgs)	Elevation at Top of Screen (feet bgs)	Elevation at Base of Screen (feet bgs)	Depth to Water (feet btoc)	Ground- water Elevation (feet msl)	Magnetic Susceptibility	Groundwater Sample for <sup>14</sup> C TCE Assay, EAP, and qPCR
	Former Plattsburgh AFB																
MW-02-006	6/6/2016	722275.88	1700372.52	245.80	2.00	8.40	PVC	3.22	249.02	27.00	37.00	218.80	208.80	33.45	215.57	1	1
MW-02-019	6/6/2016	722797.86	1700168.45	228.20	2.00	9.60	PVC	0.00	228.20	9.00	24.00	219.20	204.20	16.74	211.46	1	1
32PLTW12	6/7/2016	724106.10	1699268.69	204.72	0.75	NA	NA	NA	204.62	15.00	18.00	189.72	186.72	13.70	190.92		1
35PLT13	6/7/2016	724336.46	1698809.87	194.76	0.75	NA	NA	NA	194.58	22.00	25.00	172.76	169.76	10.35	NA		1
							T	CAAP									
01U-119	1/26/1987	486563.00	4994616.00	898.00	4.00	6.63	PVC	2.00	898.00	9.50	19.50	888.50	878.50	7.10	890.90	1	1
01U-108	8/2/1985	486497.00	4994667.00	904.00	2.00	6.63	PVC <sup>a</sup>	2.00	904.00	20.00	30.00	884.00	874.00	14.00	890.00	1	1
01U-117	1/21/1987		4994693.00	903.00	4.00	6.63	PVC	1.80	903.00	18.00	33.00	885.00	870.00	10.70	892.30	1	1
01U-115	1/19/1987	486355.00	4994726.00	901.00	4.00	6.63	PVC	1.90	901.00	17.90	32.90	883.10	868.10	12.26	888.75	1	1
							Hill A										
OU10-019	11/14/2002	NA	NA	NA	2.00	8.00	PVC	2.50	NA	81.00	91.00	NA	NA	??	NA	1	1
OU 10-025 <sup>b/</sup>	7/7/2004	1853352.83	287410.33	4493.80	2.00	8.00	PVC	Flush	4492.96	27.00	37.00	4466.80	4456.80	13.56	4479.40	1	1
OU10-043	NA	1854700.27	288430.06	4546.11	2.00	8.00	PVC	Flush	4545.29	20.00	30.00	4526.11	4516.11	10.70	4534.59	1	1
OU10-051	11/21/2004	1855416.44	289048.53	4565.74	4.00	9.63	PVC	2.04	4576.78	171.20	211.20	4394.54	4354.54	133.90	NA	1	
						Ε	[opewell	Precisi	on Site								
EPA-8S	12/22/2006	688671.47	1012878.00	303.40	2.00	6.25	PVC	Flush	303.40	20.00	30.00	283.40	273.40	15.50	287.90	1	
EPA-10S	12/11/2006	687576.84	1011997.62	296.10	4.00	6.25	PVC	Flush	296.10	25.00	35.00	271.10	261.10	9.02	287.08	1	1
EPA-10D	12/11/2006	687576.86	1011990.02	296.43	4.00	6.25	PVC	Flush	296.43	45.00	55.00	251.43	241.43	8.85	287.58	1	
EPA-12S	12/14/2006	685654.24	1010697.40	289.36	4.00	6.25	PVC	Flush	289.36	20.00	30.00	269.36	259.36	10.40	278.96	1	1
EPA-12D	12/14/2006 1/18/2007		1010701.16	289.43	4.00	6.25	PVC	Flush	289.43	35.00 30.00	45.00	254.43 262.50	244.43	10.00	279.43	1	
EPA-15D EPA-16S	1/3/2007	684810.35 685807.51	1010325.08	292.50	4.00	6.25	PVC	Flush	292.50	20.00	40.00	202.50	252.50 262.94	19.90	272.60	1	1
EPA-165 EPA-16D	12/21/2006	685807.51	1010189.44	292.86 293.00	4.00	6.25 6.25	PVC PVC	Flush Flush	292.86 293.00	40.00	50.00	272.86	262.94	13.40 13.03	279.46	1	
EPA-19S	1/23/2007	684228.48	1010150.34	295.00	2.00	6.25	PVC	Flush	293.00	15.00	25.00	255.00	243.00	23.31	259.45	1	
EPA-19D	1/22/2007	684224.29	1008560.62	282.91	2.00	6.25	PVC	Flush	282.91	40.00	50.00	242.91	232.91	23.42	259.49	1	
EPA-21S	1/23/2007	683399.18	1006836.10	267.91	2.00	6.25	PVC	Flush	267.91	15.00	25.00	252.91	242.91	16.82	251.09	1	
EPA-21D	1/24/2007	683404.55	1006841.60	267.81	2.00	6.25	PVC	Flush	267.81	33.00	38.00	234.81	229.81	17.05	250.76	1	
							Tooele A	Army D	epot								
D-19	7/15/2005	NA	NA	4494.99	4.00	10.00	PVC	2.76	4497.75	148.00	168.00	4346.99	4326.99	140.71	4357.04	1	1
D <b>-2</b> 0	9/27/2009		7385352.16	NA	4.00	8.00	PVC	NA	4398.57	68.50	88.50	NA	NA	62.09	4336.48	1	1
D-23	10/5/2011	NA	NA	4395.70	4.00	8.00	PVC	2.65	4398.35	190.00	210.00	4205.70	4185.70	58.18	4340.17	1	1
D-25	12/19/2011	NA	NA	4384.89	4.00	8.00	PVC	2.85	4387.74	175.50	195.50	4209.39	4189.39	79.75	4307.99	1	1
															Totals	26	19

#### ESTCP Project Number ER-201584

Notes:

NA = Not Available at this Time

a/ 7 feet of 4" steel protective casing, 2" PVC screen, Slide five in TCAAP Well logs. pptx

b/ Well Completion Log Says U10-026 but Todd Isackson says it's for U10-025



D:\THWWESTCP\_ER-201584\Report - TechnicaNTables\Table 4.1.1 - We I Completion Details.xtx

## Table 4.1.2. Laboratory Magnetic Susceptibility Results for Borehole Core Samples and<br/>Grab Samples for 10-20 Silica Sand

Sample Identification         Date         Depth (ft) bgs)         Elevation (ft ams)         Mass Magnetic Susceptibility (m <sup>3</sup> /sg)         Error Range (m <sup>3</sup> /sg)           Well U2-043 Hill AFB, UTAH, Operable Unit 2 <sup>st</sup> 2003-SB-A $127/-8/2015$ 73.5         – $2.03E-07$ – $\pm$ $\pm$ $1.28E-08$ U2043-SB-A $127/-8/2015$ 73.5         – $8.63E-08$ – $\pm$ $3.78E-09$ U2043-SB-A $127/-8/2015$ 75.1         – $1.09E-07$ – $\pm$ $3.78E-09$ U2043-SB-A $127/-8/2015$ 75.9         – $2.03E-07$ – $\pm$ $2.49E-09$ U2043-SB-B $127/-8/2015$ 77.8         – $9.94E-08$ – $\pm$ $5.93E-09$ U2043-SB-B $127/-8/2015$ 77.8         – $9.90E-08$ – $\pm$ $5.93E-09$ U2043-SB-B $127/-8/2015$ 70.4         – $9.58E-08$ – $\pm$ $2.79E-09$ Average of Borehole Core Laboratory Analyses For Sonde Inteval $1.40E-07$ – $ N/A$ <t< th=""><th></th><th>ESICII</th><th>Toject Numo</th><th>er ER-201584</th><th></th><th></th><th></th><th></th></t<>		ESICII	Toject Numo	er ER-201584				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Sample Identification	Date		the second secon	Susceptibility	Flag <sup>b/</sup>	110000	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Well U2-043 Hill AFB, UTAH, (	Operable Unit	t 2 <sup>a/</sup>					
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					2.03E-07		±	1.28E-08
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	U2043-SB-A	12/7-8/2015	73.5		8.63E-08		±	4.72E-09
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		12/7-8/2015	74.3		8.33E-08		±	3.78E-09
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	U2043-SB-A	12/7-8/2015	75.1		1.79E-07		±	2.49E-09
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	U2043-SB-A	12/7-8/2015	75.9		2.03E-07		±	6.21E-09
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	U2043-SB-B	12/7-8/2015	76.2		2.58E-07		±	1.47E-08
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	U2043-SB-B	12/7-8/2015	77.0	26.22	9.94E-08		±	5.93E-09
U2043-SB-B       12/7-8/2015       79.4        9.58E-08 $\pm$ 2.79E-09         Average of Borehole Core Laboratory Analyses For Sonde Inteval =       1.40E-07         N/A         Toole Army Depot        9/27/2011-       63.5        1.48E-07         N/A         Wells D23 <sup>cf</sup> 9/27/2011-       63.5        1.48E-07         N/A         Wells D23 <sup>cf</sup> 9/27/2011-       67.5        1.04E-07         N/A         Wells D23 <sup>cf</sup> 9/27/2011-       69.5        2.41E-07        N/A         Well D23 <sup>cf</sup> 9/27/2011-       73.5        3.31E-07        N/A         Well D23 <sup>cf</sup> 9/27/2011-       78.5        4.72E-07        N/A         Well D20 <sup>cf</sup> 9/25/2009-       75.5        2.25E-07        N/A         Well D20 <sup>cf</sup> 9/25/2009-       85.5        9.37E-07        N/A         Well D20 <sup>cf</sup> 9/25/2009-       89.5        1.47E-07        N/A         Well D20 <sup>cf</sup> </td <td>U2043-SB-B</td> <td>12/7-8/2015</td> <td>77.8</td> <td></td> <td>9.90E-08</td> <td></td> <td>±</td> <td>6.38E-09</td>	U2043-SB-B	12/7-8/2015	77.8		9.90E-08		±	6.38E-09
Average of Borehole Core Laboratory Analyses For Sonde Inteval =       1.40E-07         Confidence Level (95.0%) =       4.56E-08         Tooele Army Depot         Wells D23 <sup>cf</sup> 9/27/2011- 10/05/2011       63.5       -       N/A         Wells D23 <sup>cf</sup> 9/27/2011- 10/05/2011       67.5       -       N/A         Wells D23 <sup>cf</sup> 9/27/2011- 10/05/2011       69.5       -       N/A         Well D23 <sup>cf</sup> 9/27/2011- 10/05/2011       -       N/A         Well D23 <sup>cf</sup> 9/27/2011- 78.5       -       A.72E-07       -       N/A         Well D20 <sup>cf</sup> 9/25/2009- 9/25/2009- 9/27/2009       85.5       -       N/A         Well D20 <sup>cf</sup> 9/25/2009- 9/25/2009- 89.5       -       N/A         Off Horehole Core Laboratory Analyses For Sonde Inteval =       3.26E-07         Confidence Level (95.0%) =       2.29E-07         TCAAP         OIU-108       7/14/2005       19	U2043-SB-B	12/7-8/2015	78.6		9.77E-08		±	1.78E-09
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	U2043-SB-B	12/7-8/2015	79.4		9.58E-08		±	2.79E-09
Tooele Army Depot           Wells D23 <sup>cf</sup> 9/27/2011- 10/05/2011         63.5         -         N/A           Wells D23 <sup>cf</sup> 9/27/2011- 10/05/2011         67.5         -         1.04E-07           N/A           Wells D23 <sup>cf</sup> 9/27/2011- 10/05/2011         69.5          2.41E-07          N/A           Well D23 <sup>cf</sup> 9/27/2011- 10/05/2011         73.5          3.31E-07          N/A           Well D23 <sup>cf</sup> 9/27/2011- 10/05/2011         78.5          4.72E-07          N/A           Well D20 <sup>cf</sup> 9/25/2009- 9/25/2009- 9/25/2009- 9/27/2009         75.5         -         2.25E-07          N/A           Well D20 <sup>cf</sup> 9/25/2009- 9/25/2009- 9/27/2009         85.5          9.37E-07          N/A           Well D20 <sup>cf</sup> 9/25/2009- 9/25/2009- 9/27/2009         89.5          1.47E-07          N/A           Mull D20 <sup>cf</sup> 9/25/2009- 9/25/2009- 9/27/2009         89.5          1.47E-07          N/A           Mull D20 <sup>cf</sup> 9/25/2009- 9/25/2009- 9/27/2009         89.5         <	Average of Borehole Core Lab	oratory Analys	es For Son	de Inteval =				
Wells D23 <sup>cf</sup> 9/27/2011- 10/05/2011       63.5        1.48E-07        N/A         Wells D23 <sup>cf</sup> 9/27/2011- 10/05/2011       67.5        1.04E-07        N/A         Wells D23 <sup>cf</sup> 9/27/2011- 10/05/2011       69.5        2.41E-07        N/A         Wells D23 <sup>cf</sup> 9/27/2011- 10/05/2011       73.5        3.31E-07        N/A         Well D23 <sup>cf</sup> 9/27/2011- 10/05/2011       78.5        4.72E-07        N/A         Well D20 <sup>cf</sup> 9/25/2009- 9/27/2009       75.5        2.25E-07        N/A         Well D20 <sup>cf</sup> 9/25/2009- 9/27/2009       85.5        9.37E-07        N/A         Well D20 <sup>cf</sup> 9/25/2009- 9/27/2009       89.5        1.47E-07        N/A         Mell D20 <sup>cf</sup> 9/25/2009- 9/27/2009       89.5        1.47E-07        N/A         Mell D20 <sup>cf</sup> 9/25/2009- 9/27/2009       89.5        1.47E-07        N/A         Mult D20 <sup>cf</sup> 9/25/2009- 9/27/2009       89.5        1.47E-07        N/A         Mul		Confi	dence Leve	el (95.0%) =	4.56E-08			
Wells D23 <sup>cf</sup> 9/27/2011- 10/05/2011       63.5        1.48E-07        N/A         Wells D23 <sup>cf</sup> 9/27/2011- 10/05/2011       67.5        1.04E-07        N/A         Wells D23 <sup>cf</sup> 9/27/2011- 10/05/2011       69.5        2.41E-07        N/A         Wells D23 <sup>cf</sup> 9/27/2011- 10/05/2011       73.5        3.31E-07        N/A         Well D23 <sup>cf</sup> 9/27/2011- 10/05/2011       78.5        4.72E-07        N/A         Well D20 <sup>cf</sup> 9/25/2009- 9/27/2009       75.5        2.25E-07        N/A         Well D20 <sup>cf</sup> 9/25/2009- 9/27/2009       85.5        9.37E-07        N/A         Well D20 <sup>cf</sup> 9/25/2009- 9/27/2009       89.5        1.47E-07        N/A         Mell D20 <sup>cf</sup> 9/25/2009- 9/27/2009       89.5        1.47E-07        N/A         Mell D20 <sup>cf</sup> 9/25/2009- 9/27/2009       89.5        1.47E-07        N/A         Mult D20 <sup>cf</sup> 9/25/2009- 9/27/2009       89.5        1.47E-07        N/A         Mul	Tooele Army Depot							
Wells D23 <sup>°</sup> $10/05/2011$ 63.5 $1.48E.07$ N/A         Wells D23 <sup>°/</sup> $9/27/2011$ - 10/05/2011       67.5 $1.04E.07$ N/A         Wells D23 <sup>°/</sup> $9/27/2011$ - 10/05/2011       69.5 $2.41E.07$ N/A         Wells D23 <sup>°/</sup> $9/27/2011$ - 10/05/2011       73.5 $3.31E.07$ N/A         Well D23 <sup>°/</sup> $9/27/2011$ - 10/05/2011       78.5 $4.72E.07$ N/A         Well D20 <sup>°/</sup> $9/25/2009$ - 9/27/2009       85.5 $9.37E.07$ N/A         Well D20 <sup>°/</sup> $9/25/2009$ - 9/27/2009       89.5 $1.47E.07$ N/A         Well D20 <sup>°/</sup> $9/25/2009$ - 9/27/2009       89.5 $1.47E.07$ N/A         Well D20 <sup>°/</sup> $9/25/2009$ - 9/27/2009       89.5 $1.47E.07$ N/A         Mult D20 <sup>°/</sup> $9/25/2009$ - 9/27/2009       89.5 $1.47E.07$ N/A         Mult D20 <sup>°/</sup> $9/25/2009$ - 9/27/2009 <td< td=""><td></td><td>9/27/2011-</td><td></td><td></td><td></td><td></td><td></td><td></td></td<>		9/27/2011-						
Wells $D23^{c'}$ 9/27/2011- 10/05/2011       67.5        1.04E-07        N/A         Wells $D23^{c'}$ 9/27/2011- 10/05/2011       69.5        2.41E-07        N/A         Well $D23^{c'}$ 9/27/2011- 10/05/2011       73.5        3.31E-07        N/A         Well $D23^{c'}$ 9/27/2011- 10/05/2011       78.5        4.72E-07        N/A         Well $D20^{c'}$ 9/27/2009- 9/27/2009       75.5        2.25E-07        N/A         Well $D20^{c'}$ 9/25/2009- 9/27/2009       85.5        9.37E-07        N/A         Well $D20^{c'}$ 9/25/2009- 9/27/2009       89.5        1.47E-07        N/A         Well $D20^{c'}$ 9/25/2009- 9/27/2009       89.5        1.47E-07        N/A         Well $D20^{c'}$ 9/25/2009- 9/27/2009       89.5        1.47E-07        N/A         Mult D20^{c'}       9/25/2009- 9/27/2009       89.5        1.47E-07        N/A         Mult D20^{c'}       9/25/2009- 9/27/2009       89.5        1.47E-07        N/A </td <td>Wells D23</td> <td></td> <td>63.5</td> <td></td> <td>1.48E-07</td> <td></td> <td></td> <td>N/A</td>	Wells D23		63.5		1.48E-07			N/A
Wells D23 <sup>o</sup> 10/05/2011       67.5        1.04E-07         N/A         Wells D23 <sup>c/</sup> 9/27/2011-       69.5        2.41E-07         N/A         Well D23 <sup>c/</sup> 9/27/2011-       73.5        3.31E-07         N/A         Well D23 <sup>c/</sup> 9/27/2011-       73.5        3.31E-07         N/A         Well D23 <sup>c/</sup> 9/27/2011-       78.5        4.72E-07         N/A         Well D20 <sup>c/</sup> 9/25/2009-       75.5        2.25E-07         N/A         Well D20 <sup>c/</sup> 9/25/2009-       85.5        9.37E-07         N/A         Well D20 <sup>c/</sup> 9/25/2009-       89.5        1.47E-07        N/A         Well D20 <sup>c/</sup> 9/25/2009-       89.5        1.47E-07        N/A         Mult D20 <sup>c/</sup> 9/25/2009-       89.5        1.47E-07        N/A         Mult D20 <sup>c/</sup> 9/25/2009-       89.5        1.47E-07        N/A	toor -							
Interview of the system of t	Wells D23 <sup>℃</sup>		67.5		1.04E-07			N/A
Wells D23 <sup>od</sup> $10/05/2011$ $69.5$ $2.41E-07$ N/A         Well D23 <sup>od</sup> $9/27/2011 73.5$ $3.31E-07$ N/A         Well D23 <sup>od</sup> $9/27/2011 73.5$ $4.72E-07$ N/A         Well D20 <sup>od</sup> $9/25/2009 $ $2.25E-07$ N/A         Well D20 <sup>od</sup> $9/25/2009 9.5.5$ $9.37E-07$ N/A         Well D20 <sup>od</sup> $9/25/2009 9.5.5$ $9.37E-07$ N/A         Well D20 <sup>od</sup> $9/25/2009 99.5$ $1.47E-07$ N/A         Well D20 <sup>od</sup> $9/27/2009$ $89.5$ $1.47E-07$ N/A         Mell D20 <sup>od</sup> $9/27/2009$ $89.5$ $1.47E-07$ N/A         Mult D20 <sup>od</sup> $9/27/2009$ $89.5$ $1.47E-07$ N/A         Mult D20 <sup>od</sup> $9/27/2009$ $89.5$ <	u te Per - Ni per ultra di Stevender del della							
10/05/2011Well $D23^{c'}$ 9/27/2011- 10/05/201173.53.31E-07N/AWell $D23^{c'}$ 9/27/2011- 10/05/201178.54.72E-07N/AWell $D20^{c'}$ 9/25/2009- 9/27/200975.52.25E-07N/AWell $D20^{c'}$ 9/25/2009- 9/27/200985.59.37E-07N/AWell $D20^{c'}$ 9/25/2009- 9/27/200989.51.47E-07N/AWell $D20^{c'}$ 9/25/2009- 9/27/200989.51.47E-07N/AWell $D20^{c'}$ 9/25/2009- 9/27/200989.51.47E-07N/AWell $D20^{c'}$ 9/25/2009- 9/27/200989.51.47E-07N/AWell $D20^{c'}$ 9/25/2009- 9/27/200989.51.47E-07N/AOtu-1087/14/2005198856.88E-07N/AOtu-1087/14/2005198857.76E-07N/AOtu-1087/14/2005198857.76E-07N/AOtu-1087/14/2005258795.97E-07N/AOtu-1087/14/2005258795.69E-07N/AOtu-1087/14/2005258795.69E-07N/AOtu-108	Wells D23 <sup>d</sup>		69.5		2.41E-07			N/A
Well D23 <sup>o</sup> 10/05/2011       73.5        3.31E-07         N/A         Well D23 <sup>o'</sup> 9/27/2001- 10/05/2011       78.5        4.72E-07         N/A         Well D20 <sup>o'</sup> 9/25/2009- 9/25/2009       75.5        2.25E-07         N/A         Well D20 <sup>o'</sup> 9/25/2009- 9/25/2009       85.5        9.37E-07         N/A         Well D20 <sup>o'</sup> 9/25/2009- 9/25/2009       89.5        1.47E-07         N/A         Well D20 <sup>o'</sup> 9/25/2009- 9/27/2009       89.5        1.47E-07         N/A         Well D20 <sup>o'</sup> 9/27/2009       89.5        1.47E-07         N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval =       3.26E-07         N/A         O1U-108       7/14/2005       19       885       7.76E-07         N/A         O1U-108       7/14/2005       25       879       5.97E-07        N/A         O1U-108       7/14/2005       25       879       5.96E-07								
10/05/2011         Well $D23^{c'}$ 9/27/2011- 10/05/2011       78.5        4.72E-07         N/A         Well $D20^{c'}$ 9/25/2009- 9/27/2009       75.5        2.25E-07         N/A         Well $D20^{c'}$ 9/25/2009- 9/27/2009       85.5        9.37E-07         N/A         Well $D20^{c'}$ 9/25/2009- 9/27/2009       89.5        1.47E-07         N/A         Well $D20^{c'}$ 9/25/2009- 9/27/2009       89.5        1.47E-07         N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval =       3.26E-07         N/A         O1U-108       7/14/2005       19       885       6.88E-07         N/A         01U-108       7/14/2005       19       885       6.88E-07        N/A         01U-108       7/14/2005       19       885       7.42E-07        N/A         01U-108       7/14/2005       25       879       5.97E-07        N/A         01U-108       7/14/2005       25       879		9/27/2011-	72.5		3 31E 07			NI/A
Well D23 <sup>od</sup> 10/05/2011       78.5        4.72E-07         N/A         Well D20 <sup>od</sup> 9/25/2009- 9/27/2009       75.5        2.25E-07         N/A         Well D20 <sup>od</sup> 9/25/2009- 9/27/2009       85.5        9.37E-07         N/A         Well D20 <sup>od</sup> 9/25/2009- 9/27/2009       89.5        1.47E-07        N/A         Well D20 <sup>od</sup> 9/25/2009- 9/27/2009       89.5        1.47E-07        N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval =       3.26E-07        N/A         Confidence Level (95.0%) =       2.29E-07        N/A         01U-108       7/14/2005       19       885       6.88E-07        N/A         01U-108       7/14/2005       19       885       7.42E-07        N/A         01U-108       7/14/2005       25       879       5.97E-07        N/A         01U-108       7/14/2005       25       879       5.69E-07        N/A         01U-108       7/14/2005       25       879       5.69E-07	well D23	10/05/2011	/3.3		5.5112-07			IN/A
10/03/2011         Well D20 <sup>of</sup> $9/25/2009$ - 9/27/2009 $75.5$ $$ $2.25E-07$ $$ $N/A$ Well D20 <sup>of</sup> $9/25/2009$ - 9/27/2009 $85.5$ $$ $9.37E-07$ $$ $N/A$ Well D20 <sup>of</sup> $9/25/2009$ - 9/27/2009 $89.5$ $$ $1.47E-07$ $$ $N/A$ Average of Borehole Core Laboratory Analyses For Sonde Inteval $3.26E-07$ $$ $N/A$ TCAAP         01U-108 $7/14/2005$ 19 $885$ $7.76E-07$ $$ $N/A$ 01U-108 $7/14/2005$ 19 $885$ $6.88E-07$ $$ $N/A$ 01U-108 $7/14/2005$ 19 $885$ $7.42E-07$ $$ $N/A$ 01U-108 $7/14/2005$ 25 $879$ $5.97E-07$ $$ $N/A$ 01U-108 $7/14/2005$ 25 $879$ $5.69E-07$ $$ $N/A$ 01U-108 $7/14/2005$ 25 $879$ $5.69E-07$ $$ $N/A$ 01U-108 $7/14/2005$ 25 $879$ $5.69E-07$ <td></td> <td>9/27/2011-</td> <td>70.5</td> <td></td> <td>4.505.05</td> <td></td> <td></td> <td>27/4</td>		9/27/2011-	70.5		4.505.05			27/4
Well $D20^{c'}$ 9/25/2009- 9/27/200975.52.25E-07N/AWell $D20^{c'}$ 9/25/2009- 9/27/200985.59.37E-07N/AWell $D20^{c'}$ 9/25/2009- 9/27/200989.51.47E-07N/AWell $D20^{c'}$ 9/25/2009- 9/27/200989.51.47E-07N/AAverage of Borehole Core Laboratory Analyses For Sonde Inteval =3.26E-07N/AConfidence Level (95.0%) =2.29E-07N/A01U-1087/14/2005198857.76E-07N/A01U-1087/14/2005198857.42E-07N/A01U-1087/14/2005258795.97E-07N/A01U-1087/14/2005258795.69E-07N/A01U-1087/14/2005258795.69E-07N/A01U-1087/14/2005258795.76E-07N/A01U-1087/14/200528.5875.57.94E-07N/A01U-1087/14/200528.5875.58.21E-07N/A	Well D23°	10/05/2011	/8.5		4.72E-07			N/A
Well D20° $9/27/2009$ 75.5 $2.25E-07$ N/AWell D20° $9/25/2009$ $9/27/2009$ $85.5$ $9.37E-07$ N/AWell D20° $9/25/2009$ $9/27/2009$ $89.5$ $1.47E-07$ N/AAverage of Borehole Core Laboratory Analyses For Sonde Inteval = $3.26E-07$ N/AConfidence Level ( $95.0\%$ ) = $2.29E-07$ N/ATCAAPTCAAP01U-108 $7/14/2005$ 19 $885$ $7.76E-07$ N/A01U-108 $7/14/2005$ 19 $885$ $7.42E-07$ N/A01U-108 $7/14/2005$ 25 $879$ $5.97E-07$ N/A01U-108 $7/14/2005$ 25 $879$ $5.69E-07$ N/A01U-108 $7/14/2005$ $28.5$ $875.5$ $7.94E-07$ N/A01U-108 $7/14/2005$ $28.5$ $875.5$ $8.21E-07$ N/A	,							
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Well D20 <sup><math>\alpha</math></sup>		75.5		2.25E-07			N/A
Well D20° $9/27/2009$ $85.5$ $9.37E-07$ N/A         Well D20° $9/25/2009$ $89.5$ $1.47E-07$ N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval = $3.26E-07$ N/A         Confidence Level ( $95.0\%$ ) = $2.29E-07$ N/A         TCAAP         01U-108 $7/14/2005$ 19 $885$ $7.76E-07$ N/A         01U-108 $7/14/2005$ 19 $885$ $6.88E-07$ N/A         01U-108 $7/14/2005$ 19 $885$ $7.42E-07$ N/A         01U-108 $7/14/2005$ 25 $879$ $5.97E-07$ N/A         01U-108 $7/14/2005$ 25 $879$ $5.69E-07$ N/A         01U-108 $7/14/2005$ 25 $879$ $5.69E-07$ N/A         01U-108 $7/14/2005$ 28.5 $875.5$ $7.94E-07$ N/A         01U-108								
Well $D20^{o'}$ 9/25/2009- 9/27/200989.51.47E-07N/AAverage of Borehole Core Laboratory Analyses For Sonde Inteval =3.26E-07Confidence Level (95.0%) =2.29E-07TCAAP01U-1087/14/2005198857.76E-07N/A01U-1087/14/2005198856.88E-07N/A01U-1087/14/2005198857.42E-07N/A01U-1087/14/2005258795.97E-07N/A01U-1087/14/2005258795.69E-07N/A01U-1087/14/2005258795.69E-07N/A01U-1087/14/2005258795.76E-07N/A01U-1087/14/200528.5875.57.94E-07N/A01U-1087/14/200528.5875.58.21E-07N/A	Well D20 <sup>℃</sup>		85.5		9.37E-07			N/A
Well D20 <sup>o</sup> 9/27/2009         89.5          1.47E-07           N/A           Average of Borehole Core Laboratory Analyses For Sonde Inteval         =         3.26E-07           N/A           Confidence Level (95.0%)         =         2.29E-07           N/A           01U-108         7/14/2005         19         885         7.76E-07           N/A           01U-108         7/14/2005         19         885         6.88E-07           N/A           01U-108         7/14/2005         19         885         7.42E-07           N/A           01U-108         7/14/2005         25         879         5.97E-07           N/A           01U-108         7/14/2005         25         879         5.69E-07           N/A           01U-108         7/14/2005         25         879         5.76E-07          N/A           01U-108         7/14/2005         28.5         875.5         7.94E-07          N/A           01U-108         7/14/2005         28.5         875.5								
3/2//2009         Average of Borehole Core Laboratory Analyses For Sonde Inteval =       3.26E-07         Confidence Level (95.0%) =       2.29E-07         TCAAP         01U-108       7/14/2005       19       885       7.76E-07        N/A         01U-108       7/14/2005       19       885       7.76E-07         N/A         01U-108       7/14/2005       19       885       7.42E-07         N/A         01U-108       7/14/2005       25       879       5.97E-07         N/A         01U-108       7/14/2005       25       879       5.69E-07         N/A         01U-108       7/14/2005       25       879       5.76E-07        N/A         01U-108       7/14/2005       28.5       875.5       7.94E-07        N/A         01U-108       7/14/2005       28.5       875.5       8.21E-07        N/A	Well D20 <sup>d</sup>		89.5		1 47E-07			N/A
$\begin{array}{c c c c c c c c c c c c c c c c c c c $				519au	5044 Killion ( 44-35466 at 5		56260	1.011
TCAAP           01U-108         7/14/2005         19         885         7.76E-07           N/A           01U-108         7/14/2005         19         885         6.88E-07           N/A           01U-108         7/14/2005         19         885         6.88E-07           N/A           01U-108         7/14/2005         19         885         7.42E-07           N/A           01U-108         7/14/2005         25         879         5.97E-07           N/A           01U-108         7/14/2005         25         879         5.69E-07           N/A           01U-108         7/14/2005         25         879         5.76E-07          N/A           01U-108         7/14/2005         28.5         875.5         7.94E-07          N/A           01U-108         7/14/2005         28.5         875.5         8.21E-07          N/A	Average of Borehole Core Lab							
01U-108         7/14/2005         19         885         7.76E-07           N/A           01U-108         7/14/2005         19         885         6.88E-07           N/A           01U-108         7/14/2005         19         885         7.42E-07           N/A           01U-108         7/14/2005         25         879         5.97E-07           N/A           01U-108         7/14/2005         25         879         5.69E-07           N/A           01U-108         7/14/2005         25         879         5.69E-07           N/A           01U-108         7/14/2005         25         879         5.76E-07           N/A           01U-108         7/14/2005         28.5         875.5         7.94E-07          N/A           01U-108         7/14/2005         28.5         875.5         8.21E-07          N/A		Confi	dence Leve	el (95.0%) =	2.29E-07			
01U-108         7/14/2005         19         885         7.76E-07           N/A           01U-108         7/14/2005         19         885         6.88E-07           N/A           01U-108         7/14/2005         19         885         7.42E-07           N/A           01U-108         7/14/2005         25         879         5.97E-07           N/A           01U-108         7/14/2005         25         879         5.69E-07           N/A           01U-108         7/14/2005         25         879         5.69E-07           N/A           01U-108         7/14/2005         25         879         5.76E-07           N/A           01U-108         7/14/2005         28.5         875.5         7.94E-07          N/A           01U-108         7/14/2005         28.5         875.5         8.21E-07          N/A	ТСААР							
01U-108         7/14/2005         19         885         6.88E-07           N/A           01U-108         7/14/2005         19         885         7.42E-07           N/A           01U-108         7/14/2005         25         879         5.97E-07           N/A           01U-108         7/14/2005         25         879         5.69E-07           N/A           01U-108         7/14/2005         25         879         5.69E-07           N/A           01U-108         7/14/2005         25         879         5.76E-07           N/A           01U-108         7/14/2005         28.5         875.5         7.94E-07           N/A           01U-108         7/14/2005         28.5         875.5         8.21E-07          N/A		7/14/2005	19	885	7.76E-07			N/A
01U-108         7/14/2005         19         885         7.42E-07           N/A           01U-108         7/14/2005         25         879         5.97E-07           N/A           01U-108         7/14/2005         25         879         5.69E-07           N/A           01U-108         7/14/2005         25         879         5.69E-07           N/A           01U-108         7/14/2005         25         879         5.76E-07           N/A           01U-108         7/14/2005         28.5         875.5         7.94E-07           N/A           01U-108         7/14/2005         28.5         875.5         8.21E-07          N/A			19					
01U-108         7/14/2005         25         879         5.69E-07           N/A           01U-108         7/14/2005         25         879         5.76E-07           N/A           01U-108         7/14/2005         28.5         875.5         7.94E-07           N/A           01U-108         7/14/2005         28.5         875.5         8.21E-07          N/A								
01U-108         7/14/2005         25         879         5.69E-07           N/A           01U-108         7/14/2005         25         879         5.76E-07           N/A           01U-108         7/14/2005         28.5         875.5         7.94E-07           N/A           01U-108         7/14/2005         28.5         875.5         8.21E-07          N/A	01U-108	7/14/2005	25	879	5.97E-07			N/A
01U-108         7/14/2005         25         879         5.76E-07          N/A           01U-108         7/14/2005         28.5         875.5         7.94E-07          N/A           01U-108         7/14/2005         28.5         875.5         8.21E-07          N/A	01U-108	7/14/2005	25	879	5.69E-07			N/A
01U-108         7/14/2005         28.5         875.5         7.94E-07          N/A           01U-108         7/14/2005         28.5         875.5         8.21E-07          N/A	01U-108	7/14/2005	25	879	5.76E-07			N/A
		7/14/2005	28.5	875.5	8.21E-07			N/A

ESTCP Project Number ER-201584



0 ST HVVASSTO P ER-2015S4/Report - Technical/Tables/Table 4.1.2 Summary of Borehole Magnetic Susceptibility Data Used for Analysis size

# Table 4.1.2 Laboratory Magnetic Susceptibility Results for Borehole Core Samples and Grab Samples for 10-20 Silica Sand ESTCP Project Number ER-201584

	LSICF.		er ER-201584		_		
Sample Identification	Date	Depth (ft bgs)	Elevation (ft amsl)	Mass Magnetic Susceptibility (m <sup>3</sup> /kg)	Flag <sup>b/</sup>		or Range n <sup>3</sup> /kg)
01U-108	7/14/2005	31.5	872.5	1.33E-06			N/A
01U-108	7/14/2005	31.5	872.5	1.36E-06	0.101233		N/A N/A
01U-108	7/14/2005	31.5	872.5	1.39E-06			N/A N/A
Average of Borehole Core Lab							IN/A
Average of Borenoie Core Lab			$\frac{1}{1}(95.0\%) =$				
	COIII		si (93.070) –	1.10E-07			
Former Plattsburgh AFB,							
46 PLTW 8 2A	Jul-13		220	9.55E-07			N/A
46 PLTW 8 2B	Jul-13		220	1.13E-06			N/A
46 PLTW 8 2C	Jul-13	1000	220	1.21E-06	1.777		N/A
46 PLTW 8 3A	Jul-13		218	8.71E-07			N/A
46 PLTW 8 3B	Jul-13		218	1.26E-06			N/A
46 PLTW 8 3C	Jul-13		218	1.52E-06			N/A
32 PLTW 12 2A	Jul-13	( <b></b> 1	205	1.68E-06			N/A
32 PLTW 12 2B	Jul-13		205	1.65E-06			N/A
32 PLTW 12 2C	Jul-13	(222)	205	1.56E-06			N/A
32 PLTW 12 3A	Jul-13	1-11	202	5.55E-07	8222		N/A
32 PLTW 12 3B	Jul-13		202	5.75E-07			N/A
32 PLTW 12 3C	Jul-13	2 <u>11</u> 2	202	5.20E-07			N/A
35 PLTW 13 2A	Jul-13		195	1.23E-06			N/A
35 PLTW 13 2B	Jul-13		195	1.50E-06			N/A
35 PLTW 13 2C	Jul-13		195	1.32E-06			N/A
35 PLTW 13 3A	Jul-13		193	1.80E-06			N/A
35 PLTW 13 3B	Jul-13		193	1.59E-06			N/A
35 PLTW 13 3C	Jul-13		193	1.54E-06			N/A
Average of Borehole Core Lab		es For Son				0.57	1 1/1 1
			el (95.0%) =				
Hopewell Precision Site, Hopew							1 -
EPA-10S	Aug-13	25.3		1.05E-07			N/A
EPA-10S	Aug-13	26.3		1.29E-07			N/A
EPA-10S	Aug-13	28.0		1.36E-07	2.77		N/A
EPA-10S	Aug-13	28.0		1.09E-07			N/A
EPA-10S	Aug-13	30.0	()	3.92E-07			N/A
EPA-10S	Aug-13	30.3	1.—— I	1.87E-07			N/A
EPA-10S	Aug-13	31.0		1.37E-07			N/A
EPA-10S	Aug-13	31.6		1.32E-07			N/A
EPA-10S	Aug-13	32.3	1221	1.69E-07	2002		N/A
EPA-10S	Aug-13	32.9	(100 m)	1.63E-07	8000		N/A
EPA-10D	Aug-13	45.5		2.28E-07	2000		N/A
EPA-10D	Aug-13	46.4		2.09E-07			N/A
EPA-10D	Aug-13	47.2	6	2.19E-07			N/A
EPA-10D	Aug-13	47.9	1.770	2.07E-07			N/A
EPA-10D	Aug-13	50.5		2.34E-07			N/A
EPA-10D	Aug-13	51.0		2.26E-07			N/A
Average of Borehole Core Lab			de Inteval =				
			el(95.0%) =				
			`` <i>(</i>				



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# Table 4.1.2 Laboratory Magnetic Susceptibility Results for Borehole Core Samples and Grab Samples for 10-20 Silica Sand ESTCP Project Number ER-201584

Sample Identification         Date         Depth (ft)         Elevation         Mass Magnetic Susceptibility (m <sup>3</sup> /sg)         Error Range (m <sup>3</sup> /sg)           Hopewell Precision Site, Hopewell Junction, New York - Wells 12S and 12D         Error Range         Image Network (mass)         Im		LOICI	Project Numb	er ER-201504				
Hopewell Precision Site, Hopewell Junction, New York - Wells 12S and 12D           EPA-12S         Aug-13         20.5         -         1.4E-07         -         -         N/A           EPA-12S         Aug-13         21.4         -         1.1E-07         -         -         N/A           EPA-12S         Aug-13         22.3         -         1.3E-07         -         -         N/A           EPA-12S         Aug-13         25.3         -         1.2E-07         -         N/A           EPA-12S         Aug-13         25.1         -         1.5E-07         -         N/A           EPA-12S         Aug-13         35.5         -         1.8E-07         -         N/A           EPA-12D         Aug-13         36.7         -         1.8E-07         -         N/A           EPA-12D         Aug-13         40.5         -         1.4E-07         -         N/A           EPA-12D         Aug-13         41.7         -         2.3E-07         -         N/A           EPA-12D         Aug-13         43.4         -         2.1E-07         -         N/A           EPA-12D         Aug-13         42.3         -         2.2E-07	Sample Identification	Date			Susceptibility	ibility		0
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	Honewell Precision Site Honew	ell Junction	New York	Wells 12S	and 12D			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$							200	N/A
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$						2020	10000	
EPA-12D       Aug-13       41.7        2.3E-07         N/A         EPA-12D       Aug-13       42.6        2.2E-07         N/A         EPA-12D       Aug-13       42.3        2.2E-07         N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval       1.65E-07         N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval       1.65E-07         N/A         EPA-15D       Aug-13       27.4        1.98E-07         N/A         EPA-15D       Aug-13       28.2        1.93E-07        N/A         EPA-15D       Aug-13       29.0        1.89E-07        N/A         EPA-15D       Aug-13       30.5        1.70E-07        N/A         EPA-15D       Aug-13       32.5        2.35E-07        N/A         EPA-15D       Aug-13       35.5        2.32E-07        N/A         EPA-15D       Aug-13       35.5        2.32E-07        N							00040	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								
EPA-12D       Aug-13       43.4        2.1E-07         N/A         EPA-12D       Aug-13       42.3        2.2E-07         N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval       =       1.65E-07         N/A         Hopewell Precision Site, Hopewell Junction, New York - Wells 15D       EPA-15D       Aug-13       27.4        1.98E-07         N/A         EPA-15D       Aug-13       28.2        1.93E-07        N/A         EPA-15D       Aug-13       30.5        1.70E-07        N/A         EPA-15D       Aug-13       31.5        1.97E-07        N/A         EPA-15D       Aug-13       32.5       -       2.35E-07        N/A         EPA-15D       Aug-13       35.5       -       2.32E-07        N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval       2.10E-07       -       N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval       2.10E-07       -       N/A         EPA-16S       Aug-13       20.6       -								
EPA-12D       Aug-13       42.3        2.2E-07         N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval       =       1.65E-07         N/A         Hopewell Precision Site, Hopewell Junction, New York - Wells 15D        1.98E-07         N/A         EPA-15D       Aug-13       28.2        1.93E-07         N/A         EPA-15D       Aug-13       28.2        1.93E-07         N/A         EPA-15D       Aug-13       30.5        1.70E-07        N/A         EPA-15D       Aug-13       31.5        1.97E-07        N/A         EPA-15D       Aug-13       32.5        2.35E-07        N/A         EPA-15D       Aug-13       33.4        2.63E-07        N/A         EPA-15D       Aug-13       35.5        2.32E-07        N/A         EPA-16S       Aug-13       20.6        -       N/A         EPA-16S       Aug-13       21.6       -       1.016-07        N/A <td></td> <td></td> <td></td> <td>0000</td> <td></td> <td></td> <td>100000</td> <td></td>				0000			100000	
Average of Borehole Core Laboratory Analyses For Sonde Inteval = $1.65E-07$ Confidence Level (95.0%) = $2.30E-08$ Hopewell Precision Site, Hopewell Junction, New York - Wells 15D         EPA-15D         Aug-13 $27.4$ $1.98E-07$ N/A         EPA-15D         Aug-13 $27.4$ $1.93E-07$ N/A         EPA-15D         Aug-13 $29.0$ $1.89E-07$ N/A         EPA-15D         Aug-13 $30.5$ $1.70E-07$ N/A         EPA-15D         Aug-13 $31.5$ $1.97E-07$ N/A         EPA-15D         Aug-13 $32.5$ $2.35E-07$ N/A         EPA-15D         Aug-13 $35.5$ $2.32E-07$ N/A         EPA-15D         Aug-13 $35.5$ $2.32E-07$ N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval         Confidence Level (95.0%) = $2.56E-08$ Hopewell Precision Site, Hopewell Junction, New York - Wells 16S and 16D         EPA-16S         Aug-13 $25.5$ $1.41E-07$ N/A         EPA-16S         Aug-13 $26.3$ $1.00E-07$ N/A         EPA		<u>v</u>						
Confidence Level (95.0%) = 2.30E-08           Hopewell Precision Site, Hopewell Junction, New York - Wells 15D           EPA-15D         Aug-13         27.4          1.98E-07          N/A           EPA-15D         Aug-13         28.2          1.98E-07          N/A           EPA-15D         Aug-13         29.0          1.89E-07          N/A           EPA-15D         Aug-13         30.5          1.70E-07          N/A           EPA-15D         Aug-13         31.5          1.97E-07          N/A           EPA-15D         Aug-13         32.5          2.35E-07          N/A           EPA-15D         Aug-13         35.5          2.32E-07          N/A           EPA-15D         Aug-13         35.5          2.32E-07          N/A           Average of Borehole Core Laboratory Analyses For Sonde Inteval         2.10E-07          N/A           EPA-16S         Aug-13         20.6          9.71E-08          N/A           EPA-16S         Aug-13         20.5				 da Interval —				IN/A
Hopewell Precision Site, Hopewell Junction, New York - Wells 15D           EPA-15D         Aug-13         27.4          1.98E-07           N/A           EPA-15D         Aug-13         28.2          1.93E-07           N/A           EPA-15D         Aug-13         29.0          1.89E-07           N/A           EPA-15D         Aug-13         30.5          1.70E-07           N/A           EPA-15D         Aug-13         31.5          1.97E-07           N/A           EPA-15D         Aug-13         32.5          2.35E-07           N/A           EPA-15D         Aug-13         35.5          2.32E-07           N/A           EPA-15D         Aug-13         35.5          2.32E-07           N/A           EPA-16S         Aug-13         20.6          9.71E-08          -         N/A           EPA-16S         Aug-13         20.6          9.71E-08          -	Average of Borenole Core Lab							
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		Conin	laence Leve	(95.0%) =	2.30E-08			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Hopewell Precision Site, Hopew	ell Junction, 1	New York	- Wells 15D				
EPA-15D       Aug-13       29.0        1.89E-07         N/A         EPA-15D       Aug-13       30.5        1.70E-07         N/A         EPA-15D       Aug-13       31.5        1.97E-07         N/A         EPA-15D       Aug-13       32.5        2.35E-07         N/A         EPA-15D       Aug-13       33.4        2.63E-07         N/A         EPA-15D       Aug-13       35.5        2.32E-07         N/A         EPA-15D       Aug-13       35.5        2.32E-07         N/A         EPA-15D       Aug-13       25.5        2.56E-08         N/A         EPA-16S       Aug-13       20.6        9.71E-08         N/A         EPA-16S       Aug-13       25.5        1.41E-07        N/A         EPA-16S       Aug-13       26.3        1.00E-07        N/A         EPA-16S       Aug-13       40.5	EPA-15D	Aug-13	27.4		1.98E-07			N/A
EPA-15D       Aug-13 $30.5$ $1.70E-07$ N/A         EPA-15D       Aug-13 $31.5$ $1.97E-07$ N/A         EPA-15D       Aug-13 $32.5$ $2.35E-07$ N/A         EPA-15D       Aug-13 $33.4$ $2.63E-07$ N/A         EPA-15D       Aug-13 $35.5$ $2.32E-07$ N/A         EPA-15D       Aug-13 $35.5$ $2.32E-07$ N/A         EPA-15D       Aug-13 $35.5$ $2.32E-07$ N/A         EPA-15D       Aug-13 $25.5$ $2.56E-08$ N/A         EPA-16S       Aug-13 $20.6$ $9.71E-08$ N/A         EPA-16S       Aug-13 $21.6$ $1.10E-07$ N/A         EPA-16S       Aug-13 $25.5$ $1.41E-07$ N/A         EPA-16S	EPA-15D	Aug-13	28.2		1.93E-07		0000	N/A
EPA-15D       Aug-13       31.5        1.97E-07         N/A         EPA-15D       Aug-13       32.5        2.35E-07         N/A         EPA-15D       Aug-13       33.4        2.63E-07         N/A         EPA-15D       Aug-13       35.5        2.32E-07         N/A         EPA-15D       Aug-13       35.5        2.32E-07         N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval       =       2.10E-07         N/A         EPA-16S       Aug-13       20.6        9.71E-08         N/A         EPA-16S       Aug-13       21.6        1.10E-07        N/A         EPA-16S       Aug-13       25.5        1.41E-07        N/A         EPA-16S       Aug-13       26.3        1.00E-07        N/A         EPA-16S       Aug-13       40.5        1.68E-07        N/A         EPA-16D       Aug-13       45.7        1	EPA-15D	Aug-13	29.0		1.89E-07			N/A
EPA-15D       Aug-13       32.5        2.35E-07         N/A         EPA-15D       Aug-13       33.4        2.63E-07         N/A         EPA-15D       Aug-13       35.5        2.32E-07         N/A         EPA-15D       Aug-13       35.5        2.32E-07         N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval       2.10E-07         N/A         EPA-16S       Aug-13       20.6        9.71E-08         N/A         EPA-16S       Aug-13       21.6        1.10E-07        N/A         EPA-16S       Aug-13       25.5        1.41E-07        N/A         EPA-16S       Aug-13       26.3        1.00E-07        N/A         EPA-16S       Aug-13       40.5        1.68E-07        N/A         EPA-16S       Aug-13       45.7        1.84E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07	EPA-15D	Aug-13	30.5		1.70E-07			N/A
EPA-15D       Aug-13       33.4        2.63E-07         N/A         EPA-15D       Aug-13       35.5        2.32E-07         N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval       =       2.10E-07         N/A         Hopewell Precision Site, Hopewell Junction, New York - Wells 16S and 16D        9.71E-08         N/A         EPA-16S       Aug-13       20.6        9.71E-08         N/A         EPA-16S       Aug-13       21.6        1.10E-07        N/A         EPA-16S       Aug-13       25.5        1.41E-07        N/A         EPA-16S       Aug-13       26.3        1.00E-07        N/A         EPA-16S       Aug-13       40.5        1.68E-07        N/A         EPA-16D       Aug-13       45.7        1.84E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval       1.45E-07	EPA-15D	Aug-13	31.5		1.97E-07		1000	N/A
EPA-15D       Aug-13       35.5        2.32E-07         N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval       =       2.10E-07	EPA-15D	Aug-13	32.5		2.35E-07			N/A
Average of Borehole Core Laboratory Analyses For Sonde Inteval = $2.10E-07$ Confidence Level (95.0%) = $2.56E-08$ Hopewell Precision Site, Hopewell Junction, New York - Wells 16S and 16D         EPA-16S       Aug-13 $20.6$ $9.71E-08$ N/A         EPA-16S       Aug-13 $21.6$ $1.10E-07$ N/A         EPA-16S       Aug-13 $25.5$ $1.41E-07$ N/A         EPA-16S       Aug-13 $26.3$ $1.00E-07$ N/A         EPA-16S       Aug-13 $26.3$ $1.00E-07$ N/A         EPA-16S       Aug-13 $40.5$ $1.68E-07$ N/A         EPA-16D       Aug-13 $45.7$ $1.84E-07$ N/A         EPA-16D       Aug-13 $47.8$ $1.76E-07$ N/A         EPA-16D       Aug-13 $47.8$ $1.76E-07$ N/A         EPA-16D       Aug-13 $47.8$ $1.76E-07$ N/A	EPA-15D	Aug-13	33.4		2.63E-07		();	N/A
Confidence Level $(95.0\%) = 2.56E-08$ Hopewell Precision Site, Hopewell Junction, New York - Wells 16S and 16D         EPA-16S       Aug-13       20.6        9.71E-08        N/A         EPA-16S       Aug-13       21.6        1.10E-07        N/A         EPA-16S       Aug-13       25.5        1.41E-07        N/A         EPA-16S       Aug-13       26.3        1.00E-07        N/A         EPA-16S       Aug-13       40.5        1.68E-07        N/A         EPA-16D       Aug-13       45.7        1.84E-07        N/A         EPA-16D       Aug-13       45.7        1.83E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         Moreage of Borehole Core Laboratory Analyses For Sonde Inteval =       1.45E-07        N/A         Hopewell Precision Si	EPA-15D		35.5				();	N/A
Confidence Level $(95.0\%) = 2.56E-08$ Hopewell Precision Site, Hopewell Junction, New York - Wells 16S and 16D         EPA-16S       Aug-13       20.6        9.71E-08        N/A         EPA-16S       Aug-13       21.6        1.10E-07        N/A         EPA-16S       Aug-13       25.5        1.41E-07        N/A         EPA-16S       Aug-13       26.3        1.00E-07        N/A         EPA-16S       Aug-13       40.5        1.68E-07        N/A         EPA-16D       Aug-13       45.7        1.84E-07        N/A         EPA-16D       Aug-13       45.7        1.83E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         Moreage of Borehole Core Laboratory Analyses For Sonde Inteval =       1.45E-07        N/A         Hopewell Precision Si	Average of Borehole Core Lab	oratory Analys	ses For Son	de Inteval =	2.10E-07			
Hopewell Precision Site, Hopewell Junction, New York - Wells 16S and 16D         EPA-16S       Aug-13       20.6        9.71E-08        N/A         EPA-16S       Aug-13       21.6        1.10E-07        N/A         EPA-16S       Aug-13       25.5        1.41E-07        N/A         EPA-16S       Aug-13       26.3        1.00E-07        N/A         EPA-16S       Aug-13       26.3        1.00E-07        N/A         EPA-16S       Aug-13       40.5        1.68E-07        N/A         EPA-16D       Aug-13       45.7        1.84E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval =       1.45E-07        N/A         Hopewell Precision Site, Hopewell Junction, New York - Wells 19S         N/A         EPA-19S       Aug-13       15.7        1.34E-07								
EPA-16S       Aug-13       20.6        9.71E-08         N/A         EPA-16S       Aug-13       21.6        1.10E-07         N/A         EPA-16S       Aug-13       25.5        1.41E-07         N/A         EPA-16S       Aug-13       26.3        1.00E-07         N/A         EPA-16S       Aug-13       40.5        1.68E-07         N/A         EPA-16D       Aug-13       45.7        1.84E-07        N/A         EPA-16D       Aug-13       46.8        1.83E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval       1.45E-07        N/A         Moewell Precision Site, Hopewell Junction, New York - Wells 19S         N/A         EPA-19S       Aug-13       15.7        1.34E-07        -       N/A </th <th>Honewell Precision Site Honew</th> <th></th> <th></th> <th></th> <th>and 16D</th> <th></th> <th></th> <th></th>	Honewell Precision Site Honew				and 16D			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$				- *** CH3 105				N/A
EPA-16S       Aug-13       25.5        1.41E-07         N/A         EPA-16S       Aug-13       26.3        1.00E-07         N/A         EPA-16S       Aug-13       40.5        1.68E-07         N/A         EPA-16D       Aug-13       45.7        1.84E-07        N/A         EPA-16D       Aug-13       46.8        1.83E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval =       1.45E-07        N/A         Morewell Precision Site, Hopewell Junction, New York - Wells 19S         N/A         EPA-19S       Aug-13       15.7        1.34E-07         N/A         EPA-19S       Aug-13       17.0        1.36E-07        N/A				_				
EPA-16S       Aug-13       26.3        1.00E-07         N/A         EPA-16S       Aug-13       40.5        1.68E-07         N/A         EPA-16D       Aug-13       45.7        1.84E-07        N/A         EPA-16D       Aug-13       46.8        1.83E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval       1.45E-07        N/A         Confidence Level (95.0%) =       3.16E-08         Hopewell Precision Site, Hopewell Junction, New York - Wells 19S         EPA-19S       Aug-13       15.7        1.34E-07        N/A         EPA-19S       Aug-13       17.0        1.36E-07        N/A						0.000000	9/07/67	
EPA-16S       Aug-13       40.5        1.68E-07        N/A         EPA-16D       Aug-13       45.7        1.84E-07        N/A         EPA-16D       Aug-13       46.8        1.83E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval       1.45E-07        N/A         Confidence Level (95.0%) =       3.16E-08         Hopewell Precision Site, Hopewell Junction, New York - Wells 19S         EPA-19S       Aug-13       15.7        1.34E-07        N/A         EPA-19S       Aug-13       17.0        1.36E-07        N/A								
EPA-16D       Aug-13       45.7        1.84E-07        N/A         EPA-16D       Aug-13       46.8        1.83E-07        N/A         EPA-16D       Aug-13       47.8        1.76E-07        N/A         Average of Borehole Core Laboratory Analyses For Sonde Inteval       1.45E-07        N/A         Confidence Level (95.0%) =       3.16E-08         Hopewell Precision Site, Hopewell Junction, New York - Wells 19S         EPA-19S       Aug-13       15.7        1.34E-07        N/A         EPA-19S       Aug-13       17.0        1.36E-07        N/A						1993, D. X.		
EPA-16D         Aug-13         46.8          1.83E-07           N/A           EPA-16D         Aug-13         47.8          1.76E-07           N/A           Average of Borehole Core Laboratory Analyses For Sonde Inteval         1.45E-07           N/A           Confidence Level (95.0%) =         3.16E-08           Hopewell Precision Site, Hopewell Junction, New York - Wells 19S           EPA-19S         Aug-13         15.7          1.34E-07          N/A           EPA-19S         Aug-13         17.0          1.36E-07          N/A								
EPA-16D         Aug-13         47.8          1.76E-07          N/A           Average of Borehole Core Laboratory Analyses For Sonde Inteval         1.45E-07								
Average of Borehole Core Laboratory Analyses For Sonde Inteval =         1.45E-07           Confidence Level (95.0%) =         3.16E-08           Hopewell Precision Site, Hopewell Junction, New York - Wells 19S           EPA-19S         Aug-13         15.7          1.34E-07          N/A           EPA-19S         Aug-13         17.0          1.36E-07          N/A								
Confidence Level (95.0%) = 3.16E-08           Hopewell Precision Site, Hopewell Junction, New York - Wells 19S           EPA-19S         Aug-13         15.7          1.34E-07          N/A           EPA-19S         Aug-13         17.0          1.36E-07          N/A				de Interval —				18/74
Hopewell Precision Site, Hopewell Junction, New York - Wells 198           EPA-19S         Aug-13         15.7          1.34E-07          N/A           EPA-19S         Aug-13         17.0          1.36E-07          N/A	Average of Dorehole Core Lab							
EPA-19S         Aug-13         15.7          1.34E-07          N/A           EPA-19S         Aug-13         17.0          1.36E-07          N/A		Contri	idence Leve	= (0%0,0%) =	3.10E-08			
EPA-19S Aug-13 17.0 1.36E-07 N/A		ell Junction,	New York	Wells 19S				
	EPA-198	Aug-13	15.7		1.34E-07			N/A
EPA-19S Aug-13 17.9 1.12E-07 N/A		Aug-13	17.0		1.36E-07			N/A
	EPA-198	Aug-13	17.9		1.12E-07		()	N/A



D STRIVANESTOP ER-2016E4/Report - Technical/Tables/Table +.12 Summary of Botehole Magnelic Suscepibility Data Used for Analysis xisx

#### **Table 4.1.2**

#### Laboratory Magnetic Susceptibility Results for Borehole Core

Samples and Grab Samples for 10-20 Silica Sand ESTCP Project Number ER-201584

	EDICI	Tojeet Ivaino	er ER-201584		_	_	
Sample Identification	Date	Depth (ft bgs)	Elevation (ft amsl)	Mass Magnetic Susceptibility (m <sup>3</sup> /kg)	Flag <sup>b/</sup>		or Range n <sup>3</sup> /kg)
EPA-19S	Aug-13	20.6		9.63E-08			N/A
EPA-198	Aug-13	21.7		1.51E-07	1000	2010	N/A
EPA-198	Aug-13	22.6		1.02E-07			N/A
Average of Borehole Core Lab	oratory Analys	es For Son	de Inteval =	1.22E-07			
			el (95.0%) =	2.25E-08			
Hopewell Precision Site, Hopew	ell Junction.	New York	- Wells 16S	and 16D			
EPA-218	Aug-13	15.4		5.7E-07			N/A
EPA-21S	Aug-13	16.0		5.9E-07			N/A
EPA-21S	Aug-13	16.7	1	1.4E-07	-	8223	N/A
EPA-21S	Aug-13	20.6	12121	1.2E-07	1000	2002	N/A
EPA-21S	Aug-13	21.8		1.2E-07			N/A
EPA-218	Aug-13	22.9		1.1E-07			N/A
EPA-21D	Aug-13	33.3		1.1E-07			N/A
EPA-21D	Aug-13	33.8		3.0E-07			N/A
EPA-21D	Aug-13	34.3		1.6E-07	1		N/A
EPA-21D	Aug-13	34.9	1	1.5E-07	·		N/A
EPA-21D	Aug-13	35.7		1.1E-07	1 <del></del> 1		N/A
Average of Borehole Core Lab	oratory Analys	es For Son	de Inteval =	2.24E-07			
¥			el (95.0%) =				
Magnetic Susceptibility Results	for 10-20 Sili	ca Sand Us	ed to Build	Monitoring Wel	ls <sup>a/</sup>		
Premier Silica - Corner 1	6/18/2016			6.47E-09	J	± 2	2.21E-09
Premier Silica - Corner 2	6/18/2016			6.69E-09	J	$\pm 3$	.86E-09
Premier Silica - Corner 3	6/18/2016		1	6.30E-09	J	$\pm 1$	.03E-09
Premier Silica - Corner 4	6/18/2016			4.45E-09	J	± 2	.58E-09
Premier Silica - Bottom Center	6/18/2016			6.50E-09	J	± 3	.34E-09

Notes:

N/A = Not Available

a/ Analyses completed by Microbial Insights

b/J = estimated concentration between between the quantitation

and minimum detection limits.

e/ Samples collected between nested wells D20 (shallow) and D23 (deep) which are located about 20 feet apart.

01TH/WHEETCP ER-201584/Report - Technical/Tables/Table 4.1.2 Summary of Borehole Magnetic Susceptibility Data Used for Analysis size



#### 4.2 FORMER PLATTSBURGH AIR FORCE BASE, NEW YORK

This Site had existing data on magnetic susceptibility from core samples. Any potential contribution of aerobic biodegradation of the chlorinated solvents was not understood at the time the remedy was selected. An evaluation of the further contribution of aerobic co-oxidative biodegradation was not included in the last five-year review, but is completed under this investigation. In this study, the potential for abiotic TCE degradation was evaluated by measuring the magnetic susceptibility of aquifer sediment in two wells. The potential for cooxidation of TCE was evaluated in water samples from four wells.

#### 4.2.1 Site Location and History

The study site is the FT-002 site on the former Plattsburgh AFB, which is currently the Plattsburgh International Airport, Plattsburgh, New York. The Site is located in Clinton County along the western shore of Lake Champlain in northeastern New York. The base was closed on September 30, 1995 as part of the third round of base closures mandated by the Defense Base Closure and Realignment Act of 1993.

The FT-002 Site is located approximately 500 feet west of the runway and 500 feet east of the base's western boundary (Figure 4.2.1). From the mid- to late-1950s through 1989, the Site was used to meet the training requirements of the base fire department. During training exercises, fires were ignited in fire training pits on site. As a result of releases of combustible liquids (e.g., off-specification fuel and waste solvents) into the pits, the soil and groundwater were contaminated chlorinated hydrocarbons. The fuel-related compounds are naturally biodegradable in groundwater and, at the time of the remedial investigation, concentrations had attenuated below detection limits within 4,000 feet downgradient of the source. The chlorinated hydrocarbons, which are considerably less biodegradable under the conditions present at the Site, have been detected over 6,750 feet downgradient of the source.

The site has been extensively investigated and interim removal actions have been implemented, including the installation and operation of free product recovery, soil vapor extraction, and bioventing systems. A Final Record of Decision for the source was signed in September 2014 to address sources of contamination. The remedy involved a combination of soil vapor extraction and bioventing of the contaminated soil, free product recovery, water table depression enabling remediation of residual product adhering to soil below the water table, hydraulic containment of the remaining source, institutional controls, progress monitoring and sampling, and five-year site reviews.

#### 4.2.2 Site Geology/Hydrogeology

Four stratigraphic units underlie the Site: glaciomarine and glaciolacustrine sand (sand unit); glaciomarine and glaciolacustrine silt and clay (clay unit); glacial till (till unit); and bedrock (Figure 4.2.2). This stratigraphic sequence is consistent basewide, although the thicknesses of the individual units vary. Hydrogeologically, the stratigraphic sequence can be divided into the following units: an unsaturated zone and a water table aquifer present in the sand unit; a clay confining layer; a confined till water-bearing zone; and a confined bedrock aquifer. Thus far, groundwater contamination at the Site appears to be limited to the water table aquifer.

Groundwater flow which closely mimics surface topography, is predominantly from west to east across the Site, toward Lake Champlain.

#### 4.2.3 Contaminant Distribution

The current distribution of contamination in groundwater from chlorinated solvents is presented in Figure 4.2.1.

#### 4.2.4 Previous Sampling Relevant to the Current Project

Sediment samples were acquired from three locations in July 2013. See Figure 4.2.3 for the locations. Samples were acquired from 1 foot below land surface and 3 feet below land surface at each location. The samples were analyzed for mass magnetic susceptibility by staff of the R.S. Kerr Environmental Research Laboratory. These mass magnetic susceptibility data are presented in Table 4.1.2. Samples from location 46PLTW8 were acquired from elevations of 220 and 219 feet above mean sea level (amsl). Samples from location 32PLTW12 were acquired from elevations of 205 and 202 feet amsl. Samples from location 35PLTW13 were acquired from elevations of 195 and 193 feet amsl.

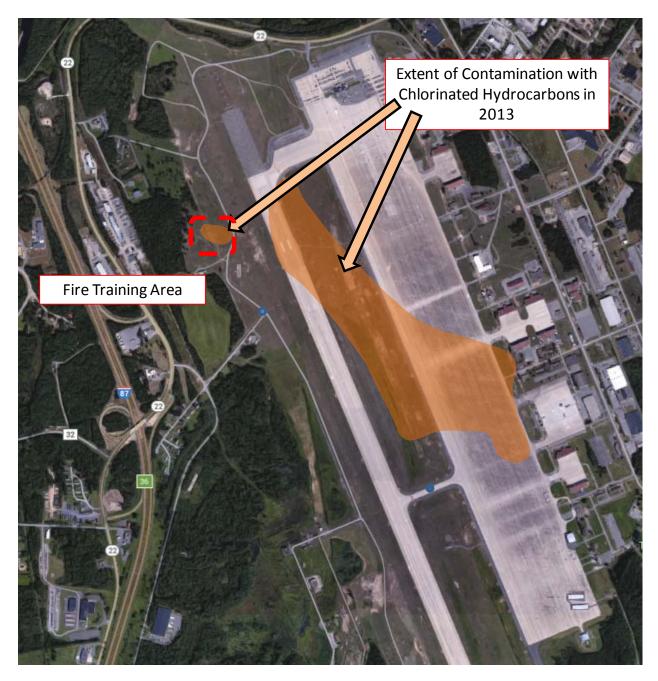


Figure 4.2.1. Location of the Former Fire Training Area (FT-002) on the Former Plattsburgh AFB, NY and Current Distribution of Groundwater Contaminated with Chlorinated Organic Compounds (URS 2009).

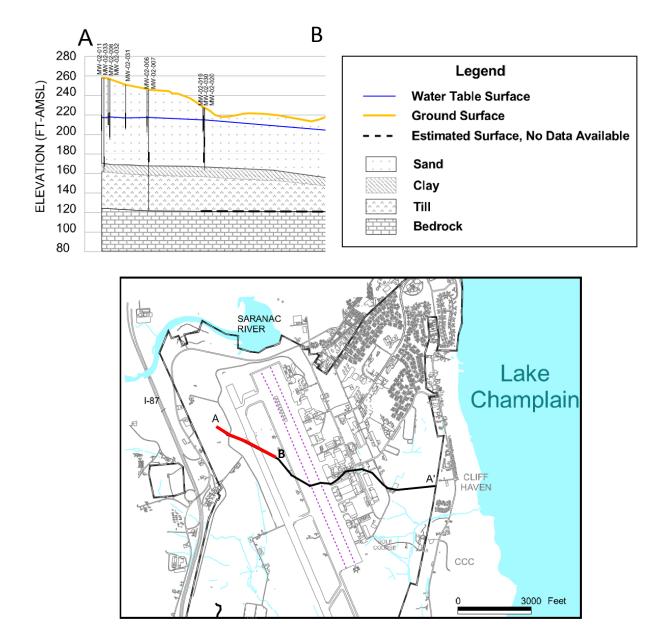


Figure 4.2.2. Geological Cross Section along the Flow Path in the Plume of Contamination from the FT-002 Site.



Figure 4.2.3. Locations of Wells where the Magnetic Susceptibility Sonde was Deployed, June 2016.

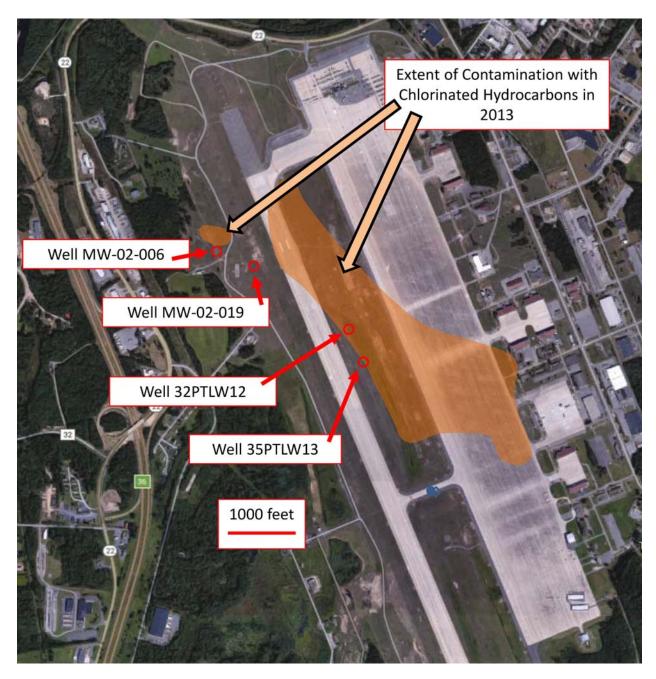


Figure 4.2.4. Sampling Locations for EAPs, qPCR, and <sup>14</sup>C-labeled TCE Assay were Well MW-02-006, Well MW-2-019, Well 32PLTW12 and Well 35PLT13.

#### 4.2.5 Sampling Locations Used for the Current Project

The locations for this project are presented in Figure 4.2.4. Water was sampled from monitoring wells MW-02-006, well MW-2-019, well 32PLTW12 and well 35PLT13 for analysis of enzyme activity probes, qPCR assays for DNA of oxygenase enzymes, and for determination of the rate of TCE co-oxidation. Magnetic susceptibility using the sonde was ultimately determined only from monitoring wells MW-20-107 and-MW-02-030 because wells MW-02-006 and MW-02-019, the wells originally proposed for magnetic susceptibility sampling were found to be compromised such that a sonde could not be lowered into them. Per the Site-specific sampling and analysis plan, purge water from the monitoring wells was disposed to the land surface near each well. Available borehole and well completion logs are included in Appendix C of the Demonstration Plan (ESTCP, 2016).

#### 4.3 NEW BRIGHTON/ARDEN HILLS SUPERFUND SITE (TCAAP)

This Site had existing data on magnetic susceptibility from core samples. These data are summarized in Table 4.1.2. Any potential contribution of aerobic biodegradation of the chlorinated solvents was not understood at the time that the remedy was selected. An evaluation of the further contribution of aerobic co-oxidative biodegradation was not included in the last five-year review, but was completed under this investigation.

In this study, the potential for abiotic TCE degradation was evaluated by measuring the magnetic susceptibility of aquifer sediment in three wells. The potential for cooxidation of TCE was evaluated in water samples from four wells.

#### 4.3.1 Site Location and History

The site is located on the north end of the former Twin Cities Army Ammunition Plant (TCAAP), in the city of Shoreview, Minnesota (Figure 4.3.1). The source of contamination is south of County Highway 3, near Shamrock Park. Two residential wells that are potential receptors of groundwater contamination are located west of Schutta Road and North of County Highway 3.

Figure 4.3.2 shows the locations of the residential wells, some of the early monitoring wells, and the extraction wells for a pump and treat remedy that was installed at the site.

Aerial photographs suggest that trenches and pits were used at the site for waste in the early 1940s. The area near well 01U108 is considered the primary source of contaminants to the aquifer (Ferrey and Wilson, 2002). In 1988, extraction well 350 was installed near monitoring well 01U108 as part of an interim response action intended to remove and treat the high concentrations of contaminants found at this location. Well 350 operated at 4 gallons per minute (gpm). Pumping at this well was stopped in 1994 based on an evaluation of its effectiveness. In 1994, eight additional extraction wells were installed downgradient of the source area to prevent the groundwater plume from reaching the off-site residential wells (Figure 4.3.2). The containment wells had a combined pumping rate of approximately 30 gpm.

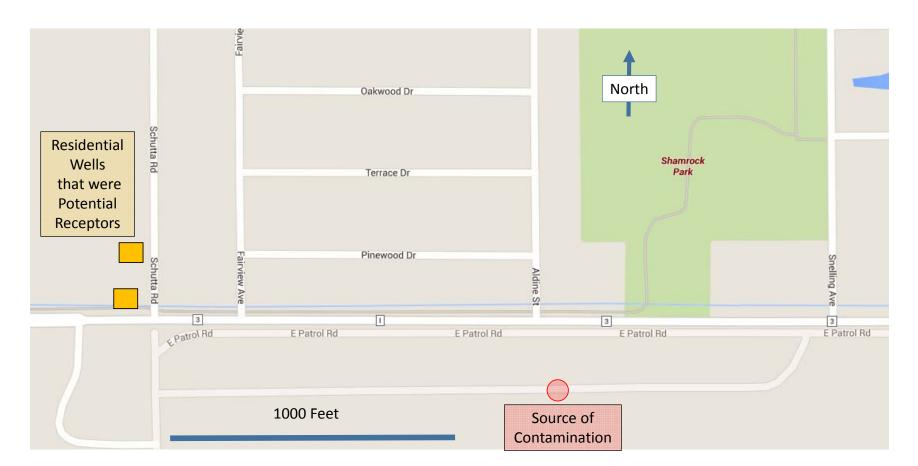


Figure 4.3.1. Location of the Source of Contamination for Site A on the Former Twin Cites Army Ammunition Plant (TCAAP) in Minnesota.

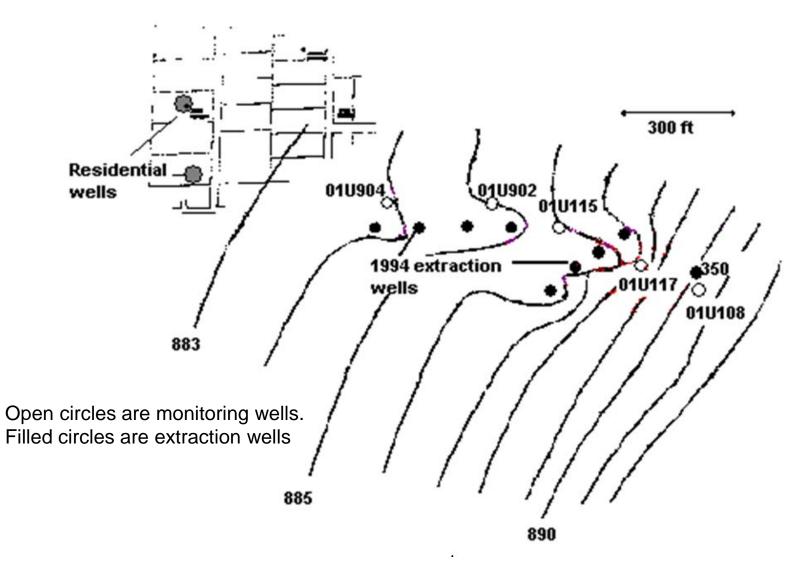


Figure 4.3.2. Locations of Monitoring Wells and Extraction Wells at Site A.

#### 4.3.2 Site Geology/Hydrogeology

There are two aquifer units at the site. Aquifer sediments in Unit 1 are composed of lacustrine silt and fine or medium sands. The water table is in Unit 1. Unit 1 is underlain by the Twin Cities Till (Unit 2) which, due to its high clay content, is an effective aquitard. The water table is 15 to 19 feet below ground surface. The Unit 1 aquifer ranges in thickness from 15 feet near the source area to 28 feet to the west (Figure 4.3.2). Unit 2 is approximately 12 to 88 feet thick.

Groundwater flows to the northwest (Figure 4.3.3) along a horizontal hydraulic gradient ranging from 0.0025 to 0.005 ft/ft. The hydraulic conductivity for Unit 1 was  $8.3 \times 10^{-3}$  cm sec<sup>-1</sup>. Using a gradient of 0.005 and a porosity of 0.2, groundwater velocity was estimated at 200 feet per year at Site A.

#### 4.3.3 Contaminant Distribution

The concentrations of PCE and its degradation products have declined over time at the site, due to a combination of active pump-and-treat and natural attenuation. Figure 4.3.4 provides the time course of attenuation in well 01U108, which was the originally the most contaminated well at the site, and the only well with laboratory analyses of borehole core samples.

The current distribution (2015) of contamination is depicted in Figures 4.3.5, 4.3.6 and 4.3.7. Only three wells at the site had concentrations of PCE above 1  $\mu$ g/L (Figure 4.3.5). The maximum concentration was 2.6  $\mu$ g/L. Only one well had a concentration of TCE above 1  $\mu$ g/L (Figure 4.3.6). That concentration was 1.8  $\mu$ g/L. Fourteen wells had concentrations of *c*DCE above 1  $\mu$ g/L (Figure 4.3.7). The maximum concentration was 310  $\mu$ g/L.

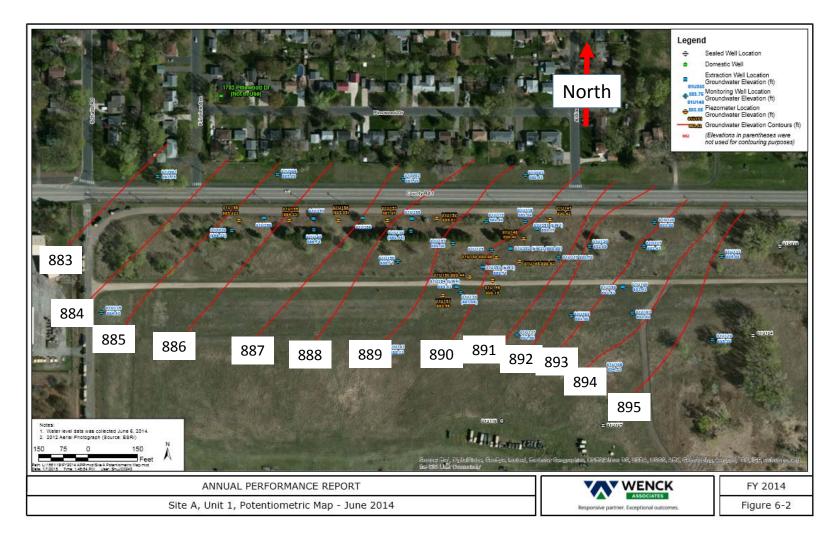
Apparently PCE was transformed to TCE and TCE was transformed to *c*DCE by sequential biological reductive dechlorination. However, vinyl chloride was never detected at Site A. The important mechanism for removal of *c*DCE was degradation by magnetite that was naturally occurring in the aquifer sediment.

#### **4.3.4** Previous Sampling Relevant to the Current Project

Core samples were acquired from a location just downgradient of the source area and well 01U108 on January 5, 2005. The samples were used to construct the microcosms described in He et al. (2009). The sediment was characterized by staff of the R.S. Kerr Environmental Research Center for mass magnetic susceptibility (Table 4.1.2). All these samples were acquired from aquifer Unit 1, the glaciofluvial sand.

#### **4.3.5** Sampling Locations for the Current Project

The locations of the four wells where groundwater was sampled for EAPS, qPCR, and the <sup>14</sup>C-TCE assay, are provided in Figure 4.3.8. These wells are not in the current "hot spot" for *c*DCE. These wells were chosen because they were the best wells available at Site A that were constructed with PVC instead of steel, and were therefore appropriate for the down-well magnetic susceptibility sonde.



#### Figure 4.3.3. Water Table Elevations across Site A.

Values are feet above mean sea level.

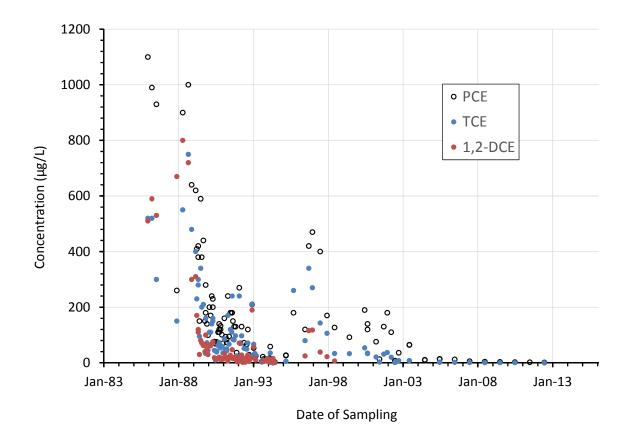


Figure 4.3.4. Decline in Concentrations of PCE, TCE, and *c*DCE + *t*-DCE Over Time in Well 01U108.

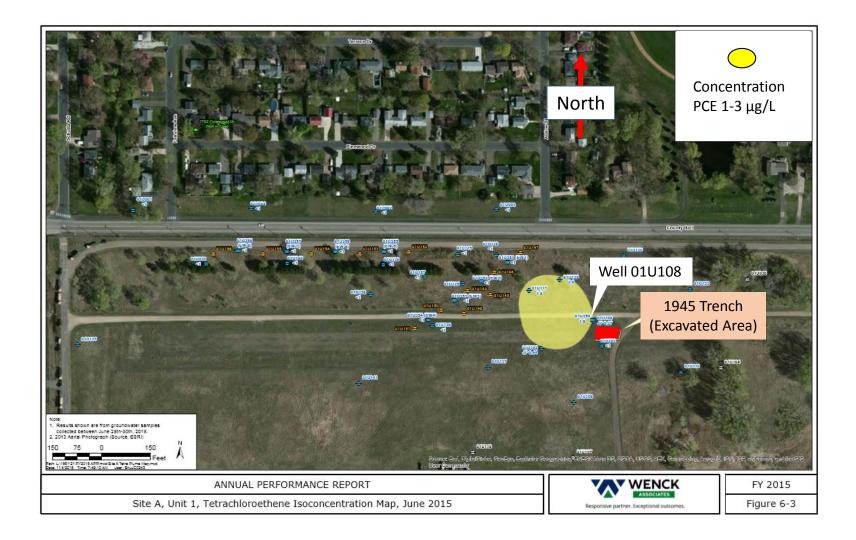


Figure 4.3.5. Distribution of PCE in Monitoring Wells at Site A in June 2015.



Figure 4.3.6. Distribution of TCE in Monitoring Wells at Site A in June 2015.

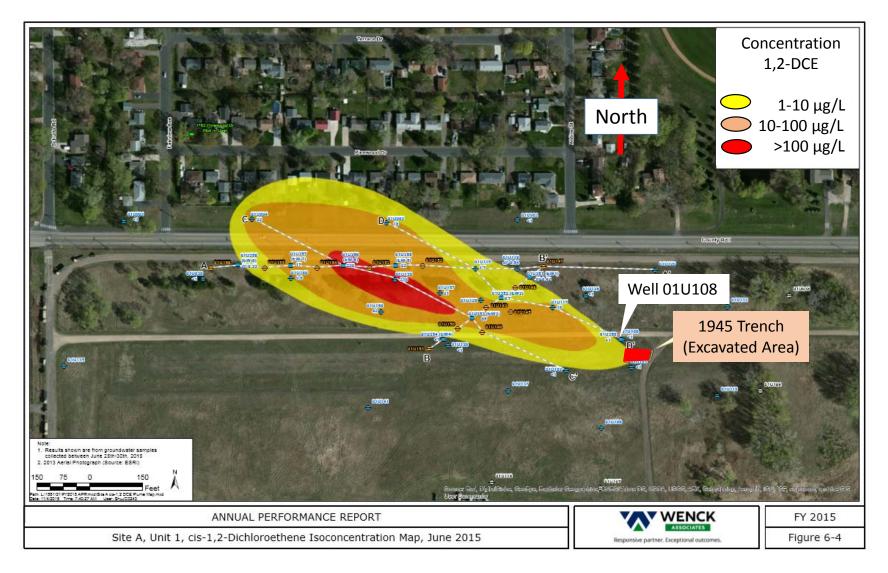


Figure 4.3.7. Distribution of *c*DCE in Monitoring Wells at Site A in June 2015.

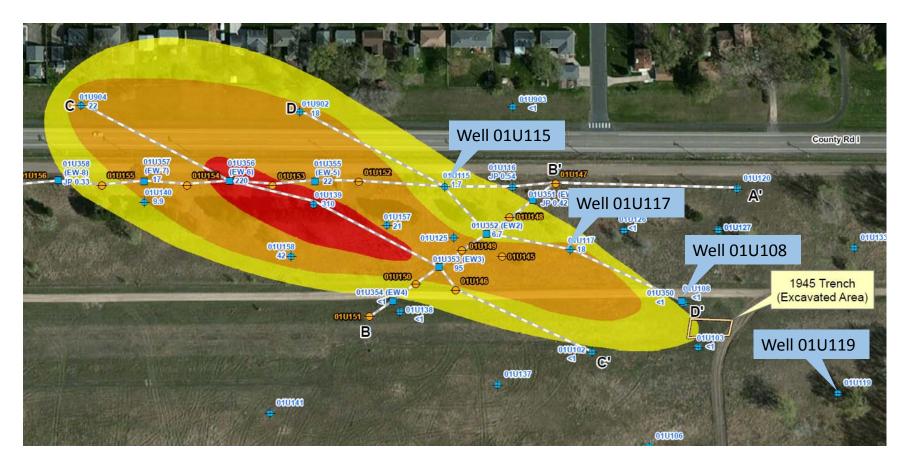


Figure 4.3.8. Location of the Four Wells at Site A to be Sampled.

Well 01U119 is an upgradient well. It provided a comparison to see if the exposure to PCE has mobilized native organic matter that would enrich aerobic microorganisms that would express a soluble monooxygenase and increase the rate of co-oxidation of TCE.

Well 01U108 is the well with the highest historical concentrations of chlorinated alkenes. Wells 01U117 and 01U115 are immediately down-gradient of well 01U108.

The concentrations of PCE, TCE, *c*DCE and vinyl chloride were each below 2  $\mu$ g/L when the four wells were sampled in 2015 (Wenck, 2015). Per the site-specific sampling and analysis plan, purge water from the monitoring wells was disposed to the land surface near the well.

Borehole and well construction logs for the wells selected for the study at TCAAP are presented in Appendix D of the Demonstration Plan (ESTCP, 2016). The wells are screened within Aquifer Unit 1, the glaciofluvial sand. Table 4.3.1 compares the screened intervals of the wells to the distribution of Aquifer Unit 1, Aquifer Unit 2, and the water table.

Table 4.3.1. Relationships between the Depth to the Water Table, the Screened Interval,and the Distribution of Aquifer Unit 1 (glaciofluvial sand) and Aquifer Unit 2 (glacial till)for the Four Wells Selected at Site A.

Well	Water Table (feet bgs)	Screened Interval (feet bgs)	Top Aquifer Unit 1 (feet bgs)	Top Aquifer Unit 2 (feet bgs)
01U119	10.5	9.5 to 19.5	1.5	23.5
01U108	11.5	20 to 30	5.6	32
01U117	10.7	18.0 to 33.0	9.5	33.5
01U115	12.6	17.9 to 32.9	2.0	39.5

bgs = below ground surface

# 4.4 HILL AIR FORCE BASE OPERABLE UNIT 10

Most of the discussion about OU-10 is taken directly from the Remedial Investigation Report (CH2MHill, 2009). In this study, the potential for abiotic TCE degradation was evaluated by measuring the magnetic susceptibility of aquifer sediment in three wells. The potential for cooxidation of TCE was evaluated in water samples from three wells.

#### 4.4.1 Site Location and History

Hill Air Force is a major U.S. Air Force base located in northern Utah, just south of the city of Ogden, near the towns of Clearfield, Riverdale, Roy, Sunset, and Layton. It is located about 30 miles north of Salt Lake City. Operable Unit 10 encompasses the Building 1200 Area along the western boundary of Hill AFB and extends off-base into the cities of Clearfield, Sunset, and Clinton.

Industrial activities at the 1200 Area of OU 10 began in the early 1940s. A variety of chemicals, including chlorinated solvents such as PCE and TCE, were used in those activities.

Most industrial activity in the 1200 Area ceased in 1959, and the majority of 1200 Area buildings were remodeled for administrative functions. Currently, the majority of buildings in the 1200 Area are still being used for administration purposes.

# 4.4.2 Site Geology/Hydrogeology

Hill AFB is located on a terrace that is a remnant of the Paleo-Weber River Delta, formed where the Weber River deposited sediments into ancient Lake Bonneville. The sediments of the Paleo-Weber River Delta are composed primarily of fine-grained delta-front sheet sands interbedded with lacustrine deposits. Fluctuations in Lake Bonneville water levels exposed the Weber River Delta to waves and currents that reworked the deltaic sediments into heterogeneous, laterally discontinuous mixtures.

The complex depositional environment is responsible for the heterogeneous geology underlying OU 10. The sediments underlying the project area have been divided into three fundamental units: (1) sand, (2) silt and clay, and (3) interbedded sand, silt, and clay. In general, the subsurface geology consists of sand deposits separated by discontinuous silt and clay lenses that vary in thickness and lateral extent.

Three principal aquifers underlie the project area. From the surface, the aquifers are (1) a shallow aquifer system, (2) the Sunset Aquifer, and (3) the Delta Aquifer. Figure 4.4.1 illustrates the relationship between the aquifers. The Delta Aquifer is the primary source of drinking water in the area, and the Sunset Aquifer is a secondary aquifer. The shallow aquifer is not a source of drinking water in the area. Groundwater contamination at OU 10 is located within the shallow aquifer system. Current site data indicate the contamination has not migrated to the Sunset or Delta Aquifers.

The shallow aquifer underlying OU 10 consists of two semi-independent water-bearing units, referred to as the Upper and Lower Zones (see Figure 4.4.2). The zones are separated by an aquitard composed of silt and clay and are characterized by distinct groundwater flow directions.

The Upper Zone consists of two hydrostratigraphic units: an aquifer and an underlying aquitard. The aquifer unit is primarily composed of fine to medium sand deposited by fluvial processes as a stream cut into lacustrine clay deposits during the regression of Lake Bonneville. The aquitard is composed of low permeability silt and clay with some interbedded sand.

The paleo-stream channel responsible for depositing the aquifer sand is an important geologic feature underlying OU 10. First, the orientation of the channel drives the groundwater flow direction in the Upper Zone. Second, the channel has substantially thinned or completely eroded the aquitard in some areas, creating localized hydraulic connections between the Upper and Lower Zones.

The depth to groundwater within the aquifer unit of the Upper Zone ranges from 3 to 33 feet below ground surface (bgs). Groundwater flows toward the southwest with an estimated average velocity of 0.5 foot per day (ft/day). In the southwestern portion of the site, in a location where the aquitard separating the Upper and Lower Zones has been completely eroded by the paleo-channel, the Upper and Lower Zones are hydraulically connected.

The Lower Zone is also composed of an aquifer unit and an aquitard. The aquifer consists of layers of sand and discontinuous lenses of silt, clay, and interbedded sand, silt, and clay that vary in thickness and lateral extent. The aquitard is a low permeability, laterally extensive, organic-rich, laminated silt and clay sequence that separates the entire OU 10 shallow aquifer system from the underlying Sunset Aquifer and deeper Delta Aquifer, the primary source of drinking water in the area.

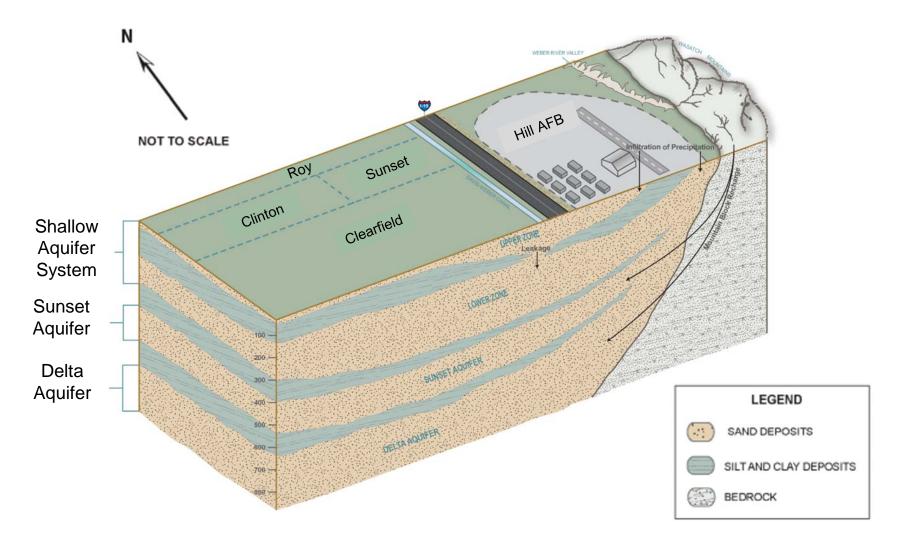


Figure 4.4.1. Major Aquifer Systems.

Zone 1 = Predominately aerobic sands (A); more silty, clayey sand environments may be anaerobic.

**Zone 2** = Predominately anaerobic sand, silt and clay interbeds **(C)**; sandy units have moderate potential to be aerobic.

Zone 3 = Mixing zone (A, B and C); potential for both aerobic and anaerobic pathways.

**Zone 4** = Predominately anaerobic sand, silt and clay interbeds **(C)**; sandy units have some potential to be aerobic.

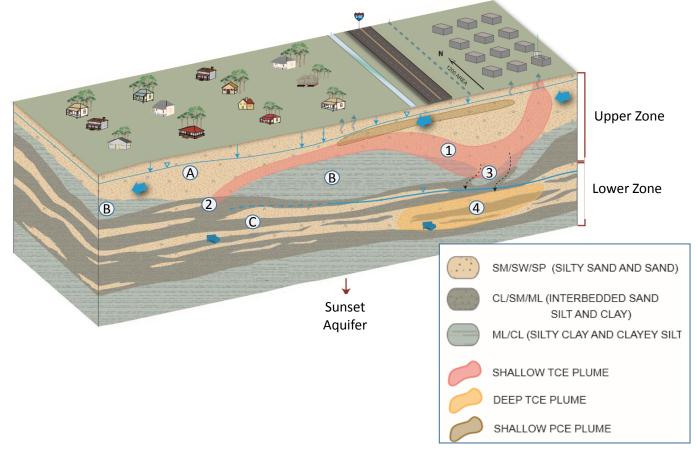


Figure 4.4.2. Relationships in the Upper and Lower Zone of the Shallow Aquifer System.

Depth to groundwater within the Lower Zone ranges between approximately 50 and 185 feet bgs. The Lower Zone is confined in the southeastern corner of the site and in the western portions of the site but is only partially saturated (unconfined) in the northeastern and central portions of the site. Groundwater within the Lower Zone flows toward the northwest. The hydraulic gradient is relatively steep in the eastern portion of the site and becomes shallower in the western portion of the site. Groundwater velocity estimates reflect the differences in hydraulic gradients, with median estimated velocities of 1.9 ft/day in the eastern portion of OU 10 and 0.6 ft/day in the west.

#### 4.4.3 Contaminant Distribution

Figure 4.4.3 compares the distribution of PCE and TCE contamination in the upper zone of the shallow aquifer system to the sources of contamination and to the current extent of groundwater restrictions associated with OU-10. Figure 4.4.4 presents the same information for the deeper zone of the shallow aquifer system.

Groundwater flow in the upper zone is generally to the southwest. Flow in the lower zone is to the north and west. The contamination in the upper zone enters the low zone through a "window" in the silty clay that separates the upper and lower zone. See location ③ in Figure 4.4.2 and the location of well U10-051 in Figure 4.4.4.

#### 4.4.4 Previous Sampling Relevant to the Current Project

As part of the Feasibility study, North Wind applied enzyme activity probes to samples of groundwater from OU-10 that were acquired in 2007 (North Wind, 2007). The results of their probing are summarized in Table 4.4.1.

# 4.4.5 Sampling Locations for the Current Project

The upper zone is generally aerobic and may support aerobic co-oxidation of TCE. Three wells in the upper zone were sampled for enzyme activity probes, qPCR assays of genes for oxygenase enzymes, and to determine the rate of TCE co-oxidation with carbon-14 labelled TCE. The three wells sampled are U10-019, U10-025, and U10-043 (Figure 4.4.3). Unfortunately, well U10-100 was scheduled to be sampled per the Demonstration Plan (Figure 4.4.3), but the sampling team was unable to find this well, and because of difficulties involved in sampling well U10-019, did not have sufficient time to sample the well and still make it to Federal Express for the requisite overnight shipping before the week ended. The magnetic susceptibility in wells U10-025, U10-043, and U10-051 also was determined.

The lower zone is anaerobic and is not expected to co oxidize TCE. None of the wells in the lower zone will be sampled for enzyme activity probes, qPCR assays of genes for oxygenase enzymes, or to determine the rate of TCE co-oxidation with <sup>14</sup>C labelled TCE. However, magnetic susceptibility was determined in the sediments around well U10-051, which is completed in the lower zone (Figure 4.4.4).

Purge water was containerized and disposed of in the Hill AFB wastewater treatment plant per the approved Waste Management Plan.

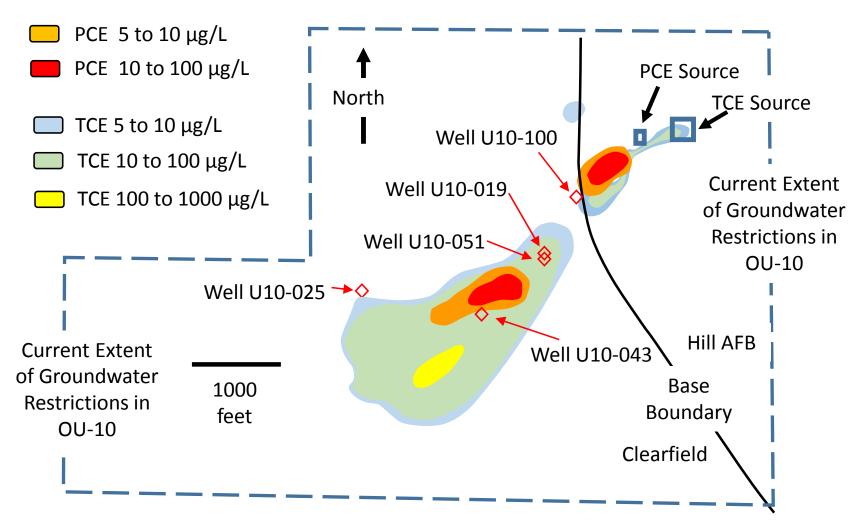


Figure 4.4.3. Comparison of the Contamination in Groundwater in the Upper Zone of the Shallow Aquifer System in 2013 to the Wells in the Upper Zone that are Selected for Sampling.

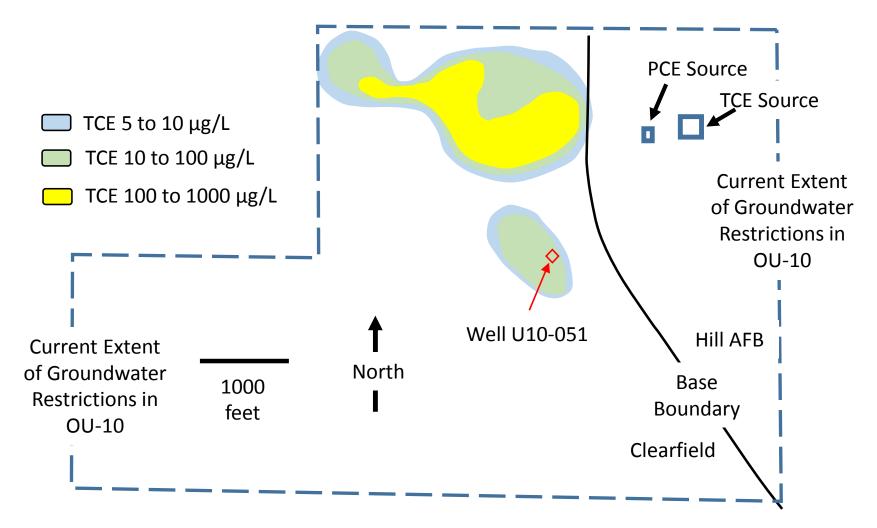


Figure 4.4.4. Comparison of the Contamination in Groundwater in the Lower Zone of the Shallow Aquifer System in 2013 to the Well in the Lower Zone that are Selected for Sampling.

	Enzyme Activity						
Well	Toluene-3-monooxygenase	Toluene-2-monooxygenase	Toluene-2,3-dioxygenase	<b>Total Cells</b>			
	Probe						
	3-Hydroxyphenylacetylene	Phenylacetylene	trans-cinnamonitrile	DAPI			
	Cells per mL						
Reported July 18, 2007							
OU10-019	Not Detected	Not Detected	3.73E+04	5.32E+05			
OU10-025	8.60E+03	3.00E+04	1.47E+03	5.44E+05			
OU10-043	2.61E+04	8.58E+02	3.57E+04	3.73E+05			

# Table 4.4.1. Expression of Toluene Oxygenase Enzymes in Groundwater from OU-1at Hill AFB.

#### 4.5 HOPEWELL JUNCTION

This site is not a DOD site. It was included in this project because it has a unique database that allowed evaluation of the downhole magnetic susceptibility sonde. Borehole core samples were acquired that corresponded to the screened interval of 11 EPA monitoring wells and analyzed in the laboratory. A total of 68 subcores were analyzed for magnetic susceptibility using laboratory methods.

The site also was evaluated using enzyme activity probes. However, it was not originally assayed using qPCR for DNA associated with oxygenase enzymes. In addition, before this project, aerobic biodegradation had not been incorporated in the site conceptual model at a quantitative level. This project includes EAPS, qPCR analyses, and a <sup>14</sup>C-TCE assay for this site, as discussed in Section 5.

In this study, the potential for abiotic TCE degradation was evaluated by measuring the magnetic susceptibility of aquifer sediment in six wells. The potential for cooxidation of TCE was evaluated in water samples from four wells.

#### 4.5.1 Site Location and History

This section is a summary of material in CDM Federal Programs Corporation (2008, 2012).

The source of contamination of groundwater with chlorinated solvents was the former Hopewell Precision facility, at 19 Ryan Drive, Hopewell Junction, NY. U.S. EPA was made aware of the potential for contamination in 1979. In February 2003, EPA sampled 75 residential wells near the Hopewell Precision facility. Analysis of these samples revealed that five residential wells were contaminated with TCE ranging from  $1.2 \mu g/L$  to  $250 \mu g/L$ . At that time, the New York State Department of Environmental Conservation (NYSDEC), on behalf of New York State Department of Health (NYSDOH), requested EPA to conduct a removal action at the site, including installation of carbon filter systems on the residential wells.

From February to November 2003, EPA collected groundwater samples from hundreds of private drinking water wells in the vicinity of Hopewell Precision. TCE and 1,1,1-TCA were both detected in numerous private well samples, at individual concentrations up to 250  $\mu$ g/L for TCE and 11.7  $\mu$ g/L for 1,1,1-TCA. In addition, 1,1-dichloroethene (1,1-DCE), a breakdown product of 1,1,1-TCA, was detected in two samples. Several instances of TCE detection exceeded the compound's Maximum Contaminant Level (MCL) of 5  $\mu$ g/L. At that time, EPA installed point-of-entry-treatment (POET) systems to remove volatile organic compounds (VOCs) at 37 homes where TCE approached or exceeded the MCL.

Since 2003, EPA's Removal Action Branch has conducted residential well sampling and collected groundwater samples from homes with POET system three times per year. As of May 2009, EPA has installed POET systems at 41 homes. In addition, NYSDEC has installed POET systems at 14 homes with 1,1,1-TCA concentrations that exceed the NYSDEC groundwater standard and NYSDOH drinking water standard.

Figure 4.5.1 compares the distribution of TCE in groundwater in 2006 and 2007. The TCE contamination extended 8,000 feet downgradient of the former Hopewell Precision facility. Figure 4.5.2 compares the distribution of TCE contamination in 2010 to the locations of POET systems and EPA monitoring wells at the site.

# 4.5.2 Site Geology/Hydrogeology

The site is situated in a glaciated valley underlain by the Hudson River Formation in the northern portion of the site and the Stockbridge Limestone in the southern portion of the site. The bedrock is overlain by unconsolidated sediments deposited by glaciers and glacial meltwater. The glacial outwash deposits are a complex mixture of boulders, gravel, sand, silt, and clay which form discontinuous beds or lenses. Due to multiple glaciation events, subsurface units are heterogeneous and highly localized. Till is also present in the overburden underlying the site. The till forms a mound in the shape of a tear drop with the long axis oriented north-south. The plume of contaminated groundwater is bifurcated by the till (Figure 4.5.1).

The unconsolidated deposits at the site have been grouped into three hydrostratigraphic units: a) sand and gravel unit (including silty sand, silty gravel, and mixtures of sand, silt, and gravel), b) silt and clay (including silty clay), and c) the till mound. The sand and gravel units have higher hydraulic conductivity than the silt and clay units, as indicated by the slug test results discussed below. The sand and gravel units are expected to be preferential flow paths for groundwater contamination. These units are localized and discontinuous, likely creating multiple complex flow paths through the overburden.

Figure 4.5.3 presents the potentiometric surface in the shallow wells and Figure 4.5.4 presents the potentiometric surface in the deep wells. In general, groundwater flow is towards the valley from the upland areas on the east and west sides of the valley. In the valley, groundwater flow is generally towards the southwest along the valley axis. The till mound impedes groundwater flow within the valley, as evidenced by horizontal gradient data. Groundwater flows preferentially in higher conductivity silty sand and gravel units. During the RI, the horizontal gradients were estimated in the following areas:

- Between monitoring wells EPA-8S and EPA-12S the horizontal gradient is  $4.09 \times 10^{-3}$ .
- Between monitoring wells EPA-16S in the north and EPA-19S south of the till unit, the gradient is  $8.7 \times 10^{-3}$ .
- The topography flattens and the horizontal gradient decreases to  $2.53 \times 10^{-3}$  between monitoring well EPA-21S and piezometer PZ-02.

The vertical gradient in most monitoring wells is upwards, indicating groundwater discharge into the valley and Whortlekill Creek which runs along the axis of the valley and also flows to the southwest. The gradient ranged from 0.06 foot at EPA-10S/EPA-10D to 6.22 feet at EPA-12S/EPA-12D. Overall, the vertical gradient at 10 of 15 well pairs was less than 1 foot.

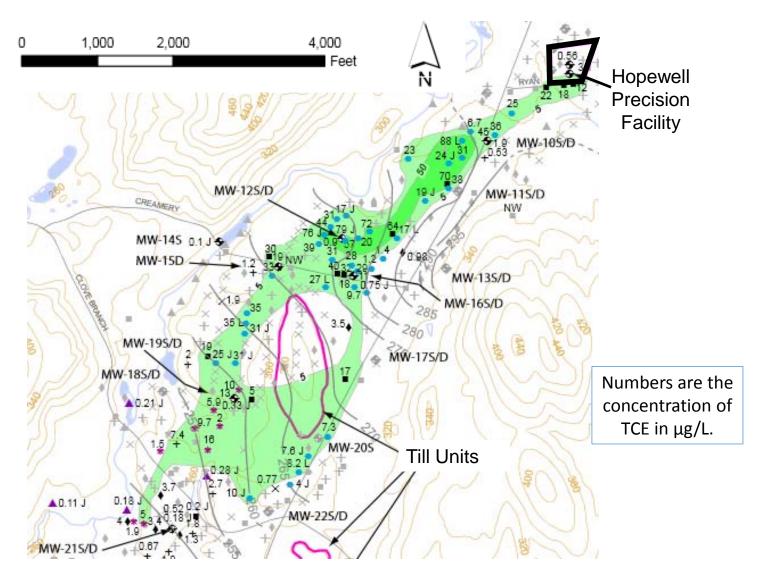


Figure 4.5.1. Distribution of TCE in Groundwater 2006 and 2007.

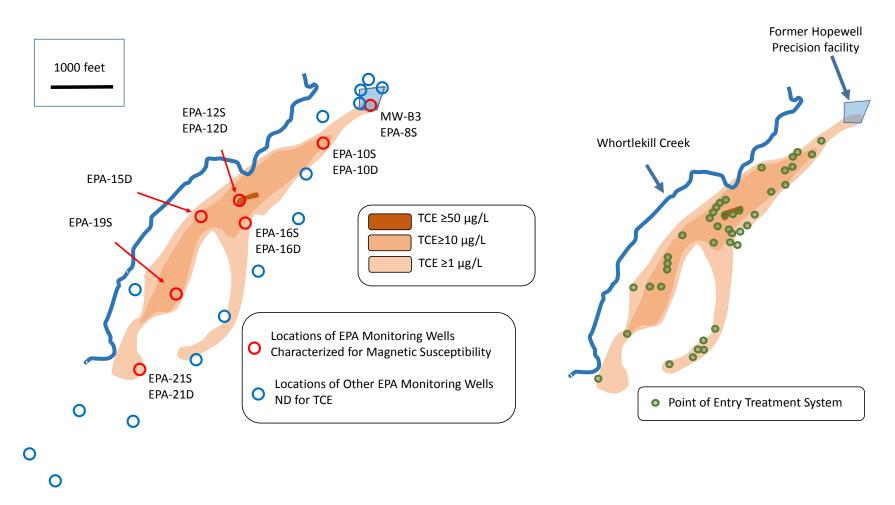


Figure 4.5.2. A Comparison of the Distribution of TCE Contamination in Groundwater in 2013 and the Location of Private Wells with Point-of-entry-treatment Systems, and the Location of EPA Monitoring Wells.

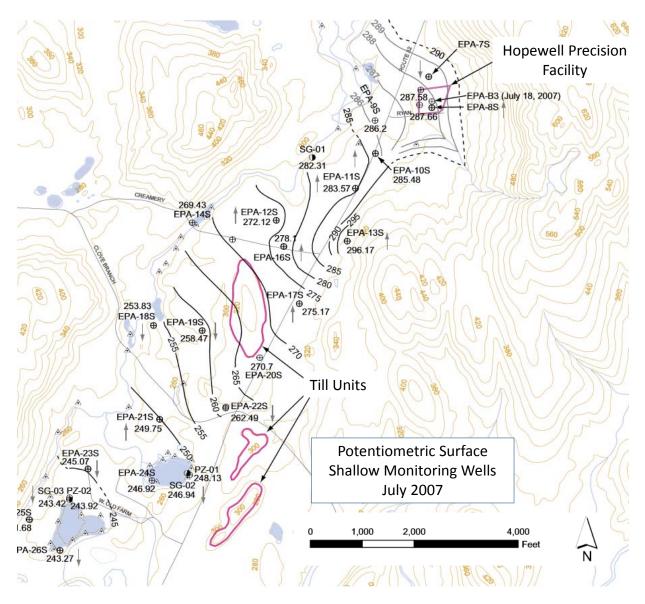


Figure 4.5.3. Potentiometric Surface in the Shallow Monitoring Wells at the Hopewell Precision Site in 2007.

From Figure 1-3 in CDM (2012).

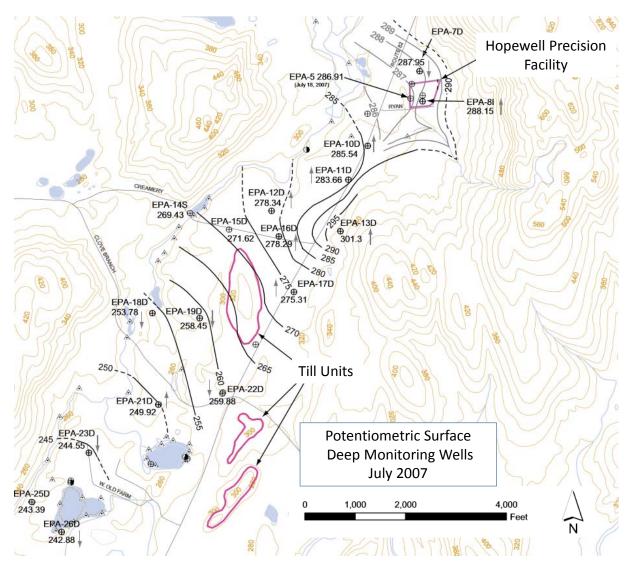


Figure 4.5.4. Potentiometric Surface in the Deep Monitoring Wells at the Hopewell Precision Site in 2007.

From Figure 1-4 in CDM (2012).

The groundwater flow velocity at the site was estimated using hydraulic conductivity values from slug tests and by evaluating movement of the TCE groundwater contaminant plume. The estimate developed by evaluating the TCE plume resulted in a hydraulic conductivity of 36 feet/day. The average hydraulic conductivity (geometric mean of the arithmetic means of results of slug tests run at each well) from slug testing was 2.53 feet/day. The average hydraulic conductivity of 2.53 feet/day represents the bulk hydraulic conductivity of unconsolidated deposits at the site and indicates that most of these deposits are fine-grained silts, silty sands, and silty clay. However, slug test results from specific wells are consistent with the higher hydraulic conductivity implied by the movement of the plume. At monitoring well EPA-18D the arithmetic mean of the nine tests conducted was 28 feet/day, while at monitoring well EPA-23S the arithmetic mean of the two tests conducted was 40 feet/day.

Based on an effective porosity of 25 percent (preferential flow paths consist of silty sand and gravel), an arithmetic mean hydraulic conductivity of 34 feet/day from slug tests at monitoring well EPA-18D and EPA-23S, groundwater flow velocities were calculated as follows:

- North portion of the flow path (EPA-8S to EPA-12S) approximately 203 feet/year
- Central portion (EPA-16S to EPA-19S) approximately 432 feet/year.
- South portion (EPA-21S to further downgradient) approximately 126 feet/year.

### 4.5.3 Contaminant Distribution

Figure 4.5.5 presents the distribution of TCE in the EPA monitoring wells at the most recent sampling date. Figure 4.5.6 compares the distribution of TCE in the private wells with a point-of-entry-treatment (POET) system 2015. The highest concentrations of TCE are less than  $40 \ \mu g/L$ .

#### 4.5.4 Previous Sampling Relevant to the Current Project

In August 2013, core samples were acquired adjacent to eleven EPA monitoring wells that were selected for this study. The cores were acquired across the vertical interval represented by the screened interval of the EPA wells. The core samples were analyzed for mass magnetic susceptibility at the R.S. Kerr Center in Ada, OK, following their in-house SOP. Table 4.1.2 summarizes the laboratory mass magnetic susceptibility data collected from this Site in August 2013.

Enzyme activity probes (EAP) were applied to groundwater samples from the Hopewell Precision site. Results were presented in Lee (2013). Results are summarized in Table 4.5.1 and Figure 4.5.7. Lee (2013) applied probes for toluene-3-monooxygenase, toluene-2-monooxygenase, toluene-2,3-dioxygenase and soluble methane monooxygenase. For this project, these probes plus a probe for the toluene side chain monooxygenase were utilized.

# 4.5.5 Sampling Locations for the Current Project

Of the eleven EPA monitoring well locations specified in the Demonstration Plan (ESTCP, 2016; Figure 4.5.8) ten locations were probed for magnetic susceptibility. The 8S/B3 location was not sampled because the wells were not accessible and the sonde could not be lowered into the well. Figure 4.5.9 identifies the four wells that were sampled for EAPs, DNA assays and determination of the rate of aerobic TCE cometabolism using the <sup>14</sup>C-TCE Assay.

Appendix D of the Demonstration Plan (ESTCP, 2016) provides construction logs and borehole lithologic logs prepared for the monitoring wells sampled during this investigation.

As is the State-approved practice, purge water was handled according to NYSDEC's DER-10. This allows discharge of purge water to the ground if the purged well has historical VOC concentrations below drinking water standards. For those monitoring wells where the VCOC concentrations are exceeded by more than 10 times, the purge water was containerized. Based on these criteria, purge water was discharged to the ground from all monitoring wells to be used for this investigation except 10S and 12S. Water from these wells was containerized and disposed of in accordance with the approved Waste Management Plan.

# Table 4.5.1. Expression of Toluene Oxygenase Enzymes in Groundwater from the<br/>Hopewell Precision Site, as Reported in Lee (2013).

	Enzyme Activity					
	Toluene-3-monooxygenase	Toluene-2-	Toluene-2,3-	Total Cells		
Well		monooxygenase	dioxygenase			
	Probe					
	3-Hydroxyphenylacetylene	Phenylacetylene	trans-cinnamonitrile	DAPI		
	Cell per mL					
EPA-10S	3.0x10 <sup>4</sup>	$1.7 \times 10^4$	9.3x10 <sup>3</sup>	7.3x10 <sup>4</sup>		
EPA-10D	2.3x10 <sup>4</sup>	$2.2x10^4$	$4.4x10^{3}$	6.2x10 <sup>4</sup>		
EPA-12S	6.7x10 <sup>4</sup>	6.7x10 <sup>3</sup>	6.4x10 <sup>3</sup>	1.6x10 <sup>5</sup>		
EPA-12D	$3.2x10^2$	8.0x10 <sup>1</sup>	1.6x10 <sup>2</sup>	1.6x10 <sup>5</sup>		
EPA-16S	$1.4x10^4$	1.1x10 <sup>4</sup>	4.9x10 <sup>3</sup>	1.2x10 <sup>5</sup>		
EPA-16D	9.7x10 <sup>4</sup>	1.1x10 <sup>4</sup>	$1.4 \times 10^4$	2.2x10 <sup>5</sup>		
EPA-21D	3.1x10 <sup>3</sup>	$4.2x10^{3}$	1.1x10 <sup>4</sup>	2.3x10 <sup>5</sup>		

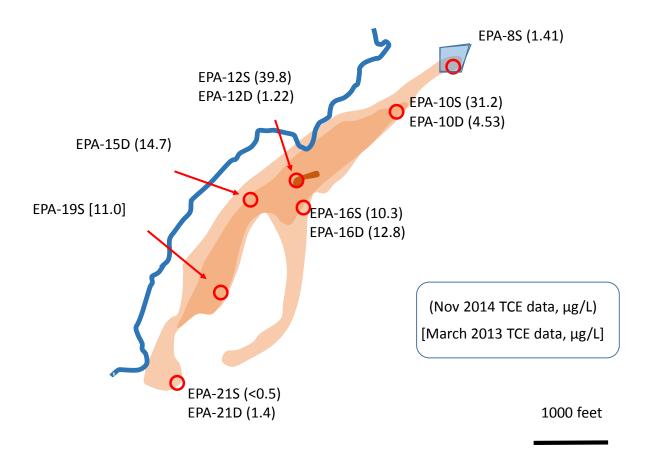


Figure 4.5.5. Concentrations of TCE in the Wells To Be Probed for Magnetic Susceptibility.

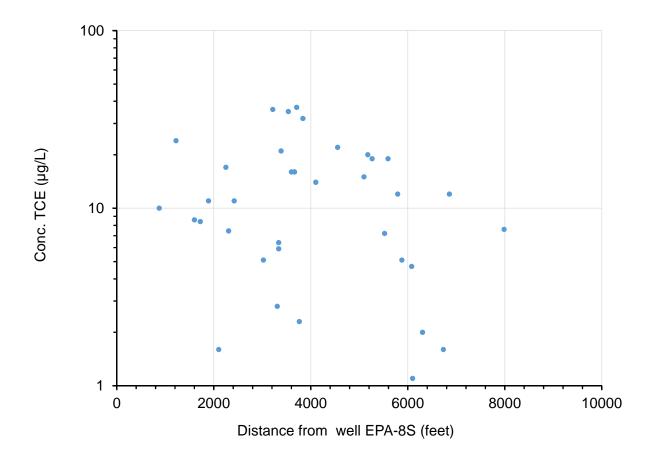
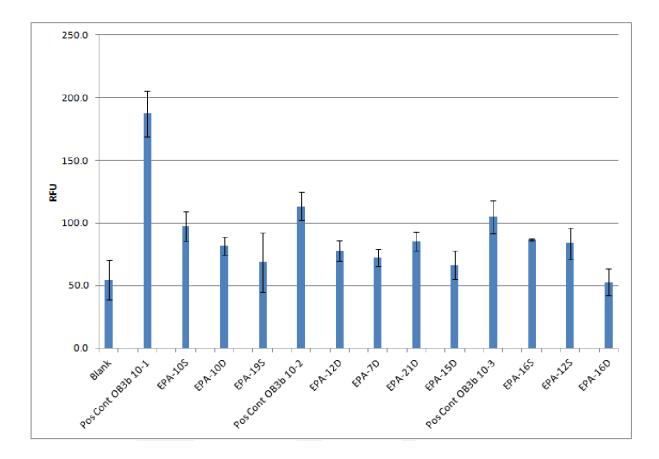


Figure 4.5.6. Concentration of TCE in the Private Wells with Point-of-entry-treatment Systems in 2015.



# Figure 4.5.7. Screenshot of Text in Lee (2013) Discussing the Expression of Soluble Methane Monooxygenase in Water Samples from the Hopewell Precision Site.

*RFU* is the response in Relative Fluorescene Units that developed after exposure to coumarin in phosphate buffer. The Blank is water filtered through a  $0.2 \mu m$  filter and then assayed.

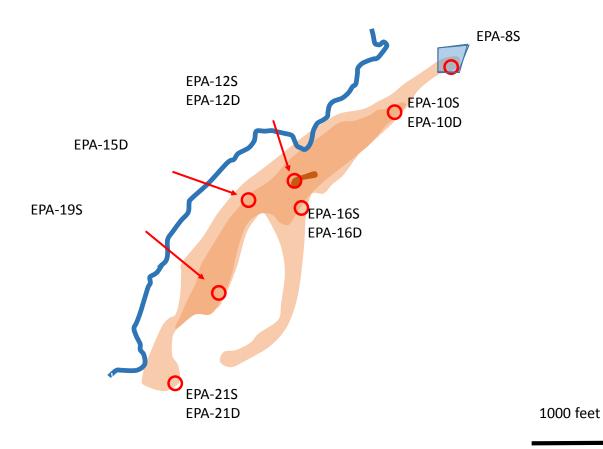
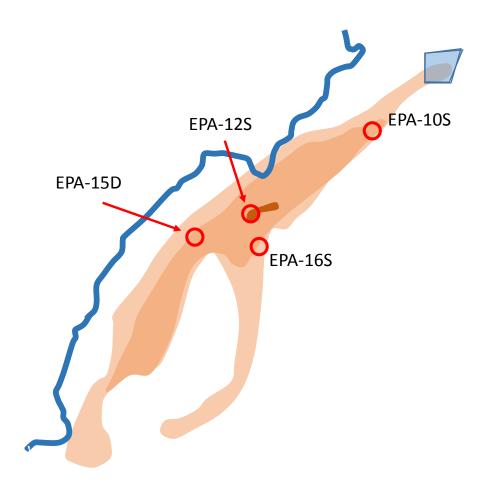


Figure 4.5.8. The Eleven Wells Proposed for Magnetic Susceptibility Sonding.

Note that well EPA-8S was not sampled because the well was compromised and the sonde could not be lowered into the well.



1000 feet

# Figure 4.5.9. The Four Wells Sampled for Enzyme Activity Probes, DNA Assays and Rate of Co-oxidation of TCE.

# 4.6 TOOELE ARMY DEPOT

Magnetic susceptibility data was collected in numerous core samples during the installation of monitoring wells at the Site. Under this effort, the project team conducted downhole magnetic susceptibility analyses and compared the results to the laboratory-based analyses that are already available. Furthermore, in their 2013 Evaluation of MNA (Parsons, 2013), Parsons recommended using EAPs to evaluate aerobic co-oxidation of TCE. Under this effort, the project team will complete EAP analysefss in the wells that were installed in the borings from which magnetic susceptibility analyses were completed. The team will also determine the rate constant for aerobic biodegradation of TCE in the groundwater.

In this study, the potential for abiotic TCE degradation was evaluated by measuring the magnetic susceptibility of aquifer sediment in one well. Three other wells were logged for the convenience of the Army Corps of Engineers. The potential for cooxidation of TCE was evaluated in water samples from four wells.

#### 4.6.1 Site Location and History

Unless otherwise specified, information in this report was taken from Army Corps of Engineers (ACE; 2013). In many cases, text is copied from ACE (2013) and pasted without modification.

The Tooele Army Depot (TEAD) is a United States Army post located in Tooele County, Utah. It is located south of the city of Grantsville, southeast of the city of Erda and southwest of the city of Tooele (Figure 4.6.1). The boundary of the model domain for a transport and fate model constructed by the U.S. Army Corps of Engineers and its contractors (ACE, 2013) was used to orient detailed maps in figures subsequent to Figure 4.6.1.

From 1942 to 1966, a large quantity of hazardous wastes was generated as a result of the maintenance and storage of military vehicles and equipment. The waste chemicals were piped through the industrial complex into a set of four unlined drainage ditches. These ditches ended at land-spreading areas and gravel pits that were used as evaporation/infiltration areas. These gravel pits collectively have been called the old industrial wastewater lagoon (OIWL). In 1966, a collector ditch was constructed to intercept the four existing ditches. This interceptor ditch ran north for 1.5 miles to an abandoned gravel quarry. This pit, the IWL, was used as an evaporation/infiltration pond until its closure in 1988. At that time, an industrial wastewater treatment plant was brought on-line. These hazardous waste disposal practices at TEAD led to groundwater contamination in the industrial area and northward. The primary contaminant of concern is the solvent TCE, which was used in the service and repair of military vehicles and equipment. The location of the OIWL and IWL are presented in Figure 4.6.2.

### 4.6.2 Site Geology/Hydrogeology

The majority of the southern and central portions of the study area are underlain by shallow bedrock. Groundwater levels indicate that the bedrock should be divided into two distinct units – the bedrock basement and an "encased," uplifted bedrock block located in the center of the study area (Figure 4.6.3).

The conceptualization of fault zones in AEC (2013) was predicated upon evidence of abrupt water level changes typical of faults in both bedrock and alluvium. The faults are labelled in Figure 4.6.2. The water elevations are presented in Figure 4.6.3. Figure 4.6.4 presents a conceptual model of the vertical distribution of the bedrock, the alluvium, faults in the bedrock and alluvium, and the water table.

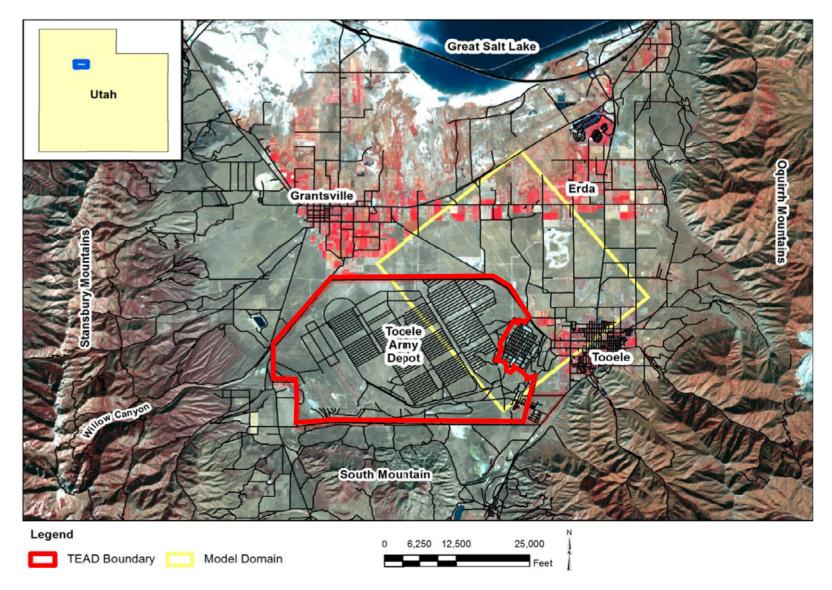


Figure 4.6.1. Location of the Tooele Army Depot (TEAD).

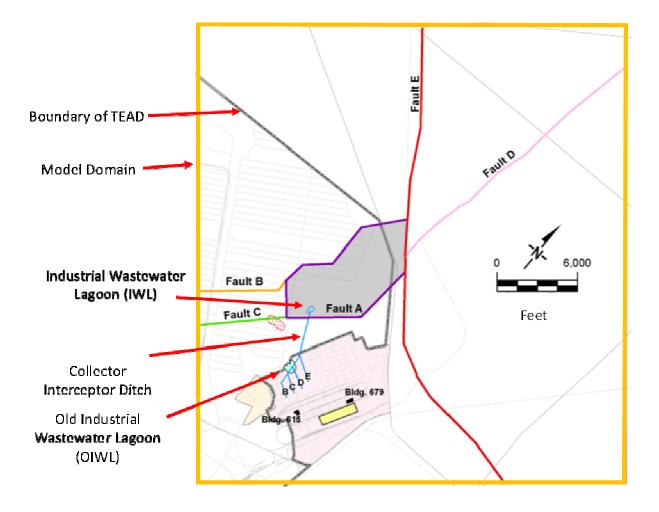


Figure 4.6.2. Location of the Industrial Wastewater Lagoons.

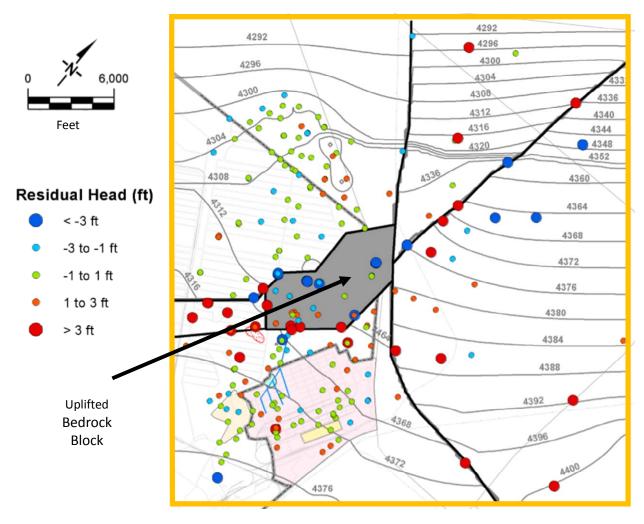


Figure 4.6.3. Elevation of the Water Table (feet above mean sea level).

The isopleths are the calibrated water levels in the groundwater flow model (ACE, 2013). The colored dots are the residuals of actual measured water table elevations from the model.

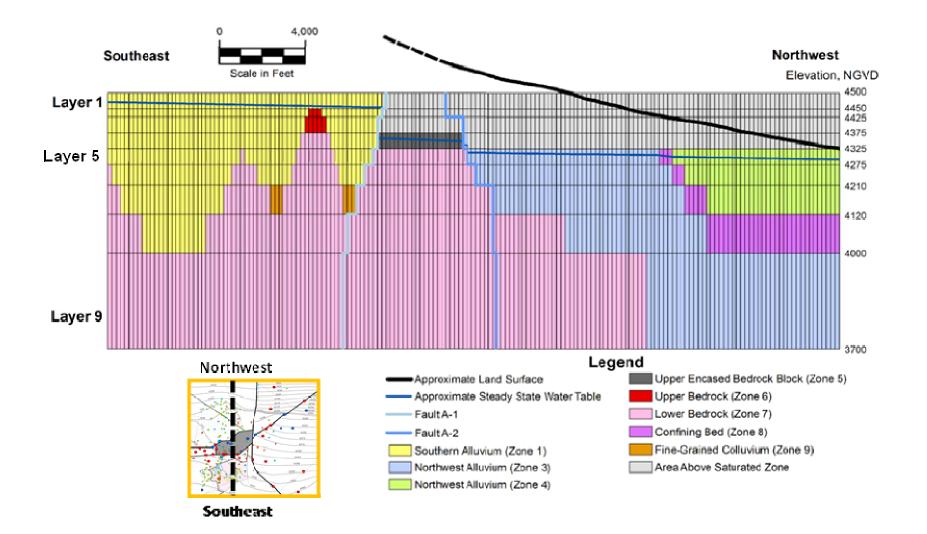


Figure 4.6.4. Conceptual Model of the Distribution of Bedrock, Alluvium, Faults in the Bedrock and Alluvium, and the Water Table in a Transect from the Southeast to the Northwest Boundaries of the Model Zone.

(See dotted black line in the insert)

ACE (2013) hypothesized that the cause of the sharp gradients across bedrock faults in bedrock was the formation of low permeability fault gouge and weathered clay products. The unconsolidated sediments, which underlie most of the study site, are heterogeneous at the scale of the computer model (ACE, 2013) and generally consist of coarser grained sand/gravel deposits with some cemented areas and inter-fingered layers of clay and silt typical of alluvial and lacustrine deposits. The alluvium on the site is conceptualized as four separate units: 1) the southeastern alluvium, located to the southeast of the uplifted bedrock block; 2) the northwestern alluvium located to the southeast of the uplifted bedrock block; 3) fine-grained material located at depth to the southeast of the uplifted bedrock block; and 4) the northward-dipping lacustrine confining bed located in the northern and northwestern quadrants of the study area. The depth of this latter lacustrine deposit increases downgradient, splitting the northwestern alluvial deposits into unconfined (shallow) and confined (deep) aquifers.

The shallow upgradient alluvium at the southeastern end of the site has a very flat gradient most likely resulting from a damming effect produced by the low conductivity fault/bedrock system downgradient. Additionally, a high percentage of permeable gravels and sands were noted in borings in the southern alluvium, relative to the northern alluvium. One hypothesis for this is that the southern alluvium is closer to the mountain front where coarser material would be deposited from alluvial outwash. At the southern end of the model area, the alluvium is very shallow with approximately 50 ft of saturated thickness between the bedrock basement, and the water table.

The northwestern alluvium, located downgradient from the bedrock block and adjacent faults, is composed of several interconnected aquifers. There are two prominent hydraulic features associated with the northwestern alluvium: 1) an abrupt drop in measured groundwater levels that occurs along a line that roughly parallels the southern extent of the Great Salt Lake; 2) vertical gradients that increase with depth towards the downgradient model boundary.

Results from a pumping test in estimated the horizontal hydraulic conductivity in the northwestern alluvium to be 200 ft/d. The estimated hydraulic conductivity of the bed rock varies from 50 to 70 ft/d. In the elevated bedrock block, the average hydraulic conductivity is approximately 30 ft/d.

#### 4.6.3 Contaminant Distribution

Figure 4.6.5 compares the distribution of TCE in wells in the domain of the solute transport model to a summary evaluation of the distribution of TCE contamination based on the transport and fate model and on kriging of the data. Figure 4.6.6 presents the distribution of TCE in the local area.

# 4.6.4 Previous Sampling Relevant to the Current Project

Core samples that had been archived from the installation of monitoring wells were provided to staff of the R.S. Kerr Environmental Research Center for analysis of mass magnetic susceptibility. Data are available from two adjacent wells, one screened across the water table (monitoring well D-20) and one deeper into the alluvial sediments (monitoring well D-23). The borehole core mass magnetic susceptibility data for these wells is summarized in Table 4.1.2.

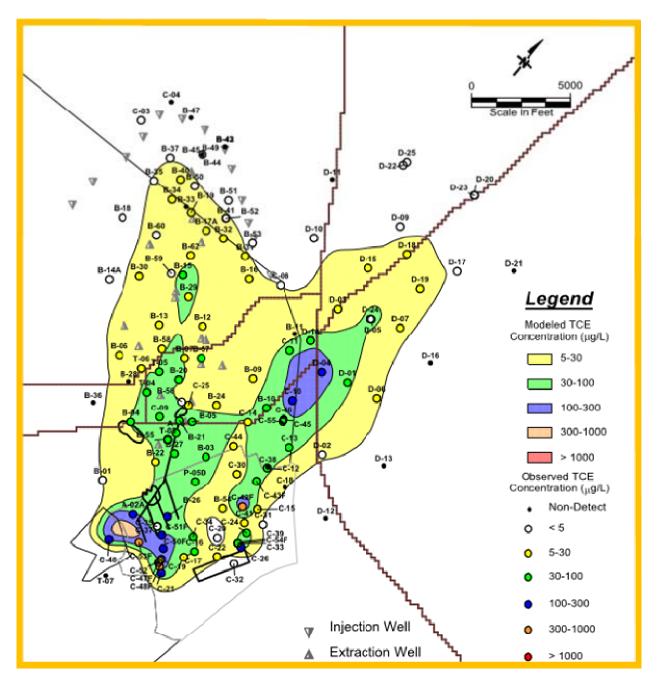


Figure 4.6.5. Distribution of TCE Contamination in Groundwater in the Model Domain.

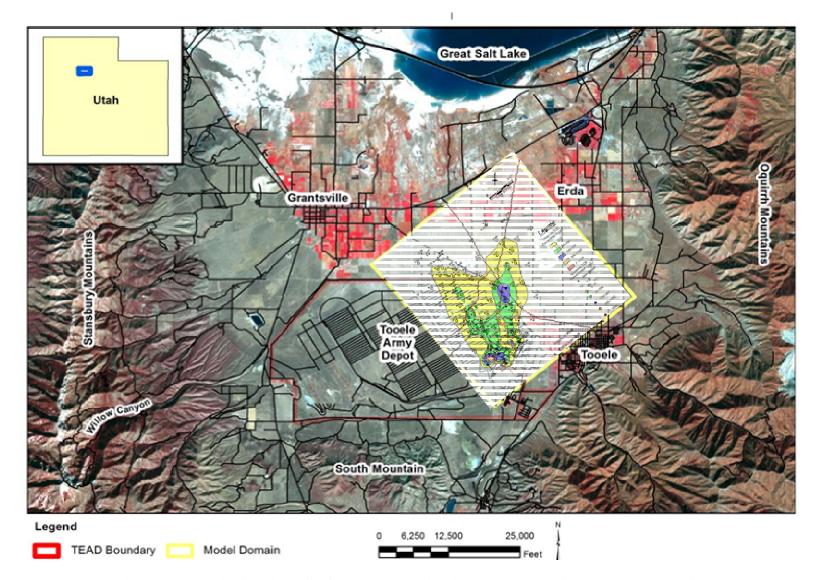


Figure 4.6.6. Distribution of TCE contamination in groundwater in the model domain.

#### 4.6.5 Locations Sampled for the Current Project

The wells circled in red in Figure 4.6.7 were sampled for Enzyme Activity Probes, determination of the rate of aerobic co-oxidation of TCE, and a sonde was inserted in the wells to determine mass magnetic susceptibility of the sediments. They are wells D-19, D-20, D-23 and D-25. Although wells D-23 and D-25 had a sonde lowered into them, they either do not have mass magnetic susceptibility data obtained from laboratory analysis of core data, or have these data from beneath the total depth of the completed well.

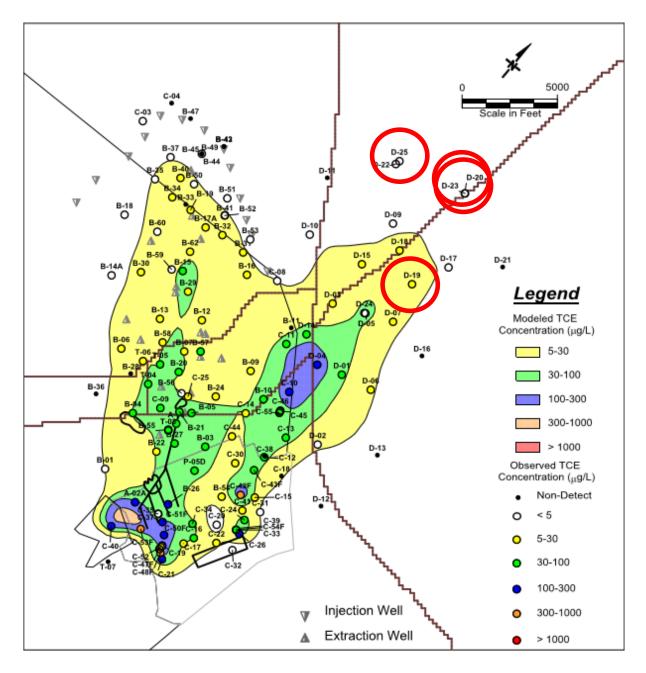


Figure 4.6.7. Locations Sampled for this Effort.

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# 5.0 TEST DESIGN

This section provides a detailed description of the system design and testing conducted during the demonstration.

# 5.1 CONCEPTUAL EXPERIMENTAL DESIGN

In order to complete the objectives outlined in the Demonstration Plan, seven (7) tasks were completed:

- Task 1 Development of Demonstration Plan/Field Sampling Plan.
- Task 2 Field Work Deployment of Magnetic Susceptibility Sonde and Field Sampling for Enzyme Activity Probes, qPCR Assays of Co-Oxidation Enzymes, and Direct Assay of Rate of Aerobic Biodegradation.
- Task 3 Develop a Carbon 14 Tracer Procedure to Directly Assay the Rate of TCE Aerobic Biodegradation.
- Task 4 Laboratory Work to Conduct Carbon 14 Tracer Direct Assay of the Rate of TCE Aerobic Biodegradation.
- Task 5 Laboratory Work to Implement Enzyme Activity Probes and the qPCR Assays for Oxygenase Enzymes that can Co-Oxidize TCE.
- Task 6 Final Report.
- Task 7 Project Management.

Each task is discussed in the following subsections.

#### 5.1.1 Task 1 - Development of Demonstration Plan/Field Sampling Plan

Under this task, a Demonstration Plan that met all ESTCP requirements and guidelines was prepared and approved by ESTCP. This document included the objectives of the demonstration, qualitative and quantitative criteria for success, the methodologies to be employed, and the measurements that were required to determine success. The Demonstration Plan was approved in April 2016.

#### 5.1.2 Task 2 – Field Work - Deployment of Magnetic Susceptibility Sonde (Probe) and Field Sampling for Enzyme Activity Probes, qPCR Assays of Co-Oxidation Enzymes, and Direct Assay of Rate of Aerobic Biodegradation

Task 2 consisted of:

- 1. Mobilization;
- 2. Collecting magnetic susceptibility data using a downhole sonde;
- 3. Collecting groundwater samples for submission to Clemson University and PNNL, and;
- 4. Demobilization.

#### Task 2.1 - Coordination and Mobilization

This task was used to coordinate field work and obtain the materials necessary for field work. The following people supported T.H. Wiedemeier & Associates, Inc. (THWA) and Scissortail Environmental Solutions, LLC (SES) to coordinate access to the sites and/or provide field assistance for the sites. Mr. Mark Ferrey with the Minnesota Environmental Pollution Control Agency, coordinated work at the TCAAP in MN. Ms. Diana Cutt with the USEPA Region 2 coordinated work at the former Plattsburgh AFB and the Hopewell Precision site in NY. Ms. Sharon Stone, AFCEC/CZO, Peterson AFB, Colorado and Mr. Todd Isakson, CH2M Hill, Taylorsville, Utah helped coordinate work at OU-10 at Hill AFB. Mr. Marc Sydow and Mr. Nicholas Montgomery with U.S. Army JMC, provided support for the effort at Tooele Army Depot, Utah. David Farnsworth with U.S. Air Force, Bryan Gamache with AECOM, Lorenzo Thantu U.S. EPA Region 2, Matt Ivers with Parsons, Travis McGuire with GSI Environmental Inc., and W. Zachary Dickson with Dickson & Associates assisted in gaining access to wells and core samples or collecting other data.

#### Task 2.2 - Field Work

For this task Todd Wiedemeier and Dr. John Wilson traveled to the five sites described in Section 4 to deploy the magnetic susceptibility sonde and collect the data necessary to compare these data to those previously collected from soil cores at the sites. The task also was used to collect the water samples that were assayed using enzyme activity probes, qPCR for oxygenase enzymes, and for the rate of aerobic biodegradation of TCE using the <sup>14</sup>C-labeled TCE assay.

Appendix B presents the daily field and sampling reports collected during Field Work. Appendix C contains the data collected using the downhole magnetic susceptibility sonde.

# 5.1.3 Task 3 - Develop a Carbon 14 Tracer Procedure to Directly Assay the Rate of TCE Aerobic Biodegradation

Task 3 was used to refine a method for purifying <sup>14</sup>C-TCE beyond what was achieved in previous studies. As indicated in sections 2.2.2 and 3.1.2, use of two GC columns in series was evaluated. It was determined that a single column provided an adequate level of purification. Although the target level for impurities was not met (i.e., less than 0.01% of the total <sup>14</sup>C added to the serum bottles), the level of impurities was sufficiently low to permit detection of first order co-oxidation rates as low as 0.00658 yr<sup>-1</sup>. This necessitated increasing the incubation time of the assay to 40-46 days, to allow for sufficient accumulation of products. A potential concern with an incubation time longer than a few days is changes in the microbial community. However, as results for the groundwater samples indicate, the rates of <sup>14</sup>C product accumulation tended to diminish with time. If changes in the microbial community did occur, it resulted in a more conservative estimate of the rates of TCE degradation. Details regarding the approach that was used to accomplish Task 3 are provided in Section 5.3.

# 5.1.4 Task 4 - Laboratory Work to Conduct Carbon 14 Tracer Direct Assay of the Rate of TCE Aerobic Biodegradation

The goal of Task 4 was to determine pseudo-first order rate constants for TCE co-oxidation in groundwater samples from five sites, with samples taken from four wells per site. The assay was performed in 160 mL clear, borosilicate glass serum bottles (Wheaton®; Boston round, 125 mL)

that were cleaned, dried, and autoclaved along with Teflon-faced gray butyl rubber septa and aluminum crimp caps (20 min, 121 °C). The bottles were labeled and massed (balance precision,  $\pm 0.01$  g) and then shipped to Wiedemeier & Asccociates for use in sample collection. In the field, triplicate 100 mL groundwater samples were collected from each monitoring well. The serum bottles were immediately capped with their respective Teflon-faced gray butyl rubber septum and crimped with an aluminum cap. The bottles were stored on ice and shipped overnight to Clemson University. Upon arrival, the bottles were removed from the packaging and warmed to room temperature (22 ± 2°C), quiescently in the dark, for approximately 24 hours before addition of the <sup>14</sup>C-TCE stock solution.

For a given site, triplicate serum bottles were received from two wells on the first day, and a second set of triplicates was received from two additional wells on the following day. When the first set of triplicates groundwater samples was prepared, a set of triplicate DDI water controls was prepared at the same time

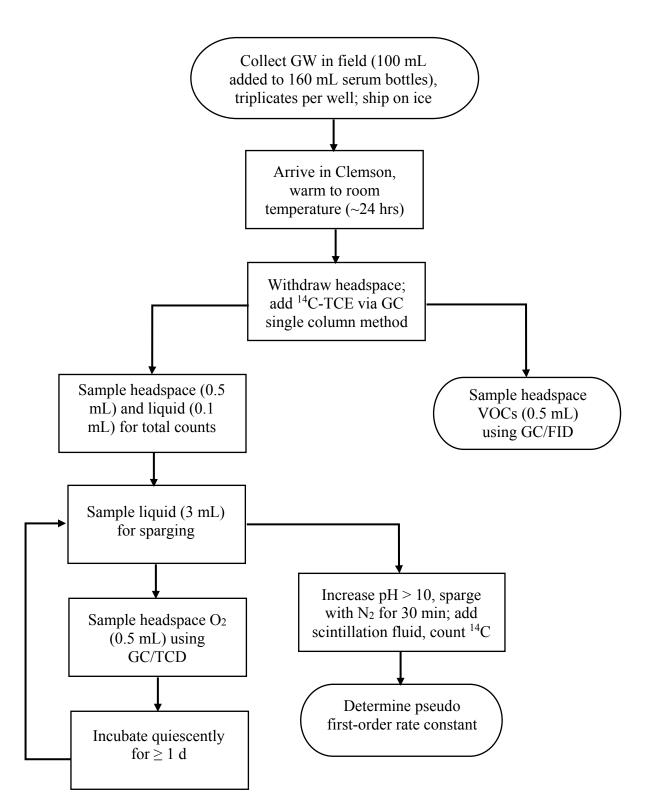
An overview of how the assay was performed is provided in Section 5.1.4.1. The following sections provide the details.

#### 5.1.4.1 <sup>14</sup>C addition and time zero monitoring, sparging, direct counts, and O<sub>2</sub> monitoring

The <sup>14</sup>C-TCE stock solution was added to groundwater samples and control bottles using the single column method described in section 3.1.2. Prior to addition of the <sup>14</sup>C-TCE, the mass of bottles was recorded (balance precision,  $\pm$  0.01 g), in order to keep track of the amount of water in the bottles. Before adding the <sup>14</sup>C-TCE stock solution, approximately 50 mL of headspace was withdrawn from each bottle using a 100-mL gas-tight syringe (SGE Analytical Science, removable Luer Lock) to ensure the bottles were not over-pressurized. After withdrawing air from the headspace, the bottles were immediately inverted to reduce gas diffusion through the punctured Teflon-faced septa. The single column method for purifying the <sup>14</sup>C-TCE stock solution was used. During the predetermined interval when TCE eluted from the column (9.6-11.1 min), the GC gas was injected into a serum bottle. Following injection of the <sup>14</sup>C-TCE, the bottles were inverted and placed on an orbital shaker table (98 ± 2 RPM) for approximately 1 h. Agitating the liquid phase facilitated establishment of equilibrium between TCE in the headspace and liquid phases.

The total amount of TCE present in the bottles was determined by injection of a headspace sample (0.5 mL, taken with a 1.0 mL gas-tight syringe, Valco® Series A-2) onto a GC (HP 5890 Series II) equipped with a a stainless-steel column packed with 1 % SP-1000 on 60/80 Carbopack B (Supelco) and a flame ionization detector (FID). The temperature program was 60 °C for 2 min, increase at 20 °C per min to 150 °C, increase at 10 °C to 200 °C and hold for 28.5 min. GC/FID analysis also permitted detection of other VOCs in the groundwater samples.

Time zero monitoring for <sup>14</sup>C products was conducted after each bottle was injected with <sup>14</sup>C-TCE using the single column GC method and headspace checks for VOCs were completed using the GC/FID. The bottles were processed at the same time following addition of <sup>14</sup>C-TCE. The sampling procedure is outlined in Figure 5.1.1 and details are provided below. The sampling schedule and monitoring included the following sequence of events: 1) direct headspace and liquid counts; 2) sparging test; and/or 3) O<sub>2</sub> headspace monitoring (groundwater bottles only). After each sampling event, the bottles were incubated quiescently in the dark at ambient room temperature ( $22 \pm 2$  °C).



# Figure 5.1.1. Overview of the Methodology Used for Experimental Wells, Including from TCAAP, Plattsburgh, Hopewell, Tooele, and Hill.

Deviations from the steps listed were made for different experiments or treatments.

Direct counts were made to quantify the total amount of radioactive material in each bottle. The headspace sample (0.5 mL gas) was removed using a gas-tight syringe (Valco® Series A-2). The liquid sample (0.1 mL) was removed using a 1.0 mL liquid syringe (Valco® Series C). The samples were injected immediately into a 20 mL borosilicate glass scintillation vial (Fisherbrand<sup>TM</sup>) containing 15 mL of liquid scintillation cocktail (LSC). A hole (2.38 mm) was drilled in the polypropylene cap and a Teflon-faced gray butyl rubber septa was placed inside the cap. Inecting the samples through the septum minimized any losses of <sup>14</sup>C due to volatilization. The following equation was used to determine the total amount of <sup>14</sup>C present per bottle:

$$C_{tot,l,m} = \frac{S_{h,l}}{V_{h,s}} \cdot V_{h,b} + \frac{S_{l,l}}{V_{l,s}} \cdot V_{l,b}$$

$$(5.1)$$

where  $C_{tot,i,m}$  = total measured dpm in a serum bottle;  $S_{h,i}$  = dpm in a headspace sample;  $V_{h,s}$  = volume of headspace sample (0.5 mL);  $V_{l,b}$  = volume of headspace in a serum bottle (60 mL);  $S_{l,i}$  = dpm in liquid sample;  $V_{l,s}$  = volume of liquid sample (0.1 mL); and  $V_{l,b}$  = volume of liquid in a serum bottle (100 mL).

The sparging test was conducted to determine the accumulation of <sup>14</sup>C products. Prior to removing liquid, 3 mL of room air was injected into the serum bottle using a 5 mL syringe (Valco® Series C). The liquid sample was immediately withdrawn and injected into a 20 mL borosilicate glass scintillation vial. Approximately 12 µL of 8 M NaOH was added to the 3 mL liquid sample using a 100 µL liquid syringe (Valco® Series C) to raise the pH above 10.5. The pH of the sample was confirmed qualitatively using a pH strip (BDH® VWR Analytical, pH 7.0-14.0, gradation of 0.5 units). The purpose of raising the pH above 10.5 was to ensure the retention of <sup>14</sup>CO<sub>2</sub> in the aqueous phase as carbonate. The alkaline sample was sparged with N<sub>2</sub> gas (Airgas®) at a flow rate of 550±50 mL/min for approximately 30 min. The flow rate was controlled using air flow meters (Cole-Parmer, 1.4 LPM) connected to latex rubber tubing that terminated in a sterile, disposable needle (BD PrecisionGlide<sup>™</sup>, 22 G x 1 <sup>1</sup>/<sub>2</sub> in.). The vials were tilted on a 30-degree angle to facilitate better contact between the N<sub>2</sub> and liquid. The purpose of sparging was to remove VOCs, principally <sup>14</sup>C-TCE, so that any radioactivity remaining in the vial would be attributable to product formation and not residual <sup>14</sup>C-TCE. Following the sparging, 15 mL of LSC was added to the vials, which were then incubated quiescently in the dark for approximately 24 h before counting the beta radiation.

In order to prevent oxygen from becoming a limiting factor for co-oxidation of TCE, the concentration was measured in 0.5 mL samples using a GC equipped with a thermal conductivity detector (TCD) and a stainless-steel column packed with 100/120 Carbosieve S-II support (Supelco). The flow rate was approximately  $50.5 \pm 0.2$  mL/min with N<sub>2</sub> gas as the carrier and reference gas. An isothermal temperature program (105 °C, 4 min) was used. O<sub>2</sub> eluted at 3.3 min. Room air (21% O<sub>2</sub>) was used for calibration. After 40 to 46 days of incubation, the average O<sub>2</sub> level in the groundwater bottles was 12.0±0.28%; the lowest level observed was 7.50 %. This was considered adequate to avoid any limitation on co-oxidation, so that none of the experimental groundwater bottles received additional O<sub>2</sub>.

#### 5.1.4.2 Monitoring and <sup>14</sup>C product distribution

The groundwater samples and control bottles were monitored for a period of 40 to 46 d using the sequence of sampling events described in Figure 5.1.1, including direct headspace and liquid counts for total <sup>14</sup>C activity, sparging samples at alkaline pH to determine <sup>14</sup>C product accumulation, and O<sub>2</sub> headspace monitoring. Samples were analyzed most frequently over the first week of incubation.

On the last day that bottles were incubated, they were evaluated for routine parameters, along with a final analysis of VOCs in the headspace using the GC/FID method. Following the alkaline sparging test, an acidic sparging test (pH < 4) was used to determine the percentage of <sup>14</sup>CO<sub>2</sub> in the <sup>14</sup>C products. The difference between the radioactivity remaining after alkaline sparging and acidic sparging tests was presumptively <sup>14</sup>CO<sub>2</sub>. The acidic sparging test was also performed with a 3 mL liquid sample that was added to a 20 mL glass scintillation vial; 12  $\mu$ L of 6 M HCl was added decrease the pH below 4. The pH was confirmed using pH strips (BDH® VWR Analytical, pH 0-6.0, gradation of 0.5 units). The acidified sample was sparged with N<sub>2</sub> (550 ± 50 mL/min) for approximately 30 min using the same sparging apparatus described above. After sparging, 15 mL of LSC was added, the vials were incubated quiescently in the dark for approximately 24 h, followed by counting of the beta radiation.

For groundwater samples that exhibited a statistically signicant rate of <sup>14</sup>C product accumulation. additional confirmation of <sup>14</sup>CO<sub>2</sub> was obtained by precipitation of the alkaline sparge water with barium. To do so, a larger liquid sample was used (10 mL). The sample was added into a 15 mL sterile, polypropylene centrifuge tube (VWR®). Approximately 50 µL of 8 M NaOH was injected to raise the pH above 10.5; the pH was checked using a pH strip. The samples were sparged with N<sub>2</sub> (550±50 mL/min) for approximately 30 min using the sparging apparatus described above. After 30 min, 3 mL of the alkaline solution was withdrawn from the 15 mL centrifuge tube and added to a 15 mL of LSC; this replicated the analysis performed with only a 3 mL liquid sample. Next, approximately 1.35 g of Ba(OH)2·8H2O (Alfa Aesar, CAS: 12230-71-6) was added to the remaining 7 mL of the sparged, alkaline liquid in the centrifuge tubes and vigorously mixed using a constant speed vortex mixer. The tubes were then centrifuged for 20 min (2,700 rpm). An aliquot of the centrate (2 mL) was withdrawn from the alkaline samples and added to 15 mL of LSC. The LSC vials were incubated quiescently in the dark for approximately 24 h before counting beta radiation. The centrate remaining in the centrifuge tubes was presumed to contain <sup>14</sup>C products other than <sup>14</sup>CO<sub>2</sub>, since <sup>14</sup>CO<sub>2</sub> formed a barium carbonate precipitate. The soluble products are hereafter referred to as nonstrippable residue (NSR); the composition of the NSR was not investigated any further.

#### 5.1.4.3 Determination of pseudo first-order decay constants (k)

#### <u><sup>14</sup></u>C Measured Data

It was necessary to relate the <sup>14</sup>C products measured in the 3 mL sparged samples (*Ss,i*) to the total amount of <sup>14</sup>C products accumulated in a serum bottle (*Ssb,i*). This was accomplished by finding the product of the 3 mL liquid sparge counts (*Ss,i*) and the volume per sparge sample ( $V_{s,r}$  or 3.0 mL) over the total liquid volume in the bottle ( $V_{l,i}$ ) for that time interval:

$$S_{sb,t} = \left(S_{s,t}\right) \left(\frac{V_{s,t}}{V_{l,t}}\right)$$
(5.2)

 $V_{l,i}$  was determined by using the initial, measured volume of the liquid (i.e., through gravitmetric analysis) and subtracting 3.1 mL for each time interval.

#### Introduction to the Model:

Pseudo first-order rate constants (k) were determined by fitting measured <sup>14</sup>C product accumulation data (equation 2) to the summation of the following equation:

$$\Delta_{i} = C_{li-1,a} - C_{li-1,a} (e^{-k\Delta t})$$
<sup>(5.3)</sup>

(5.3)

where  $\Delta_i$  = the increase in <sup>14</sup>C products over the *i*<sup>th</sup> interval between sampling events (*i* = 0 to 8 or 9, representing the number of sampling events);  $C_{l,i,a}$  = concentration of <sup>14</sup>C products in the aqueous phase after removing the liquid and headspace samples, i.e., the beginning of the *i*<sup>th</sup> interval; and  $\Delta t$  is the time between sampling events. It was assumed that  $\Delta_i$  was zero at *i*=0 (i.e., there was no accumulation of <sup>14</sup>C products at time zero). Therefore, equation 5.3 only applies to the time intervals greater than *i* = 0.

The value for k was determined using MATLAB by minimizing the sum of squared errors between the prediction and the <sup>14</sup>C product data over time. Triplicate bottles were fit simultaneously to obtain a single value for k (i.e., as opposed to determining a k for each bottle and then taking the average).

Calculations were performed in two stages, with the first stage corresponding to the initial conditions and the second stage to all subsequent data points. Figure 5.1.2 provides an overview of the procedure used for several time intervals. The following sections describe the different stages of the model and the corresponding equations for each stage.

#### <u><sup>14</sup>C Calculations for Time Zero</u>

Prior to determining  $\Delta_i$ , the initial conditions for the model were established using measured data. The initial liquid concentration of <sup>14</sup>C-TCE in the bottles before sampling ( $C_{l,i,b}$ ) was calculated based on the total <sup>14</sup>C-TCE present and Henry's Law constant:

$$C_{l,t,b} = C_{tot,t,m} \left( \frac{V_{l,t}}{V_{l,t} + V_{g,t}H_c} \right)$$
(5.4)

where  $C_{tot,i,m}$  = total dpm in the bottle (determined using equation 5.1);  $V_{l,i}$  = the initial volume of liquid in the bottle (~100 mL at i = 0);  $V_{g,i}$  is initial gas volume (~60 mL at i = 0); and  $H_c$  is the dimensionless Henry's Law constant for TCE (0.349 at 23 °C; Gossett, 1987). Equation 5.4 corresponds to point 1 on Figure 5.1.2.

The amount of <sup>14</sup>C removed due to withdrawal of the liquid at time zero ( $S_{l,r}$ ) was calculated as follows:

$$S_{l,r} = C_{l,t,b} \left( \frac{V_{l,r}}{V_{l,t}} \right)$$
(5.5)

where  $V_{l,r}$  = volume of liquid sample removed (3.1 mL = 3.0 mL for the sparging test + 0.1 mL for direct addition to LSC).

<sup>14</sup>C was also removed during gas sampling. For the groundwater bottles, gas samples were removed to determine the total <sup>14</sup>C in the headspace and to measure  $O_2$ . The amount of <sup>14</sup>C removed in these samples ( $S_{g,r}$ ) was calculated as follows:

$$S_{g,r} = \left(C_{tot,t,m} - C_{l,t,b}\right) \left(\frac{V_{g,r}(0.5)}{V_{g,t}} + \frac{V_{g,r}(0.5)}{V_{g,t} + V_{l,r}}\right)$$
(5.6)

where  $V_{g,r}$  = total volume of gas removed at a sampling event (1.0 mL); and  $V_{g,i}$  = total volume of gas in the bottle at the time step.

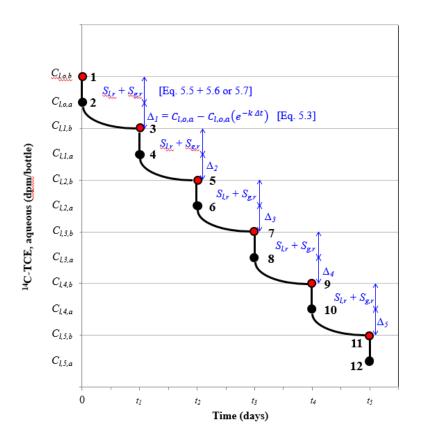


Figure 5.1.2. General Overview of Sampling Events and Respective Equations Used to Generate First-order Rate Constants with the MATLAB Model.

The red cirlces indicate the  ${}^{14}C$  in the aqueous before sampling and the black circles indicate the  ${}^{14}C$  in the aqueous phase after sampling.

For the DDI water controls and FSGW controls, only one headspace sample was removed per sampling event, to determine the total <sup>14</sup>C in the headspace; it was not necessary to measure  $O_2$  in these bottles. Consequently, the amount of <sup>14</sup>C removed in the gas phase of the controls simplified to:

$$S_{g,r} = (C_{tot,t,m} - C_{l,t,b}) \left( \frac{V_{g,r}(0.5)}{V_{g,t}} \right)$$
(5.7)

The total <sup>14</sup>C removed during each sampling event ( $S_{tot,r}$ ) was:

$$S_{tot,r} = S_{lx} + S_{g,r} \tag{5.8}$$

Equation 5.8 was used to determine the vertical line from point 1 to 2 in Figure 5.1.2.

The calculated <sup>14</sup>C-TCE concentration in the bottle after the initial sampling event ( $C_{tot,i}$ ) was:

$$C_{tot,t} = (C_{tot,t,m}) \cdot (S_{tot,r})$$
(5.9)

Therefore, the <sup>14</sup>C-TCE liquid concentration in the bottle after the initial sampling event ( $C_{l,i,a}$ ) was the product of  $C_{tot,i}$  and the percent of TCE in the aqueous phase:

$$C_{l,t,a} = C_{tot,t} \left( \frac{V_{l,t} - V_{l,r}}{(V_{l,t} - V_{l,r}) + (V_{tot} - (V_{l,t} - V_{l,r})) \times H_{c}} \right)$$
(5.10)

where  $V_{tot}$  = total volume of the serum bottles (160 mL). Equation 5.10 corresponds to point 2 in Figure 5.1.2.

For the initial conditions, it was assumed that no <sup>14</sup>C degradation products had formed. Therefore,  $\Delta_i$  was set to zero for the time zero measurements because the initial point was not dependent on *k*, rather it was determined from the measured direct liquid and headspace counts.

#### <sup>14</sup>C Calculations for Conditions Following Time Zero

For all samples taken after time zero, the quantity of <sup>14</sup>C products that accumulated was measured based on processing of the 3 mL aqueous samples. The amount of <sup>14</sup>C removed from a bottle as a consequence of sampling was calculated. The increase in <sup>14</sup>C products formed during incubation between sampling points ( $\Delta_i$ ) was calculated by evaluating first-order degradation reaction kinetics using the value for the previous <sup>14</sup>C-TCE concentration in the aqueous phase ( $C_{l,i-1,a}$ ) and the pseudo first-order rate constant (k):

$$\Delta_t = C_{l,t-1,a} \left( 1 - e^{-k(t_t - t_{t-1})} \right) \tag{5.11}$$

where  $i \ge 1$ . Equation 5.11 represents the curved path from points 2 to 3, 4 to 5, 6 to 7, 8 to 9, and 10 to 11 in Figure 5.1.2. The accumulated <sup>14</sup>C products in the bottle was calculated as the sum of the products formed during incubation between sampling events ( $\Delta_i$ ) and the previous summation of the products ( $\sum \Delta_{i-1}$ ):

$$\Sigma \Delta_{t} = \Delta_{t} + \Sigma \Delta_{t-1} \tag{5.12}$$

The resulting accumulated <sup>14</sup>C products in the bottle determined from the model was compared to the experimental data using squared differences. In addition,  $\Delta_i$  (equation 5.11) was used to determine the concentration of <sup>14</sup>C-TCE in the liquid phase ( $C_{l,i,b}$ ):

$$C_{l,t,p} = C_{l,t-1,a} - \Delta_{t,p} \tag{5.13}$$

Equation 5.13 corresponds to points 3, 5, 7, 9 and 11 in Figure 5.1.2.

The result from equation 5.13 was used to determine the amount of dpm removed from the liquid and gas during sampling events. The dpm removed in the liquid is the same as equation 5.5 for time zero. The dpm removed from the gas in the experimental bottles was a modified version of equation 5.6:

$$S_{g,r} = (C_{tot,l-1} - C_{l,l,b}) \left( \frac{V_{g,r}(0.5)}{V_{g,l}} + \frac{V_{g,r}(0.5)}{V_{g,l} + V_{l,r}} \right)$$
(5.14)

Additionally, the dpm removed from the gas in the DDI and FSGW control bottles was a modified version of equation 5.7:

$$S_{g,r} = (C_{tot,t-1} - C_{l,t,b}) \left( \frac{V_{g,r}(0.5)}{V_{g,t}} \right)$$
(5.15)

The total dpm removed was the same as shown in equation 5.8. The removal of the total dpm corresponds to the vertical lines between points 3 to 4, 5 to 6, 7 to 8, 9 to 10, and 11 to 12 in Figure 5.1.2.

Once the total dpm removed was known, the final, total calculated <sup>14</sup>C-TCE liquid concentration in a bottle after sampling ( $C_{tot,i}$ ) was determined:

$$C_{tot,t} = C_{tot,t-1} - S_{tot,r} - \Delta_t \tag{5.16}$$

 $C_{tot,i}$  combines the headspace and liquid TCE concentrations, so it must be appropriately distributed between the headspace and liquid to find  $C_{l,i,a}$  using the percent in the aqueous phase, similar to equation 5.10:

$$C_{l,t,a} = C_{tot,t} \left( \frac{V_{l,t} - V_{l,r}}{(V_{l,t} - V_{l,r}) + (V_{tot} - (V_{l,t} - V_{l,r})) \times H_c} \right)$$
(5.17)

Equation 5.17 was used to determine points 4, 6, 8, 10, and 12 in Figure 5.1.2.

#### Model Fitting

In the MATLAB script, the valve of k was iterated using equation 5.11 to 5.17 until a minimum valve was obtained for the sums of squares of error determined as the squared difference between the experimental  $(S_{sb.i})$  and estimated <sup>14</sup>C product  $(\sum \Delta_{i-1})$  values.

The MATLAB function used for the iterative approach was *lsqcurvefit*, which is a nonlinear curvefitting solver function that uses the trust-region-reflective algorithm. The 95% confidence intervals were determined using the *nlparci* MATLAB function with the Jacobian matrix and residual vector determined from *lsqcurvefit*. The full MATLAB script can be found in Appendix D.

#### 5.1.4.4 Liquid scintillation counter

Beta radiation was quantified using a Wallac 1220 Quantulus (PerkinElmer, Inc.) liquid scintillation counter. The counter was connected to a desktop computer equipped with proprietary WinQ software (PerkinElmer, Inc.). The <sup>14</sup>C (high energy beta) configuration was used in the WinQ program to count the <sup>14</sup>C samples, with modifications. Windows 1 and 2 (used to detect beta radiation) in the program were modified and expanded from the default sizes of 50-650 and 70-500 to 5-700 and 1-700, respectively, to capture the entire range of beta radiation emission. The samples were counted for 15 min and the external standard quench parameter (SQP) was used for quench correction. The quench efficiency curve for the counting protocol was determined using prepared <sup>14</sup>C standards (Beckman Instruments Inc., quenched carbon-14 standards set) with a counting time of 15 min. The quenching curve data (Appendix D) follows the following parabolic equation:

$$-4.25 \times 10^{-4} x^{2} + 8.06 \times 10^{-1} x - 2.92 \times 10^{2}$$
(5.18)

where x is the measured SQP value. The efficiency values were determined using the measured counts per min (*cpm<sub>measured</sub>*) from the <sup>14</sup>C standards over the known dpm (*dpm<sub>known</sub>*) values of the standards:

$$Efficiency = \left(\frac{cpm_{measured}}{dpm_{knewn}}\right) \times 100\%$$
(5.19)

<sup>14</sup>C samples were incubated for different time periods prior to counting. Direct headspace and liquid samples were counted within 3 h of the sampling event. The sparged samples were incubated, quiescently in the dark for approximately 24 h before counting. The long incubation time for the sparged samples reduced chemilumenscence arising from the high pH of the 3 mL of groundwater mixed with the LSC.

#### 5.1.5 Task 5 - Laboratory Work to Implement Enzyme Activity Probes and the qPCR Assays for Oxygenase Enzymes that can Co-Oxidize TCE

PNNL assayed water samples for the density of bacteria that react to one of three Enzyme Activity Probes. The probes determine if the bacteria express an oxygenase enzyme that can carry out aerobic co-oxidation of PCE or TCE. PNNL also used qPCR to assay water samples for the abundance of gene copies for selected oxygenase enzymes. PNNL assayed water from the same wells that were sampled for Task 4. This allowed a statistical comparison of the abundance of cells that respond to an enzyme activity probe, or gene copies of oxygenase enzymes, to the directly measured rate of aerobic biodegradation.

#### Aromatic Oxygenase Activity

Groundwater was vacuum filtered onto 0.22 µm, 25 mm diameter, black, polycarbonate filters.

Samples were then exposed to 5 mM of an enzyme activity-dependent probe (phenylacetylene, *trans*-cinnamonitrile, 3-hydroxyphenylacetylene) for 10 minutes. Table 2.2.1 presents the list of the enzymes targeted by individual EAPs. Filters were mounted on a glass microscope slide with non-fluorescent immersion oil and a cover slip, and examined for fluorescent cells by epifluorescent microscopy. Triplicate slides, and a minimum of 20 random fields on each slide were counted for each sample and each EAP. A suite of aromatic oxygenase-containing bacteria, including *Pseudomonas putida* F1, were used as a positive control to verify EAP signal.

#### SMMO Enzyme Activity

To monitor for the presence of soluble methane monooxygenase, whole water (unaltered) groundwater samples were filtered onto 25mm Supor filters, and placed into separate glass Petri plates. One-mL of 5mM coumarin solution in phosphate buffer was pipetted onto each filter, and incubated for 10 minutes at room temperature. Following the incubation, phosphate buffer was used to wash the product from each filter. Solution fluorescence was determined (excitation wavelength 338 nm, emission wavelength 450 nm) using a fluorescence spectrophotometer, with a quartz cuvette of 1 cm path length. Fluorescent scans were performed in triplicate for each of the samples. *Methylosinus trichosporium* OB3b was used as a positive control to verify the signal from coumarin.

#### DNA Extraction and PCR amplification

Approximately one liter of groundwater was filtered and then DNA was isolated from cells trapped on filters. DNA extraction was performed using both FastDNA and the MoBio Soil DNA kit as described by the manufacturers; two kits were used to ensure that biases associated with one kit or another did not provide a false positive for the presence of the gene of interest. DNA yield from the experiments was determined using a Bioanalyzer and quantification using Picogreen assays.

PCR amplification reactions were performed in 50  $\mu$ L (total volume) reaction mixtures in 0.2 mL thin-walled tubes using a DNA thermocycler. All qPCR assays were performed using a Bio-Rad CFX96 Real-Time PCR Detection System (Bio-Rad Laboratories, Hercules, CA). A SsoAdvanced SYBR Green supermix kit (Bio-Rad Laboratories, Hercules, CA) was used for amplification and real-time fluorescence measurement. Following amplification, qPCR product size was confirmed using a DNA 1000 Chip Kit, which was run on a 2100 Bioanalyzer. The PCR conditions for the toluene oxygenase primers was modified from Baldwin et al. (2003), using a large number of target organisms. The PCR primers that were used during a first round of testing are designated: RMO-F/R, which amplify the toluene-3 and -4-monooxygenase genes, TOD-F/R which amplifies the toluene 2,3-dioxygenase gene, and PHE-F/R which amplifies the toluene-2, -3, -4-monooxygenase genes (Baldwin et al., 2003). The sMMO enzyme was targeted using the mmoX primer pair (McDonald et al., 1995). Depending on results from the first round, other enzymes such as catechol 2,3-dioxygenase, alkane monooxygenase, and particulate methane monooxygenase were also targeted.

# Comparison of EAP and qPCR Targets

The relationship between the EAPs and the qPCR analyses are shown in Table 2.2.1. Some of the targets for the qPCR analyses do not directly correspond to EAP analyses and were completed in order to target other oxygenase enzymes which are also known to cometabolize contaminants such as chlorinated solvents. While there are dozens of known enzymes, some are

more commonly found in environmental systems and/or are potential targets for remediation strategies such as bioaugmentation or biostimulation (propane, methane, benzene etc.). Table 2.2.1 provides a list of all of the qPCR targets that were used for the current Sites.

#### 5.1.6 Task 6 – Analyze Data, Validate Cost and Performance Data, and Prepare Final Report

This task represents what is presented in this report, which details the findings of the work described in the Demonstration Plan (ESTCP, 2016). The contribution of abiotic degradation and aerobic biodegradation at each site is evaluated herein. This is accomplished by comparing the rate constant for attenuation associated with abiotic degradation by magnetite in the aquifer matrix and the rate constant associated with aerobic co-oxidation to the bulk rate constant for natural attenuation at the site. If the rates of abiotic degradation by magnetite or the rates of aerobic biodegradation can meet the goals for MNA, this has the potential to save the DOD significant amounts of money in unnecessary remediation costs.

Project ER-201129 showed the relationship between magnetic susceptibility and degradation rate using magnetic susceptibility data from soil core samples. The material presented in this report shows that a relatively inexpensive downhole probe can be used for measurement of magnetic susceptibility in lieu of using soil core samples, the acquisition of which can be quite expensive at sites where intrusive site characterization activities have already been completed. This has the potential to save the DOD significant amounts of money in unnecessary drilling costs.

This report also evaluates the utility of Enzyme Activity Probes and qPCR assays by comparing the rate constant for aerobic co-oxidation to the abundance of cells that react with EAPs or the abundance of genes copies for oxygenase enzymes. To allow extrapolation of this approach to other sites, this report provides protocols for collecting and analyzing magnetic susceptibility data, how to perform the <sup>14</sup>C-TCE assay and the Enzyme Activity Probe assay, and the procedures to submit samples for qPCR evaluation.

Cost and performance data are provided for down-hole determination of magnetic susceptibility, for the Enzyme Activity Probes, for the qPCR assays, and for the direct assay of the rate constant for aerobic biodegradation. Cost and performance data are validated to determine if the performance objectives established in Section 3 have been met.

# 5.1.7 Task 7 – Project Management

This task was used for project management and project communication, and is a fairly common task.

# BASELINE CHARACTERIZATION

Section 4 provides an in-depth discussion for the majority of baseline characterization activities. Baseline characterization was conducted for magnetic susceptibility using borehole core samples and fixed-base laboratory analyses at all of the sites discussed in Section 4 except Hill AFB OU-10. The results of baseline sampling for magnetic susceptibility using core samples and fixed-base laboratory analyses are summarized in Table 4.1.2, and discussed in Section 4. Previous baseline characterization for EAP was completed for Hill AFB OU-10 and for the Hopewell Precision Site prior to the field work conducted under this effort, as described in Section 4. For Hill AFB, qPCR analyses were also performed. For the other sites, baseline for EAP and qPCR was established during this demonstration. No direct correlation between quantification of oxygenase enzymes to TCE transformation rates was performed prior to this work, so a baseline for this comparison is provided in this report.

The only additional baseline characterization that was required for this demonstration was development of the <sup>14</sup>C-TCE assay. Since the <sup>14</sup>C-TCE assay had not previously been deployed for the purposes proposed in this study, it was not possible to precisely define baseline activities. However, as described in Section 3.2.2.2, a preliminary evaluation was performed with locally sourced water from a seep that presumptively contained a high level of dissolved organic matter. It was anticipated that the naturally occurring organics included aromatic compounds that would support the induction of oxygenases. A net rate coefficient of  $2.37 \times 10^{-2} \pm 1.67 \times 10^{-2}$  yr<sup>-1</sup> was determined, which gives a half-life of 29 yr (95% confidence interval = 17-99 yr). This result suggested that the <sup>14</sup>C assay is adequately sensitive to detect TCE co-oxidation in groundwater samples at rates that are meaningful for evaluating natural attenuation.

The waste generated from this part of the project is mixed waste due to the presence of TCE and <sup>14</sup>C. However, the level of <sup>14</sup>C activity is sufficiently low that disposal as a hazard waste is acceptable. All procedures required by Clemson University for disposal of liquid hazardous waste were followed.

# 5.2 TREATABILITY OR LABORATORY STUDY RESULTS

# 5.2.1 Treatability or Laboratory Studies Performed by Clemson

The use of <sup>14</sup>C-labeled compounds to determine the rate at which a parent compound degrades, as well as the identity of the products formed, has been in practice for decades. This includes the fate of <sup>14</sup>C-TCE and other chlorinated organic contaminants. The Freedman laboratory has extensive experience in the use of <sup>14</sup>C-labeled compounds. For example, Darlington et al. (2008, 2013) evaluated biotic and abiotic degradation of <sup>14</sup>C-TCE and <sup>14</sup>C-cDCE in groundwater plus crushed sandstone from a site in California. Shan et al. (2010) used <sup>14</sup>C-labeled carbon tetrachloride and chloroform to evaluate biostimulation and bioaugmentation for in situ treatment of groundwater at a different site in California. Fullerton et al. (2013) synthesized <sup>14</sup>C-labeled ethene by supplying <sup>14</sup>C-*c*DCE to a halorespiring culture enriched in *Dehalococcoides*. The <sup>14</sup>C-ethene was then used to evaluate anaerobic oxidation of ethene under sulfate reducing conditions.

Although there is an extensive collection of literature on experiments with <sup>14</sup>C-labeled environmental contaminants, it is noteworthy that the frequency of using <sup>14</sup>C has diminished over the last decade or so. As a consequence, many <sup>14</sup>C-labeled compounds such as TCE are no longer commercially available as a stock item. Custom systems is required to obtain the compound, including the <sup>14</sup>C-TCE used for this project.

The most common way for vendors to deliver <sup>14</sup>C-labeled compounds is dissolved in a solvent. For this project, the <sup>14</sup>C-TCE was purchased from Moravek Biochemicals dissolved in acetonitrile. This necessitated separating the TCE from the solvent. The same GC approach described in previous research (Darlington et al., 2008, 2013) was used; this also resulted in an increase in the purity of the <sup>14</sup>C-TCE added to groundwater samples.

An important feature of the assay developed for this project in comparison to past work is that water samples were repeatedly removed from the same serum bottles over time, in order to measure the accumulation of <sup>14</sup>C-products. The size of the aqueous samples (3.1 mL) was large enough so that it became necessary to take into account the <sup>14</sup>C activity removed with each sample. Consequently, a mass balance model was needed in order to account for both the <sup>14</sup>C products that accumulated and the <sup>14</sup>C removed during sampling. Fitting of the <sup>14</sup>C product data to the mass balance model permitted determination of the pseudo first order rate coefficient. In the previous studies, the distribution of <sup>14</sup>C was determined using the entire contents of a serum bottle. As such, in order to determine a rate, it was necessary to sacrifice replicate bottles over time. This was not feasible for the current project, due to the large number of bottles that would have needed to be prepared. This led to development of an assay that allowed for repeat sampling from the same bottle.

#### 5.2.2 Treatability or Laboratory Studies Performed by PNNL

A suite of EAPs was designed that permitted the determination of specific aerobic cometabolism of chlorinated ethylenes, most notably TCE. EAPs that serve as alternate substrates for TCE cometabolizing enzymes have been developed for four separate aromatic oxygenases (Keener et al., 1998; 2001; Miller et al., 2001; Clingenpeel et al., 2005), and for the soluble methane monooxygenase (SMMO; Miller et al., 2001). Specific EAP and the targeted co-metabolic enzymes are shown in Table 5.3.1. These non-fluorescent probes are transformed by the enzymes into a quantifiable fluorescent signal upon transformation, thus providing direct evidence of cometabolic enzyme activity. Enzyme probes have been evaluated at a number of DOE (9), DOD (16), EPA (5) and industrial sites (9) over the last ten years (Lee et al., 2005; Lee et al., 2007; Wymore et al., 2007). Based on these analyses of groundwater with TCE concentrations ranging from <100  $\mu$ g/L to >10,000  $\mu$ g/L, it appears that enzyme probes provide a direct estimate of aerobic cometabolic enzyme activity for subsurface populations.

Application of EAP's at contaminated sites has provided valuable information regarding the presence and activity of in situ microbial enzyme systems important for aerobic cometabolism for plume-wide assessment of intrinsic assessment of degradation.

Probe	Pathway
3-hydroxyphenylacetylene	toluene-2-monooxygenase
(3HPA)	toluene-3-monooxygenase
	toluene-2,3-dioxygenase
Phenylacetylene (PA)	toluene-2,3-dioxygenase
	toluene-3-monooxygenase
	toluene-2-monooxygenase
trans-cinnamonitrile (CINN)	toluene-2,3-dioxygenase
Coumarin, naphthalene	Soluble methane monooxygenase

Table 5.2.1. EAP and Targeted Oxygenase(s)/Pathway

Two recent examples where EAP, and combined EAP/qPCR for one, was applied, led to an additional line of evidence for natural attenuation that was accepted by regulators and include in the final records of decision (ROD) for the sites (Lee and Lee 2012). At Travis Air Force Base, wells within TCE plumes and control wells outside of these locations were analyzed using EAP and qPCR.

Results from these analyses indicated that there were communities with oxygenase enzymes that were active and when coupled with receding contaminant plumes, indicated an additional line of evidence for natural attenuation.

At an industrial site, groundwater samples (14) from the Wichita Northern Industrial Corridor (NIC) were assayed using enzyme activity probes (Lee et al. 2016). Samples were filtered and EAP for aromatic oxygenase enzymes (phenylacetylene, 3-hydroxyphenylacetylene and cinnamonitrile) and one for soluble methane monooxygenase (coumarin) were applied.

Eight of the groundwater samples assayed showed the presence of enzymes that oxidized all three probes to a fluorescent product, while only three showed no significant fluorescence. The remaining three samples showed fluorescence with only one or two aromatic oxygenases. All samples showed some fluorescence when treated with coumarin, but only four showed moderate to high levels of fluorescence. Based on the EAP data, there is evidence that there is potential for significant intrinsic aerobic biodegradation at most locations tested; with eight of the sampling sites showing activities for all three aromatic EAPs under in situ conditions. All samples showed some SMMO activity, while three showed moderate activity and one groundwater sample showed high SMMO activity.

# 5.3 DESIGN AND LAYOUT OF TECHNOLOGY COMPONENTS

This section provides a description of all technology components. Provided is a subsection for each significant technology component describing its design and locations where it was implemented. Sampling locations are presented in Section 4.

#### 5.3.1 Magnetic Susceptibility Sonde

Figure 5.4.1 shows the exterior of the magnetic susceptibility sonde. This figure also includes probe dimensions and operating parameters. As can be seen from this figure, the magnetic susceptibility sonde has a diameter of 45 mm (1.77 inches).

For the HM-453S used in this study, the Tx-Rx spacing (Section 2.2.1) is 25 cm (9.84 inches). This equates to optimal readings being made at roughly 20 cm (~8 inches) from the sonde, with the accuracy of the magnetic susceptibility measurements dropping off beyond this distance. Based on this, boreholes less than about 40 cm (~16 inches) in diameter are optimal for the HM-453S. Magnetic susceptibility readings made in boreholes larger than this will not be as accurate as those made in smaller boreholes.

In addition to borehole diameter, and well construction materials, the magnetic susceptibility sonde is particularly sensitive to temperature. Because of this, the sonde must be lowered into the formation water and allowed to equilibrate for at least 15 minutes prior to calibration and subsequent use.

The sonde reports volume magnetic susceptibility in S.I. units (International System of Units or Système International d'unités). The volume magnetic susceptibility values were converted to mass magnetic susceptibility by dividing by an assumed bulk density for aquifer material. The porosity of the aquifer material was assumed to be 0.35, and the particle density was assumed to be 2,650 kg/m<sup>3</sup>, resulting in an assumed bulk density of 1,700 kg/m<sup>3</sup>. Following these assumptions, the working range of the HM-453S sonde extends from 4.12E-9 m<sup>3</sup>/kg to 4.12E-5 m<sup>3</sup>/kg.

The sonde was recalibrated immediately prior to use in each monitoring well. The sonde was first calibrated against air, which was taken to have a value of 0, and then against a standard that was equivalent to a magnetic susceptibility of 2.94E-6 m<sup>3</sup>/kg. The standard was contained in a holder that positioned the standard at a fixed location alongside the sonde. The response of the sonde was adjusted to match the value of the standard. The holder containing the standard was removed and the sonde was introduced into either 5.1 cm (2 inch) and 10.2 cm (4 inch) inner diameter polyvinyl chloride (PVC) groundwater monitoring wells using a Mount Sopris Instruments R-4200-1000-200 Mini Winch (Figure 5.4.2). Data from the sonde were recorded using the Mount Sopris Instruments R-5MXA-1000 Matrix Console (Figure 5.4.2). The sonde is capable of taking measurements when it is being lowered into, or raised from, a monitoring well. The sonde was lowered into, or raised from, monitoring wells at a rate of about 9 feet per minute, and magnetic susceptibility measurements were collected about every 1.3 seconds. This equates to about 8.7 readings being taken for every foot the sonde travels down or up the borehole. The sonde was not centered in the well or intentionally forced against the sidewall as it was introduced into the well. The magnetic susceptibility sonde was found to fit down both 2-inch (50.8 mm) and 4-inch (101.6 mm) PVC monitoring wells. However, if a 2-inch PVC monitoring well was compromised, such as with uneven joints or casing that was not sufficiently straight, then it was problematic to get this sonde into the well.

The sonde will interact with steel or iron used in the construction of the well and cause erroneous readings. Magnetic susceptibility measurements using a sonde can be successfully made in uncased wells or in cased wells constructed entirely of PVC or other materials containing no steel or iron. Steel centralizers used to center the well in the borehole can cause local interference with magnetic susceptibility measurements. In addition, any dedicated sampling equipment such as sampling pumps and piping, or Hydrasleeve<sup>®</sup> samplers must be removed prior to magnetic susceptibility sampling.

The components required to collect downhole data using a magnetic susceptibility sonde such as that shown in Figure 5.4.1 include (Figures 5.4.2 and 5.4.3):

- 1) Sonde with coaxial cable.
- 2) Tripod with pulley to guide the wireline cable with the sonde attached down the well.
- 3) Winch.
- 4) Data recorder to record and reduce data.
- 5) WellCAD or similar to analyze and display data.



#### **Probe Parameters**

Diameter	45 mm
Length	125 cm
Weight	4.5 kg
Max. Working Temperature/Pressure	75°C/20 MPa
Min. No. of Cable Conductors	2
Supply Voltage Range	30 – 45 V <sub>DC</sub>
Max./Nominal Current Consumption	100/40 mA <sub>DC</sub>
Supply Voltage Polarity	+ on central cond
	- on probe casing

#### **Measuring Parameters**

Sensor	four coil system
Intercoil Spacing 1. channel	25 cm
Intercoil Spacing 2. channel	30 cm
Operating Frequency	≈2 kHz
Communication (negative pulse)	0-20 000 cps
Measuring range	10 <sup>-5</sup> – 0.5 SI units
	10 <sup>-4</sup> – 2 SI units
Accuracy	< 3% F.S.
Zero Drift	< 2 10 <sup>-5</sup> SL units/1080

Figure 5.4.1

W&R Instruments HMM-453-S Borehole Magnetic Susceptibility Sonde With Dimensions



Date: 10/15/16 Client: ESTCP Revision Number: 0 Drawn By: THW

Figure 5.4.1. W&R Instrument HMM-453-S Borehole Magnetic Susceptibility Sonde With Dimensions



Figure 5.4.2. Data Logger, Winch and Tripod with Pulley for Magnetic Susceptibility Sonde

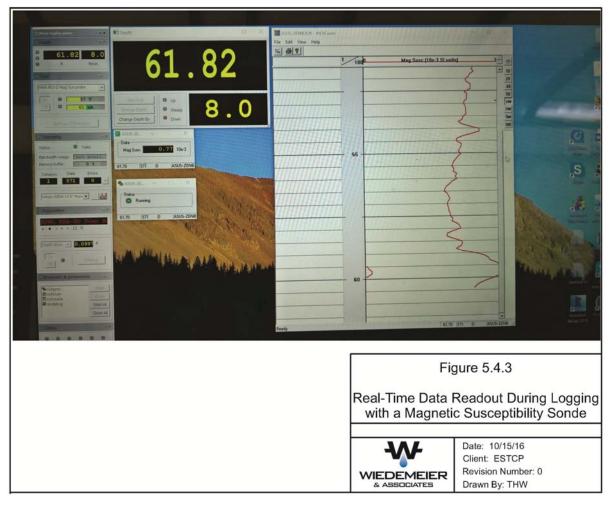


Figure 5.4.3. Real-Time Data Readout During Logging with a Magnetic Susceptibility Sonde

Figure 5.4.2 shows the data logger, winch, and tripod (various configurations) used to lower the magnetic susceptibility sonde into a monitoring well to collect magnetic susceptibility data. The data logger is attached directly to the winch and is then connected to a computer. The tripod and attached pulley are situated over the well and the sonde is slowly lowered, at a rate on the order of 10 feet per minute, into a 2-inch or 4-inch PVC monitoring well using the winch. A 1000- or 2000-watt invertor generator was used to power the winch and data logger assembly. After testing, a 1000-watt invertor generator was found to be sufficient for this configuration, with the sonde being lowered to depths as great as 450 feet below ground surface (bgs). As with any downhole equipment, the magnetic susceptibility sonde was thoroughly decontaminated between each well, as described in Section 5.6.6.

The data from the data logger was reduced using WellCAD, a PC-based composite log package, which combines comprehensive graphic editing mechanisms and data processing tools. It combines display, editing and analysis capabilities for well data, and is used in a wide range of applications. The basic module incorporates all features and tools necessary to import, edit, process, and display monitoring well data acquired using a magnetic susceptibility sonde. After processing with WellCAD, data were exported to Microsoft Excel for final data analysis.

# 5.3.2 Develop a <sup>14</sup>C-Labeled Tracer Procedure to Directly Assay the Rate of TCE Aerobic Biodegradation

Details on development of the <sup>14</sup>C-TCE assay are presented in sections 2.2.2.1; 3.1.2; 3.2.2; 5.1.3; and 5.1.4. The first task was to evaluate an improved method for purifying the <sup>14</sup>C-TCE stock solution, with the goal of minimizing the amount of <sup>14</sup>C impurities added to the serum bottles that accompany the <sup>14</sup>C-TCE. The lower the initial level of impurities, the easier it becomes to detect a statistically significant increase in <sup>14</sup>C products over a relatively short timeframe (e.g., several days). In previous studies (e.g., Darlington et al., 2008, 2013), a single GC column was used for purification. In this study, two columns in series were also evaluated. It turned out that the dual column approach did not yield a statistically significant lower level of impurities. With the single and dual column methods, the target of 0.01% impurities was not met; the initial level of impurities was closer to 0.05% of the total <sup>14</sup>C added to the serum bottles. However, this was compensated for by increasing the duration of the assay, allowing for detection of an increase in <sup>14</sup>C products above the initial level impurities in the bottles. Using this approach, the lowest rate constant measured was 0.00658 yr<sup>-1</sup>, which translates to a half-life of 105 yr. While it may be possible to lower the detection limit of the assay, lower rates would not likely have any practical value from the standpoint of assessing MNA.

The assay involved addition of ~100 mL of groundwater, DDI water, or FSGW to 160 mL serum bottles. Following addition of purified <sup>14</sup>C-TCE, accumulation of <sup>14</sup>C products was measured in 3 mL samples removed eight or nine times, over 40 to 46 days of incubation. The pH of the 3 mL samples was raised above 10 to retain <sup>14</sup>CO<sub>2</sub>, and then the water was sparged for 30 min to remove the residual <sup>14</sup>C-TCE, leaving behind only the <sup>14</sup>C products. An experiment was performed to determine if 30 min of sparging was adequate to remove all of the unreacted TCE. Sparging for 60 min was tested and shown not to further lower the <sup>14</sup>C products left after sparging. Consequently, a 30 min sparging time was used.

In order to determine a first order rate constant, the rate of <sup>14</sup>C product accumulation in groundwater must be greater than the rate of accumulation in sterile controls. Initially, DDI water was used as the negative control. It was subsequently determined that FSGW controls are a better representation of the background level of product formation; these were used to calculate net first order rate constants for eight of the 19 wells evaluated.

Section 5.1.4 specifics how the first order decay rate constant was calculated. A mass balance model that included the first order decay coefficient was fit to the measured amounts of <sup>14</sup>C products formed. The optimum value for the rate coefficient was found by minimizing the sums of squares of error between the measured and predicted amount of <sup>14</sup>C products over time. Details on the methods for counting <sup>14</sup>C activity are provided, as are the methods to quantify and/or detect VOCs by GC/FID and the amount of oxygen present in the headspace by GC/TCD.

When the incubation period was complete (40-46 days), samples were evaluated using both alkaline and acidic sparging. The difference between the two allowed for calculation of the percentage of product in the form of <sup>14</sup>CO<sub>2</sub>. <sup>14</sup>CO<sub>2</sub> was further confirmed by precipitation with barium.

The <sup>14</sup>C assay was validated using locally sourced water from a seep with a high content of organic debris. A statistically significant rate of TCE co-oxidation was observed, confirming the viability of the assay. Additional evidence for the efficacy of the assay was obtained using a propanotrophic enrichment culture that is known to co-oxidize TCE.

The propanotrophic culture was used to evaluate the potential impact of sample storage conditions on the rate of <sup>14</sup>C product accumulation. Storage at 4 °C overnight, followed by warming to room temperature overnight, did moderately reduce the first order reaction rate coefficient when considering the full incubation period (40 d). This suggested that results for the groundwater samples are conservative with respect to in situ conditions. Nevertheless, shipment of groundwater sample to a laboratory that is licensed to handle <sup>14</sup>C is a requirement for the assay, and shipment on ice is recommended to avoid even more significant decreases in co-oxidation activity that may occur if the samples are left at ambient temperature.

#### **5.3.3** Application of EAP and qPCR

Processing of samples using EAP and qPCR was accomplished using the parallel workflow outlined in Figure 5.4.4. Replicate samples, positive/negative controls, matrix spikes and blanks are processed and then results are compared.

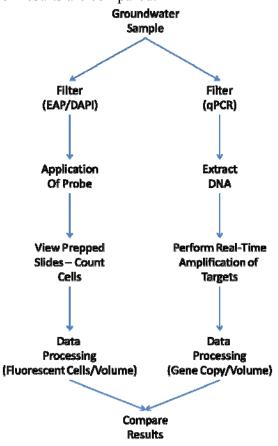


Figure 5.4.4. Schematic of Process for Application of Molecular Biological Tools (EAP and qPCR).

#### 5.4 FIELD TESTING

Field testing consisted of collection of groundwater samples from the wells discussed in Section 4 for the analyses listed in Section 5.6. In addition, a magnetic susceptibility sonde as described in Section 5.4.1 was lowered into the wells identified in Section 4. Magnetic susceptibility versus depth data were collected using the downhole sonde in monitoring wells that were installed in boreholes from which magnetic susceptibility data were collected from soil borehole core data and analyzed in a fixed-base analytical laboratory.

An additional site not described in Section 4 was used for the magnetic susceptibility analysis. Specifically, monitoring well U2-043 at OU-2 at Hill AFB was analyzed for mass magnetic susceptibility. This is because borehole core samples were collected from the borehole in which this well was installed on December 7<sup>th</sup> and 8<sup>th</sup> 2015. Because the sampling team was so close to this Operable Unit during sampling at Hill AFB, OU-10, groundwater monitoring well U2-043 was sampled with the downhole sonde upon completion of sampling at OU-10.

# 5.5 SAMPLING METHODS

This section describes the procedures that were used for the collection of groundwater samples for laboratory analysis and, as appropriate, the procedures for using the downhole sonde. Groundwater samples and sonde measurements were collected from existing monitoring wells, as described in Section 4. In order to maintain a high degree of quality control (QC) during this sampling event, the procedures described in the following sections were followed.

### 5.5.1 Preparation for Sampling

All equipment to be used for sampling was assembled and properly cleaned and calibrated (if required) prior to the beginning of the sampling event. In addition, all record keeping materials were immediately available at the sampling site. A brief organizational meeting was held prior to field mobilization to ensure proper communication between the project management staff and field personnel. Field personnel consisted of Dr. John T. Wilson and Todd H. Wiedemeier.

Prior to starting sampling procedures, the area around the monitoring well or sampling location was cleared of foreign materials, such as brush, rocks, and debris. These procedures prevented sampling equipment from inadvertently contacting debris around the monitoring well.

# 5.5.1.1 Equipment Calibration

As required, field analytical equipment was calibrated according to the manufacturer's specifications prior to field use. This applies to equipment used for onsite chemical measurements such as pH, electrical conductivity, temperature, dissolved oxygen, oxidation reduction potential (ORP), Fe(II), and volume magnetic susceptibility.

# 5.5.1.1.1 Calibration of YSI-556

The YSI-556 multi-parameter meter was used to temperature, pH, dissolved oxygen, oxidationreduction potential, and specific conductance. The meter was calibrated daily using the procedures detailed in the YSI-556 manual, which is available from YSI (https://www.ysi.com/). pH was calibrated using standards of 4, 7, and 10 standard pH units. ORP was calibrated using a 220 mV standard. Dissolved oxygen was calibrated using atmospheric oxygen content adjusted automatically for altitude. Specific conductance was calibrated using a 1,413 µS/cm standard.

#### 5.5.1.1.2 Calibration of Hach DR-890 Colorimeter

The HACH DR-890, which was used only for Fe(II) concentrations was calibrated by zeroing with DDI water, per the user's manual.

#### 5.5.1.1.3 Calibration of Magnetic Susceptibility Sonde

The magnetic susceptibility sonde was calibrated using the following procedures:

- 1) The sonde was lowered below the water table in the well for a minimum of 15 minutes so that the sonde could equilibrate to the environment in which magnetic susceptibility measurements would be made. It was found that the magnetic susceptibility sonde is very sensitive to variations in temperature.
- 2) The sonde was then raised to the surface and placed it at least 20 feet from any metallic object and not near any power lines.
- The sonde was then calibrated to various calibration standards by running the included computer program. For this work the sonde was calibrated to ambient conditions (zero) and 5E-3 SI units.

#### 5.5.1.1.4 Calibration of Equipment at Clemson

Counts per minute from the liquid scientillation counter were corrected for quench using the quench curve described in section 5.1.4.4.

The amount of TCE in serum bottles was determined using a calibration curve (known amount of TCE per bottle versus GC peak area response from a 0.5 mL headspace injection). For  $O_2$ , a single point calibration was used based on the GC response to a sample of room air containing 21%  $O_2$ .

Determination of rate coefficients with MATLAB were confirmed using the solver function in EXCEL.

#### 5.5.1.1.5 *Calibration of Equipment at PNNL*

Enzyme activity probe staining and qPCR were calibrated using the following procedures:

- 1) Fluorescence of each EAP was verified using positive control organisms known to contain the enzyme being tested.
- 2) Response of the fluorometer for SMMO was calibrated using the positive control microorganisms *Methylosinus trichosporium* OB3b.
- 3) For qPCR, known masses of positive control DNA for each primer pair were serially diluted to make a standard curve for analysis. Cycle threshold values for each unknown was compared to the standard curve and copy numbers of genes determined.

#### 5.5.2 Sampling Procedures

Special care was taken to prevent contamination of groundwater samples. The two primary ways in which sample contamination can occur are through contact with improperly cleaned equipment and by cross-contamination through insufficient decontamination of equipment between wells. To prevent such contamination, the pump and water level probe and cable used to determine static water levels were thoroughly cleaned before and after field use and between uses at different sampling locations according to the procedures presented in this Section. In addition to the use of properly cleaned equipment, a clean pair of new, disposable nitrile gloves was worn each time a different well was sampled. Dedicated polyethylene, and in many cases, silicone tubing was used for the pumps used for this effort. This tubing was disposed of between each well. This tubing was always stored away from any substances that could cause contamination. Wells were sampled sequentially from areas suspected to be least contaminated to areas suspected to be more contaminated.

The following paragraphs present the procedures used for groundwater sample acquisition from groundwater sampling locations. These activities were performed in the same order as presented below.

#### 5.5.2.1 Water Level and Total Depth Measurements

Prior to removing any water from monitoring wells, the static water level was measured. An electrical water level probe was used to measure the depth to groundwater below the datum to the nearest 0.01 foot. None of the wells sampled had nonaqueous-phase liquid.

#### 5.5.2.2 Purging

Prior to sample collection, groundwater was withdrawn from the well using a peristaltic pump, a Grundfos Redi-Flo II<sup>®</sup> pump, a weighted disposable bailer, or a Hydrasleeve<sup>TM</sup>. The Hydrasleeve<sup>TM</sup> was used only to collect samples at Tooele Army Ammunition Depot because of groundwater disposal requirements and because of the depth to groundwater. The Grundfos pump was used only for sampling in OU10-019. Purging and sample collection was performed at the monitoring wells listed in Table 4.1.1. Where possible, field measurements for dissolved oxygen, ORP, pH, temperature, specific conductance were collected during well purging using a flow through cell. In addition, field measurements for Fe(II) concentration were made immediately after well purging using a Hach DR 890 Colorimeter (Wiedemeier et al., 1999). Laboratory samples for the analytes listed in Tables 5.6.1 and 5.6.2 were collected immediately following well purging. Analytes collected during well purging are summarized in Table 5.6.3. Completed groundwater purge and sampling forms are included in Appendix B.

Because the pH, temperature, and specific conductance of a groundwater sample can change significantly within a short time following sample acquisition, these parameters were measured in the field in unfiltered, unpreserved, "fresh" water collected using the same technique as the samples taken for laboratory analyses. The measurements were made in a flow-through cell.

# Table 5.6.1. Total Number and Types of Samples Collected and Types of Analyses Performed

Component	Matrix	Samples		Location
Pre-	Solids	NA	NA	NA
demonstration sampling	Distilled deionized water	24	Accumulation of <sup>14</sup> C products from purified <sup>14</sup> C-TCE, added to glass serum bottles prepared in lab	Clemson University
	Seep Water, Twin Lakes	3 samples of seep water	Accumulation of <sup>14</sup> C products from purified <sup>14</sup> C-TCE added to glass serum bottles preped in field	Twin Lakes Recreation Area, Pendleton, SC
	ENV487 Propanotrophic Enrichment Culture	27	Accumulation of <sup>14</sup> C products from purified <sup>14</sup> C-TCE, added to glass serum bottles prepared in the lab	Clemson University
Technology performance sampling	Aquifer Sediment	23	Magnetic Susceptibility Using a Sonde	Monitoring wells as described in Section 4 and MW U2-043 at OU-2, Hill AFB.
	Groundwater	19	Dissolved Oxygen	All monitoring wells sampled
	Groundwater	19	Fe(II)	All monitoring wells sampled
	Groundwater	19	Oxidation-Reduction Potential	All monitoring wells sampled
	Groundwater	19	рН	All monitoring wells sampled
	Groundwater	19	Temperature	All monitoring wells sampled
	Groundwater	19	Specific Conductance	All monitoring wells sampled
	Groundwater	5 sites, 4 samples per site for 4 sites, 3 samples for 1 site, 3 bottles per well: total = 57	Accumulation of <sup>14</sup> C products from purified <sup>14</sup> C-TCE, added to glass serum bottles prepared at the well head	All monitoring wells sampled
	Filter Sterilized Groundwater	5 sites, total 11 wells	Accumulation of <sup>14</sup> C products from purified <sup>14</sup> C-TCE, added to glass serum bottles prepared in lab	Subset of the monitoring wells
	Groundwater	5 sites, 4 samples for 4 sites, 3 samples for 1 site, 4 analytes = 16 samples for 4 sites and 12 samples for one site, total=76	Enzyme Activity Probes	All monitoring wells sampled – Ship to PNNL
Post- demonstration sampling <sup>a/</sup>	NA	NA	NA	NA

Notes: NA = Not Applicable

a/ Post-demonstration sampling not conducted under this program

Matrix	Analyte	Method	Container(s)	Preservative /Chilled?	•	
Soil	NA	NA	NA	NA	NA	NA
Ground -water	Magnetic Susceptibility	Magnetic Susceptibility Sonde	NA	NA	Field	NA
	Dissolved Oxygen	Direct Reading Probe in a Flow- Through-Cell per USEPA (1998)	NA	NA	Field	NA
	Fe(II) Hach Colorimetric Technique Done Immediately After Well Purging		NA	NA	Field	NA
Oxidation- Direct Reading Probe in a Flow		NA	NA	Field	NA	
	рН	Direct Reading Probe in a Flow- Through-Cell per USEPA (1998)	NA	NA	Field	NA
	Temperature	Direct Reading Probe in a Flow- Through-Cell per USEPA (1998)	NA	NA	Field	NA
	Specific Conductance	Direct Reading Probe in a Flow- Through-Cell per USEPA (1998)	NA	NA	Field	NA
	VOCs, O <sub>2</sub>	GC/FID for VOCs, TCD for O <sub>2</sub> , using headspace samples	160 mL serum bottles with Teflon-faced butyl rubber septa	Store at ~4°C until use	Clemson University	Overnigh t
	<sup>14</sup> C	Various, described in journal articles	160 mL serum bottles	NA	Clemson University	NA
	EAP	EAP	1 1L HDPE Narrow-mouth	Ship at 4°C	PNNL	24 hours
	qPCR	qPCR	1 1L HDPE Narrow-mouth	Ship at 4°C	PNNL	24 hours

Table 5.6.2. Analytical Methods for Sample Analysis

Notes:

NA = Not Applicable Preservatives are not required for these samples; however, all samples will be stored and shipped at 4°C. FID = Flame Ionization DetectorTCD = Thermal Conductivity Detector

# Table 5.6.3. Summary of Groundwater Geochemical Data

ESTCP Project Number ER-201584

		Field Measurements						
		Temperature	Temperature			Dissolved		Ferrou
		(degrees	(degrees		Conductivity		ORP	Iron
Well I.D.	Date	Celsius)	Fahrenheit)	pН	(μS/cm)	(mg/L)	(mV)	(mg/L
TCAAP O1U108								
Conventional Purge Data Using	6/1/2016	11.42	52.56	5.20	502	0.61	153.7 <sup>a/</sup>	<0.0
Peristaltic Pump	6/3/2016	10.64	51.15	6.97	468	0.86	242.6	
TCAAP 01U115								
Conventional Purge Data Using	6/1/2016	10.97	51.75		391	0.54		0.01
Peristaltic Pump	6/3/2016	10.03	50.05	7.35	412	0.58	225.6	
TCAAP 01U117								
Conventional Purge Data Using								
Peristaltic Pump	6/2/2016	10.67	51.21	6.98	462	4.71	243.8	<0.0
TCAAP 01U119								
Conventional Purge Data Using Peristaltic Pump	6/2/2016	8.84	47.91	6.77	865	0.96	223.2	0.10
Peristallic Pump	144000 NOC NE 40041 1		201910-002935	11005.000	2120-0140-22	17. 1744 (1974) 1	<ul> <li>Press (2002) Posta</li> </ul>	11.38720115
Plattsburgh MW-02-006 <sup>/b</sup>								
Data Collected Using Disposable	C/C/004C	40.40	50.40	C CE	004	0.40	440.0	4.00
Bailer	6/6/2016	10.10	50.18	6.65	824	0.42	-110.3	1.25
Plattsburgh MW-02-019								
Conventional Purge Data Using								
Peristaltic Pump	6/6/2016	10.95	51.71	6.94	412	0.40	-106.9	1.12
Plattsburgh 32PLTW12								
Conventional Purge Data Using	6/7/2016	11.39	52.50	5.60	227	8.89	264.3	<0.0
Peristaltic Pump								
Plattsburgh 35PLT13								
Conventional Purge Data Using	6/7/2016	12.31	54.16	7.11	540	1.58	45.4	<0.0
Peristaltic Pump	0.112010	12.01	01.10		0.0		10.1	0.0
Hopewell EPA-16S								or warden
Conventional Purge Data Using	6/8/2016	40.02	54.40	0.00	070	c 7c	000.0	-0.0
Peristaltic Pump	6/8/2016	10.83	51.49	6.09	672	5.75	222.6	<0.0
Hopewell EPA-15D	2							
Conventional Purge Data Using								
Peristaltic Pump	6/8/2016	11.04	51.87	6.95	743	4.14	163.0	<0.0
Hopewell EPA-12S Conventional Purge Data Using								
Peristaltic Pump	6/9/2016	10.53	50.95	6.61	1004	6.72	270.9	<0.0
	0/9/2010		101010101010			11 How 20 Miles		
Hopewell EPA-10S								
Conventional Purge Data Using	6/9/2016	9.82	49.68	6.31	771	5.86	172.8	
Peristaltic Pump			10.000					
Tooele D-20 <sup>/b</sup>								
Hydrasleeve <sup>™</sup> /Peristaltic Pump	7/25/2016	17.38	63.28	6.90	1417	7.00	190	<0.0
Tooele D-23 <sup>/b</sup>	5							
Hydrasleeve™/Peristaltic Pump	7/25/2016			7.05	10200	1 0 0	244	<0.0
	112512016			7.05	19290	1.88	211	<0.0
Tooele D-25 <sup>/b</sup>								
Hydrasleeve™/Peristaltic Pump	7/26/2016		0440	7.14	4772	5.41	200	<0.0
Tooele D-19 <sup>/b</sup>								
Hydrasleeve <sup>™</sup> /Peristaltic Pump	7/26/2016	10.04	CE A4	6 47	1010	60	100.0	-0.0
Tyurasieeve /Peristallic Pullip	112012016	18.34	65.01	6.47	1010	6.9	189.6	<0.0

D.1THWA\ESTCP ER-201584\Report - Technical/Tables/Table 5.6.3 Geochemical Data-8-30-16.xls 10/17/2016

ESTCP Project Number ER-201584								
		Field Measurements						
Well I.D.	Date	Temperature (degrees Celsius)	Temperature (degrees Fahrenheit)	pН	Conductivity (μS/cm)	Dissolved Oxygen (mg/L)	ORP (mV)	Ferrous Iron (mg/L)
Hill AFB U10-043 Conventional Purge Data Using Peristaltic Pump	7/27/2016	15.27	59.49	7.00	1145	0.75	168.2	<0.03
HIII AFB U10-025 Conventional Purge Data Using Peristaltic Pump	7/27/2016	18.87	65.97	7.17	1453	0.29	-51.5	<0.03
Hill AFB U10-019 <sup>/b</sup>								
Conventional Purge Data Grundfos Pump, Well went dry multiple times	7/28/2016	23.08	73.54	8.12	1325	7.45	-51.7	0.69

#### Table 5.6.3 Summary of Groundwater Geochemical Data

Notes:

Milligrams per liter Microsiemens per centimeter Oxidation Reduction Potential (Millivolts)

mg/L uS/cm ORP (mV) ---/a

/b

Variously applied to indicate: Not Applicable, Not Available, Not Measured, or Not Reported, as appropriate. PH/ORP probe not working properly during this sampling Results suspect because insufficient volume of water was removed during purging



Well purging, where possible, continued until those parameters measured using a flow-through cell, including dissolved oxygen, pH, temperature, ORP, and specific conductance stabilized. This includes less than 0.2 standard pH units or a 10% change for the other parameters over a 5-minute period. Because of constraints on purge water disposal, this was not possible for the wells sampled at Tooele Army Depot. In addition, this was not possible for monitoring well MW-02-006 at the former Plattsburgh AFB because groundwater was too deep for the peristaltic pump, and well OU10-019 at Hill AFB OU-10, because the well went dry using the Grundfos pump and had to be allowed to recharge before samples could be collected. All purge waters were disposed of in accordance with the specifications identified in this document.

#### 5.5.2.3 Sample Extraction

Water from sampling devices was directly discharged into the sample container. The water was carefully poured down the inner walls of the sample bottle to minimize aeration of the sample. Four sample acquisition techniques were used to collect groundwater samples, including:

- 1) Use of a peristaltic pump with tubing placed directly into the well (majority of wells);
- 2) Use of a Grundfos submersible pump (one well, U10-019);
- 3) Use of a bailer and draining the groundwater out of the base of the bailer (well MW-02-006 at the former Plattsburgh AFB), and;
- 4) Use of a Hyrdasleeve<sup>TM</sup> in conjunction with a peristaltic pump. The Hydrasleeve<sup>TM</sup> was lowered into the well to collect the water sample, raised to the surface and temporarily hung from the lip of the well. A peristaltic pump was then used to remove water from the Hydrasleeve<sup>TM</sup>. This technique was used for all of the wells sampled at Tooele Army Ammunition Depot because no purge water could be generated.

Sample containers were filled as follows:

- 1) For samples sent to PNNL for EAP analyses, the sample containers were filled so that no air space (headspace) remained in the container, and;
- 2) For samples sent to Dr. Freedman's lab at Clemson, 160 mL serum bottles were filled with approximately 100mL of groundwater and sealed with a crimp cap with a Teflon septum.

Excess water collected during sampling was handled according to the specifications identified in the Demonstration Plan (ESTCP, 2016).

#### 5.5.3 Handling of Samples for Laboratory Analysis

This section describes the handling of samples to be analyzed by the PNNL and Clemson University from the time of sampling until the samples arrive at the laboratory. A summary of details regarding requirements for containers, preservation techniques, sample volumes, and holding time is provided in Table 5.6.2.

#### 5.5.3.1 Sample Container and Labels

Sample containers and appropriate container lids and labels were provided by the analytical laboratories at Clemson University and PNNL. The sample containers were filled as described in Section 5.6.2.3, and the container lids were tightly closed or crimped. Container lids were not removed at any time prior to sample collection. Sample labels were firmly attached to the container side, and the following information was legibly and indelibly written on the label:

- Facility name;
- Sample identification;
- Sample type (groundwater, surface water, etc.);
- Sampling date;
- Sampling time;
- Preservatives added (none for this effort); and
- Sample collector's initials.

#### 5.5.3.2 Sample Preservation

No chemical preservatives were added to the sample containers for this effort. Samples were properly prepared for transportation to the laboratory by placing the samples in a cooler containing ice to maintain a shipping temperature of  $4^{\circ}$ C

#### 5.5.3.3 Sample Shipment

After the samples were sealed and labeled, they were packaged for transport to the analytical laboratory. Samples were shipped priority overnight via Federal Express<sup>®</sup>. The following packaging and labeling procedures were followed:

- The sample was packaged so that it would not leak, spill, or vaporize from its container;
- The shipping container was labeled with:
  - Sample collector's name, address, and telephone number;
  - Laboratory's name, address, and telephone number;
  - Description of sample;
  - Quantity of sample; and
  - Date of shipment.

The packaged samples were delivered to the laboratory the day after sample acquisition to ensure testing within method-specific holding times.

# 5.5.3.4 Chain-of-Custody Procedures

After the samples were collected, chain-of-custody procedures were followed to establish a written record of sample handling and movement between the sampling site and the laboratory. Each shipping container had a chain-of-custody form completed in triplicate by the sampling personnel. One copy of this form was kept by the sampling team and the other two copies were sent to the laboratory. The chain-of-custody contains the following information:

- Sample identification number;
- Sample collector's printed name and signature;
- Date and time of collection;
- Place and address of collection;

- Sample matrix;
- Analyses requested;
- Signatures of individuals involved in the chain of possession; and
- Inclusive dates of possession.

The chain-of-custody documentation was placed inside the shipping container so that it was immediately apparent to the laboratory personnel receiving the container, but was not damaged or lost during transport. The shipping container was sealed with custody seals so that it would have been obvious if the seal had been tampered with or broken. Appendix B contains chain-of custody records.

#### 5.5.3.5 Sampling Records

In order to provide complete documentation of the sampling event, detailed records were maintained by field personnel. At a minimum, these records include the following information:

- Sample location (facility name);
- Sample identification;
- Date and time of sampling;
- Sampling method;
- Field observations of
  - Sample appearance,
  - Sample odor;
- Weather conditions;
- Water level prior to purging;
- Total well depth;
- Approximate Purge volume;
- Well condition;
- Sampler's identification;
- Field measurements of pH, temperature, and specific conductivity; and
- Any other relevant information.

Groundwater sampling activities were recorded on the Groundwater Purge and Sampling Form found in the Demonstration Plan (ESTCP, 2016). These completed forms are found in Appendix B.

# 5.5.4 Laboratory Analyses

All samples collected for laboratory analysis were shipped to Clemson University and PNNL. Prior to sampling, arrangements were made with the laboratory to provide a sufficient number of appropriate sample containers for the samples to be collected. All containers, preservatives, and shipping requirements were consistent with laboratory protocols. Quality Control samples were prepared and acquired as described Section 5.6.6. For EAP and qPCR analyses, trip blanks sterile distilled water) were shipped with each cooler and analyzed with samples from each site.

Shipping containers with adequate padding and cooling media were sent by the laboratory to the site. Sampling personnel filled the sample containers and returned the samples to the laboratory.

#### 5.5.4.1 Assay of Rate of TCE Co-Oxidation Using <sup>14</sup>C-Labeled TCE

Details on development of the <sup>14</sup>C-TCE assay are presented in sections 2.2.2.1; 3.1.2; 3.2.2; 5.1.3; and 5.1.4. The first task was to evaluate an improved method for purifying the <sup>14</sup>C-TCE stock solution, with the goal of minimizing the amount of <sup>14</sup>C impurities added to the serum bottles that accompany the <sup>14</sup>C-TCE. The lower the initial level of impurities, the easier it becomes to detect a statistically significant increase in <sup>14</sup>C products over a relatively short timeframe (e.g., several days). In previous studies (e.g., Darlington et al., 2008, 2013), a single GC column was used for purification. In this study, two columns in series was also evaluated. It turned out that the dual column approach did not yield a statistically significant lower level of impurities. With the single and dual column methods, the target of 0.01% impurities was not met; the initial level of impurities was closer to 0.05% of the total <sup>14</sup>C added to the serum bottles. However, this was compensated for by increasing the duration of the assay, allowing for detection of an increase in <sup>14</sup>C products above the initial level impurities in the bottles. Using this approach, the lowest rate constant measured was 0.00658 yr<sup>-1</sup>, which translates to a half-life of 105 yr. While it may be possible to lower the detection limit of the assay, lower rates would not likely have any practical value from the standpoint of assessing MNA.

The assay involved addition of ~100 mL of groundwater, DDI water, or FSGW to 160 mL serum bottles. Following addition of purified <sup>14</sup>C-TCE, accumulation of <sup>14</sup>C products was measured in 3 mL samples removed eight or nine times, over 40 to 46 days of incubation. The pH of the 3 mL samples was raised above 10 to retain <sup>14</sup>CO<sub>2</sub>, and then the water was sparged for 30 min to remove the residual <sup>14</sup>C-TCE, leaving behind only the <sup>14</sup>C products. An experiment was performed to determine if 30 min of sparging was adequate to remove all of the unreacted TCE. Sparging for 60 min was tested and shown not to further lower the <sup>14</sup>C products left after sparging. Consequently, a 30 min sparging time was used.

In order to determine a first order rate constant, the rate of <sup>14</sup>C product accumulation in groundwater must be greater than the rate of accumulation in sterile controls. Initially, DDI water was used as the negative control. It was subsequently determined that FSGW controls are a better representation of the background level of product formation; these were used to calculate net first order rate constants for eight of the 19 wells evaluated.

Section 5.1.4 specifics how the first order decay rate constant was calculated. A mass balance model that included the first order decay coefficient was fit to the measured amounts of <sup>14</sup>C products formed. The optimum value fopr the rate coefficient was found by minimizing the sums of squares of error between the measured and predicted amount of <sup>14</sup>C products over time. Details on the methods for counting <sup>14</sup>C activity are provided, as are the methods to quantify and/or detect the VOCs by GC/FID and the amount of oxygen present in the headspace by GC/TCD.

When the incubation period was complete (40-46 days), samples were evaluated using both alkaline and acidic sparging. The difference between the two allowed for calculation of the percentage of product in the form of  ${}^{14}\text{CO}_2$ .  ${}^{14}\text{CO}_2$  was further confirmed by precipitation with barium.

The <sup>14</sup>C assay was validated using locally sourced water from a seep with a high content of organic debris. A statistically significant rate of TCE co-oxidation was observed, confirming the viability of the assay. Additional evidence for the efficacy of the assay was obtained using a propanotrophic enrichment culture that is known to co-oxidize TCE.

The propanotrophic culture was used to evaluate the potential impact of sample storage conditions on the rate of <sup>14</sup>C product accumulation. Storage at 4 °C overnight, followed by warming to room temperature overnight, did moderately reduce the first order reaction rate coefficient when considering the full incubation period (40 d). This suggested that results for the groundwater samples are conservative with respect to in situ conditions. Nevertheless, shipment of groundwater sample to a laboratory that is licensed to handle <sup>14</sup>C is a requirement for the assay, and shipment on ice is recommended to avoid even more significant decreases in co-oxidation activity that may occur if the samples are left at ambient temperature.

# 5.5.4.2 Enzyme Activity Probes and qPCR Assays

#### Enzyme Activity Determination

Samples were received in the laboratory and inspected to ensure there was very little headspace in bottles containing groundwater. Observations were recorded and photos taken to go along with the description. For EAP analysis, samples were processed individually. Groundwater sample bottles were inverted for mixing. Once the sample was mixed, bottles were opened and an aliquot immediately pipetted (3-10 mL) onto a sterile manifold set up with GF/F (backing filter) and 0.22 µm, 25-mm diameter, black, polycarbonate filter. A vacuum was used to pull the sample through the filter, trapping the microorganisms on the surface. The vacuum was released to facilitate staining and 0.25 ml of the appropriate EAP in 40 mM phosphate buffer was filtered onto the polycarbonate filter. The manifold system was covered with aluminum foil or placed in the dark for 15 minutes of exposure time with the probe; after 15 minutes, the vacuum was reapplied to remove the probe solution. Cells on filter were counterstained with DAPI (4,6diamidino-phenylindole), a total cell, DNA stain, by adding 60 µl of DAPI to the filter and incubated, in the dark for < 5 minutes. The filter was washed with 1 mL of nanopure water or phosphate buffer to remove any unbound EAP and DAPI. The filter was then placed onto a glass microscope slide, cell side up, and mounted with non-fluorescent citifluor solution and a cover slip.

The filters were examined and visualized for fluorescent cells on a Nikon Eclipse E600 fluorescence microscope equipped with a PLAN Fluor 100x 1.30 oil objective. A UV2E/C filter (excitation 340-380 nm, dichromatic mirror 400 nm, emission 435-485 nm) was used to count DAPI stained cells, while a B-2E/C filter (excitation 465-495 nm, dichromatic mirror 505 nm, emission 515-555 nm) was used to visualize probe positive cells.

#### DNA extraction and PCR amplification

Groundwater samples were filtered (typically 250ml, up to 1L) onto  $0.22\mu m$ , 47mm diameter, Supor filters to capture bacteria. If DNA from the samples are not to be extracted immediately, the filters are placed into eppendorf tubes, whirlpack bags, or 50mL falcon tubes depending on the size of the Supor filters used. Samples are stored at -80 °C.

When ready to extract, samples are removed the -80 °C and the DNA from the cells trapped on filters is extracted using both Bio 101 and the MoBio UltraClean Soil DNA kits, as described by the manufacturers. Two kits were used to ensure that biases associated with one kit or another did not provide a false positive or negative for the presence of the gene of interest. DNA concentrations were quantified using a Nanodrop instrument; quality and quantity of DNA were determined and recorded.

Polymerase chain reaction (PCR) and qPCR amplification reactions were performed in 50 mL and 25 mL reaction mixtures, respectively. PCR/qPCR conditions for the primers, are as stated in (Baldwin et al., 2003; 2008 or Hendrickx et al., 2006; 2008). For those primers that were either developed or modified for use in qPCR reaction mixtures, procedures for the amplification are similar to those in the published literature. Standards for qPCR were used to determine the concentration of cells in each reaction. Positive control organisms served as standards for these analyses. Concentrations of DNA were standardized for all reactions; PCR reactions were carried out with a 50 ng starting concentration, while qPCR is initialized with 10 ng. Thus products/positive amplifications of products are comparable.

PCR and qPCR products were separated and visualized using an Agilent 2100 Bioanalyzer and DNA 1000 LabChips. Each LabChip has 16 wells, twelve of which are used for experimental samples, one well was used for a molecular weight DNA ladder, and three were used for loading the gel-dye mix. DNA 1000 LabChips were prepared and loaded with samples as recommended by the manufacturer with minor modifications. Microchannels were filled by pipetting 9  $\mu$ l of gel-dye mix (consisting of a linear polymer and a fluorescent, intercalating dye of a proprietary nature) into the appropriate well and then forcing the mix into the microchannels by applying pressure to the well via a 1-ml syringe. Five microliters of marker mix was loaded into each sample well, followed by 1  $\mu$ l of molecular weight ladder into the ladder well or samples into the sample well. The contents of each well on the chip was mixed using an IKEA vortexer supplied with the instrument. After being vortexed, chips were immediately inserted into the bioanalyzer and processed. All experiments were performed using Agilent Biosizing software.

# 5.5.5 Equipment Decontamination Procedures

#### 5.5.5.1 Portable Sampling Equipment

All portions of non-disposable sampling and test equipment that contacted groundwater from which a sample was collected were thoroughly cleaned before each use. This equipment included the water-level probe, the Grundfos pump, and the downhole mass magnetic susceptibility sonde. The following decontamination protocol was used:

- Clean with potable water and phosphate-free laboratory detergent (Liquinox® or equivalent);
- Rinse with potable water;
- Rinse with distilled or deionized water;
- Rinse with isopropanol; and
- Air-dry the equipment prior to use.

The Grundfos pump used for purging or sampling was decontaminated by placing the pump and discharge hose into a DDI water/laboratory detergent (e.g., Liquinox) solution, washing the pump and discharge hose exterior, and pumping the solution through the pump and hose. The pump and hose exterior was then rinsed with potable water, and potable water was pumped through the pump and hose until all of the detergent solution was removed.

If pre-cleaned, dedicated sampling equipment is used, the decontamination protocol specified above will not be required. Laboratory-supplied sample containers will be cleaned and sealed by the laboratory and therefore will not need to be cleaned in the field.

# 5.5.6 Quality Assurance/Quality Control Samples

#### 5.5.6.1 Field Quality Assurance/Quality Control Samples

For magnetic susceptibility measurements using the sonde, a minimum of two runs was made in each well where previously-collected magnetic susceptibility data from borehole core samples were available.

#### 5.5.6.2 Quality Assurance/Quality Control Samples Used by Clemson

Calibration curves for TCE and O<sub>2</sub> were included on control charts to ensure that response factors were within one standard deviation of historical means.

For each site, the <sup>14</sup>C assay was performed with one set of DDI water controls along with the groundwater samples. The DDI water served as a negative control, to assess the rate of <sup>14</sup>C product accumulation in the absence of microbes. For 10 of the wells, FSGW controls were also prepared, also serving as negative controls. FSGW controls exhibited lower rates of product accumulation versus DDI water, likely due to the presence of quenching compounds in the groundwater that reduced the magnitude of <sup>14</sup>C-TCE autoradiolysis.

The quench efficiency curve for the <sup>14</sup>C counting protocol was determined using prepared <sup>14</sup>C standards (Beckman Instruments Inc., quenched carbon-14 standards set).

# 5.5.6.3 Quality Assurance/Quality Control Samples Used by PNNL

Multiple laboratory blank samples were prepared and analyzed. One blank will be prepared and analyzed each calendar day a sample is received for analyses in the laboratory. Water will be filtered onto black polycarbonate filters and viewed with epifluorescent microscopy. The purpose of these blanks is to establish that there is no background fluorescence that could potentially influence the results of the assay. If background fluorescence is detected, solutions will be filter-sterilized or replaced. Pre-sterilized filters will also be analyzed as laboratory blanks. Each lot of filters used in the laboratory will be analyzed for clarity and background or other fluorescent interference. If any of the blank sample analyses are positive, actions will be taken to correct and/or eliminate all possible contamination issues.

Laboratory standards involve the application of EAPs to positive control microorganisms kept in culture in the laboratory. Positive control organisms are actively grown under enzyme induction conditions and subsequently exposed to EAP. If the standards do not provide positive results with the EAP analysis, the analysis will be considered inaccurate and void.

One matrix spike sample will be analyzed per batch of shipment. A known number of organisms with active oxygenases will be added to a given site sample and analyzed with EAP. If the spike recovery is not within the 70-130% range, the sample will be reanalyzed. If subsequent analyses are not within range, the sample will be considered void.

# 5.5.7 Handling of Investigation-Derived Waste (IDW)

Purge and decontamination water (IDW) was disposed of for each site as discussed in Section 4 of the Demonstration Plan (ESTCP, 2016). For the majority of wells, purge water was discharged to the ground. Exceptions to this included:

- Any purge water collected at OU-10 was containerized in a Department of Transportation-(DOT) rated and approved 125 gallon container and disposed of at the base waste water treatment plant.
- No excess purge water was collected from Tooele.
- Purge water from monitoring wells 10S and 12S at Hopewell was containerized in Department of Transportation-(DOT) rated and approved containers. A total of 5 gallons of excess purge water was generated from these wells.

# 5.6 SAMPLING RESULTS AND DATA ANALYSIS

This section provides a detailed summary of sampling results in terms of both temporal and spatial dependence, as appropriate.

# 5.6.1 Sampling Results and Data Analysis for Magnetic Susceptibility

# 5.6.1.1 Introduction

The quantity of magnetite in aquifer sediment can be characterized with good sensitivity and at low cost by measuring the magnetic susceptibility of the aquifer matrix (Section 2). To date, this has been accomplished by collecting borehole core data and submitting it to an analytical laboratory. Unfortunately, the cost of acquiring core samples at many sites is too high to make an evaluation of abiotic degradation by magnetite economically feasible. This is especially true if no additional drilling activities are anticipated.

The purpose of this work was to determine if downhole sondes report a magnetic susceptibility that is equivalent to that determined by borehole core samples evaluated in the laboratory. To accomplish this, values of magnetic susceptibility provided by the downhole sonde were compared to borehole core samples.

# 5.6.1.2 Results – Correspondence Between Sonde and Core Samples

Appendix C contains the data collected using the sonde. Figure 5.7.1 compares the data from core samples to the data from the sonde for four of the sites. The panels in the figure are identified by the site and by the monitoring well that was investigated by the sonde. At each of the sites, there was significant variation in the values from the core samples and from the in-well sonde. At a vertical scale of meters, there was significant variation between different depth intervals and within the same depth intervals in both the core data and the sonde data.

Variation in sediment properties, which is caused by variations in depositional environments, is often a function of the vertical scale over which a sample is collected. Samples collected over larger vertical intervals may have less variation because they tend to average out the vertical variation that occurs in samples collected at a smaller vertical scale. Samples collected using boreholes also have recoverability issues. This is not the case with the magnetic susceptibility sonde. At the TCAAP, Plattsburgh and Hill AFB Sites, the scatter in the core data and the sonde data at a particular depth were roughly equivalent (Panels a, b, c in Figure 5.7.1). At the Tooele Site there was less scatter in the sonde data at a particular depth (Panel d in Figure 5.7.1).

The sonde data for wells at Plattsburgh, Hill AFB and Tooele represent the entire length of the screen and riser for these wells (Panels b, c, d in Figure 5.7.1). There is no data below an elevation of 268.5 m from the well at the TCAAP because the sonde bound up against the sides of the well casing and could not be lowered further into the well (Panel a in Figure 5.7.1). The well casing had a diameter of 5.1 cm (2.0 inch). There was no problem with binding in a well at Plattsburgh which had a diameter of 5.1 cm (2.0 inch) or in the wells at Hill AFB or Tooele that had a diameter of 10.2 cm (4.0 inch).

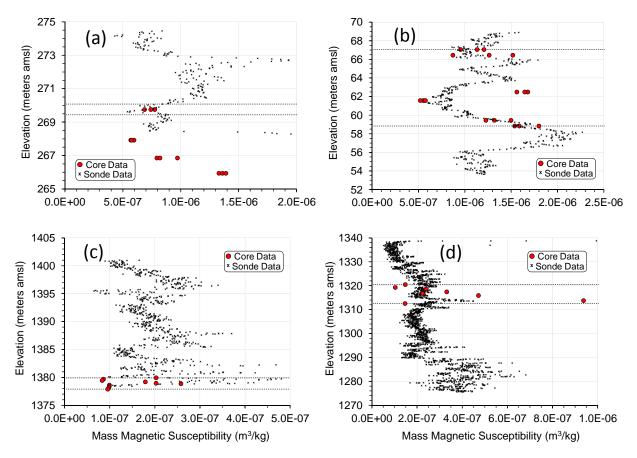


Figure 5.7.1. Comparison of Mass Magnetic Susceptibility from Core Samples to the Mass Magnetic Susceptibility from a Sonde in a Monitoring Well for Wells at the TCAAP, Plattsburgh, Hill AFB and Tooele Sites.

The dashed horizontal lines enclose the interval over which the core data were compared to the sonde data. Panel (a) is well TCAAP 01U108, Panel (b) is Plattsburgh MW-02-030, Panel (c) is Hill AFB OU2-043, Panel (d) is Toole D-23.

Figure 5.7.2 compares the data from core samples to the data from the sonde for six wells at the Hopewell site. This site was selected to provide information on the variation in magnetic susceptibility from well to well across a single site. The flow path of groundwater extends from Well EPA-10D to Wells EPA-12D and EPA-16D and EPA-15D, then to Well EPA-19S and finally to Well EPA-21D. Well EPA-12S is 440 m downgradient of Well EPA-10D, Well EPA-19S is 570 m further downgradient of Well EPA-12S, and Well EPA-21D is 430 m even further downgradient of Well EPA-19S. At this site, the distribution of magnetic susceptibility varied widely both laterally and vertically. At some depth intervals, the data from the sonde tracked the magnetic susceptibility compared to ex-situ measurements of core samples.

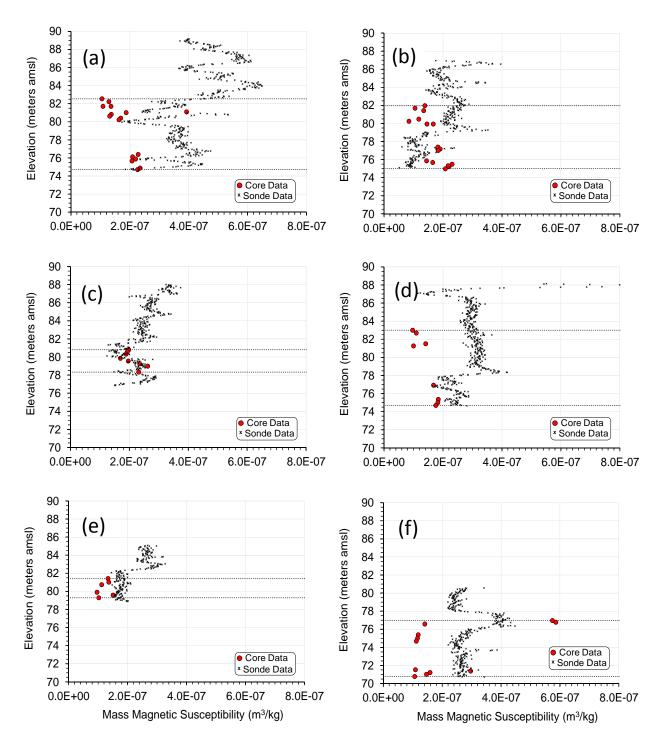
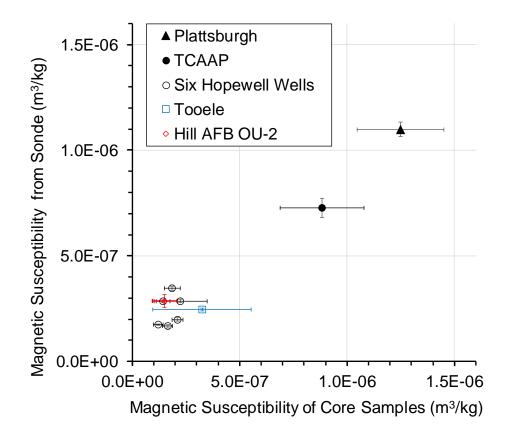


Figure 5.7.2. Comparison of Mass Magnetic Susceptibility from Core Samples to Mass Magnetic Susceptibility from a Sonde in a Monitoring Well for Wells at the Hopewell Site.

The dashed horizontal lines enclose the interval over which the core data were compared to the sonde data. Panel (a) is well EPA 10D, Panel (b) is EPA 12D, Panel (c) is EPA 15D, Panel (d) is EPA 16D, Panel (e) is EPA 19S and Panel (f) is EPA 21D.

For each of the ten wells, Figure 5.7.3 compares the mean of the mass magnetic susceptibility obtained from the HM-453S sonde to the mean that was obtained from core samples. At each well location, the mean for the sonde data and the mean for the core samples were calculated from data collected over the same depth interval. The interval that contains the data that was included in the means is bounded by the horizontal longitudinal dotted lines in each Panel of Figure 5.7.1 and Figure 5.7.2. The error bars in Figure 5.7.3 are the 95% confidence interval on the means. The Pearson Correlation Coefficient between the core means and the sonde means was R= 0.936.



### Figure 5.7.3. Relationship between Magnetic Susceptibility from Core Data and the Downhole Sonde.

Each data point is the mean of data from an individual well. The error bars are the 95% confidence interval on the mean.

Notice that the error bars are much narrower on the means of the sonde data (Figure 5.7.3), even though the apparent scatter in the data is about the same (Figures 5.7.1 and 5.7.2). The confidence intervals are calculated from the standard error of the mean, which is the standard deviation of the samples divided by the square root of the number of samples. The sonde provided many more data points to contribute to the average. However, it is important to distinguish precision from accuracy. We had no independent standard to evaluate the accuracy of the sonde compared to the accuracy of the laboratory analyses.

In general, the means of the data from the sonde were in good agreement with the means of the data from the core samples. Table 5.7.1 compares the mean of the sonde analyses for each monitoring well to the mean of the core sample analyses. The means were compared with a *t*-test for the difference of means with unequal variance. For six of the ten wells, the test failed to reject the null hypothesis that there was no difference in the means at 95% confidence (P > 0.05). At four of the wells the means were different at 95% confidence. However, the mean of the sonde analyses varied from the mean of the core sample analyses by less than a factor of two (Table 5.7.1). The variation between data reported by the sonde and the laboratory analysis of core samples is acceptable for the purpose of evaluating a site for abiotic degradation of TCE.

The wells at the Hopewell site, OU-2 at Hill AFB, and at Tooele were 4-inch ID. The wells at TCAAP and Plattsburgh were 2-inch ID. The larger wells would have more air in the annular space, and would be more likely to have a greater radius of engineered sand pack between the wall of the bore and the screen or casing. This should tend to reduce the response in the sonde. Despite this expectation, the ratio of the response of the sonde to the core samples was generally higher in the 4-inch wells compared to the 2-inch wells (Table 5.7.1). The well at Tooele was the only exception. In the wells in the survey, there was no indication of a systematic bias in the magnetic susceptibility reported by the sonde in 4-inch ID wells.

Location	Well	Mean of Magnetic Susceptibility		Ratio of Means	Number of Values in Mean		<b>p</b> *
		m <sup>3</sup> kg <sup>-1</sup>		Sonde/Cores			
		Sonde	Cores		Sonde	Cores	
Hopewell	EPA 19	1.8E-07	1.2E-07	1.44	71	6	1.8E-03
Hill OU-2	OU2-043	2.7E-07	1.4E-07	1.91	58	10	4.7E-05
Hopewell	EPA 16	2.8E-07	1.4E-07	1.96	273	8	7.4E-06
Hopewell	EPA 12D	1.7E-07	1.6E-07	1.03	223	15	0.65
Hopewell	EPA 10D	3.5E-07	1.9E-07	1.86	258	16	9.3E-08
Hopewell	EPA 15D	2.0E-07	2.1E-07	0.95	82	8	0.38
Hopewell	EPA 21	2.9E-07	2.2E-07	1.28	204	11	0.29
Tooele	D-23	2.2E-07	2.6E-07	0.76	261	8	0.44
TCAAP	O1U108	7.3E-07	8.8E-07	0.82	22	12	0.11
Plattsburgh	MW-02-030	1.2E-06	1.2E-06	0.95	302	18	0.51

 Table 5.7.1. Comparison of Estimates of Mass Magnetic Susceptibility from a Downhole

 Sonde to Estimates from Laboratory Analysis of Core Samples

\*Probability of error, two tailed.

#### 5.6.1.3 Summary

If appropriate monitoring wells are available, downhole magnetic susceptibility sondes in groundwater monitoring wells can provide a less expensive alternative to the collection and analysis of borehole core data, and can provide data that can be used to evaluate field-scale rate constants for abiotic degradation of PCE, TCE, and *c*DCE by magnetite.

Wells or segments of wells are appropriate for use with a magnetic susceptibility sonde when (1) they are constructed with PVC screens and risers, (2) they do not contain iron or steel, and (3) they have an internal diameter of 5.1 cm (2 inches) or 10.2 cm (4 inches).

If a well with a casing diameter of 5.1 cm (2 inches) is not straight, there is a possibility that the sonde will bind against the sides of the casing or screen. In this survey, there was no indication of a problem with wells with a casing diameter of 10.2 cm (4 inches).

Because there were many more data points provided from the sonde compared to core samples, the sonde data provided more precision in the estimate of average value for magnetic susceptibility.

At the five sites that were investigated, the downhole sonde reported values of magnetic susceptibility that were similar to values reported on borehole core samples analyzed in the laboratory. In most cases, the means of the two measurements could not be distinguished at 95% confidence. When the means could be distinguished, they still agreed within a factor of two.

If possible, the magnetic susceptibility data should be collected in the same wells that provided the concentration data used to extract the field-scale rate constant. In the *BioPIC Tool*, the purpose of surveying a site for magnetic susceptibility is to evaluate a field-scale rate constant for abiotic degradation. The rate constant is extracted by analyzing monitoring data from several wells that lie along a transect in the direction of groundwater flow. The rate constant represents that segment of the aquifer. The value for magnetic susceptibility used to evaluate the rate constant should also represent that same segment of the aquifer.

If information is available on the vertical distribution of hydraulic conductivity, or on the texture of unconsolidated porous media, use that information to filter the data on magnetic susceptibility, and take the mean of the data points that are associated with the regions that carry the major portion of groundwater flow.

Use magnetic susceptibility to provide a second line of evidence as defined by USEPA (1999). Use magnetic susceptibility to evaluate whether abiotic degradation by magnetite is a plausible explanation for a rate constant that is extracted from the monitoring data and the geological and hydrological properties of the site. Do not use magnetic susceptibility to estimate or predict a rate constant for degradation.

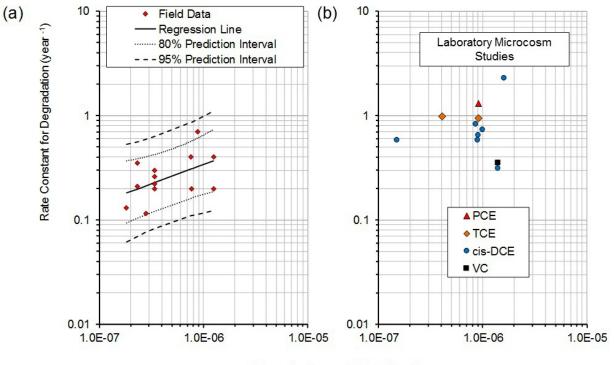
If the groundwater in the aquifer is sulfate reducing, do not use magnetic susceptibility as a line of evidence for abiotic degradation by magnetite, unless it can be shown that the magnetic susceptibility is associated with magnetite and not greigite. Greigite can be distinguished from magnetite by comparing total Sulfur and total Iron(II) in the sediment.

Review the data provided by the sonde. Exclude from interpretation any data where there is a sharp transition to a very high magnetic susceptibility. These data may be associated with steel or iron in centralizers in the well, or with tools that might have been dropped into the borehole.

Figure 5.7.4 shows the relationship between first order rate constant for abiotic degradation and the magnetic susceptibility of aquifer materials. This figure is modified from ESTCP (2015) and He (2009) with additional data collected during this work. Figure 5.7.4 compares the first-order rate constant for degradation of chlorinated ethenes in unconsolidated aquifer sediments to the mass magnetic susceptibility of the sediment. Panel (a) of Figure 5.7.4 compares field-scale rate constants for removal of PCE, TCE, DCE, or VC. The rate constants were extracted from monitoring data at seven sites. Depending on the site, each data point may represent a rate constant for an individual chlorinated alkene, or it may represent a composite rate constant for PCE, TCE and DCE.

The dashed lines in Panel (a) of Figure 5.7.4 are prediction intervals on a new observation. The 95% prediction interval is an order of magnitude wide. This may reflect error and uncertainty in the estimates of the rate constants; however, this may also reflect true variation in the rate constants from one site to another. Lee and Batchelor (2002) noted in their laboratory experiments that adding 42.6 mM Fe(II) to a suspension of magnetite increased the rate constant for degradation of *c*DCE and VC by an order of magnitude. Iron(II) was present in groundwater at some of the sites depicted in Panel (a) of Figure 5.7.4, but not in others.

The rate constants in Panel (a) of Figure 5.7.4 are bulk rate constants and may include aerobic biodegradation of DCE in addition to abiotic degradation by magnetite. Panel (b) of Figure 5.7.4 summarizes a series of microcosm studies that are reported in He et al. (2009). The sediment used to construct the microcosms was autoclaved to kill any microorganisms. The rate constants for removal of the chlorinated alkenes in the microcosms can be safely attributed to degradation by magnetite. Only one of the sites used to extract field-scale rate constants was used for microcosm studies (TCAAP). Nevertheless, the range of field-scale rate constants and the range of rate constants in the microcosm studies were similar. There is no evidence that the field-scale rate constants are substantially faster than the rate constants from the microcosm studies.



Magnetic Susceptibility (m<sup>3</sup> kg<sup>-1</sup>)

Figure 5.7.4. Relationship between First Order Rate Constant for Abiotic Degradation and the Magnetic Susceptibility of Aquifer Materials (Modified from ESTCP [2015] and He [2009]).

#### 5.6.2 Sampling Results for Data Generated by <sup>14</sup>C-Labeled TCE Assay

Pseudo-first order rate coefficients (Table 5.7.2) were determined as described in Section 5.1.4, based on a mass balance that incorporated a decay rate for <sup>14</sup>C-TCE in the serum bottles.

## Table 5.7.2. Pseudo First-order Rate Constants Based on the Difference between Experimental Rate Constants and Respective FSGW Rate Constants.

Net rates were only determined for wells that were statistically significant compared to the respective FSGW controls.

	FSGW	Controls	Experimental				
Site		k		Net k	Half Life		
Location	Well	(yr <sup>-1</sup> )	Well	( <b>yr</b> <sup>-1</sup> )	( <b>yr</b> )		
TCAAP	01U115	$0.032 \pm 0.007$	01U108	0	-		
TCAAP	01U115	$0.032 \pm 0.007$	01U115	0	-		
TCAAP	01U115	$0.032 \pm 0.007$	01U117	0	-		
ТСААР	01U115	$0.032 \pm 0.007$	01U119	0	-		
Plattsburgh	MW-02-019	$0.029\pm0.009$	MW-02-006	$0.511 \pm 0.042$	$1.4 \pm (1.3, 1.5)$		
Plattsburgh	MW-02-019	$0.029\pm0.009$	MW-02-019	$0.129 \pm 0.014$	$5.4 \pm (4.8, 6.1)$		
Plattsburgh	32PTLW12	$0.084 \pm 0.017$	32PTLW12	0	-		
Plattsburgh	35PTLW13	$0.014 \pm 0.004$	35PTLW13	0	-		
Hopewell	EPA-16S	$0.021 \pm 0.006$	EPA-16S	0	-		
Hopewell	EPA-15D	$0.020 \pm 0.004$	EPA-15D	0	-		
Hopewell	EPA-12S	$0.011 \pm 0.003$	EPA-12S	0	-		
Hopewell	EPA-10S	$0.031 \pm 0.016$	EPA-10S	0	-		
Tooele	D-20	$0.011 \pm 0.003$	D-20	$0.085 \pm 0.013$	8.1 ± (7.0, 9.6)		
Tooele	D-20	$0.011 \pm 0.003$	D-23	$0.024 \pm 0.004$	$29 \pm (25, 35)$		
Tooele	D-20	$0.011 \pm 0.003$	D-25	$0.058 \pm 0.005$	$12 \pm (11, 13)$		
Tooele	D-20	$0.011 \pm 0.003$	D-19	0	-		
Hill	U10-043	$0.013 \pm 0.004$	U10-043	$0.006 \pm 0.005$	107 ± (62, 395)		
Hill	U10-025	$0.015 \pm 0.004$	U10-025	$0.011 \pm 0.004$	$63 \pm (45, 106)$		
Hill	U10-025	$0.015 \pm 0.004$	U10-019	$2.652 \pm 0.138$	$0.3 \pm (0.2, 0.3)$		

#### 5.6.2.1 Results for Rate Constants

The net pseudo first-order rate constant for the degradation of <sup>14</sup>C-TCE was determined for experimental bottles that were statistically significant compared to DDI water or FSGW controls, as shown in Table 5.7.2. The net rate constant represents the difference between the degradation of the radioactive material from biotic and/or abiotic factors in the experimental bottles and the auto-degradation of the 14C-TCE stock solution in the control bottles. The likely reason for degradation of the radioactive material in the DDI water controls and consequently, the positive pseudo first-order rate constants (Table 5.7.3) was due to the radiolysis phenomenon.

Briefly, the radiolysis phenomenon occurs when the energy emitted from the radioactive material auto-degrades the radioactive material itself. Therefore, degradation of <sup>14</sup>C-TCE to <sup>14</sup>C products in the DDI water controls would be detectable with the assay developed for this project. Bottles with groundwater that exhibited less accumulation of <sup>14</sup>C products compared to the DDI or FSGW controls may be attributable to constituents in the unfiltered groundwater that quenched the radicals generated from radiolysis of the <sup>14</sup>C-TCE. The quenching of radicals by constituents in unfiltered groundwater could contribute to lower dpm values in the groundwater bottles compared to control bottles.

Site Location	Identification	k (yr <sup>-1</sup> )
ТСААР	IA	$0.032 \pm 0.004$
Plattsburgh	IIA	$0.040 \pm 0.004$
Hopewell	IIIA	$0.027 \pm 0.007$
Tooele	IVA	$0.034 \pm 0.005$
Hill	VA	$0.026 \pm 0.003$

Table 5.7.3. Pseudo First-order Rate Constants for DDI Water Controls Prepared with
Each Respective Group of Groundwater Samples.

In general, the DDI water controls monitored concurrently with the groundwater bottles from a particular site had higher rates of <sup>14</sup>C product accumulation compared to the FSGW controls from wells at that site. There are some exceptions, including the FSGW bottles from 32PTLW12 and EPA-10S, as shown in Figure 5.7.5, which have higher average pseudo first-order rate constants compared to the DDI water controls. It should be noted that not all the experimental wells had accompanying FSGW controls because the FSGW samples were tested as a forethought following evaluation of the groundwater samples. Therefore, there was insufficient additional groundwater to run FSGW controls for each well. When the 11 FSGW controls (M =  $2.56 \times 10^{-2}$  yr<sup>-1</sup>, SD =  $4.40 \times 10^{-4}$  yr<sup>-1</sup>) were compared to the five DDI water controls (M =  $3.18 \times 10^{-1}$ <sup>2</sup> yr<sup>-1</sup>, SD =  $3.08 \times 10^{-5}$  yr<sup>-1</sup>), there was no significant difference (Student's *t*-test, p = 0.53). However, the 32PTLW12 control has a pseudo first-order rate constant that is an extreme outlier (i.e. > [upper quartile +  $(3 \times interquartile range)$ ]) compared to the other 10 FSGW bottles, as depicted in Figure 5.7.6. The outer fence of Figure 5.7.6 was determined to be  $8.2 \times 10^{-2}$  yr<sup>-1</sup> and the rate constant for 32PTLW12 was  $8.4 \times 10^{-2}$  yr<sup>-1</sup>. When this FSGW outlier is excluded (M =  $1.97 \times 10^{-2}$  yr<sup>-1</sup>, SD =  $6.68 \times 10^{-5}$  yr<sup>-1</sup>), a Student's *t*-test indicates that the <sup>14</sup>C product accumulation rate coefficient for DDI water was higher (p = 0.01). Consequently, net rates for calculated by substracting out the rate for the corresponding FSGW sample, not the DDI water control.

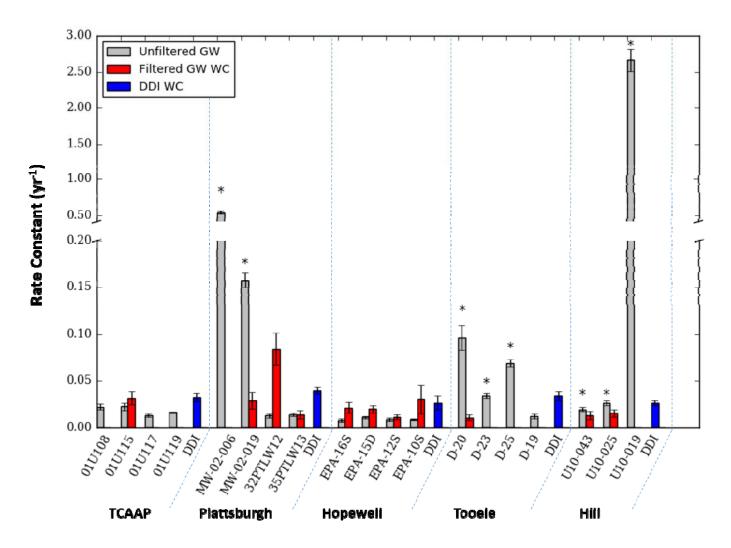


Figure 5.7.5. Average Pseudo First-order Rate Constants for Experimental Wells (gray), FSGW Controls (red), and DDI Water Controls (blue).

*Error bars represent the 95% CI. Asterisks indicate the groundwater samples that were statistically significant compared to their respective FSGW controls.* 

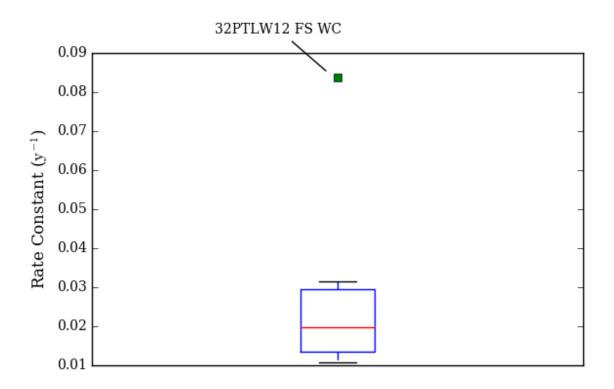


Figure 5.7.6. Boxplot Showing an Extreme Outlier for the Average Pseudo First-order Rate Constant for the FSGW Control from 32PTLW12 at Plattsburgh, Denoted by the Green Square.

The lower whisker represents the smallest first-order rate constant in the lower inner fence  $(Q_1 - 1.5 \times IQR)$ , whereas the upper whisker represents the highest first-order rate constant in the upper inner fence  $(Q_3 + 1.5 \times IQR)$ . The red line indicates the median value for the rate constants. The upper line of the blue box represents the third quartile  $(Q_3)$  and the lower line represents the first quartile  $(Q_1)$ .

Use of FSGW controls instead of DDI water controls was important for several of the well samples. Figure 5.7.5 shows that the average pseudo first-order rate constants for the experimental bottles from U10-043 and U10-025 at Hill and D-23 at Tooele are lower or approximately equal to the DDI water control. Paired *t*-tests comparing U10-043, U10-025, and D-23 to their respective DDI water controls indicates that the differences are not statistically significant. However, comparing the rate constants for the same groundwater samples to their respective FSGW controls indicates that the groundwater pseudo first order rate constants are statistically higher. Therefore, a net rate for U10-043, U10-025, and D-23 can be determined only using the FSGW controls, not the DDI water controls. In general, using the FSGW controls results in a higher net rate for the groundwater, which translates to a shorter half-life. It appears that constituents in the FSGW dampen autoradiolysis of the <sup>14</sup>C-TCE, which would explain the lower rate of <sup>14</sup>C product accumulation compared to DDI water. Therefore, FSGW controls provide a more representative degradation rate constant by accounting for groundwater constituents from a particular site compared to the DDI water controls.

Accumulation of <sup>14</sup>C products in groundwater samples is shown in Figures 5.7.7 - 5.7.11 for sites at which at least one of the wells had a statistically significant pseudo first order rate constant.

Several of the groundwater samples were actually lower than the FSGW and/or DDI water controls (Figure 5.7.5). In particular, the average rate constants for all of the groundwater samples from TCAAP and Hopewell were not statistically different from the respective FSGW controls. The average rate constant value for 32PTLW12 at Plattsburgh was lower than its respective FSGW control. Additionally, the average rate constants for the all experimental wells at TCAAP and Hopewell, as well as 32PTLW12 and 35PTLW13 for Plattsburgh, D-19 for Tooele, and U10-043 from Hill were lower than the DDI water controls.

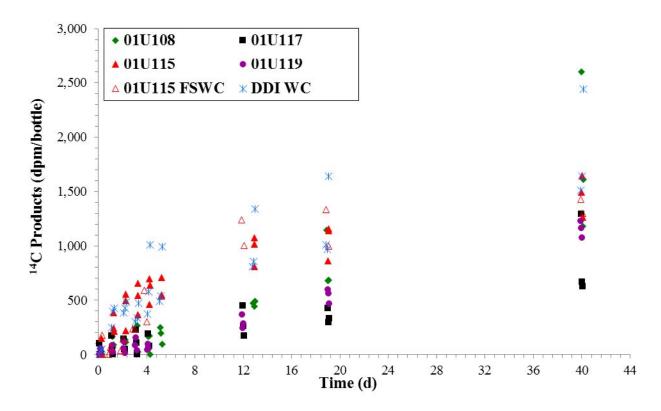


Figure 5.7.7. <sup>14</sup>C Product Accumulation in Samples from TCAAP (color-filled symbols), FSGW Controls (open symbols) and DDI Water Controls (asterisks).

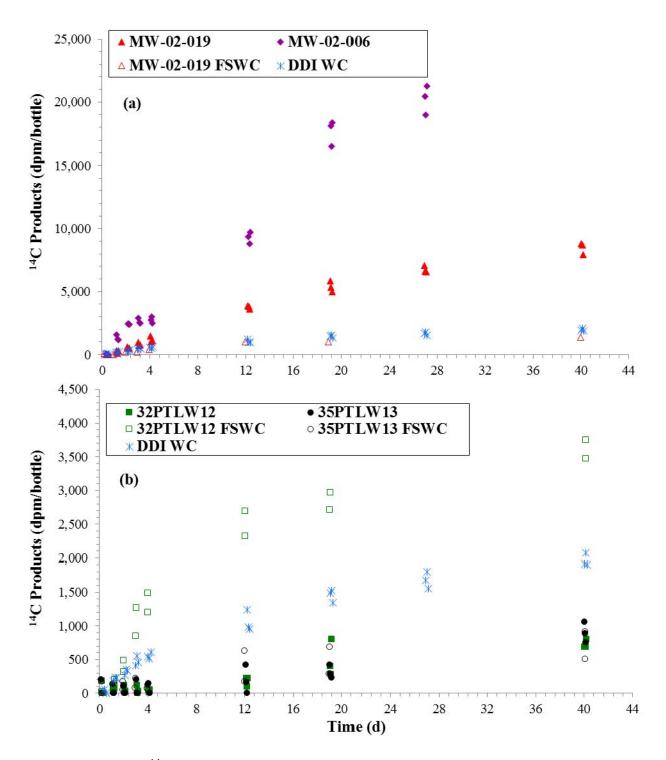


Figure 5.7.8. <sup>14</sup>C Product Accumulation in Samples from Plattsburgh (color-filled symbols), FSGW Controls (open symbols) and DDI Water Controls (asterisks), for Treatments (a) with a Statistically Significant Rate of Co-oxidation and (b) Without.

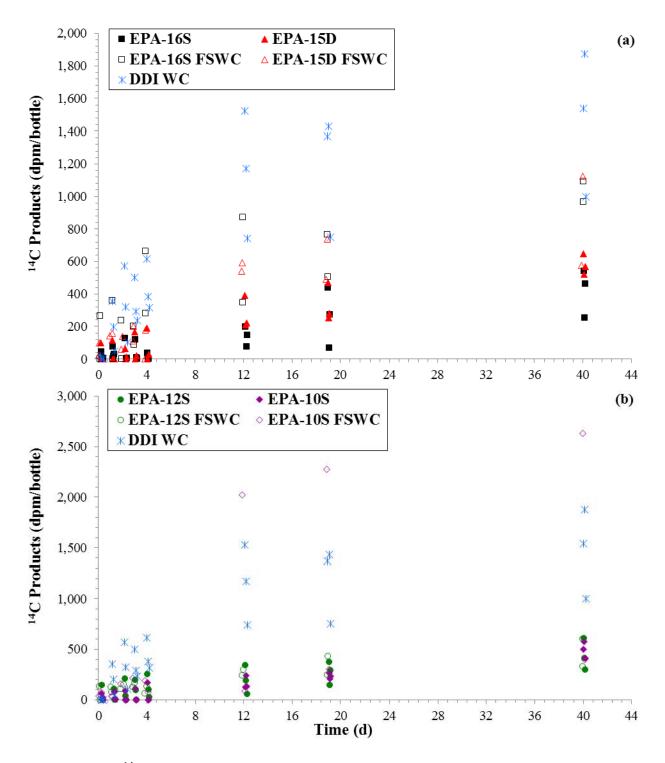


Figure 5.7.9. <sup>14</sup>C Product Accumulation in Samples from Hopewell (color-filled symbols), FSGW Controls (open symbols) and DDI Water Controls (asterisks), for Treatments (a) with a Statistically Significant Rate of Co-oxidation and (b) Without.

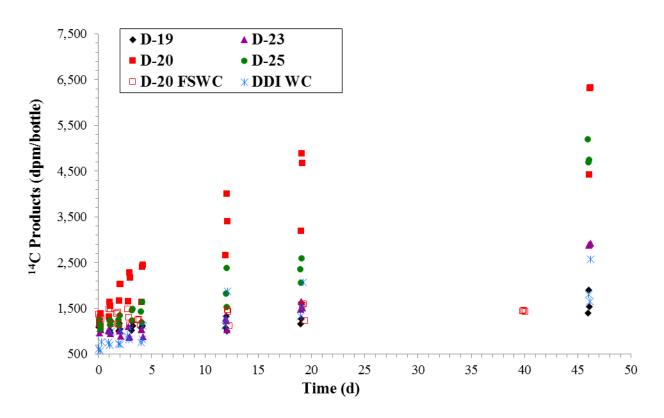


Figure 5.7.10. <sup>14</sup>C Product Accumulation in Samples from Tooele (color-filled symbols), FSGW Controls (open symbols) and DDI Water Controls (asterisks).

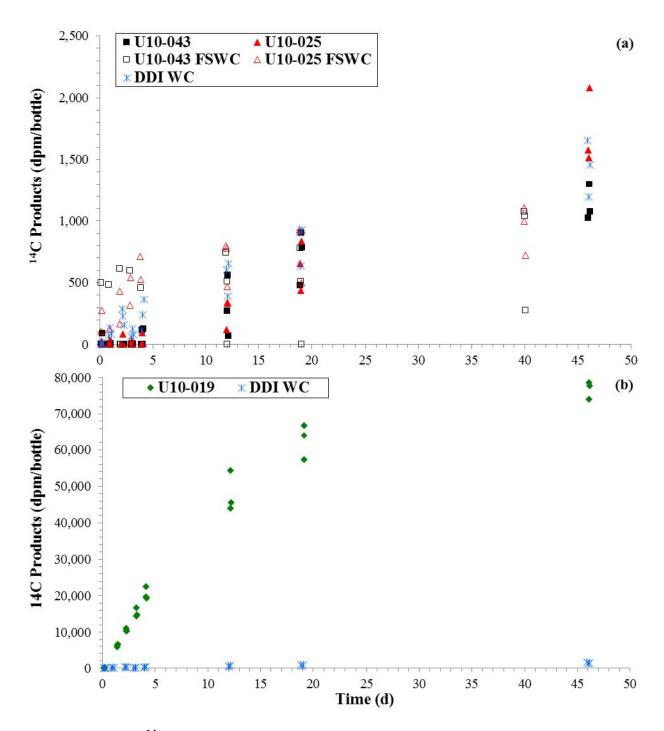


Figure 5.7.11. <sup>14</sup>C product Accumulation in Samples from Hill Air Force Base (colorfilled symbols), FSGW Controls (open symbols) and DDI Water Controls (asterisks), for Treatments (a) with a Statistically Significant Rate of Co-oxidation and (b) Without.

There were eight groundwater samples that had average pseudo first-order rate constants statistically greater than respective FSGW control bottles, as denoted with asterisks in Figure 5.7.5. Additionally, five of those eight wells (MW-02-006, MW-02-019, D-20, D-25, and U10-019) had rate constants that were statistically significant compared to the respective DDI water control for that site. The rate constants from these five wells indicates that biotic activity accounted for the majority of byproduct formation in the groundwater samples.

The pseudo first-order rate constants were determined by fitting a mass balance model for the microcosms to the measured data for <sup>14</sup>C product accumulation. Comparisons of the model fit to the data for each serum bottle with groundwater are shown in Figure 5.7.12 to Figure 5.7.19. Symbols in these figures represent experimental data points collected from triplicate bottles over the monitoring period and lines represent the nonlinear model fit used to determine the average pseudo first-order rate constant. For a number of the bottles, the model overpredicted at the final data point (~day 40). This may have been a consequence of the microbes running out of the resources (e.g., reducing power) needed to sustain the oxygenases, and/or a cumulative toxicity effect caused by reactive byproducts from TCE co-oxidation. In other bottles, the model overpredicted early on; the lag in product accumulation may have had something to do with the microbial population readjusting the temperature shock.

#### 5.6.2.2 End-of-Incubation Results

GC headspace measurements were conducted for groundwater and control bottles at time zero and at the end of the monitoring period using the methodology described previously. The purpose was to confirm the presence of TCE remaining in the bottles after the monitoring period, and to track the fate of other VOCs present in the groundwater samples. The GC chromatographs from Day 0 for several samples indicated the presence of VOCs in addition to TCE. These compounds may have served as primary substrates to induce expression of oxygenase enzymes that are responsible for co-oxidation of <sup>14</sup>C-TCE. Not all groundwater samples had additional VOCs on Day 0 (e.g. D-20 and D-23, Appendix D, Figure D.22). Other wells had significant VOCs in the groundwater at Day 0. GC chromatographs for groundwater samples that had additional VOCs are shown in Appendix D (Figures D.6-D.11). The GC chromatographs for other wells without additional VOCs are not shown. I n the two wells from Plattsburgh that had statistically significant rates of TCE co-oxidation (MW-02-006 and MW-02-019), the non-TCE VOCs were consumed over the monitoring period (Appendix D, Figures D.6-D.11). In the wells from Tooele that had statistically significant rates of TCE co-oxidation (D-20, D-23, and D-25), there were no apparent VOCs present other than TCE; a chromatogram for well D-25 is provided in Appendix D (Figure D.24). In the wells at Hill that exhibited statistically significant rates of TCE co-oxidation (U10-043, U10-025, and U10-019), there was some change in VOC levels over the monitoring period (Appendix D, Figures D.26-D.32). The identity of the peaks was not established. Based on elution the elution times for authenic material, it was possible to rule out vinyl chloride, 1,1-dichloroethene, cDCE, tetrachloroethene, benzene, toluene, ethylbenzene, oxylene, and *p*-xylene. Additional effort to identify the non-TCE VOCs is warrented but was beyond the scope of this project.

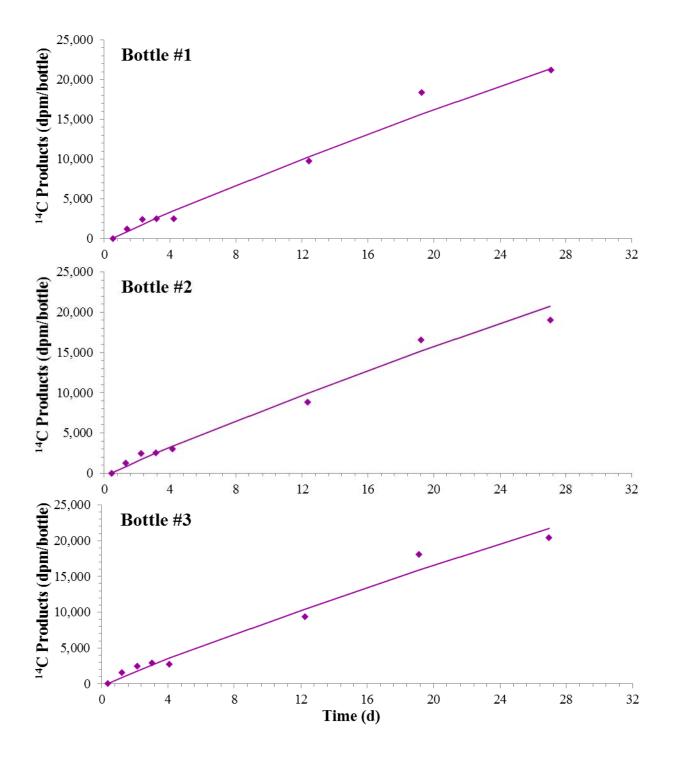


Figure 5.7.12. Comparison of the Measured Accumulation of <sup>14</sup>C Products in Triplicate Serum Bottles of Groundwater from Monitoring Well MW-02-006 at Plattsburgh to the Model Used to Determine k.

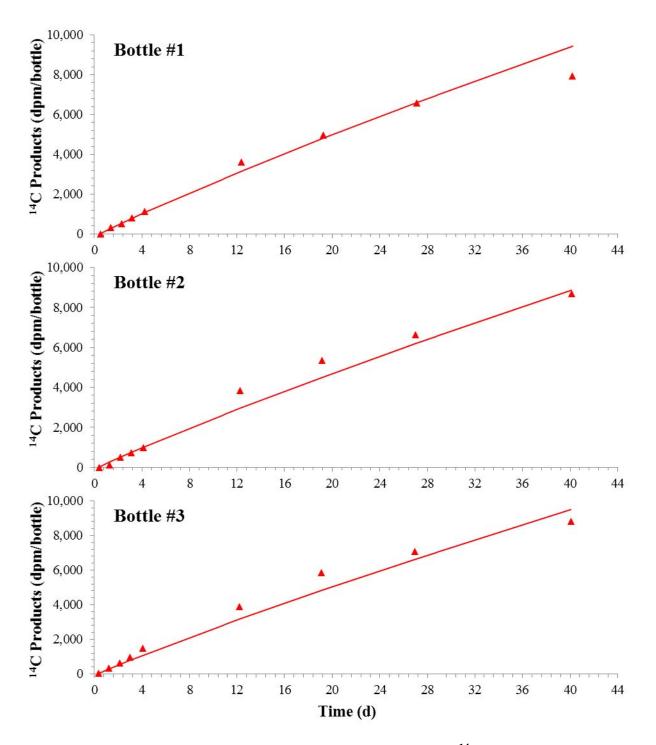


Figure 5.7.13. Comparison of the Measured Accumulation of <sup>14</sup>C Products in Triplicate Serum Bottles of Groundwater from Monitoring Well MW-02-019 at Plattsburgh to the Model Used to Determine k.

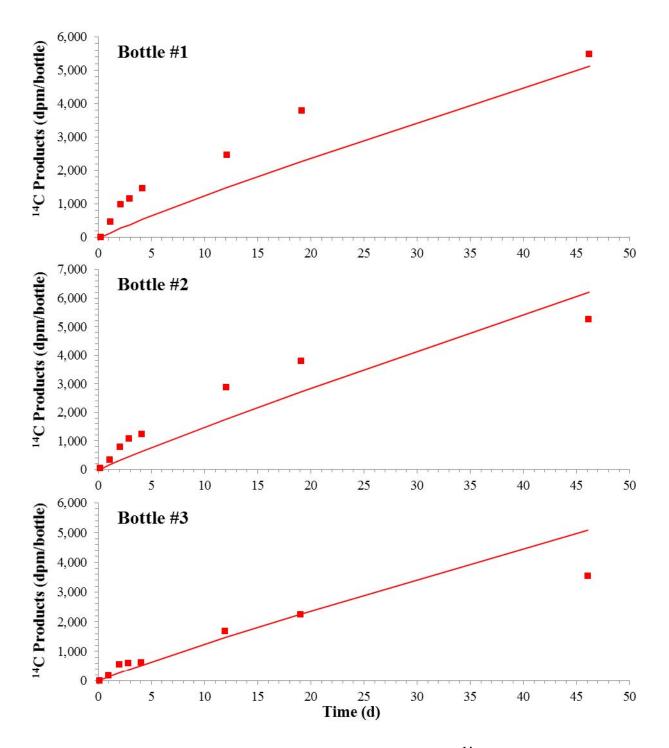


Figure 5.7.14. Comparison of the Measured Accumulation of <sup>14</sup>C Products in Triplicate Serum Bottles of Groundwater from Monitoring Well D-20 at Tooele to the Model Used to Determine k.

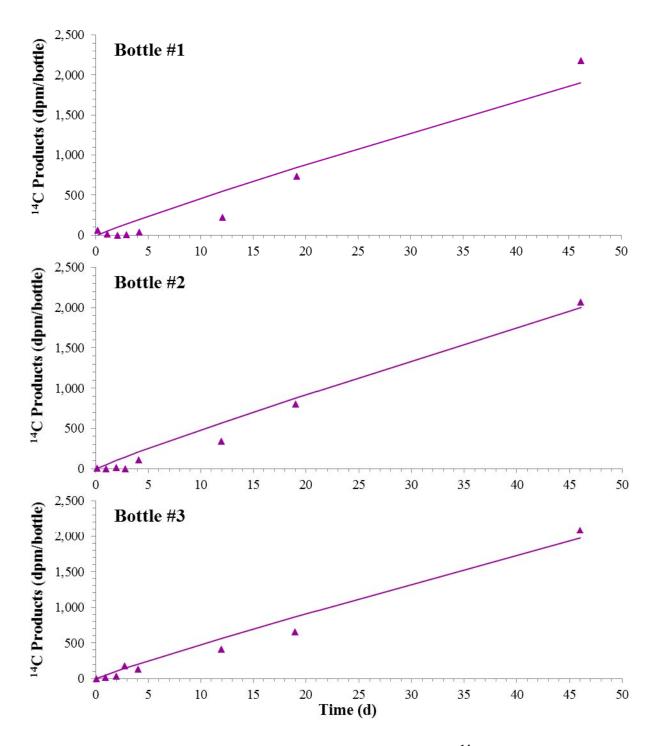


Figure 5.7.15. Comparison of the Measured Accumulation of <sup>14</sup>C Products in Triplicate Serum Bottles of Groundwater from Monitoring Well D-23 at Tooele to the Model Used to Determine k.

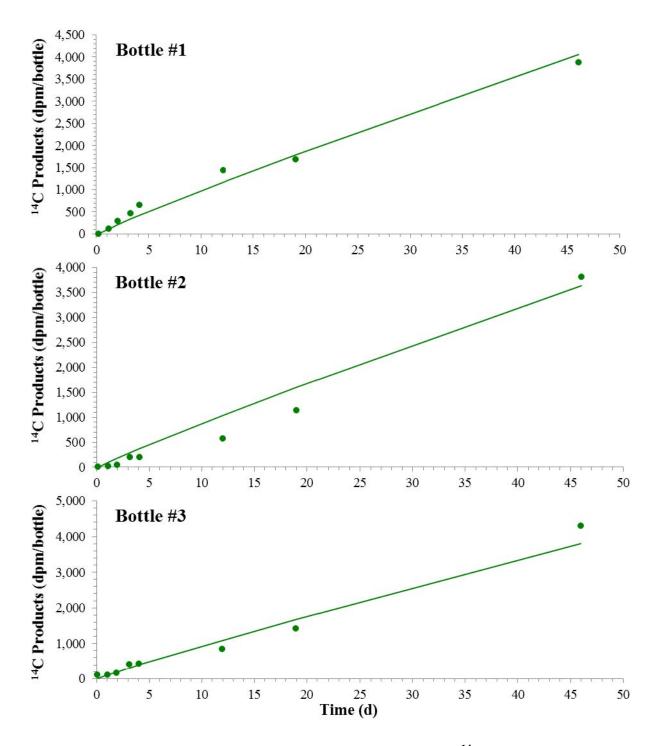


Figure 5.7.16. Comparison of the Measured Accumulation of <sup>14</sup>C Products in Triplicate Serum Bottles of Groundwater from Monitoring Well D-25 at Tooele to the Model Used to Determine k.

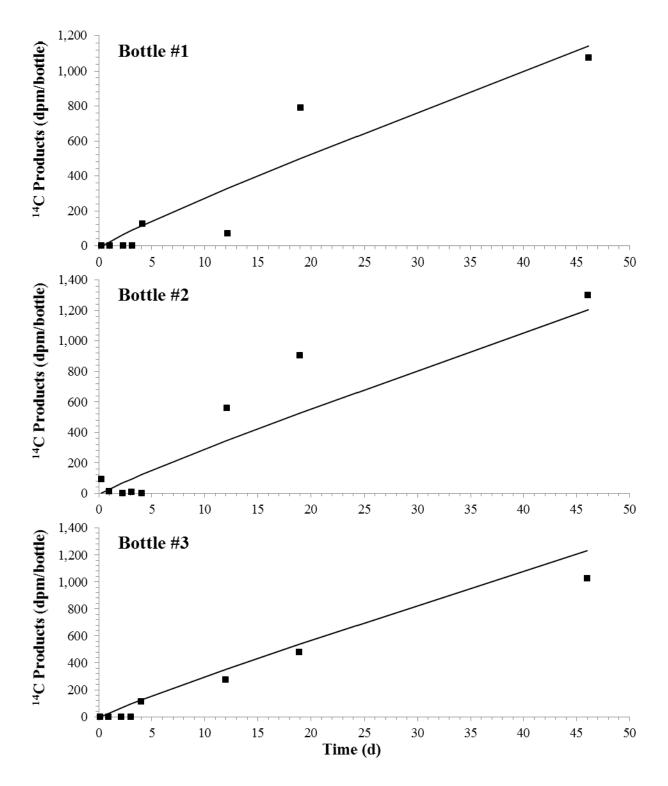


Figure 5.7.17. Comparison of the Measured Accumulation of <sup>14</sup>C Products in Triplicate Serum Bottles of Groundwater from Monitoring U10-043 at Hill AFB to the Model Used to Determine k.

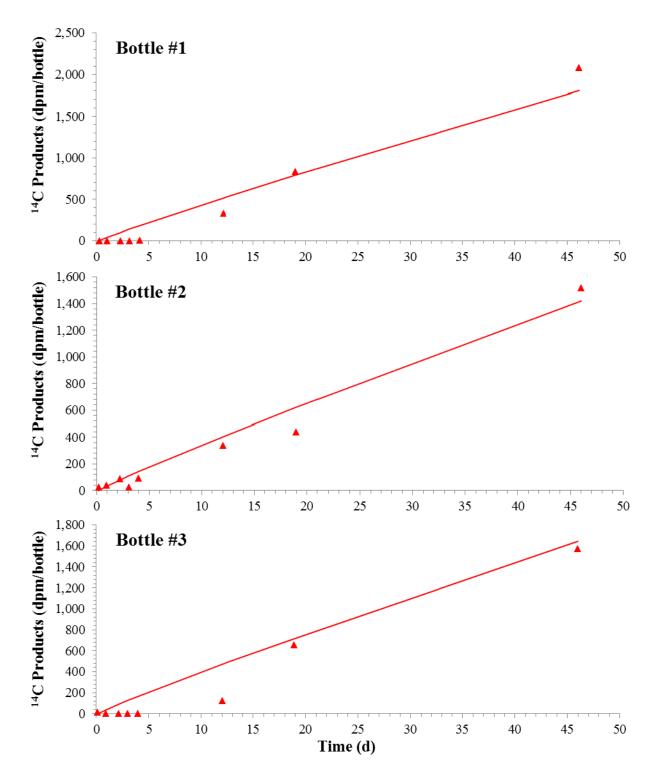


Figure 5.7.18. Comparison of the Measured Accumulation of <sup>14</sup>C Products in Triplicate Serum Bottles of Groundwater from Monitoring U10-025 at Hill AFB to the Model Used to Determine k.

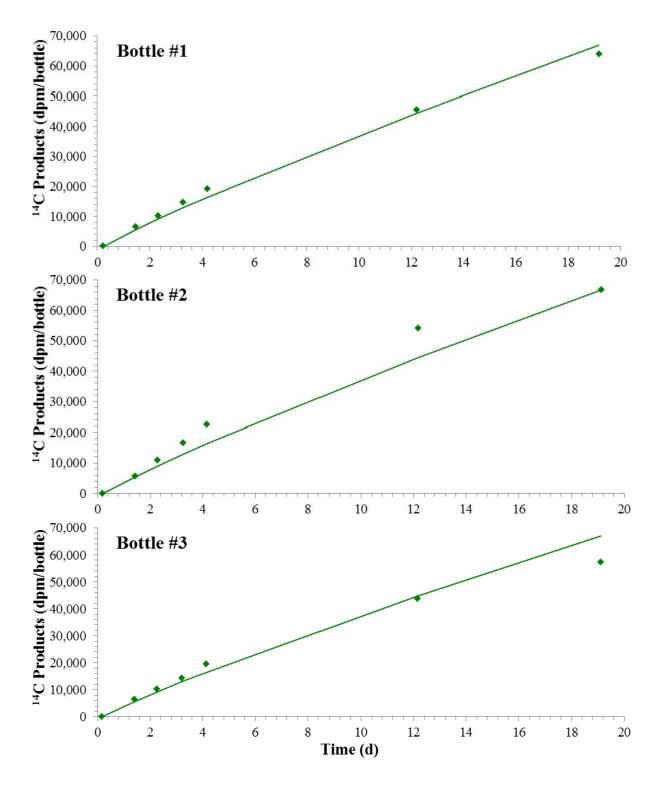


Figure 5.7.19. Comparison of the Measured Accumulation of <sup>14</sup>C Products in Triplicate Serum Bottles of Groundwater from Monitoring U10-019 at Hill AFB to the Model Used to Determine k.

For groundwater bottles that exhibited statistically significant accumulation of <sup>14</sup>C products, additional testing was performed at the end of the monitoring period to determine the percentage of <sup>14</sup>CO<sub>2</sub> and <sup>14</sup>C-NSR that formed. One method utilized barium hydroxide to precipitate the <sup>14</sup>C-carbonate byproducts from alkaline sparged groundwater. The difference between the alkaline sparged sample and centrate following barium hydroxide precipitation was assumed to be the amount of <sup>14</sup>CO<sub>2</sub> in solution. Results based on this method are found in Figure 5.7.20a and Table 5.7.4. The other method involved acidic sparging of the groundwater, which removed <sup>14</sup>C-TCE and <sup>14</sup>CO<sub>2</sub>, leaving only <sup>14</sup>C-NSR. <sup>14</sup>CO<sub>2</sub> was calculated based on the difference between the alkaline and acidic sparged samples. Results are presented in Figure 5.7.20b and Table 5.7.4. There was no statistically significant difference in the percentage of <sup>14</sup>CO<sub>2</sub> determined by both methods (Student's *t*-test, *p*=0.39).

<sup>14</sup>CO<sub>2</sub> was more prevalent as a product than <sup>14</sup>C-NSR in the groundwater samples (Figure 5.7.20), indicating that the groundwater contained a sufficient diversity of microbes to accomplish minerlization of the products from the initial oxygenase attack on TCE. In contrast, the propanotrophic treatments had increasing levels of <sup>14</sup>C-NSR as the dilution increased. This is likely a consequence of propanotrophs lacking the ability to achieve mineralization, plus the low density of non-propanotrophs in the enrichment that possess this capability.

#### 5.6.2.3 Summary

The <sup>14</sup>C-TCE assay allowed for quantification of pseudo first order rate constants in groundwater samples from eight of the 19 wells evaluated, at rates ranging from ranging from 0.00658 to 2.65 yr<sup>-1</sup>. This translates to half-lives of 0.26 to 105 yr. In groundwater from the other 11 wells, the rate of <sup>14</sup>C product accumulation was not statistically different from the FSGW controls, so that no rate is reported. Although only a single GC column was used for purification of the <sup>14</sup>C-TCE, the level of impurities delievered to the serum bottles was sufficiently low to allow for detection of a half-life as long as 105 yr. This was due in part to extension of the incubation period from a few days to as long as 46 days, which permitted accumulation of a sufficient level of <sup>14</sup>C products to be distinguishable from the controls.

The initial plan was to use DDI water as the negative control. It was determined, however, that FSGW is more appropriate for this purpose. The rate of <sup>14</sup>C product accumulation in FSGW controls was statistically lower than in DDI water, likely due to the presence of constitutes that quench the autoradiolysis associated with decay of <sup>14</sup>C-TCE.

<sup>14</sup>CO<sub>2</sub> constituted the majority of the <sup>14</sup>C product quantified, followed by <sup>14</sup>C-NSR. This indicated that the groundwater samples that exhibited co-oxidation of TCE contained microbes with the ability to mineralize the products formed from the initial oxygenase attack on the compound.

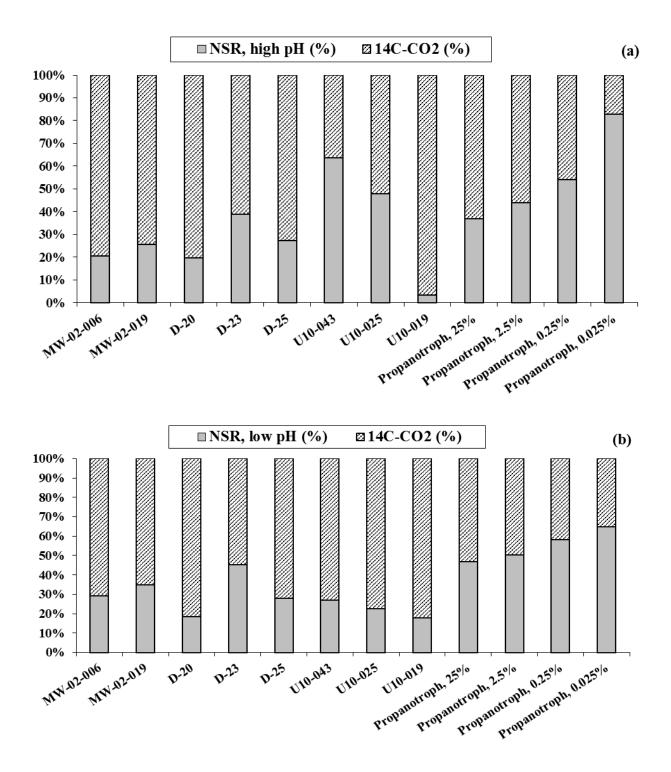


Figure 5.7.20. <sup>14</sup>CO<sub>2</sub> and <sup>14</sup>C-NSR Present at the End of Incubation for Groundwater Samples that Were Statistically Significant Compared to their Respective Controls and the Propanotrophic Dilution Bottles.

*Two methods were used: (a) alkaline sparging followed by barium hydroxide precipitation and (b) acidic sparging method.* 

# Table 5.7.4. Comparison of Methods Used to Determine the Amount of <sup>14</sup>CO2 and<sup>14</sup>C-NSR in the Groundwater Samples with a Statistically Significant k and the<br/>Propanotrophic Cultures.

		Barium Hydroxide		Acidic Sparging	
Site Location	Well	<sup>14</sup> CO <sub>2</sub> (dpm/mL)	NSR, high pH (dpm/mL)	<sup>14</sup> CO <sub>2</sub> (dpm/mL)	NSR, low pH (dpm/mL)
Plattsburgh	MW-02-006	296	76	211	87
Plattsburgh	MW-02-019	113	39	80	43
Tooele	D-20	83	20	65	15
Tooele	D-23	36	23	22	18
Tooele	D-25	59	22	50	19
Hill	U10-043	11	19	20	7
Hill	U10-025	20	18	26	8
Hill	U10-019	1107	37	783	171
-	Propanotroph, 25%	3927	2293	3301	2919
-	Propanotroph, 2.5%	1101	858	744	750
-	Propanotroph, 0.25%	111	130	101	140
-	Propanotroph, 0.025%	9	43	18	33

#### 5.6.3 Sampling Results for EAPs and qPCR

#### 5.6.3.1 Introduction

Microbial metabolism is the means by which a microbe obtains the energy and carbon it needs to live and reproduce. Microbes use many different types of metabolic strategies and species can often be differentiated from each other based on metabolic characteristics. The specific metabolic characteristics of a microbe are the major factors in determining that microbe's ecological niche, and often allow for that microbe to be useful in industrial processes, breaking down anthropogenic compounds, or responsible for biogeochemical cycles. All microbial metabolisms can be arranged according to three groups based on the primary carbon metabolized: (1) autotrophic organisms obtain carbon from carbon dioxide (CO<sub>2</sub>), (2) heterotrophic organisms obtain carbon from organic compounds, and (3) mixotrophic organisms obtain carbon from both organic compounds and by fixing carbon dioxide. Most microbes, particularly environmentally relevant microbes, are heterotrophic, using organic compounds as both carbon and energy sources. These microbes are extremely abundant in nature and are responsible for the breakdown of large organic polymers such as cellulose, chitin or lignin which are generally indigestible to larger organisms. Some heterotrophic organisms are even able to degrade more recalcitrant compounds such as petroleum compounds or pesticides, making them useful in bioremediation.

There is a diversity of compounds that can serve as carbon for microbial metabolism. One subgroup of organisms is those that biodegrade one organic substance to obtain carbon and energy for growth, simultaneously transforming other compounds that cannot be used for growth (Thomas and Ward, 1989). This process is known as cometabolism and it describes the ability of microorganisms to fortuitously transform non-growth-supporting substrates, such as pollutants.

Cometabolic transformations are catalyzed by existing microbial enzymes and yield no carbon or energy benefits to the transforming cells (Horvath, 1972), thus a growth substrate must be available at least periodically to grow new cells, provide an energy source, and induce production of the cometabolic enzymes. Although some studies have found that naturally occurring humic substances (an organic residue of decaying organic matter; Wymore et al., 2007; Lee et al., 2008) and the chlorinated solvents themselves can act as inducers of the cometabolic enzymes, the extent of and time for activation, as well as the mechanism for cell energy and growth in these instances, are poorly understood (Shingleton et al., 1998; Park et al., 2002; Yeager et al., 2004).

Cometabolic processes were first studied in the 1950s and 60s and focused on the microbial degradation of important classes of industrial chemicals including aromatics (Dagley and Pate, 1957), chlorinated organics (Jensen, 1957, 1963), pesticides (Alexander, 1967) and petroleum hydrocarbons (Foster, 1962). Decades of research have concluded that the following compounds are among those that are readily cometabolized: trichloroethene (TCE), dichloroethene (DCE), vinyl chloride (VC), trichloroethane (TCA), dichloroethane (DCA), chloromethane (CM), dichloromethane (DCM), and chloroform (CF) (Vandenwijngaard, 1992; Hartmans, 1985; Hartmans and Debont, 1992; Munakata-Marr, 1997; Vannelli, 1998; McCarty et al., 1998; Braus-Stromeyer, 1993; Gisi, 1998; Edwards and Cox, 1997; McCarty, 1997a; Bradley and Chapelle, 1998; Travis and Rosenberg, 1997). Collectively, these studies established that microorganisms could transform many compounds/contaminants without concurrent microbial growth on those compounds, and the enzymes responsible for these transformations are mono- and dioxygenases.

Oxygenase enzymes in general are a subset of the enzymes classified as oxidoreductases, one of the six major classes of enzymes. Oxygenases serve a myriad of functions in cells including biosynthesis, detoxification, and catabolism (metabolic breakdown of complex compounds). Oxygenases catalyze the reduction of O2 with incorporation of one (monooxygenases) or two (dioxygenases) of the oxygen atoms into the substrate that is being oxidized. In the context of contaminant degradation, the oxygenase reaction generates chlorinated solvent oxidation products that may react with cellular macromolecules or may be hydrolyzed spontaneously into carbon dioxide, chloride, or other non-volatile products that are easily mineralized by microorganisms (Little et al., 1988; Tsien et al., 1989; Oldenhuis et al., 1989; Fox et al., 1990; Nelson et al., 1986, 1987; Rasche et al., 1991). Unlike anaerobic biological reductive dechlorination, aerobic cometabolism does not proceed through sequential dechlorination steps producing daughter products such as DCE, VC, and ethene; thus, signature aerobic degradation products, such as Cl- and CO2, are difficult to attribute to aerobic degradation in situ using geochemistry alone. The end result is that the only evidence for aerobic cometabolism is the disappearance of the contaminants themselves.

Chlorinated solvents and other contaminants can be oxidized by a wide range of oxygenaseexpressing microorganisms including those that utilize methane (Wilson & Wilson, 1985; Strand & Shippert, 1986; Fogel et al., 1986; Little et al., 1988; Tsien et al., 1989; Oldenhuis et al., 1989), propane (Fliermans et al., 1988; Wackett et al., 1989; Phelps et al., 1990; Malachowsky et al., 1994), propene (Ensign et al., 1992; Saeki et al., 1999), isoprene (Ewers et al., 1990), isopropylbenzene (Pflugmacher et al., 1996; Dabrock et al., 1992; Kesseler et al., 1996), toluene (Nelson et al., 1986;Wackett et al., 1988; Zylstra et al., 1989; Shields et al., 1989), phenol (Folsom et al., 1990; Harker & Kim, 1990; Segar, 1995), butane (Kim et al., 1997; 2000), ethene and ethane (Freedman & Herz, 1996; Koziollek et al., 1999), and ammonia (Arciero et al, 1989; Vannelli et al., 1990; Rasche et al., 1991; Hyman et al., 1995) as energy and/or carbon sources. Representative cultured organisms, their primary growth substrates, and kinetic data with regards to TCE are included in Table 5.7.5 (modified from Arp review 2001). The enzyme responsible for TCE oxidation in these organisms is also listed. The majority of these organisms are capable of growth on many substrates, several of which may stimulate expression of the TCE-degrading oxygenase enzymes. While some oxygenase enzymes are very specific for particular substrates, others oxygenase enzymes have remarkably broad substrate ranges. It is important to note that the TCE oxidation rates presented in Table 5.7.5 are based on cultured organisms maintained and evaluated under controlled laboratory settings, and as such may not reflect the true potential for degradation under field conditions.

In order to monitor aerobic cometabolism given the challenge of monitoring the process through groundwater chemistry, subsurface microbial communities have been interrogated using validated biomarkers including enzyme activity probes (EAP) and quantitative polymerase chain reaction (qPCR). EAPs have been applied at almost 20 contaminated sites that are oxic for their reliability, reproducibility and sensitivity in evaluating aerobic cometabolic enzymes, while qPCR has been evaluated for at least a subset of the potential aerobic oxygenase genes (McDonald et al., 1995; Baldwin et al., 2003; 2005; 2008; 2009; Bowman et al., 1993; Hendricks et al., 2006a; 2006b; Domiguez et al., 2008). These approaches provide information about both the presence of the genes of interest, which is important if evaluating the potential for enhanced attenuation of the contaminant in situ, and the activity of the oxygenases, which is important in evaluating degradation capacity and long-term sustainability. When these technologies are simultaneously evaluated and compared with more traditional approaches such as geochemical analyses, they provide a comprehensive assessment that can potentially quantitatively relate the qPCR and EAP results to contaminant biotransformation.

Several methods assess the in-situ activity of microbes in the subsurface (Keift and Phelps, 1997); however, these methods can be time consuming and frequently provide overestimates of the actual rates of activity (Phelps et al., 1994). The recent design of a suite of EAPs has permitted the determination of specific aerobic cometabolism of chlorinated ethenes, most notably TCE. EAPs that serve as alternate substrates for TCE cometabolizing enzymes have been developed for four separate aromatic oxygenases (Keener et al., 1998; 2001; Miller et al., 2001; Clingenpeel et al., 2005), and for the soluble methane monooxygenase (SMMO; Miller et al., 2001). Specific EAP and the targeted co-metabolic enzymes are shown in Table 5.7.6. These non-fluorescent probes are transformed by the enzymes into a quantifiable fluorescent signal upon transformation, thus providing direct evidence of cometabolic enzyme activity. Enzyme probes have been evaluated at a number of DOE and DOD sites over the last five years (Lee et al., 2005; Lee et al., 2007; Wymore et al., 2007). Based on these analyses of contaminated groundwater, ranging in TCE concentrations from <100 µg/L to over 10,000 µg/L, it appears that enzyme probes provide a direct estimate of aerobic cometabolic enzyme activity for subsurface populations. Application of EAP's at contaminated sites can provide valuable information regarding the presence and activity of in situ microbial enzyme systems important for aerobic cometabolism for plume-wide assessment of intrinsic assessment of degradation.

Growth Substrate	Organism	Enzyme	TCE oxidation rate (nmol min-1 mg of protein -1)	Reference
Ethene/	Xanthobacter Py2	Alkene	8.6	Ensign, 1992; Reij, 1995
propene		monooxygenase	16-95	
Propene	Rhodococcus corallimus	Alkene monooxygenase	2.4	Saeki, 1999
Isopropylben zene	Pseudomonas sp strain JP1 Rhodococcus erythropolis BD2	Isopropylbenzene dioxygenase; Toluene dioxygenase	0.5-2	Pflugmacher et al., 1996; Dabrock et al., 1992; Kesseler et al., 1996
Ammonia	Nitrosomonas europaea	Ammonia monooxygenase	10.9	Bedard, 1989; Ely, 1995b; Hyman, 1995; Rasche, 1991
Phenol	JMP 134	Phenol monooxygenase	0.2	Harker , 1990
Butane	Pseudomonas butanavora	Butane monooxygenase	.06	Hamamura, 1997
Propane	Mycobacterium vaccae JOB5	Propane monooxygenase		Wackett, 1989
Methane	Methylosinus trichosporium OB3b	Particulate methane monooxygenase	4.1	DiSpirito, 1992; Lontoh, 1998
Methane	Methylosinus trichosporium OB3b	Soluble methane monooxygenase	16.6 37.5	Koh, 1993; Oldenhuis, 1989; 1991; Tsien, 1989
Methane	Methylosinus methanica	Soluble methane monooxygenase	38.8	Koh, 1993
Toluene	Pseuodomonas putida F1	Toluene dioxygenase	8 1.8 0.5	Heald, 1994; Leahy, 1996; Wackett, 1988; Zylstra, 1989
Toluene	Burkholderia cepacia G4	Toluene-2- monooxygenase	8 10 9 3	Folsom, 1990; Landa, 1994; Leahy, 1996; Shields, 1991
Toluene	Pseuodomonas mendocina KR1	Toluene-4- monooxygenase	20 2.4	Leahy, 1996; Winter 1989
Toluene	Ralstonia pickettii PK01	Toluene-3- monooxygenase	2.4	Leahy, 1996

## Table 5.7.5. Cometabolic Enzyme Systems with Respective Organisms and TCE Oxidation Rates.

Probe	Pathway
3-hydroxyphenylacetylene	toluene-2-monooxygenase
(3HPA)	toluene-3-monooxygenase
	toluene-2,3-dioxygenase
Phenylacetylene (PA)	toluene-2,3-dioxygenase
	toluene-3-monooxygenase
	toluene-2-monooxygenase
3-ethynylbenzoate	toluene-side-chain-monooxygenase
trans-cinnamonitrile (CINN)	toluene-2,3-dioxygenase
Coumarin, naphthalene	Soluble methane monooxygenase

#### Table 5.7.6. EAP and Targeted Oxygenases/ Pathways

#### 5.6.3.2 Results

#### 5.6.3.2.1 Enzyme Activity Probes:

Enzyme activity probes (EAP) have been developed for four separate toluene oxygenases (Keener et al. 1998; Keener et al. 2001; Kauffman et al. 2003) and for the soluble methane monooxygenase (SMMO) (Miller et al. 2002) all five of which can be fluorescently monitored. The probes consist of non-fluorescent compounds ("substrates") that are transformed by specific oxygenases into strongly fluorescent products. A clear, quantifiable signal (i.e., fluorescence) can be detected only when the targeted enzyme is actively functioning. As TCE can be cometabolically degraded by these aforementioned oxygenases, quantifying bacterial enzyme activity provides insight into the microbial capacity of a given samples to break down TCE as has been previously described (Lee et al. 2008).

The quantitative processing of samples for probe activity includes collecting 20 random fields (or appropriate number of fields to count a minimum 200 total cells) with a microscope-attached digital camera. Labeled (fluorescent) cells are counted to estimate the activity in the original sample in standard reporting units (cells/mL). The resulting mean and standard deviations for all of the data generated was recorded using three different enzyme probes, this data is reflected in Table 5.7.7.

#### 5.6.3.2.2 Quantitative Polymerase Chain Reaction:

qPCR is a means to quantify the abundance of DNA in a given sample. For this work we quantified the abundance of bacteria that encoded one of five oxygenase genes. In total 200 ml of groundwater from the 76 samples representing 19 wells were vacuum filtrated onto 0.22 micron filters. For each filter 1/8 of the total surface area was processed using the Mo Bio Powersoil DNA extraction kit. DNA was subsequently analyzed after purification using a nanodrop spectrophotometer. From a 100 uL final DNA elution volume, 1 uL was analyzed by SYBR Green qPCR (see below).

#### Table 5.7.7. EAP Counting Data.

DAPI- total cell counts. PA (T2-mono)- phenylacetylene and 3HPA (T3-mono)- 3-hydroxyphenylacetylene target toluene-2-monooxygenase and toluene-3-monoxygenase, respectively. CINN (T23-di)-trans-cinnamonitrile targets toluene-2,3-dioxygenase

	DAPI (total)	Standard	PA (T2-mono)	Standard	Cinn (T23-di)	Standard	3HPA (T3-mono)	Standard
Sample ID	cells/ml	Error	cells/ml	Error	Cells/ml	Error	cells/ml	Error
01U119	7.11E+05	4.29E+04	1.38E+03	8.37E+02	1.55E+03	1.06E+03	5.31E+03	2.80E+03
01U108	6.91E+05	4.64E+04	2.03E+03	1.21E+03	5.46E+02	4.89E+02	2.36E+03	1.67E+03
01U117	4.07E+05	2.36E+04	4.06E+02	4.06E+02	4.55E+02	3.42E+02	5.91E+02	4.85E+02
01U115	5.85E+05	2.90E+04	1.41E+05	1.49E+04	1.52E+05	1.66E+04	1.91E+05	1.51E+04
MW-02-006	1.12E+06	7.19E+04	4.01E+04	8.49E+03	1.43E+04	4.53E+03	2.47E+04	6.28E+03
MW-02-019	1.39E+05	7.82E+03	1.50E+03	8.72E+02	7.13E+02	4.71E+02	2.02E+03	9.37E+02
32PTLW12	1.69E+05	1.03E+04	2.27E+03	1.06E+03	1.76E+03	1.04E+03	1.46E+03	8.88E+02
35PTLW13	3.94E+05	2.91E+04	8.39E+02	6.81E+02	9.25E+02	7.88E+02	9.84E+02	6.40E+02
EPA-10S	1.15E+05	5.67E+03	6.82E+02	5.20E+02	2.91E+02	2.62E+02	1.11E+03	6.33E+02
EPA-12S	1.25E+05	6.35E+03	3.05E+03	1.12E+03	1.74E+03	8.30E+02	2.29E+03	8.97E+02
EPA-15D	3.22E+05	1.95E+04	9.68E+03	2.85E+03	5.51E+03	2.12E+03	1.00E+04	3.01E+03
EPA-16S	1.81E+05	9.16E+03	8.63E+03	2.58E+03	7.09E+03	2.16E+03	1.31E+04	2.83E+03
D-20	4.18E+05	2.50E+04	2.84E+03	1.57E+03	1.00E+03	8.88E+02	2.62E+03	1.11E+03
D-23	6.28E+05	4.50E+04	6.61E+03	2.91E+03	4.05E+03	2.01E+03	5.58E+03	2.29E+03
D-25	6.01E+05	4.20E+04	1.46E+03	1.12E+03	6.37E+02	5.24E+02	2.53E+03	1.35E+03
D-19	6.46E+05	3.80E+04	3.17E+03	1.71E+03	2.82E+03	1.20E+03	1.60E+03	1.14E+03
U10-043	1.97E+05	1.18E+04	8.80E+02	6.25E+02	3.03E+02	2.28E+02	7.87E+02	4.11E+02
U10-025	2.66E+05	1.15E+04	3.79E+02	3.19E+02	7.58E+01	7.58E+01	6.05E+02	4.35E+02
U10-019	1.21E+06	5.60E+04	5.73E+03	2.67E+03	5.40E+03	2.84E+03	3.12E+03	2.04E+03

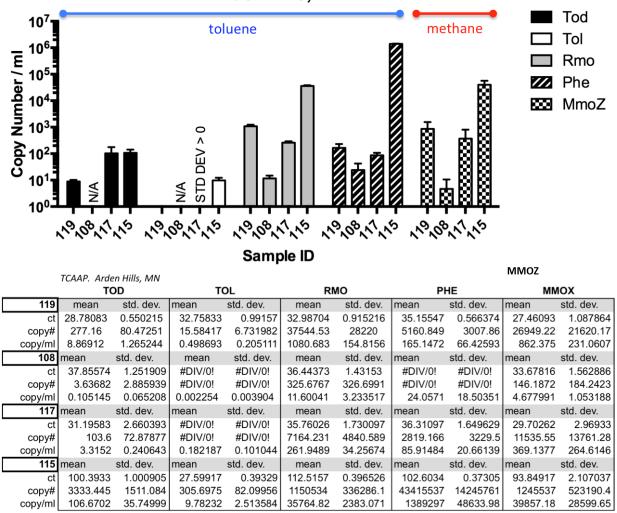
Four qPCR primer pairs specific to four types of toluene monoxygenases and one primer pair specific to methane monooxygenase were assessed (Table 5.7.8). Reference organisms within our laboratory inventory known to encode these enzymes served as positive controls and were also incorporated into our assays to accurately quantify enzyme copy numbers for our groundwater samples. Based on previous literature (McDonald et al. 1995; Baldwin et al. 2003) these primer pairs were predicted to have target gene specificity, however the published mmoX primer sequence gave robust positive readings in our negative control samples ( $C_t$  values ~24). Further analysis revealed that the mmoX primer reverse sequence was self-dimerizing and was the likely reasons for qPCR false positives. Additional analysis using a different sequence from the enzyme DNA expression cassette (*mmoZ* gene) gave little background and high specificity and is therefore used in subsequent data results.

Table 5.7.8. qPCR Primer Pairs and Reference Organisms
--

		qPCR or PCR
Organism	Oxygenase of interest	primers
Pseudomonas putida F1	Toluene 2,3 dioxygenase	TOD
Ralstonia pickettii PKO1	Toluene 3-monooxygenase	RMO, PHE
Burkholderia cepacia G4	Toluene 2-monooxygenase	PHE
Pseudomonas putida mt-2	Toluene side chain monooxygenase	TOL
Methylosinus trichosporium OB3b	Soluble methane monooxygenase	mmoX, mmoZ*

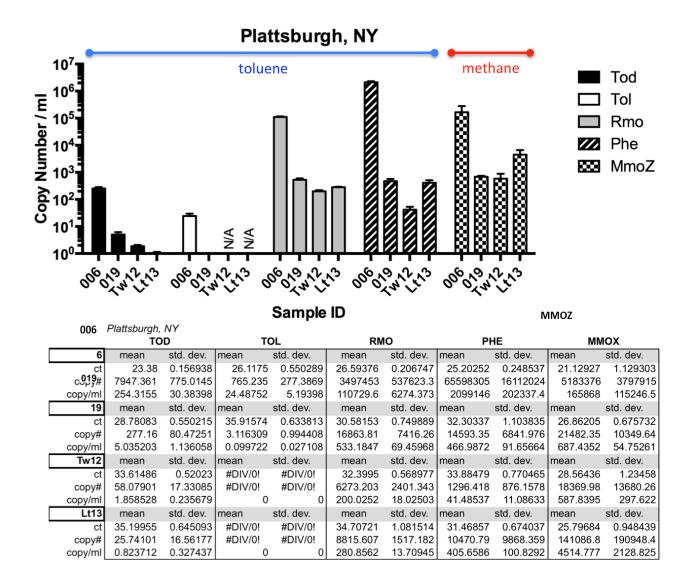
\* denotes mmoZ primer pairs were later used after failure of mmoX.

Outlined in Figures 5.7.21 through 5.7.25 are the results for the five oxygenase primer sets based on sample location. Values that contain "#DIV/0!" represent one or multiple samples in which DNA was below detection limits giving zero values in our calculations.

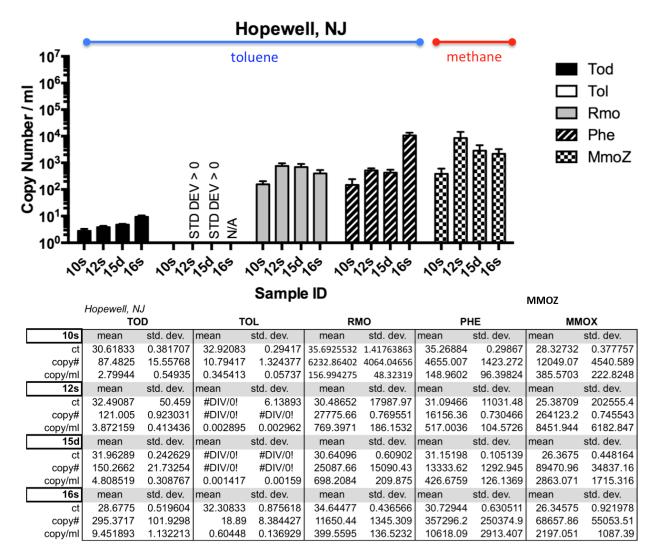


#### Arden Hills, MN

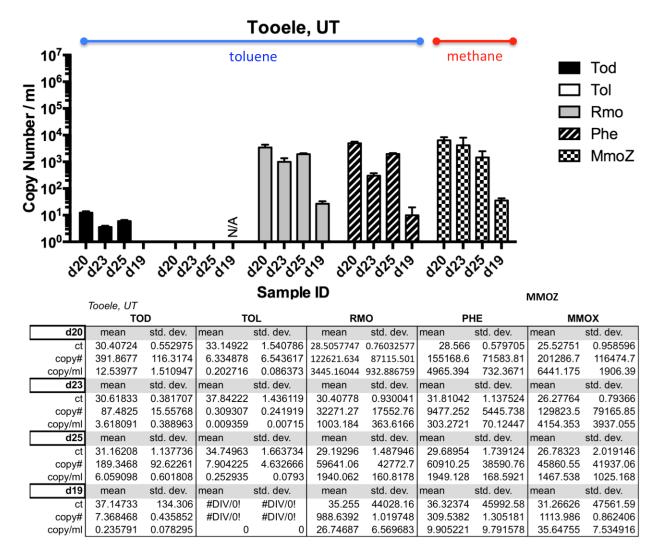
#### Figure 5.7.21. qPCR Results for the Arden Hills, MN Site for Samples Wells TCAAP01U119 (119), TCAAP01U108 (108), TCAAP01U117 (117), TCAAP01U115 (115).



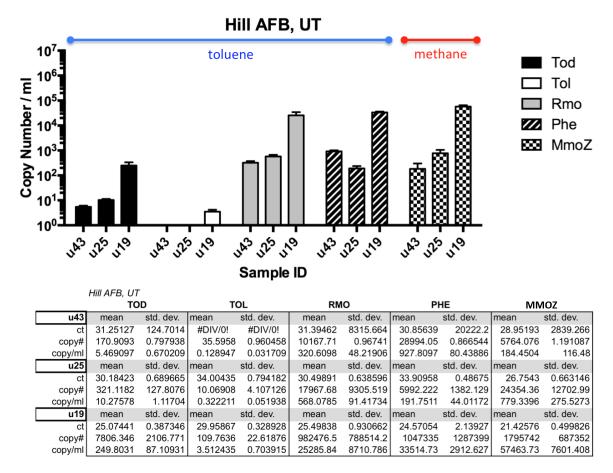
#### Figure 5.7.22. qPCR Results for the Plattsburgh, NY Site for Samples Wells Plattsburgh MW-02-006 (006), Plattsburgh MW-02-019 (019), Plattsburgh 32PLTW12 (Tw12), Plattsburgh 35PTL13 (Lt13).



#### Figure 5.7.23. qPCR Results for the Hopewell, NJ Site for Samples Wells Hopewell EPA-10S (10s), Hopewell EPA-12S (12s), Hopewell EPA-15D (15d), and Hopewell EPA-16S (16s).



#### Figure 5.7.24. qPCR Results for the Tooele, UT Site for Samples Wells Tooele D-20 (d20), Tooele D-23 (d23), Tooele D25 (d25) and Tooele D19 (d19).



#### Figure 5.7.25. qPCR Results for the Hill Air Force Base, UT Site for Samples Wells HillAFB U10-043 (u43), HillAFB U10-025 (u25), HillAFB U10-019 (u19).

Standard deviations reflect the average Ct values of qPCR run in triplicate for each of the four samples for a given well. Values that contain "#DIV/0!" represent one or multiple samples in which DNA was below detection limits giving zero values in our calculations.

#### 5.6.3.2.3 Comparison of qPCR and EAP Results:

When comparing qPCR data with fluorescent EAP data, similarities emerged for the most abundant samples (Fig. 5.7.26 - 5.7.29). This indicates that the qPCR primer sets amplified DNA that was associated with enzymes in the cells that could cooxidize TCE. For example, sample Plattsburgh MW-02-006 from the Plattsburgh, NY site had the most abundant oxygenase counts when cumulatively adding the results from all five primer sets (Fig. 5.7.26, left). The PHE primer set specific to Toluene 3-monooxygenase and Toluene 2-monooxygenase contributed the most qPCR signal to the overall counts (Fig. 5.7.26, middle). In comparison to DAPI fluorescent staining which measures the abundance of bacteria, MW-02-006 gave the second highest counts of the samples. These results show good agreement between samples for MW-02-006. Additionally, sample HillAFB U10-019 from Hill Air Force Base, UT was third highest through qPCR assays versus but the most abundant bacteria in DAPI fluorescent staining.

	qPCR	copy # all 5		qPCR	PHE primer		EAP	DAPI (total)	
	Sample ID		rank	Sample ID		rank	Sample ID	cells/ml	rank
	01U119	2118		01U119	165		01U119	7.11E+05	3
Arden Hills, MN	01U108	40		01U108	24		01U108	6.91E+05	
	01U117	720		01U117	86		01U117	4.07E+05	
	01U115	1465036	2	01U115	1389297	2	01U115	5.85E+05	
	MW-02-006	2376022	1	MW-02-006	2099146	1	MW-02-006	1.12E+06	2
	MW-02-019	1693		MW-02-019	467		MW-02-019	1.39E+05	
Plattsburgh, NY	32PTLW12	831		32PTLW12	41		32PTLW12	1.69E+05	
	35PTLW13	5202		35PTLW13	406		35PTLW13	3.94E+05	
	EPA-10S	695		EPA-10S	149		EPA-10S	1.15E+05	
Hopewell, NJ	EPA-12S	9742		EPA-12S	517		EPA-12S	1.25E+05	
nopewen, no	EPA-15D	3993		EPA-15D	427		EPA-15D	3.22E+05	
	EPA-16S	13225		EPA-16S	10618		EPA-16S	1.81E+05	
	D-20	14864		D-20	4965		D-20	4.18E+05	
Tooele, UT	D-23	5464		D-23	303		D-23	6.28E+05	
	D-25	5363		D-25	1949		D-25	6.01E+05	
	D-19	73		D-19	10		D-19	6.46E+05	
	U10-043	1438		U10-043	928		U10-043	1.97E+05	
Hill AFB, UT	U10-025	1550		U10-025	192		U10-025	2.66E+05	
	U10-019	116518	3	U10-019	33515	3	U10-019	1.21E+06	1

#### Figure 5.7.26. qPCR Copy Number Counts (left, middle) versus DAPI Nuclear Staining Counts (right).

*The top 3 highest samples are ranked.* 

When analyzing qPCR primers specific to toluene-2-monooxygenase (PHE primers) (Fig. 5.7.27, left) versus enzyme fluorescent activity (Fig. 5.7.27, right), there was good agreement with the top 3 sample wells.

Toluene-2-monooxygenase							
qPCR	Josh P.	PHE pr EA	NP	Joe M.	PA (T2-mono)		
	Sample ID		rank	Sample ID	cells/ml	rank	
	01U119	1081		01U119	1.38E+03		
Arden Hills, MN	01U108	12		01U108	2.03E+03		
	01U117	262		01U117	4.06E+02		
	01U115	35765	2	01U115	1.41E+05	1	
	MW-02-006	110730	1	MW-02-006	4.01E+04	2	
Plattsburgh, NY	MW-02-019			MW-02-019			
Flattsbulgh, N	32PTLW12			32PTLW12			
	35PTLW13			35PTLW13			
	EPA-10S	157		EPA-10S	6.82E+02		
Hopewell, NJ	EPA-12S	769		EPA-12S	3.05E+03		
	EPA-15D	698		EPA-15D	9.68E+03		
	EPA-16S	400		EPA-16S	8.63E+03		
	D-20	3445		D-20	2.84E+03		
Tooele, UT	D-23	1003		D-23	6.61E+03		
	D-25	1940		D-25	1.46E+03		
	D-19	27		D-19	3.17E+03		
	U10-043	321		U10-043	8.80E+02		
Hill AFB, UT	U10-025	568		U10-025	3.79E+02		
	U10-019	25286	3	U10-019	5.73E+03	3	

#### Figure 5.7.27. qPCR Copy Number Counts (left) Versus PA Fluorescent Activity

#### Assay (right).

The top 3 highest samples are ranked.

When analyzing qPCR primers specific to toluene-3-monooxygenase (both PHE primers and RMO primers) (Fig. 5.7.28, left, middle) versus 3HPA enzyme fluorescent activity (Fig. 5.7.28, right), there was good agreement for 3 of the top 4 sample wells.

	qPCR	PHE primer		qPCR	RMO primer		EAP	3HPA (T3-mono)	
	Sample ID	1	rank	Sample ID		rank	Sample ID	cells/ml	rank
Arden Hills.	01U119	1081		01U119	165		01U119	5.31E+03	
MN	01U108	12		01U108	24		01U108	2.36E+03	
	01U117	262		01U117	86		01U117	5.91E+02	
	01U115	35765	2	01U115	1389297	2	01U115	1.91E+05	1
	MW-02-006	110730	1	MW-02-006	2099146	1	MW-02-006	2.47E+04	2
Plattsburgh, 3	MW-02-019	533		MW-02-019	467		MW-02-019	2.02E+03	
	32PTLW12	200		32PTLW12	41		32PTLW12	1.46E+03	
	35PTLW13	281		35PTLW13	406		35PTLW13	9.84E+02	
	EPA-10S	157		EPA-10S	149		EPA-10S	1.11E+03	
	EPA-12S	769		EPA-12S	517		EPA-12S	2.29E+03	
	EPA-15D	698		EPA-15D	427		EPA-15D	1.00E+04	4
Hopewell, N	EPA-16S	400		EPA-16S	10618	4	EPA-16S	1.31E+04	3
	D-20	3445	4	D-20	4965		D-20	2.62E+03	
	D-23	1003		D-23	303		D-23	5.58E+03	
Tooele, UT	D-25	1940		D-25	1949		D-25	2.53E+03	
	D-19	27		D-19	10		D-19	1.60E+03	
	U10-043	321		U10-043	928		U10-043	7.87E+02	
	U10-025	568		U10-025	192		U10-025	6.05E+02	
Hill AFB, UT	U10-019	25286	3	U10-019	33515	3	U10-019	3.12E+03	

Figure 5.7.28. qPCR Copy Number Counts (left, middle) Versus 3HPA T3-mono Fluorescent Activity Assay (right).

The top 4 highest samples are ranked.

When analyzing qPCR primers specific to toluene-2,3-monooxygenase (TOD primers) (Fig. 5.7.29, left) versus 3HPA enzyme fluorescent activity (Fig. 5.7.29, right), there was good agreement for 3 of the top 4 sample wells.

Toluene-2,3-monooxygenase						
	qPCR	TOD primer		EAP	Cinn (T23-di)	
	Sample ID		rank	Sample ID	Cells/ml	rank
	01U119	8.87		01U119	1.55E+03	
Arden Hills, MN	01U108	0.11		01U108	5.46E+02	
	01U117	3.32		01U117	4.55E+02	
	01U115	106.67	3	01U115	1.52E+05	1
Plattsburgh, NY	MW-02-006	254.32	1	MW-02-006	1.43E+04	2
	MW-02-019	5.04		MW-02-019	7.13E+02	
	32PTLW12	1.86		32PTLW12	1.76E+03	
	35PTLW13	0.82		35PTLW13	9.25E+02	
	EPA-10S	2.80		EPA-10S	2.91E+02	
Hopewell, NJ	EPA-12S	3.87		EPA-12S	1.74E+03	
	EPA-15D	4.81		EPA-15D	5.51E+03	
	EPA-16S	9.45		EPA-16S	7.09E+03	3
	D-20	12.54	4	D-20	1.00E+03	
Tooele, UT	D-23	3.62		D-23	4.05E+03	
	D-25	6.06		D-25	6.37E+02	
	D-19	0.24		D-19	2.82E+03	
UNILACE UT	U10-043	5.47		U10-043	3.03E+02	
Hill AFB, UT	U10-025	10.28		U10-025	7.58E+01	
	U10-019	249.80	2	U10-019	5.40E+03	4

Figure 5.7.29. qPCR Copy Number Counts (left) versus CINN (T2,3-di) Fluorescent Activity Assay (right).

The top 4 highest samples are ranked.

#### 5.6.3.3 Summary

Quantitative polymerase chain reaction provides evidence for the presence of cometabolism genes in groundwater samples, while EAP provided lines of evidence that there are active cometabolic enzymes in a groundwater sample. Groundwater from five sites across the U.S. were analyzed using qPCR and EAP, and surprisingly few of the samples showed the presence and activity of the cometabolic oxygenase enzymes probed for during the project. Four of the 19 wells analyzed using the phenylacetylene and 3-hydroxyphenylacetylene EAP, showed activity considered to be statistically significant (>8x10<sup>3</sup> cells/ml). Cinnamonitrile only showed positive results for two of the nineteen wells tested.

In general, qPCR results corresponded to the EAP results for the PHE and RMO primer sets, but not for the TOD and TOL primer sets. Gene targets for SMMO were only detected significant levels (> $10^3$  cells/ml) at three of the 19 wells tested.

#### 5.6.4 Analysis of Relationship Between TCE Assay, EAP, and qPCR Data

#### 5.6.4.1 Introduction

In Section 5.7.2, first order rate constants for TCE co-oxidation were determined on water samples from four wells at each of four sites and three wells from one site for a total of nineteen water samples. One set of rate constants was determined on groundwater samples as acquired from the well. The rate constant for degradation included the rate constant for biological cooxidation and the rate constant for abiotic radiolysis of the <sup>14</sup>C- labelled TCE. A *t*-test was used to determine if the rate constant was different from zero at 95% confidence. In all nineteen wells, the rate constant was different from zero.

A second set of samples was filtered to remove the bacteria, before the water was incubated with <sup>14</sup>C-labelled TCE. In these samples, the rate constant for degradation of TCE is the rate constant for radiolysis of the <sup>14</sup>C-labelled TCE.

To estimate the rate constant for biodegradation of TCE by cooxidation, the rate constant for TCE degradation in the filtered samples was subtracted from the rate constant for TCE degradation in the samples that were not filtered. For eight of the nineteen water samples, the rate constant for cooxidation minus the 95% confidence interval on the rate constant for cooxidation was greater than zero. For these eight wells, data on TCE degradation are reported as the rate of cooxidation. For the other eleven wells, data on TCE degradation are reported as the overall rate of degradation. Because the overall rate included the rate of TCE radiolysis, the overall rate is an upper boundary on the rate of cooxidation.

As reported in Section 5.7.3, the abundance of bacteria that respond to each of the EAP probes, and the abundance of gene copies for each of the qPCR targets were determined in the same nineteen water samples. The abundance of the EAP probe or qPCR target was determined in three separate subsamples from each of four samples of groundwater from each well. This provided a total of twelve estimates of the abundance of each EAP probe or qPCR target in each groundwater from each well. The standard error of the mean was calculated by dividing the standard deviation of the samples by the square root of 12. The 95% confidence interval on the mean was calculated using the standard error of the mean and the critical value of the *t* distribution.

A second set of samples were provided to Microbial Insights, Inc. (Knoxville, TN). Water samples were filtered in the field onto Sterivex-GS filter units. Filter units for analysis of mRNA were preserved with RNAprotect Cell Reagent (QIAGEN Inc., Valencia, CA). One filter unit for DNA and one filter unit for mRNA was analyzed from each well sampled. The reporting limit for DNA and mRNA samples varied between 5 and 8.3 cells per mL.

The abundance of cells that react with each EAP and the abundance of DNA or mRNA gene copies that was amplified by each qPCR primer was compared to the first order rate constants for TCE co-oxidation. The relationship was evaluated by a linear regression of the common logarithm of the rate constant on the common logarithm of the abundance of the marker.

Under ideal conditions, the rate constant for TCE cooxidation should be directly proportional to the abundance of the genetic marker that predicts biological activity. The slope of a regression of the rate constant on abundance should have a value of 1.0. The figures are scaled so that when the slope is 1.0, the line has an angle of 45° above the x-axis.

#### 5.6.4.2 Results

#### 5.6.4.2.1 Enzyme Activity Probes

Panel (a) of Figure 5.7.30 compares the distribution of the rate constant to the abundance of cells that react to the Phenylacetylene (PA) probe. Panel (b) of Figure 5.7.30 is a regression of the rate constants on the abundance of reactive cells.

In the eight wells where cooxidation of TCE was detected, the density of bacteria that reacted with the PA probe varied from 4E+02 to 4E+04 per mL. The density of total bacteria in the eight wells varied from 1E+05 to 1E+06 per mL. The bacteria that reacted with the PA probe were less than 10% of the total bacterial population. In the eleven wells where the rate constant for TCE degradation in the water sample was not different from the rate in the filtered controls, the rate constants were  $\leq 0.02$  per year. However, the abundance of cells that were reactive to PA varied from 4E+02 to 1E+05 per mL. This range is greater than the range in abundance of reactive cells in the water samples where TCE cooxidation was detected.

The same general pattern applied for the distribution of the rate constant to the abundance of cells that react to the 3-Hydroxyphenylacetylene (3HPA) Probe [Panel (a) of Figure 5.7.31] and to the *trans*-Cinnamonitrile (CINN) Probe [Panel (a) of Figure 5.7.32].

When the abundance of cells that reacted with the PA or 3-HPA probe was low (on the order of 1E+03 cells per mL) the rate constants were low (near or less than 0.02 per year). If the abundance of cells that reacted with the CINN probe was low (on the order of 3E+02 cells per mL) the rate constants were low (near or less than 0.002 per year). However, when the abundance of reactive cells was higher (on the order of (1E+04 cells per mL), the rate constants varied from <0.02 per year to 2.7 per year. Based on this behavior, the abundance of the cells that react to the Enzyme Activity Probes cannot be used as the sole criterion to associate a rate constant for TCE cooxidation to a plume.

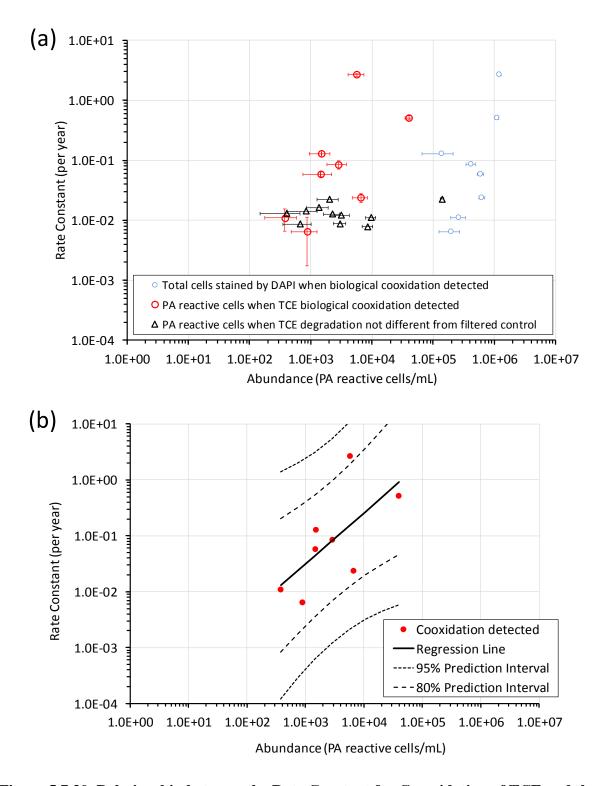
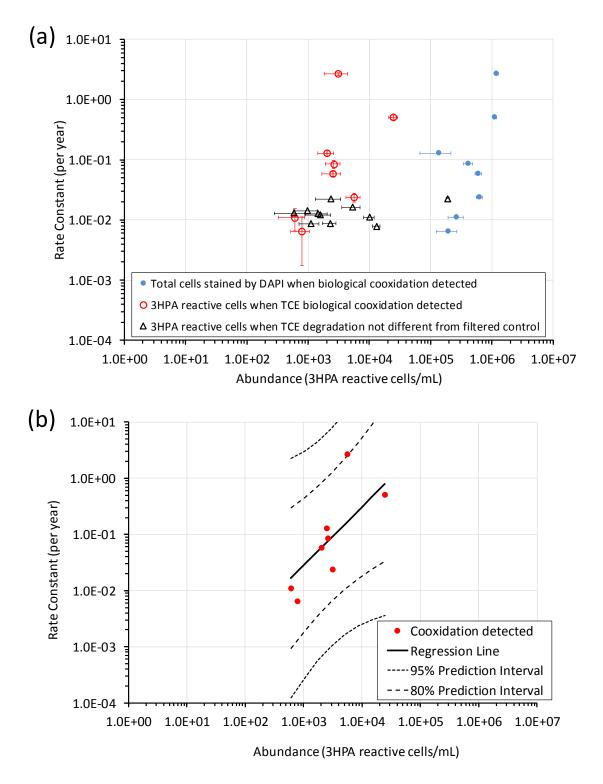


Figure 5.7.30. Relationship between the Rate Constant for Co-oxidation of TCE and the Abundance of Cells that React with the Phenylacetylene (PA) Enzyme Activity Probe.

*Error bars in Panel (a) are 95% confidence intervals on the estimate of the parameter.* 



#### Figure 5.7.31. Relationship between the Rate Constant for Co-oxidation of TCE and the Abundance of Cells that React with the 3-Hydroxyphenylacetylene (3HPA) Enzyme Activity Probe.

*Error bars in Panel (a) are 95% confidence intervals on the estimate of the parameter.* 

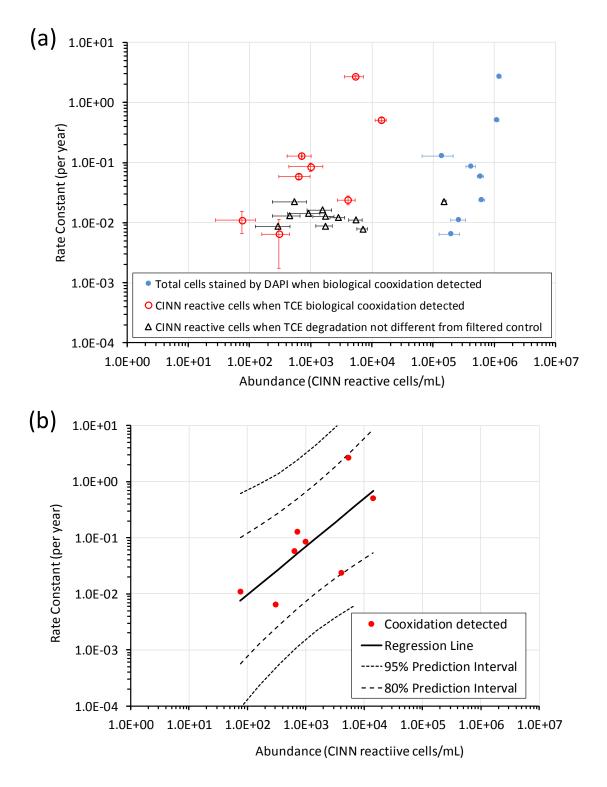


Figure 5.7.32. Relationship between the Rate Constant for Co-oxidation of TCE and the Abundance of Cells that React with the *trans*-Cinnamonitrile (CINN) Enzyme Activity Probe.

*Error bars in Panel (a) are 95% confidence intervals on the estimate of the parameter.* 

#### 5.6.4.2.2 The PHE Primer for Phenol Monooxygenase Enzyme

Panel (a) of Figure 5.7.33 compares the distribution of the rate constants to the abundance of DNA gene copies amplified by the PHE primer in the samples that were analyzed by PNNL. Panel (b) of Figure 5.7.33 is a regression of the rate constants on the abundance of gene copies.

In the eight wells where cooxidation of TCE was detected, the density of DNA gene copies that were amplified by the PHE primer varied from 2E+02 to 2E+06 per mL. The density of total bacteria in the eight wells varied from 1E+05 to 1E+06 per mL. With one exception, abundance of PHE gene copies was less than 10% of the total bacterial population. In one well, the abundance of PHE gene copies exceeded the number of cells that were stained by DAPI. This has not been explained.

In eleven wells where the rate constant for TCE degradation in the water sample was not different from the rate in the filtered controls, the rate constants were  $\leq 0.02$  per year. However, the abundance of PHE gene copies varied from 1E+01 to 1E+06 per mL. This range is equivalent to the range in abundance of PHE gene copies in the water samples where TCE cooxidation was detected.

Panel (a) of Figure 5.7.34 compares the distribution of the rate constants to the abundance of gene copies amplified by the PHE primer in the samples that were analyzed by Microbial Insights. The pattern was similar to the pattern for PNNL.

See Panel (a) of Figure 5.7.33 and Figure 5.7.34. If the abundance of PHE gene copies was low (on the order of 1E+02 cells per mL) the rate constants were low (near or less than 0.02 per year). However, when the abundance of PHE gene copies was higher (on the order of (1E+04 cells per mL), the rate constants varied from <0.02 per year to 2.7 per year. Based on this behavior, the abundance of DNA gene copies amplified by the PHE primer cannot be used as the sole criterion to associate a rate constant for TCE cooxidation in a plume.

Figure 5.7.35 compare the distribution of the rate constants to the abundance of gene copies amplified by the PHE DNA primer and the PHE mRNA primer in the samples that were analyzed by Microbial Insights. PHE mRNA copies were detected in three of the eight wells where TCE cooxidation was detected, and three of the eleven wells where the rate of TCE degradation was not different in the filtered controls. In contrast, PHE DNA copies were detected in all eight wells where TCE cooxidation was detected, and seven of eleven wells where the rate of TCE degradation was not different in the filtered controls. In contrast, PHE DNA copies were detected in all eight wells where TCE cooxidation was detected, and seven of eleven wells where the rate of TCE degradation was not different in the filtered controls. At lower abundance, the distribution of DNA gene copies and mRNA genes copies were similar. At higher abundance, there were many more DNA gene copies than mRNA genes copies. The mRNA data showed that the PHE genes were being transcribed in some of the wells, but the mRNA data did not have a closer and more direct association to the rate constants than the DNA data.

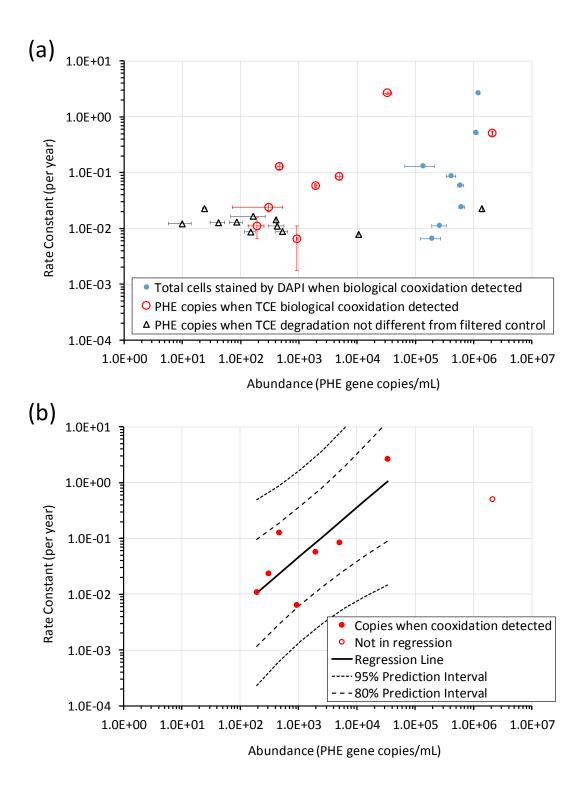


Figure 5.7.33. Relationship between the Rate Constant for Co-oxidation of TCE and the Abundance of DNA that is Amplified by the PHE Primer.

*The qPCR and total cell data are from PNNL. Error bars in Panel (a) are 95% confidence intervals on the estimate of the parameter.* 

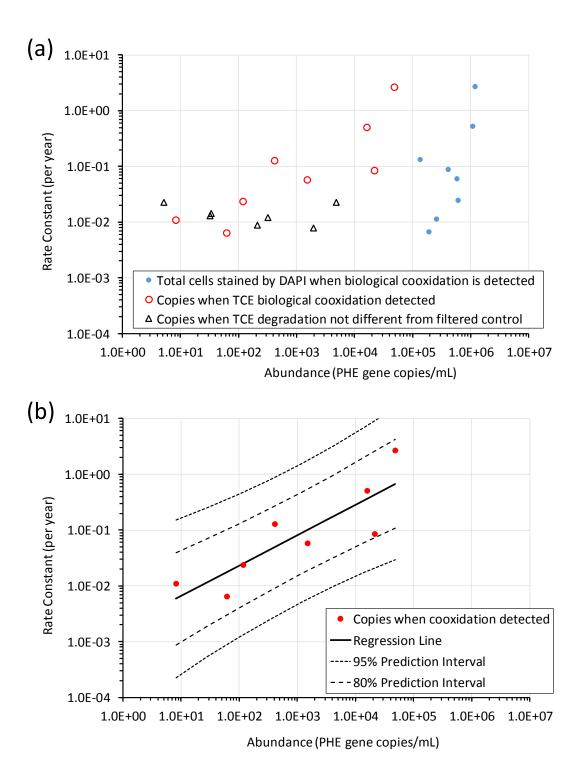
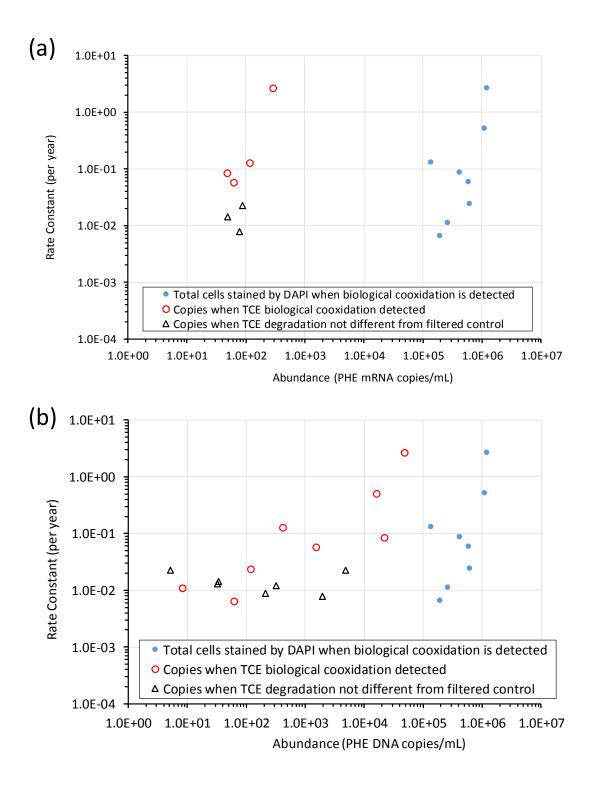


Figure 5.7.34. Relationship between the Rate Constant for Co-oxidation of TCE and the Abundance of DNA that is Amplified by the PHE Primer.

The qPCR data are from Microbial Insights. The total cell data are from PNNL.



#### Figure 5.7.35. Comparison of the Relationship between the Rate Constant for Cooxidation of TCE and the Abundance of DNA or mRNA that is Amplified by the PHE Primer.

The qPCR data are from Microbial Insights. The total cell data are from PNNL.

#### 5.6.4.2.3 The RMO Primer for Ring-Hydroxylating Toluene Monooxygenease Enzyme

Panel (a) of Figure 5.7.36 compares the distribution of the rate constants to the abundance of DNA gene copies amplified by the RMO primer in the samples that were analyzed by PNNL. Panel (b) of Figure 5.7.36 is a regression of the rate constants on the abundance of gene copies. In the eight wells where cooxidation of TCE was detected, the density of DNA gene copies that were amplified by the RMO primer varied from 3E+02 to 1E+05 per mL. The density of total bacteria in the eight wells varied from 1E+05 to 1E+06 per mL. The abundance of RMO gene copies were less than 10% of the total bacterial population. In eleven wells where the rate constant for TCE degradation in the water sample was not different from the rate in the filtered controls, the rate constants were  $\leq 0.02$  per year. However, the abundance of RMO gene copies varied from 1E+01 to 4E+04 per mL. This range is significantly overlaps the range in abundance of RMO gene copies in the water samples where TCE cooxidation was detected.

Panel (a) of Figure 5.7.37 compares the distribution of the rate constants to the abundance of gene copies amplified by the RMO primer in the samples that were analyzed by Microbial Insights. The pattern was similar to the pattern for PNNL. However, the reporting limit from the Microbial Insights samples was higher, in general 5E+00 gene copies/mL. DNA amplified by the RMO primer was not detected in four of the eight wells where TCE cooxidation was detected, and nine of the eleven wells where TCE was not different in the filtered controls.

See Panel (a) of Figure 5.7.36 and Figure 5.7.37. If the abundance of RMO gene copies was low (on the order of 3E+02 cells per mL) the rate constants were low (near or less than 0.02 per year). However, when the abundance of RMO gene copies was higher (on the order of 1E+04 cells per mL), the rate constants varied from 0.02 per year to 2.7 per year. Based on this behavior, the abundance of DNA gene copies amplified by the RMO primer cannot be used as the sole criterion to associate a rate constant for TCE cooxidation in a plume.

Figure 5.7.38 compares the distribution of rate constants to the abundance of gene copies amplified by the RMO DNA primer and RMO mRNA primer in the samples that were analyzed by Microbial Insights. RMO mRNA copies were not detected in any of the 19 wells sampled.

#### 5.6.4.2.4 The RDEG Primer for Ring-Hydroxylating Toluene Monooxygenease Enzyme

DNA gene copies amplified by the RDEG primer were not analyzed by PNNL. Panel (a) of Figure 5.7.39 compares the distribution of the rate constants to the abundance of gene copies amplified by the RDEG primer in the samples that were analyzed by Microbial Insights. Figure 5.7.39, Panel (b) is a regression of rate constants on the abundance of gene copies. The pattern was similar to the pattern for the RMO primer (Figure 5.7.37) and particularly for PHE primer (Figure 5.7.34). See Panel (a) of Figure 5.7.39. If the abundance of RDRG gene copies was low (less than 1E+02 cells per mL) the rate constants were low (near or less than 0.02 per year). However, when the abundance of RDEG gene copies was higher (on the order of (1E+04 cells per mL), the rate constants varied from <0.02 per year to 2.7 per year. Based on this behavior, the abundance of DNA gene copies amplified by the RDEG primer cannot be used as the sole criterion to associate a rate constant for TCE cooxidation in a plume.

Figure 5.7.40 compares the distribution of the rate constants to the abundance of gene copies amplified by the RDEG DNA primer and the RDEG mRNA primer in the samples that were analyzed by Microbial Insights. RDEG mRNA copies were detected in only two of the 19 wells that were sampled, and there is no logical relationship between the rate constants and the abundance of RDEG mRNA.

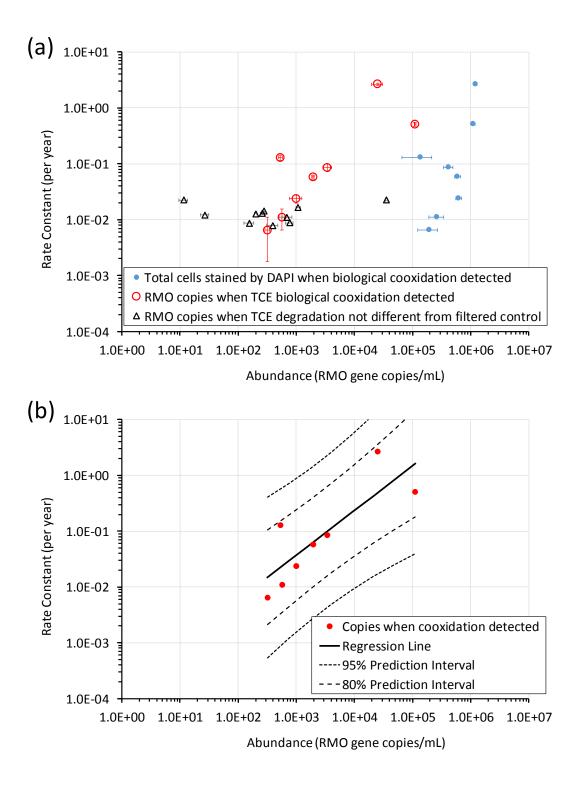
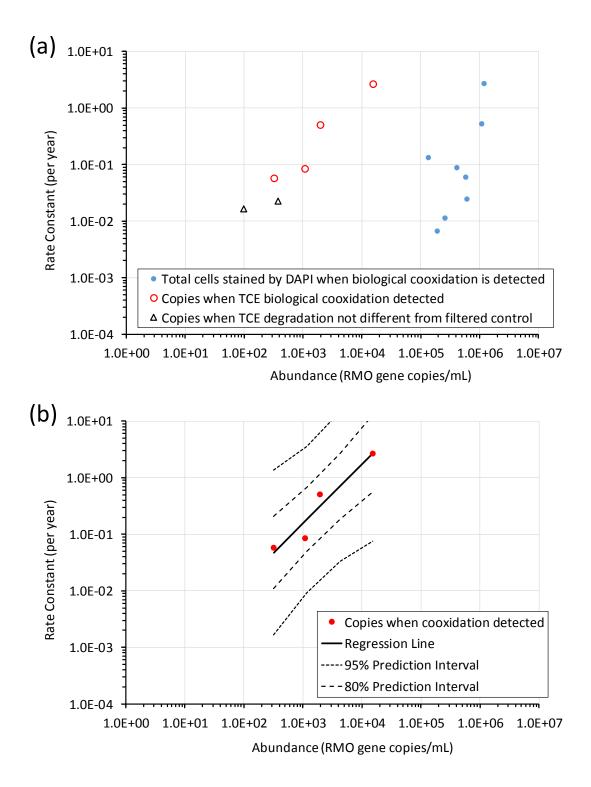


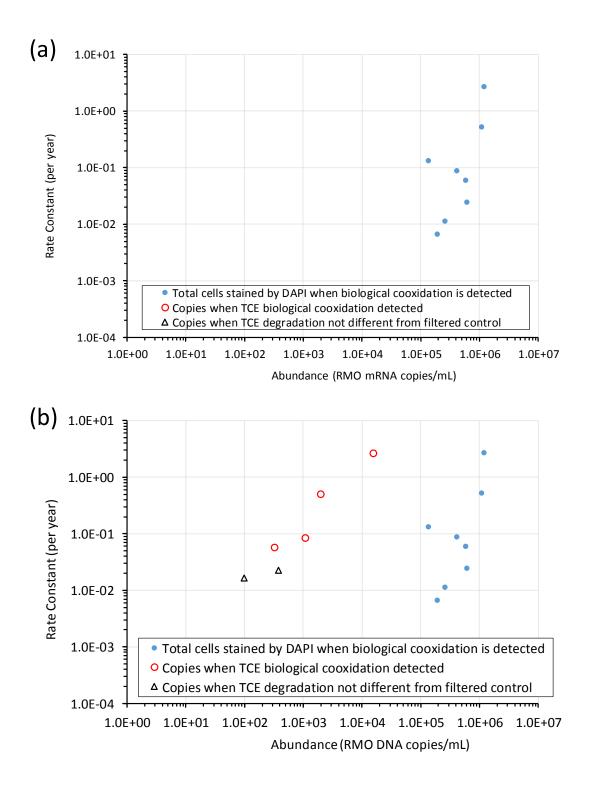
Figure 5.7.36. Relationship between the Rate Constant for Co-oxidation of TCE and the Abundance of DNA that is Amplified by the RMO Primer.

*The qPCR and total cell data are from PNNL. Error bars in Panel (a) are 95% confidence intervals on the estimate of the parameter.* 



## Figure 5.7.37. Relationship between the Rate Constant for Co-oxidation of TCE and the Abundance of DNA that is Amplified by the RMO Primer.

The qPCR data are from Microbial Insights. The total cell data are PNNL.



#### Figure 5.7.38. Comparison of the Relationship between the Rate Constant for Cooxidation of TCE and the Abundance of DNA or mRNA that is Amplified by the RMO Primer.

The qPCR data are from Microbial Insights. The total cell data are from PNNL.

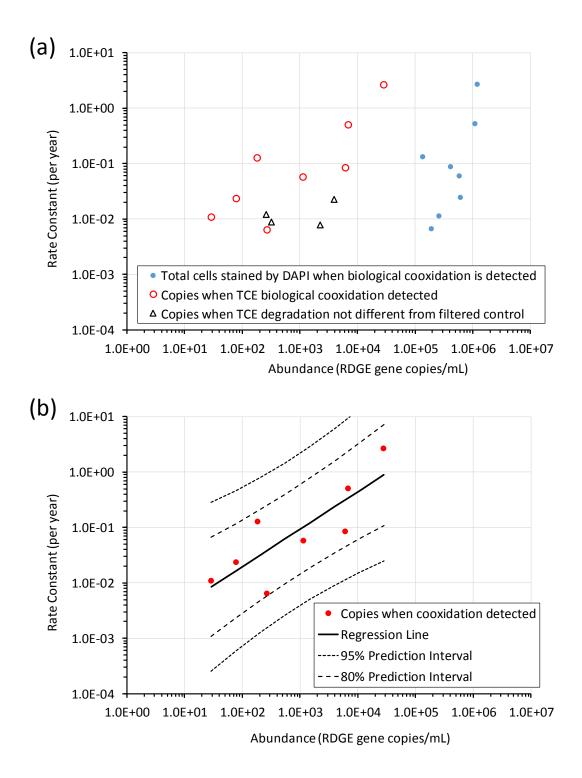
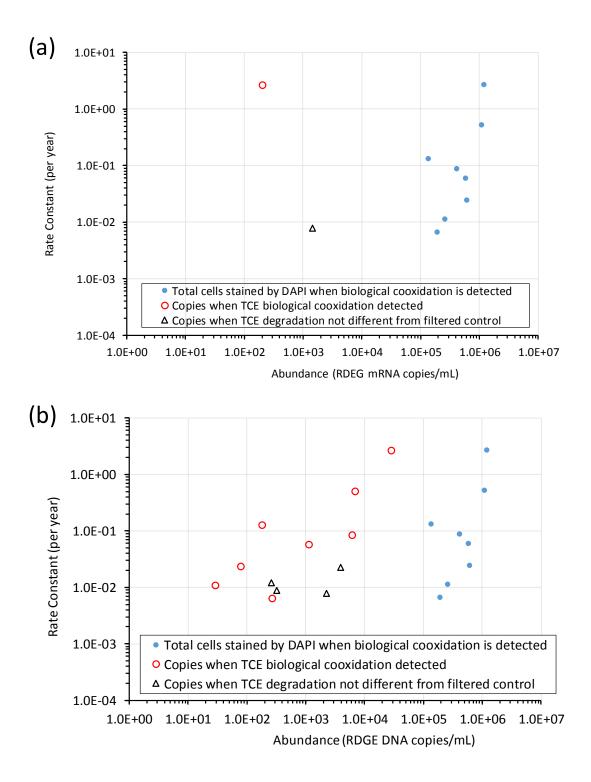


Figure 5.7.39. Relationship between the Rate Constant for Co-oxidation of TCE and the Abundance of DNA that is Amplified by the RDEG Primer.

The qPCR data are from Microbial Insights. The total cell data are PNNL.



#### Figure 5.7.40. Comparison of the Relationship between the Rate Constant for Cooxidation of TCE and the Abundance of DNA or mRNA that is Amplified by the RDEG Primer.

The qPCR data are from Microbial Insights. The total cell data are from PNNL.

#### 5.6.4.2.5 The SMMO or mmoZ Primers for Methane Monooxygenease Enzyme

Panel (a) of Figure 5.7.41 compares the distribution of the rate constants to the abundance of DNA gene copies amplified by the mmoZ primer in the samples that were analyzed by PNNL. Panel (b) of Figure 5.7.41 is a regression of the rate constants on the abundance of gene copies.

In the eight wells where cooxidation of TCE was detected, the density of DNA gene copies that were amplified by the mmoZ primer varied from 2E+02 to 2E+05 per mL. The density of total bacteria in the eight wells varied from 1E+05 to 1E+06 per mL. The abundance of mmoZ gene copies were equal to or less than 10% of the total bacterial population.

In eleven wells where the rate constant for TCE degradation in the water sample was not different from the rate in the filtered controls, the rate constants were  $\leq 0.02$  per year. However, the abundance of mmoZ gene copies varied from 5E+00 to 4E+04 per mL. This range is significantly overlaps the range in abundance of mmoZ gene copies in the water samples where TCE cooxidation was detected.

Panel (a) of Figure 5.7.42 compares the distribution of the rate constants to the abundance of gene copies amplified by the SMMO primer in the samples that were analyzed by Microbial Insights. The pattern was roughly similar to the pattern for PNNL. However, the geometric mean of the MI samples was 10 SMMO gene copies per mL while the mean of the PNNL analyses was 36 mmoX gene copies per mL. DNA amplified by the SMMO primer was detected in all nineteen wells.

See Pane (a) of Figure 5.7.41 and Figure 5.7.42. If the abundance of mmoZ gene copies was low (on the order of 3E+02 cells per mL) the rate constants were low (near or less than 0.02 per year. However, when the abundance of mmoZ gene copies was higher (on the order of (1E+03 cells per mL), the rate constants varied from 0.02 per year to 2.7 per year. If the abundance of SMMO gene copies was low (on the order of 1E+02 cells per mL) the rate constants were low (near or less than 0.002 per year. However, when the abundance of SMMO gene copies was higher (on the order of (1E+03 cells per mL), the rate constants varied from 0.02 per year. However, when the abundance of SMMO gene copies was higher (on the order of (1E+03 cells per mL), the rate constants varied from 0.02 per year to 2.7 per year. Based on this behavior, the abundance of DNA gene copies amplified by the mmoZ primer or the sMMO primer cannot be used as the sole criterion to associate a rate constant for TCE cooxidation in a plume.

Figure 5.7.43 compare the distribution of the rate constants to the abundance of gene copies amplified by the SMMO DNA primer and the SMMO mRNA primer in the samples that were analyzed by Microbial Insights. SMMO mRNA copies were detected in two of the eight wells where cooxidation of TCE was detected and six of the eleven wells where the rate constant for TCE degradation was not different in the filtered control. However, there was no logical relationship between the value of the rate constants and the abundance of the gene copies.

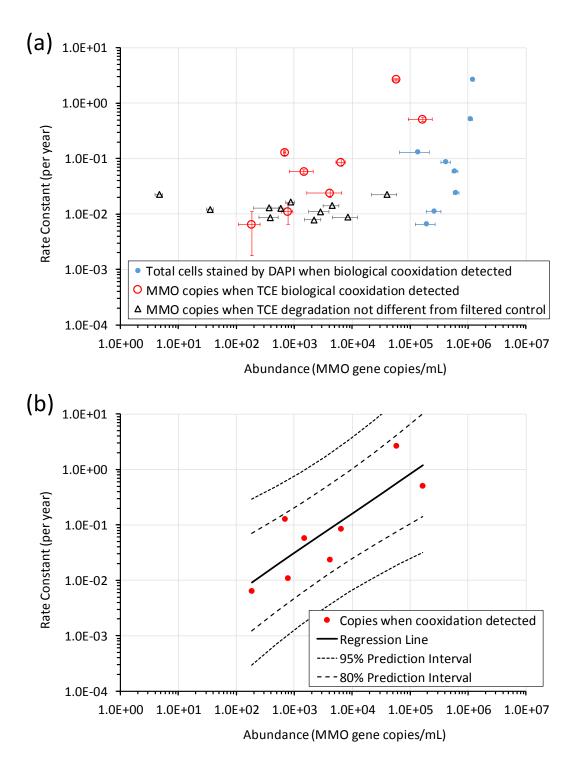
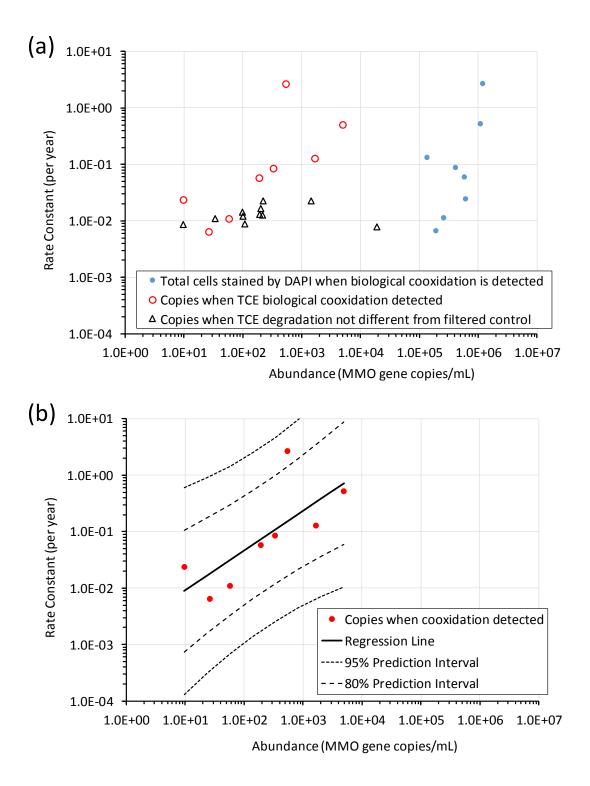


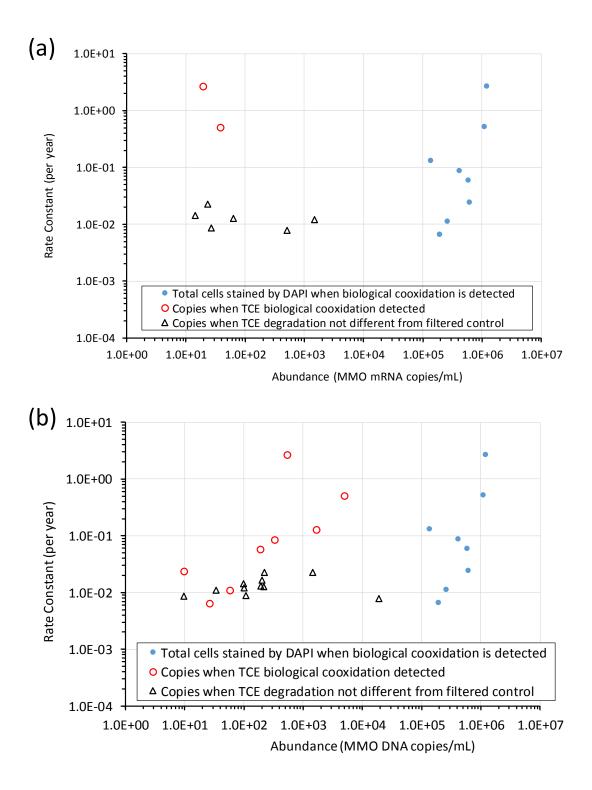
Figure 5.7.41. Relationship between the Rate Constant for Co-oxidation of TCE and the Abundance of DNA that is Amplified by the mmoZ Primer.

*The qPCR and total cell data are from PNNL. Error bars in Panel (a) are 95% confidence intervals on the estimate of the parameter.* 



# Figure 5.7.42. Relationship between the Rate Constant for Co-oxidation of TCE and the Abundance of DNA that is Amplified by the SMMO Primer.

The qPCR data are from Microbial Insights. The total cell data are PNNL.



#### Figure 5.7.43. Comparison of the Relationship between the Rate Constant for Cooxidation of TCE and the Abundance of DNA or mRNA that is Amplified by the SMMO Primer.

The qPCR data are from Microbial Insights. The total cell data are from PNNL.

#### 5.6.4.2.6 The TOD Primer for Toluene Dioxygenase Enzyme

Panel (a) of Figure 5.7.44 compares the distribution of the rate constants to the abundance of DNA gene copies amplified by the TOD primer in the samples that were analyzed by PNNL. Panel (b) of Figure 5.7.44 is a regression of the rate constants on the abundance of gene copies.

In the eight wells where cooxidation of TCE was detected, the density of DNA gene copies that were amplified by the RMO primer varied from 4E+00 to 3E+02 per mL. The density of total bacteria in the eight wells varied from 1E+05 to 1E+06 per mL. The abundance of RMO gene copies were less than 0.1% of the total bacterial population.

In eight of eleven wells where the rate constant for TCE degradation in the water sample was not different from the rate in the filtered controls, the rate constants were  $\leq 0.02$  per year. However, the abundance of TOD gene copies varied from 2E+00 to 1E+02 per mL. This range significantly overlaps the range in abundance of TOD gene copies in the water samples where TCE cooxidation was detected.

Panel (a) of Figure 5.7.45 compares the distribution of the rate constants to the abundance of gene copies amplified by the TOD primer in the samples that were analyzed by Microbial Insights. The pattern was similar to the pattern for PNNL. However, the reporting limit from the Microbial Insights samples was higher, in general 5E+00 gene copies/mL. DNA amplified by the TOD primer was not detected in four of the eight wells where TCE cooxidation was detected, and three of the eleven wells where TCE was not different in the filtered controls.

See Panel (a) of Figure 5.7.44 and Figure 5.7.45. If the abundance of TOD gene copies was low (on the order of 3E+00 cells per mL) the rate constants were low (near or less than 0.03 per year (Figure 5.7.44). However, when the abundance of TOD gene copies was higher (on the order of (1E+02 cells per mL), the rate constants varied from 0.02 per year to 2.7 per year. Based on this behavior, the abundance of DNA gene copies amplified by the TOD primer cannot be used as the sole criterion to associate a rate constant for TCE cooxidation in a plume.

Figure 5.7.46 compare the distribution of the rate constants to the abundance of gene copies amplified by the TOD DNA primer and the TOD mRNA primer in the samples that were analyzed by Microbial Insights. TOD mRNA copies were detected in one of the eight wells where cooxidation of TCE was detected and three of the eleven wells where the rate constant for TCE degradation was not different in the filtered control.

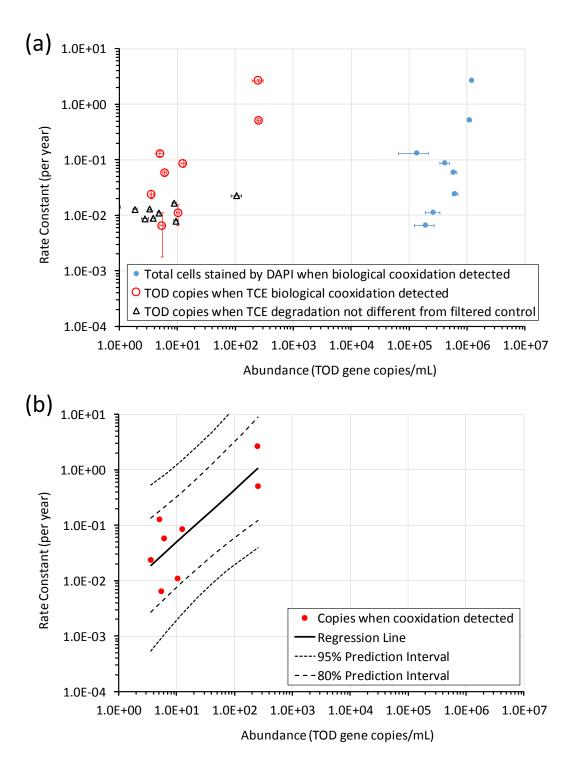


Figure 5.7.44. Relationship between the Rate Constant for Co-oxidation of TCE and the Abundance of DNA that is Amplified by the TOD Primer.

*The qPCR and total cell data are from PNNL. Error bars in Panel (a) are 95% confidence intervals on the means.* 

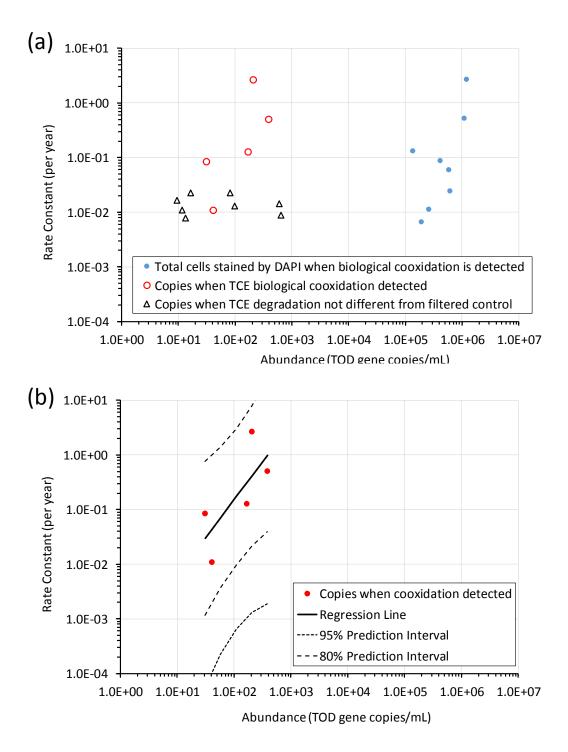


Figure 5.7.45. Relationship between the Rate Constant for Co-oxidation of TCE and the Abundance of DNA that is Amplified by the TOD Primer.

The qPCR data are from Microbial Insights. The total cell data are PNNL.

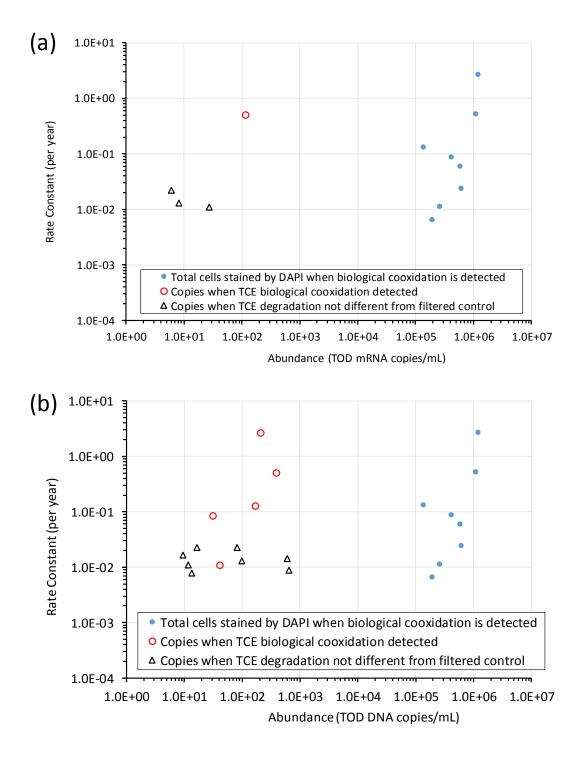


Figure 5.7.46. Comparison of the Relationship between the Rate Constant for Cooxidation of TCE and the Abundance of DNA or mRNA that is Amplified by the TOD Primer.

The qPCR data are from Microbial Insights. The total cell data are from PNNL.

#### 5.6.4.2.7 The TOL Primer for Toluene Monooxygenase Enzyme

Panel (a) of Figure 5.7.47 compares the distribution of the rate constants to the abundance of DNA gene copies amplified by the TOL primer in the samples that were analyzed by PNNL. Panel (b) of Figure 5.7.47 is a regression of the rate constants on the abundance of gene copies.

In the eight wells where cooxidation of TCE was detected, the density of DNA gene copies that were amplified by the TOL primer varied from 1E-02 to 2E+01 per mL. The density of total bacteria in the eight wells varied from 1E+05 to 1E+06 per mL. The abundance of RMO gene copies were less than 0.01% of the total bacterial population.

In nine wells where the rate constant for TCE degradation in the water sample was not different from the rate in the filtered controls, the rate constants were  $\leq 0.02$  per year. However, the abundance of TOL gene copies varied from 1E-03 to 1E+01 per mL. This range significantly overlaps the range in abundance of TOL gene copies in the water samples where TCE cooxidation was detected.

See Panel (a) of Figure 5.7.47 and Figure 5.7.48. If the abundance of TOL gene copies was low (on the order of 1E-02 cells per mL) the rate constants were low (near or less than 0.04 per year (Figure 5.7.47). However, when the abundance of TOL gene copies was higher (on the order of (1E+01 cells per mL), the rate constants varied from 0.02 per year to 2.7 per year. Based on this behavior, the abundance of DNA gene copies amplified by the TOL primer cannot be used as the sole criterion to associate a rate constant for TCE cooxidation in a plume.

Panel (a) of Figure 5.7.48 compares the distribution of the rate constants to the abundance of gene copies amplified by the TOL primer in the samples that were analyzed by Microbial Insights. The pattern was similar to the pattern for PNNL. However, the reporting limit from the Microbial Insights samples was higher, in general 5E+00 gene copies/mL. DNA amplified by the TOD primer was not detected in five of the eight wells where TCE cooxidation was detected, and ten of the eleven wells where TCE was not different in the filtered controls.

Figure 5.7.49 compares the distribution of the rate constants to the abundance of gene copies amplified by the TOL DNA primer and the TOL mRNA primer in the samples that were analyzed by Microbial Insights. TOD mRNA copies were not detected in any of the nineteen wells that were sampled.

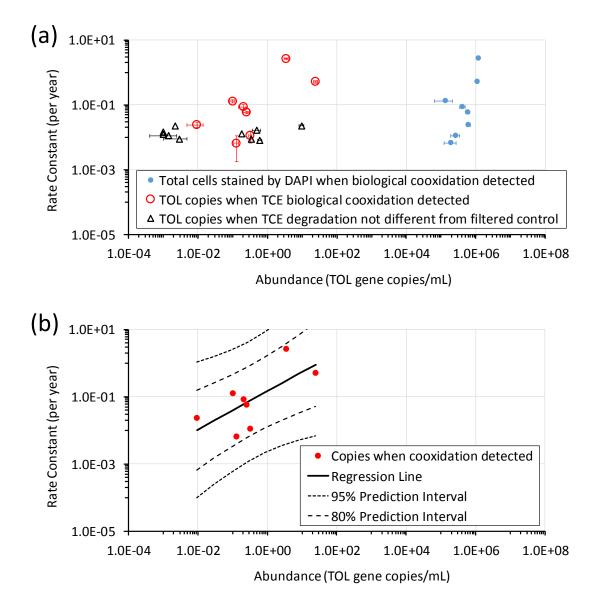
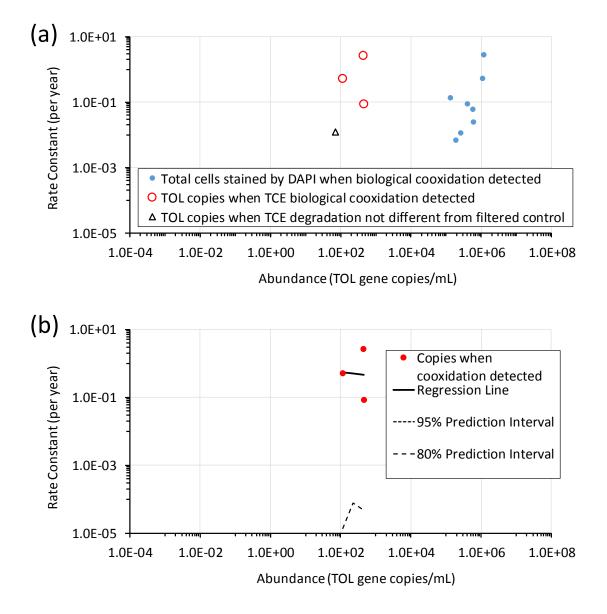
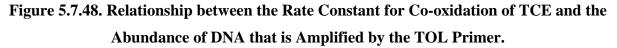


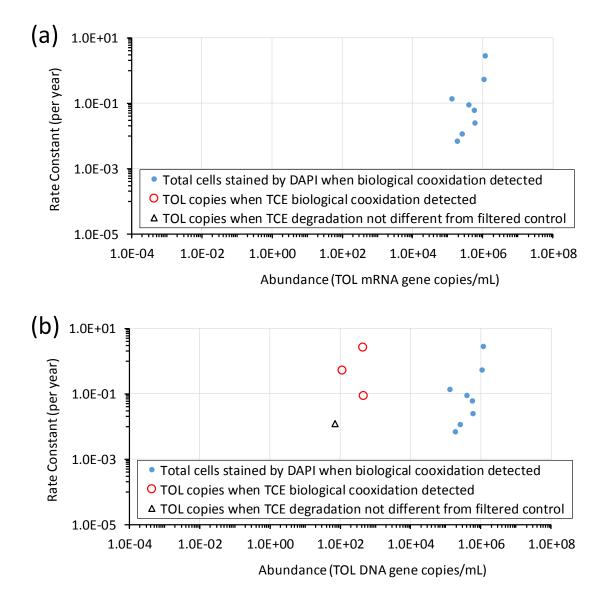
Figure 5.7.47. Relationship between the Rate Constant for Co-oxidation of TCE and the Abundance of DNA that is Amplified by the TOL Primer.

*The qPCR and total cell data are from PNNL. Error bars in Panel (a) are 95% confidence intervals on the estimate of the parameter.* 

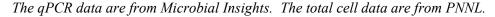




The qPCR data are from Microbial Insights. The total cell data are PNNL.



#### Figure 5.7.49. Comparison of the Relationship between the Rate Constant for Cooxidation of TCE and the Abundance of DNA or mRNA that is Amplified by the TOL Primer.



#### 5.6.4.3 Discussion and Summary

Table 5.7.9 compares the geometric mean of the abundance of cells reacting to the three Enzyme Activity Probes and the abundance of DNA amplified by the seven qPCR primers in the eight wells where cooxidation of TCE was detected. The abundance of cells that reacted with the PA and 3-HPA probes was essentially identical. The abundance of cells that reacted to the CINN probe may have been less, but any difference was not significant at 95% confidence.

Marker	Analyzed by	Geometric Mean	Lower 95% Confidence Interval	Upper 95% Confidence Interval	Number Wells where DNA Detected	Number Wells where mRNA Detected
		Gene Copy per mL	Gene Copy per mL	Gene Copy per mL		
PA	PNNL	2,700	820	9,100		
3-HPA	PNNL	2,700	1,000	7,000		
CINN	PNNL	1,200	280	4,800		
PHE	MI	950	69	1,300	8	3
PHE	PNNL	1,400	300	6000	8	
RMO	MI	1,800	140	24,000	4	0
RMO	PNNL	2,600	500	14,000	8	
RDEG	MI	790	103	6,000	8	1
SMMO	MI	210	37	1,200	8	2
mmoZ	PNNL	3,700	540	26,000	8	
TOD	MI	110	29	430	5	1
TOD	PNNL	16	3.8	67	8	
TOL	MI	280	40	2,000	3	0
TOL	PNNL	0.34	0.05	2.5	8	

 Table 5.7.9. Relative Abundance of Markers in the Eight Wells Where TCE Cooxidation

 Was Detected

No differences between the abundance of DNA amplified by the PHE primer, the RMO primer, the RDEG primer and the mmoZ primer could be distinguished that were significant at 95% confidence, and no differences between the abundance of DNA amplified by these primers and the abundance of cells that reacted with the Enzyme Activity Probes could be distinguished at 95% confidence. It is likely that the Probes and the primers were interacting with the same population of cells. If this is true, then much of the DNA amplified by the primers is associated with living cells that are capable of supporting the activity of an oxygenase enzyme.

There is no explanation for the behavior of the bacteria in the eleven wells where the cells reacted with the Enzyme Activity Probes, but did not cooxidize TCE at detectable rates. If the cells would react with the Probe, then why did they not react with TCE? It is possible that the cells were in a dormant state in the groundwater, and the presence of the Probe, or some other factor in the performance of the assay, restored the cells to an active state. This phenomenon will require further study before the behavior can be explained.

The abundance of DNA that was amplified by the TOD and TOL primers was orders of magnitude lower than the abundance of DNA amplified by the PHE primer, the RMO primer, the RDEG primer and the mmoZ primer. It is unlikely that enzymes coded by DNA amplified by the TOD and TOL primers are responsible for a significant fraction of TCE cooxidation.

Assays for DNA amplified by PHE primer, the RMO primer, the RDEG primer are commercially available. The PHE primer may be the best primer to describe TCE cooxidation. In addition to a high abundance of DNA amplified by this primer, there was a reasonably high abundance of mRNA that was amplified by this primer.

Table 5.7.9 compares the slope of the regession line for the three EAP markers and the qPCR markers. According to the criterion in Table 3.2.1 and Section 3.2.4.2, a marker will be useful to predict the value of the rate constant when the slope of the regression of the logarithm of the rate constant on the logarithm of the abundance of the marker is greater than zero at 95% confidence. The CINN EAP marker met this criterion, though just barely, but the PH and 3-HPA EAP markers did not. The PHE, RMO, and MMO primers analyzed by both PNNL and MI met the criterion. The TOD marker as analyzed by PNNL met the criterion, but the TOD marker as analyzed by MI did not. This difference is due to the greater sensitivity of the analyses performed by PNNL.

The TOL marker as analyzed by either PNNL or MI did not meet the criterion.

Marker	Analyzed by	Slope of Regression Line	Lower 95% Confidence Interval	Upper 95% Confidence Interval	Number of Wells in Regression
PA	PNNL	0.91	-0.13	1.95	8
3-HPA	PNNL	1.04	-0.34	2.42	8
CINN	PNNL	0.86	0.06	1.66	8
PHE	MI	0.55	0.22	0.87	8
PHE	PNNL	0.90	0.18	1.61	8
RMO	MI	1.05	0.10	1.98	4
RMO	PNNL	0.81	0.26	1.35	8
RDEG	MI	0.68	0.21	1.14	8
SMMO	MI	0.70	0.07	1.34	8
mmoZ	PNNL	0.71	0.23	1.20	8
TOD	MI	1.40	-0.94	3.72	5
TOD	PNNL	0.94	0.29	1.60	8
TOL	MI	-0.10	-27.59	27.39	3
TOL	PNNL	0.57	-0.04	1.18	8

### Table 5.7.10. Relative Abundance of Markers in the Eight Wells Where TCE Cooxidation Was Detected

#### 5.6.4.4 Appropriate Use of EAP and qPCR Data

As described previously, the number of cells that reacted to the Enzyme Activity Probes or the abundance of DNA gene copies amplified by the qPCR primers should not be used as the sole criterion to associate a rate constant for TCE cooxidation in a plume. However, there are two useful applications for these data. The data can be used to screen a site to determine whether cooxidation of TCE is a possible mechanism for a natural attenuation remedy. The data can also be used to provide a second line of evidence to evaluate a rate constant that is extracted from other information.

To use the biological markers to determine whether TCE cooxidation might provide a remedy, it is necessary to know the value of the rate constant that is required to provide the desired environment outcome. The value is site specific. It may depend on the travel time of groundwater from a source to a property boundary, sentry well, or a vulnerable receptor. If further contamination of the groundwater is prevented, it may depend on the time available before the cleanup goal is to be attained. For the sake of illustration, assume that a rate constant  $\geq 0.03$  per year can lead to a desirable outcome. This is equivalent to a half-life of 23 years.

The next step is to compare the required site-specific value of the rate constant to the rate constant that might plausibly be expected from the abundance of the biomarkers. The best candidates are the PHE primer and the RMO primer.

The process will be illustrated by data for the PHE primer. Figure 5.7.50 repeats information provided in Panel (b) of Figure 5.7.34. The lower 80% two-tailed prediction interval in Panel (b) of Figure 5.7.34 also corresponds to the 90% one-tailed prediction interval in Figure 5.7.50. If the measured abundance of DNA that is amplified by the PHE primer is 1E+04 gene copies per mL, there is a 50% chance the rate constant is greater than 0.2 per year, and a 90% confidence that the rate constant is greater than 0.05 per year. In this example, both exceed the rate constant that would produce the desired outcome. This would justify collecting the information necessary to provide a valid rate constant

Valid rate constants could be obtained using the <sup>14</sup>C assay for TCE cooxidation. Valid rate constants can also be extracted from long term monitoring data and the geohydrological properties of the site using the method described in Lebrón et al. (2015). If rate constants for TCE degradation are already available at a site, the qPCR data could be used to provide a line of evidence that aerobic TCE cooxidation is a plausible mechanism to explain the degradation rate.

After the PHE primer, the RMO primer is the most useful qPCR marker. Figure 5.7.51 provides the regression line and the lower one-tailed 90% prediction interval for the RMO primer. The CINN marker was the only EAP that met the criterion that the slope of the regession line will be greater than zero at 95% confidence. Figure 5.7.52 provides the regression line and lower one-tailed 90% prediction interval for the CINN EAP.

Use caution when extraplating rate contants for groundwater with Fe(II). The <sup>13</sup>C-TCE assay provides adequate dissolved oxygen to support aerobic biological cooxidation. Oxygen reacts readiy with Fe(II). If there is measureable Fe(II) in groundwater, that water is devoid of oxygen. If both oxygen and Fe(II) are present in a sample of well water, some portion of the flowlines to the well have oxygen and no Fe(II), and other portions have Fe(II) and no oxygen.

Three of the wells in the survey had measurable concentrations of Fe(II), and the same three wells had the highest rate constants for TCE cooxidation (Table 5.6.3 and Table 5.7.2). The well with the highest rate constant (U10-019 at Hill AFB) had 0.69 mg/L Fe(II). The well with the next highest rate constant (MW-01-006 at Plattsburgh AFB) had 1.25 mg/L Fe(II). The well with the third highest rate constant (MW-02-019 at Plattsburgh AFB) had 1.12 mg/L Fe(II). The concentration of Fe(II) was <0.03 mg/L in the other wells. Data points from these wells are enclosed within a  $\Box$  shape in Figure 5.7.50, Figure 5.7.51 and Figure 5.7.52.

If Fe(II) is present in the well water, some portion of the aquifer sampled by the well does not have oxygen to support cooxidation of TCE. As a result, the rate constant determined using the <sup>13</sup>C-TCE assay will overestimate the true rate constant in the aquifer. If the well water has measurable Fe(II), supplement and validate the rate constant provided from the assaywith a rate constant extracted from the long-term monitoring data and the geohydrological properties of the aquifer.

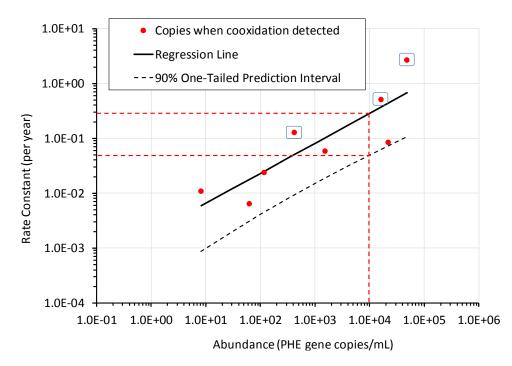


Figure 5.7.50. Predicting Provisional Rate Constants for TCE Co-oxidation from the Abundance of DNA Amplified by the PHE Primer.

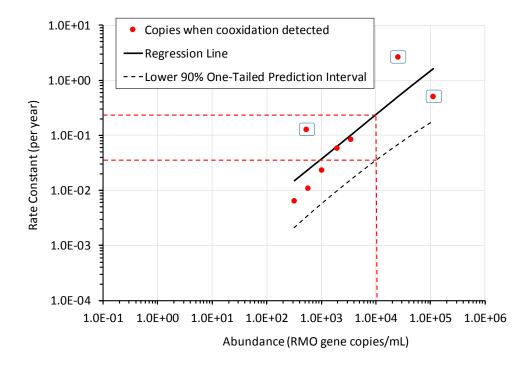


Figure 5.7.51. Predicting Provisional Rate Constants for TCE Co-oxidation from the Abundance of DNA Amplified by the RMO Primer.

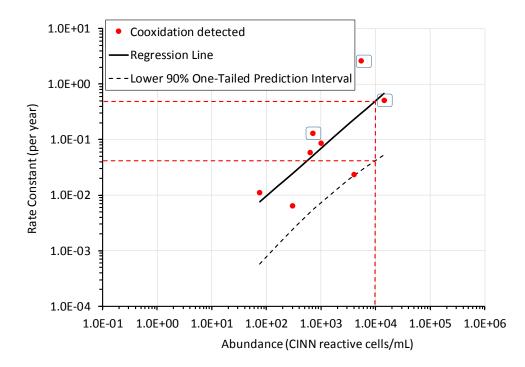


Figure 5.7.52. Predicting Provisional Rate Constants for TCE Co-oxidation from the Abundance of Cells that React with the CINN EAP.

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### 6.0 PERFORMANCE ASSESSMENT

Qualitative and quantitative performance metrics were initially established and performance assessed through project execution. Performance was assessed using the performance objectives listed in Section 3 as a benchmark. The following subsections relate to the results that pertain to these metrics and goals.

#### 6.1 QUALITATIVE PERFORMANCE OBJECTIVES

This section discusses the qualitative performance objectives for this project, which are summarized in Table 3.1.1.

#### 6.1.1 Develop an Easy to Use Procedure for Collecting Magnetic Susceptibility Data

To be able to readily assess abiotic degradation by magnetite, reliable, yet relatively inexpensive magnetic susceptibility data for the aquifer matrix along the solute flowpath must be available. In order to achieve this performance objective, the implementation of a magnetic susceptibility sonde at various depths and in various conditions was tested. Specifically, the field testing of existing, readily-available technology to quantify magnetic susceptibility in existing PVC monitoring wells using a commercially-available magnetic susceptibility sonde was conducted to determine ease of use and accuracy. This performance objective was met for the following reasons:

- 1) Based on the experience of the field crew (i.e., Mr. Wiedemeier and Dr. Wilson), the sonde was very easy to use. After the initial learning curve, which will be much reduced for people reading this document, the field crew was able to set up and have the sonde down-hole and ready to obtain measurements within 0.5 hour of arriving at a given sampling location. Of course, this assumes that the field crew has no problems gaining access to the sampling point.
- 2) Based on the data and discussion presented in Section 5.7.1.2, the sonde used for this project produces accurate magnetic susceptibility data.

# 6.1.2 Develop an Assay Based on <sup>14</sup>C-TCE That Will Allow TCE Co-Oxidation Rates in Groundwater Samples

The <sup>14</sup>C-TCE assay allowed for quantification of pseudo first order rate constants in groundwater samples from eight of the 19 wells evaluated, at rates ranging from ranging from 0.00658 to 2.65 yr<sup>-1</sup>. This translates to half-lives of 0.26 to 105 yr. In groundwater from the other 11 wells, the rate of <sup>14</sup>C product accumulation was not statistically different from the FSGW controls, so that no rate is reported. Although only a single GC column was used for purification of the <sup>14</sup>C-TCE, the level of impurities delivered to the serum bottles was sufficiently low to allow for detection of a half-life as long as 105 yr. This was due in part to extension of the incubation period from a few days to as long as 46 days, which permitted accumulation of a sufficient level of <sup>14</sup>C products to be distinguishable from the controls.

In several of the groundwater samples, VOCs were detected in addition to TCE. These decreased in amount during the incubation period, often at a faster rate than the TCE. It is not yet known if these co-contaminants contributed to co-oxidation of TCE. The fact that co-oxidation occurred in some of the groundwater samples that did not contain VOCs other than TCE indicates their presence is not a requirement. Demonstration of co-oxidation in a surface water sample obtained from a seep with no prior exposure to chlorinated contaminants indicated that naturally occurring processes can support TCE co-oxidation at a meaningful rate.

The initial plan was to use DDI water as the negative control for the <sup>14</sup>C-TCE assay. It was determined, however, that FSGW is more appropriate for this purpose. The rate of <sup>14</sup>C product accumulation in FSGW controls was statistically lower than in DDI water, likely due to the presence of constitutes that quench the autoradiolysis associated with decay of <sup>14</sup>C-TCE.

A propanotrophic culture that co-oxidized TCE was used as a positive control to evaluate the <sup>14</sup>C-TCE assay. ENV485 was used to assess the effect of storage conditions on the co-oxidation rate. It was determined that handling the culture in the same manner as the groundwater samples (i.e., 24 h at 4 °C to mimic shipping on ice, followed warming overnight to room temperature) caused a modest decrease in the first order rate coefficient. This suggests that the co-oxidation rates for the groundwater are conservative with respect to in situ conditions.

# 6.1.3 Methods for Identifying Presence and Activity of Co-Metabolic Bacteria for TCE Oxidation

Results from the experiments demonstrated that both qPCR and EAP performed as expected for analysis of cometabolism genes in groundwater samples. While responses from most wells was considered low, the qPCR primer sets and EAP provided lines of evidence that there are active cometabolic enzymes in a groundwater sample.

In general, qPCR results corresponded to the EAP results for the PHE and RMO primer sets, but not for the TOD and TOL primer sets.

## 6.1.4 Demonstrate Baseline Method for Linking TCE Transformation Rates to Numbers of Bacteria with Co-oxidation Enzymes

The <sup>13</sup>C-TCE assay was an effective tool to determine rate constants for TCE cooxidation at some sites, but not at others. At 95% confidence, the <sup>14</sup>C-TCE assay could extract a rate constant for TCE cooxidation from 8 of 19 water samples. The rate rate constant for total degradation of TCE is an upper boundary on the rate constant for biological cooxidation. The highest rate constant in any well where biological cooxidation could not be distinguished from radiolysis was 0.084 per year. This corresponds to a half-life of 8.3 years. At many sites, a rate constant of 0.084 per year would be make biological cooxidation a plausible mechanism for a MNA remedy. The <sup>13</sup>C-TCE assay will provide a rate constant for TCE cooxidation at may many sites where cooxidation is a plausible remedy, but not all of them.

In every well sampled, whether the TCE cooxidation was detected or not detected, the abundance of cells reacting to each of the EAPs was above the quantitation limit. In every well sampled, the abundance of DNA that was amplified by the PHE, RMO, and MMO primers was above the quantition limit.

#### 6.2 QUANTITATIVE PERFORMANCE OBJECTIVES

This section discusses the qualitative performance objectives for this project, which are summarized in Table 3.2.1.

#### 6.2.1 Evaluate the Accuracy of Data for Magnetic Susceptibility

To verify the validity of the data collected using the magnetic susceptibility sonde, the sonde was deployed in wells where soil samples were previously collected from soil borings prior to well installation and analyzed for mass magnetic susceptibility in an analytical laboratory. The data collected using the downhole sonde were then compared to the previously-collected borehole soil data.

The correlation between magnetic susceptibility determined using the sonde and magnetic susceptibility data collected using laboratory analysis of soil/sediment data was determined (Figure 5.7.3). The Pearson's correlation coefficient, r, was calculated and determined to be r = 0.94 ( $R^2 = 0.88$ ). Based on the quantitative performance objective for this task of a Pearson's correlation coefficient greater than 0.75 (r > 0.75), this performance objective is considered met. Thus, the magnetic susceptibility sonde provides a good tool for collecting representative magnetic susceptibility data from existing non-metallic (e.g., PVC) monitoring wells.

Based on this, if appropriate monitoring wells are available, downhole magnetic susceptibility sondes in groundwater monitoring wells can provide a less expensive alternative to the collection and analysis of borehole core data, and can provide data that can be used to evaluate field-scale rate constants for abiotic degradation of PCE, TCE, and *c*DCE by magnetite.

#### 6.2.2 Determine First-Order Rates of TCE Co-Oxidation Using a <sup>14</sup>C-TCE Assay

The <sup>14</sup>C-TCE assay allowed for quantification of pseudo first order rate constants in groundwater samples from eight of the 19 wells evaluated, at rates ranging from ranging from 0.00658 to 2.65 yr<sup>-1</sup>. This translates to half-lives of 0.26 to 105 yr. In groundwater from the other 11 wells, the rate of <sup>14</sup>C product accumulation was not statistically different from the FSGW controls, so that no rate is reported. Although only a single GC column was used for purification of the <sup>14</sup>C-TCE, the level of impurities delievered to the serum bottles was sufficiently low to allow for detection of a half-life as long as 105 yr. This was due in part to extension of the incubation period from a few days to as long as 46 days, which permitted accumulation of a sufficient level of <sup>14</sup>C products to be distinguishable from the controls.

In several of the groundwater samples, VOCs were detected in addition to TCE. These decreased in amount during the incubation period, often at a faster rate than the TCE. It is not yet known if these co-contamiants contributed to co-oxidation of TCE. The fact that co-oxidation occurred in some of the groundwater samples that did not contain VOCs other than TCE indicates their presence is not a requirement. Demonstration of co-oxidation in a surface water sample obtained from a seep with no prior exposure to chlorinated contaminants indicated that naturally occurring processes can support TCE co-oxidation at a meaningful rate.

The initial plan was to use DDI water as the negative control for the <sup>14</sup>C-TCE assay. It was determined, however, that FSGW is more appropriate for this purpose. The rate of <sup>14</sup>C product accumulation in FSGW controls was statistically lower than in DDI water, likely due to the presence of constitutes that quench the autoradiolysis associated with decay of <sup>14</sup>C-TCE.

A propanotrophic culture that co-oxidized TCE was used as a positive control to evaluate the <sup>14</sup>C-TCE assay. ENV485 was used to assess the effect of storage conditions on the co-oxidation rate. It was determined that handling the culture in the same manner as the groundwater samples (i.e., 24 h at 4 °C to mimic shipping on ice, followed warmining overnight to room temperature) caused a modest decrease in the first order rate coefficient. This suggests that the co-oxidation rates for the groundwater are conservative with respect to in situ conditions.

#### 6.2.3 Quantification of Bacteria with Active Enzymes Associated with TCE Co-Metabolism

Quantitative polymerase chain reaction provides evidence for the presence of cometabolism genes in groundwater samples, while EAP provided lines of evidence that there are active cometabolic enzymes in a groundwater sample. Groundwater from five sites across the U.S. were analyzed using qPCR and EAP, and surprisingly few of the samples showed the presence and activity of the cometabolic oxygenase enzymes probed for during the project. Four of the 19 wells analyzed using the phenylacetylene and 3-hydroxyphenylacetylene EAP, showed activity considered to be statistically significant (>8x10<sup>3</sup> cells/ml). Cinnamonitrile only showed positive results for two of the nineteen wells tested.

In general, qPCR results corresponded to the EAP results for the PHE and RMO primer sets, but not for the TOD and TOL primer sets. Gene targets for SMMO were only detected significant levels (> $10^3$  cells/ml) at three of the 19 wells tested.

#### 6.2.4 Demonstrate Ability to Predict TCE Co-Oxidation Rates by Quantifying Number of Bacteria With Active Co-oxidation enzymes

In the eight wells where biological cooxidation could be distinguished from radiolysis, the CINN EAP assay and the PHE and RMO qPCR determination provided a useful prediction of the rate constant for TCE cooxidation, although the prediction intervals in the regression are broad. However, in many of the wells where cooxidation was not detected, the abundance of cells reacting with the CINN EAP and the abundance of DNA that is amplified by the PHE and RMO primer was high. The EAP and qPCR data do not provide an unequivocal prediction of the rate constant for TCE cooxidation.

Because the CINN EAP marker or the PHE and RMO qPCR markers do not provide an unequivocal prediction of the rate constant, the CINN EAP marker or the PHE and RMO qPCR markers can only be used to identify groundwater where the predicted rate constants are possible. To use cooxidation of TCE as part of a MNA remedy, it will be necessary to validate the predictions from the CINN EAP marker or the PHE and RMO qPCR markers by obtaining rate constants using the <sup>13</sup>C-TCE assay or by extracting rate constants from the long-term monitoring data and the geohydrologial properties of the aquifer.

If the groundwater used to perform the <sup>13</sup>C-TCE assay has measureable concentrations of Fe(II), it would be good practice to supplement and validate the rate constant produced by the assay with a rate constant that is extracted from the long-term monitoring data and the geohydrological properties of the aquifer.

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### 7.0 COST ASSESSMENT

This section provides information on the costs for implementing the various technology elements described in this report at a given site. In addition, this section provides a discussion of the cost benefit of the technology.

#### 7.1 COST MODEL

A simple cost model for the technology is presented so that a remediation professional can understand costing implications. The cost model reflects all cost elements required for implementing the technology at a real site. For each cost element, the cost data that was tracked during the demonstration and the associated cost as incurred during the demonstration are presented.

Each cost element includes the following information:

- A description to briefly explain the cost element and the need for it in the implementation of the technology.
- A description and, if appropriate, supporting analysis as to what data supports the listed cost estimate or range.
- A description of how issues of scale are addressed is included by providing per-well costs.

#### 7.2 COST DRIVERS

Anticipated cost drivers in selecting the technology for future implementation are discussed in this cost assessment. The only site-specific characteristic that would significantly impact cost/implementibility is if only 2inch wells that have been compromised are available for a given site. Wells that are considered compromised include those wells that are insufficiently straight to allow insertion and lowering of the downhole magnetic susceptibility sonde. In addition, compromised wells could have joints that are not flush, and the sonde cannot move past the joint. In such cases the sonde cannot be used and a drilling rig will have to be mobilized if the interested party wants to collect magnetic susceptibility data.

#### 7.3 COST ANALYSIS

This section provides estimates for the costs of the technology when implemented. The basic site description for which costs were developed includes a site contaminated with chlorinated ethylenes that contains 2- or 4-inch monitoring wells installed to 100 feet in unconsolidated sediment or fractured rock. In order for the technology elements described in this document to be the most useful, monitoring wells used for sample collection should be located as near as possible to the plume centerline, parallel to the direction of solute flow.

This section describes and quantifies the operational costs for the various components of the technologies being developed and/or refined under this demonstration. For the purposes of developing the cost model presented herein, the technology has been broken down into cost elements, which are discussed and quantified in the following sections.

#### 7.3.1 COST ELEMENT 1 – DOWNHOLE MAGNETIC SUSCEPTIBILITY MEASUREMENTS

This cost element includes mobilization of a two-person field crew to the field for three days to collect continuous downhole magnetic susceptibility measurements. Mobilization includes making all arrangements for equipment rental and site access. It is assumed that the wells to be analyzed have already been selected. Included in the costs for magnetic susceptibility measurements using a magnetic susceptibility sonde are the continuous sampling of up to eight wells to a depth of 100 feet below ground surface over a period of three days. These costs include the rental of all necessary equipment as well as labor hours. Table 7.1 summarizes the costs for this cost element. These costs can be scaled up and down by taking the mobilization cost, which includes the costs for renting and obtaining the equipment, of \$1,200 and adding it to the per-well cost of \$800 times the number of wells to be sampled. Thus, sonding one well would cost roughly \$2,000, two wells would cost \$2,800, and so on.

These costs are considerably cheaper than mobilizing a drilling rig specifically for the collection of soil/sediment cores for the analysis of magnetic susceptibility. This is the primary advantage of using the in-well sonde. If a drilling rig is already on site, samples can be obtained from the proper location, and continuous coring is already occurring, then using soil borehole samples analyzed in a fixed-based laboratory is probably the more economical way to go. As shown in this report, both the downhole sonde and soil borehole data analyzed in a fixed-base laboratory give similar results, so the choice of which methodology to utilize will depend primarily upon where the site characterization effort for the site stands. Because rental costs are fixed and well sampling must be completed at a specific rate, economies of scale are not likely to be significant with downhole sonde measurements.

#### 7.3.2 COST ELEMENT 2 – GOUNDWATER SAMPLE COLLECTION FOR <sup>14</sup>C-LABELED TCE ASSAY, EAPS, AND qPCR ANALYSES

This cost element includes mobilization of a two-person field crew to the field for three days to collect eight (8) groundwater samples for the <sup>14</sup>C-Labeled TCE assay as well as EAPs and qPCR analyses. Mobilization includes making all arrangements for equipment rental and site access. It is assumed that the wells to be analyzed have already been selected. Included in the costs are purging of up to three (3) casing volumes for wells up to 100 feet deep and the collection of DO, ORP, pH, temperature, and specific conductance data using a flow-through cell during well purging. It is assumed that sampling of these eight (8), 100 foot-deep wells will take three (3) days. These costs include the rental of all necessary equipment as well as labor hours. Table 7.1 summarizes the costs for this cost element. These costs for renting and obtaining the equipment, and adding it to the per-well cost of \$1,220 times the number of wells to be sampled. Thus, sampling one well would cost roughly \$2,620, two wells would cost \$3,840, and so on. This cost element is required for implementation of cost elements 3, 4, and 5.

#### 7.3.3 COST ELEMENT $3 - {}^{14}C$ -TCE ASSAY

The cost estimate is based on custom-synthesized <sup>14</sup>C-TCE and associated supplies, including liquid scintillation cocktail, liquid scintillation vials, supplies for the gas chromatograph (gases, septa, syringes), serum bottles, and reagents. The cost of the custom synthesized <sup>14</sup>C-TCE is based on 1 mCi (\$11,000) and a total of 500 bottles. Assuming triplicate bottles per groundwater sample, the sample cost of \$66. Other material and supply costs are estimated at ~\$150 per sample, for a total supply cost of ~\$216 per sample.

Staff labor to perform the assay was estimated at four hours per sample (from preparation through clean-up, plus data reduction). At \$50/hr, the staff labor is estimated at \$200 per sample. Time for supervisory labor is estimated at 10% of the staff and \$150/hr, or \$60 per sample. This brings the total cost to \$476 per sample.

As the assay matures, there will no doubt be opportuties to bring the costs down. This has certainly been the experience with application of molecular tools to groundwater contamination. Regardless, the pay-off from using the <sup>14</sup>C-assay may be considerable. An assay based on <sup>14</sup>C product accumulation from <sup>14</sup>C-TCE affords an opportunity to determine realistic decay rates that can be used in groundwater models to predict if MNA will be successful. Absent this type of information, there is considerable uncertainty in what constitutes an appropriate rate to use in modeling.

#### 7.3.4 COST ELEMENT 4 – ENZYME ACTIVITY PROBES

EAP and qPCR will be applied to groundwater samples taken from monitoring wells. This cost element includes sample bottles and material for sample processing for shipment to lab, EAP probes, filters, microscope slides, other reagents required for sample preparation. This cost analysis assumes that equipment such as vacuum pumps or house vacuum supply, fluorometer (coumarin) and a microscope with epifluorescence capability is available for use. Total supplies costs for eight samples will be approximately \$200.

Staff labor is estimated at five hours per probe per sample. For eight groundwater samples and triplicate analysis per sample, a total of 20 hours will be required for the analysis, which includes sample filtration and manual enumeration using epifluorescence microscopy. Blanks, positive controls and matrix spikes are included in per unit cost for the analyses, so these analyses will require an additional 20 hours per sample. The time for the project Principal Investigator is approximately 10% of the staff time, or 4 hours. Staff time for data reduction is estimated to require 10% of the analysis time, or 4 hours. The time for the project Principal is estimated to be 5% of the analysis time, or 2 hours. Table 7.1 summarizes the costs for this cost element. These costs are for the demonstration and include PNNL cost schedule and burden rates. For analysis of eight samples with four EAP (3-hydroxyphenylacetylene, phenylacetylene, cinnamonitrile and coumarin), and counterstaining with 4',6-Diamidino-2-phenylindole dihydrochloride (DAPI) by a commercial laboratory or university core facility is estimated to be approximately \$400 per EAP per sample. Eight samples could be analyzed for \$13,000 which includes the supplies estimate from above. Adding the costs for analyzing the data (data reduction and reporting), the per-sample cost for this analysis is about \$1,900. Table 7.1 summarizes the costs for this cost element. These costs are for this demonstration. It is anticipated that unit costs will decrease significantly if this process is commercialized.

Because the CINN EAP marker does not provide an unequivocal prediction of the rate constant, the CINN EAP marker can only be used to identify groundwater where the predicted rate constants are possible.

#### 7.3.5 COST ELEMENT 5 – qPCR ANALYSES

This cost element includes sample bottles and material for sample processing for shipment to lab, DNA extraction kits, filters, oligonucleotide primers, DNA polymerase core kits, 96-well PCR plates and other reagents required for sample preparation and preservation.

Due to the nature of the analyses, blanks, standards, and positive controls can be processed in parallel in the same PCR plate. Blanks, and positive controls are included in per unit cost for the analyses and do not require additional time. Staff time for data reduction and reporting is estimated to require 8 hours. The time for the project Principal Investigator is estimated to be 3 hours.

Table 7.1 summarizes the costs for this cost element, not including sample collection costs. These costs include CENSUS-DNA data and are based on a cost estimate from Microbial Insights in Knoxville, TN. CENSUS-DNA data included in the costs presented in Table 7.1 include costs for:

- Toluene Monooxygenase--RMO
- Toluene Monooxygenase 2--RDEG
- Phenol Hydroxylase--PHE
- Toluene Dioxygenase--TOD
- Xylene Monooxygenase--TOL
- Soluble Methane Monooxygenase--SMMO

The per-sample cost for these analyses is roughly \$835 per sample, including data analysis and reporting costs. The benefit of the *q*PCR analyses is that they allow the user to determine if aerobic cometabolism is possible. Because the PHE and RMO qPCR markers do not provide an unequivocal prediction of the rate constant, the PHE and RMO qPCR markers can only be used to identify groundwater where the predicted rate constants are possible. The markers should to be used as a primary line of evidence to predict a rate constant.

#### Table 7.3.1. Cost Model

#### Eight samples each for magnetic susceptibility, <sup>14</sup>C-labeled TCE assay, EAPs, and qPCR

	1           1         \$400           4         4           2         2           2         \$500           3         \$476           3         \$476	(total) 3 3 3 8	daily TASK : each each	\$1,200 SUBTOTAL \$1,500 SUBTOTAL \$3,808	\$ \$ \$ \$ \$ \$ \$	3,200 1,600 1,600 7,600 1,400 6,400 1,700 1,640 11,140 3,808 1,460
	1 \$400 4 2 2 2 3 \$500 3 \$476	3	TASK : daily TASK : each each	SUBTOTAL \$1,500 SUBTOTAL \$3,808	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	1,600 1,600 7,600 1,400 6,400 1,700 1,640 1,700 1,640 1,140 3,808 1,460
	1 \$400 4 2 2 2 3 \$500 3 \$476	3	TASK : daily TASK : each each	SUBTOTAL \$1,500 SUBTOTAL \$3,808	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	3,200 1,600 1,600 7,600 1,400 6,400 1,700 1,640 11,140 3,808 1,460
2	4 2 2 \$500 3 \$476	3	TASK : daily TASK : each each	SUBTOTAL \$1,500 SUBTOTAL \$3,808	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	1,600 1,600 7,600 1,400 6,400 1,700 1,640 1,700 1,640 1,140 3,808 1,460
2	4 2 2 \$500 3 \$476	3	TASK : daily TASK : each each	SUBTOTAL \$1,500 SUBTOTAL \$3,808	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	1,600 7,600 1,400 6,400 1,700 1,640 1,700 1,640 11,140 3,808 1,460
2 2 	2 2 \$500 3 \$476		daily TASK : each each	\$1,500 SUBTOTAL \$3,808	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$	7,600 1,400 6,400 1,700 1,640 11,140 3,808 1,460
	2 \$500 3 \$476		TASK and the each each	SUBTOTAL \$3,808	\$ \$ \$ \$ \$ \$	6,400 1,700 1,640 11,140 3,808 1,460
	2 \$500 3 \$476		TASK and the each each	SUBTOTAL \$3,808	\$ \$ \$ \$ \$ \$	6,400 1,700 1,640 <b>11,140</b> 3,808 1,460
2	\$500 3 \$476		TASK and the each each	SUBTOTAL \$3,808	\$ \$ \$ \$	1,640 11,140 3,808 1,460
	3 \$476		TASK and the each each	SUBTOTAL \$3,808	\$ \$ \$ \$	<b>11,140</b> 3,808 1,460
	3 \$476		TASK and the each each	SUBTOTAL \$3,808	\$ \$ \$ \$	1,640 11,140 3,808 1,460
	\$476	8	each each	\$3,808	\$ \$ \$	<b>11,140</b> 3,808 1,460
		8	each each	\$3,808	\$ \$	3,808 1,460
		8	each	,	\$	1,460
				SUBTOTAL	\$	5,26
	4 \$1,625	8	each	\$13,000	\$	13,800
2	3		each		\$	1,460
			TASK	SUBTOTAL	\$	15,260
	\$275	8	each	\$2,200	\$	2,200
	\$75	8	each	\$600	\$	600
	\$75	8	each	\$600	\$	600
						600
						600
		ð		2000		600
÷	2			SUBTOTAL		1,460 6,660
2	26		Total			21,22 24,70
8 56	8	\$75 \$75 \$75 \$75 \$75	\$75 8 \$75 8 \$75 8 \$75 8 8 3	\$75         8         each           \$75         8         each           \$75         8         each           \$75         8         each           8         3         each           TASK	\$75         8         each         \$600           \$75         8         each         \$600           \$75         8         each         \$600           \$75         8         each         \$600           8         3         each         TASK SUBTOTAL           56         26         Total Labor Costs	\$75       8       each       \$600       \$         \$8       3       each       \$       \$         TASK SUBTOTAL       \$

#### Notes and Assumptions

a/ Other direct cost in the form of laboratory analyses, field analyses, or equipment rental

b/ Assumes sonding of 8 boreholes to depths of 100 feet below ground surface.

c/ Assumes purging 3 casing volumes from 8 groundwater monitoring wells that are completed to a depth of 100 feet below ground surface and collecting groundwater samples for submission to the analytical laboratory.

d/ Does not include the cost of obtaining the sample, the costs for which are included under Item 2, Groundwater Sample Collection.

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### 8.0 IMPLEMENTATION ISSUES

This section provides information that will aid in the future implementation of the technology. A brief description and references for other documents such as guidance or protocols are provided. The technology elements described in this document were developed or refined because of shortcomings identified in ESTCP (2015). Specifically, the lack of a way to quantify the degradation of the chlorinated ethylenes by magnetite after intrusive site characterization activities (i.e., drilling) had been completed, and the lack of a method to conclusively show and quantify aerobic cometabolism of TCE. The technologies presented in this report represent an improvement over that presented in ESTCP (2015).

Lessons learned during the demonstration are as follows:

- The only regulations that apply to the use of the technologies presented in this report are the permits required to use of the <sup>14</sup>C assay. The analytical laboratory must obtain certification in order to handle <sup>14</sup>C.
- The magnetic susceptibility sonde provides a readily-accessible and accurate alternative to intrusive soil borehole data collection for magnetic susceptibility.
- The magnetic susceptibility sonde cannot be used in stainless steel wells. Wells larger than 4 inches in diameter may be problematic for collecting accurate magnetic susceptibility data using the sonde identified in this report because of the size of the borehole required for such wells. However, larger sondes, with a larger radius of influence, are available.
- Metallic tools dropped into boreholes in which monitoring wells are subsequently installed will interfere with the magnetic susceptibility sonde, but are readily identifiable.
- As mentioned above, <sup>14</sup>C assays can only be performed in laboratories that are permitted to use radioactive material. Furthermore, the cost for <sup>14</sup>C-labeled TCE is considerable (~\$11,000 per mCi), mainly because it is no longer available as a stock compound and must therefore be custom synthesized. If the assay is adopted for more frequent use, suppliers may opt to once again provide <sup>14</sup>C-labeled TCE as a stock item, which will decrease the cost.
- The <sup>14</sup>C assay is not yet commercialized. It is hypothesized that the successful demonstration of the protocol presented in this report will provide considerable motivation for private companies to offer the service. An analogous situation was the use of compound specific isotope analyses (CSIA). At one time, use of this technology for groundwater samples was limited to a select few academic laboratories. As the value of the approach became apparent, commercial laboratories stepped in to meet the growing demand. We anticipate that a similar outcome will develop for the <sup>14</sup>C assay proposed in this study.
- EAP at the current level of development are only a qualitative predictor of aerobic bioremediation, since probe response was never adequately calibrated to the actual rate of contaminant biodegradation in groundwater at field sites. EAP analytical services are currently only available through PNNL.

• *q*PCR can be affected by biases associated with DNA extraction, as well as issues associated with efficiency of DNA amplification.

Overall, implementation issues are negligible, and the technologies presented herein should allow the decision framework (and BioPIC) presented in ESTCP (2015) to be updated so that additional degradation pathways can be readily elucidated and quantified.

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## APPENDIX A POINTS OF CONTACT

Point of Contact Name	Organization Name	Phone Email	Role in Project
Todd Wiedemeier (deceased)	T.H. Wiedemeier & Associates, Inc.	(303) 670-7999 todd@thwa.com	Principal Investigator
Dr. John T. Wilson	Scissortail Environmental, LLC	(580) 421-3551 john@scissortailenv.com	Senior technical advisor to the team on MNA and abiotic processes, participation in field work, and report development.
Dr. David L. Freedman	Clemson University	864-656-5566 dfreedm@clemson.edu	Senior technical advisor on aerobic microbial aspects. Lead on <sup>14</sup> C-labeled TCE assay for degradation rates.
Dr. Brady Lee	Pacific Northwest National Laboratory (Federal Partner)	509-375-4593 brady.lee@pnnl.gov	Senior technical advisor for enzyme activity probes and qPCR assays.

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## APPENDIX B DAILY FIELD AND SAMPLING REPORTS

5-31-16

DAILY FIELD ACTI	Page / of
DAILT FIELD ACT	
Client Name: Project Name: <u>ESTCP - 201584 TCAAP</u> SI Contractor: Weather:	Project Number: TE A Date: $M \partial uy \exists 1, 201/b$ Arrival Time: $TCAHP T: 30 Am$
Time Breakdown: Drive: Work:	Standby:
Location and Description of Activities: Onste 10:20 mm	
Equipment Used on Project:	
Activity Summary and General Remarks: 13.87 dept to water Well policitor to top on Case	Well 014/08 Ma = 2 inches
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#### DAILY FIELD ACTIVITY REPORT

	Client Name: Project Name: <u>FSTCP201584</u> TCAAP Contractor: Weather:	Project Number: Date: Arrival Time:
	Time Breakdown: Drive: Work:	Standby:
	Location and Description of Activities:	
	Equipment Used on Project:	Calip 2? Calip 2?
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## GROUNDWATER PURGE AND SAMPLING FORM

Project Name: ESTCP -201584 - TCAAA Site Acoc Number: Well ID: OIU108 Date of Collection: 5731/16

Sample Collected by:\_\_\_\_

#### EQUIPMENT

Purging Equipment:

Sampling Equipment:

Filtering Equipment:

Equipment Decontamination:

Per Work Plan - Alconox Wash with Triple Rinse and Isopropyl Alcohol Rinse + Calibration

	Serial Number	Date Calibrate		
Equipment/Model	05C1520 AA			
YSI 556 Multi Parameter Meter	00010201	N/A		
HACH DR 890 Colorimeter		INIX		

#### FIELD PARAMETERS

Ambient Air Temperature (°F):\_ Sampling Depth (ft): Pump Inlet@ Weather Conditions:\_

Reference Point: Top of inner PVC casing

Flow meter (gallons)	Flow rate _/min	Depth to water	Time	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comments
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D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach	Filtered Manganese mg/l Hach	Filtered Manganese mg/l Chemetrix (Visual)	Non Filtered Manganese mg/l Hach	Comments

#### PURGE INFORMATION

Starting Flow meter Reading:	Ending Flow me	ter Reading:	Flow Rate:
	Purged Dry (Y/N):		
	<u>2</u> <sup>"</sup> Initial Depth to W n) Tubing & Pump Volum (psi) Discharge (sec.) Re	me (ml)	

Casing Volume Calculation (gallons): 2" well = 0.17 x WCT 4" well = 0.66 x WCT 6" well = 1.47 x WCT

Where WCT = Water Column Thickness (feet)



Title: Date Rev By Date Ck WIEDEMEIER Job: Of Sheet Author: 014108 Distance between Site Protective Casing & top of PVC = 2" Steel is 32" Tall from Evound TOC (PVC) = 30" above four Surface For the 453 the depth Correction is 4,768-6 1,700 For the EMP Probe the Dipth Corvention is 5,68 fut Left Right Z- Point Calibration

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#### DAILY FIELD ACTIVITY REPORT

Client Name: <u>ESTOP 201584 TOAA</u> P Project Name: Contractor: Weather:	Project Number: Date: <i>Dib</i> Arrival Time:?; 30
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Location and Description of Activities:	
Equipment Used on Project:	
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		Decontamin	ation:											
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							Seri	al Number			Date Calibrated			
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### Figure 5.5.1

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#### DAILY FIELD ACTIVITY REPORT

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Project Name: ESTCP 2015R4	Date: $b - i - l_{\phi}$
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Equipment Used on Project:	
Activity Summary and General Remarks:	
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Casing Volume Calculation (gallons): 2" well = 0.17 x WCT 4" well = 0.66 x WCT 6" well = 1.47 x WCT

Where WCT = Water Column Thickness (feet)

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### **GROUNDWATER PURGE AND SAMPLING FORM - Continued**

Project Name: <u>FSTCA 2015</u>84 Well ID: <u>TCAAA 010115</u> Sample Collected by: <u>TTW/BHW</u> Date of Collection: <u>6/1/16</u>

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Trind 2014115 #3 6-1-1	6			7		,
-TCDAP01415 ## [6-1-1	16 1			2		
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Trip Blank le-1-16	e					
						,
Possible Hazard Identification	Unknown	Sample Disposal	Disposal By Lab	(A fee may be (A fee may be a volume for)	(A fee may be assessed if samples are retained ionger than 1 month)	
Required 74.0			Š			•
		Time	1. Received By		Date	
all the contract of the second	(	16:48	o Dominad Bu	1	Data Tima	1.43 •
2. Helinquished By	Date	aun				· · · · ·
3. Relinquished By	Date	Time	3. Received By		Date	
Comments				1		
DISTRIBUTION: WHITE - Returned to Client with Report: CANARY - Stays with the Sample: PINK - Field Copy	ays with the Sample: Pli	VK - Field Copy				

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Chain of		SEVERN TRENT	T STL	STL Denver
Custody Record		Severn Tr	Severn Trent Laboratories, Inc.	4333 10100 30000 Arvada, CO 80002
STL-4124 (0901)			~	
	Project Manager			Chain of Custody Number 345882
	Telephone Numb	x Number	Lab Number	
COUNT ON ONALD DI TO COM		$\frac{1}{2} \frac{1}{2} \frac{1}$	Analysis (Attach list if	
			o more space is needed)	
	Carrier/Waybill Number		0 =	Special Instructions/
Contract/Purchase Order/Quote No.	Matrix	Containers & Preservatives	UT C	Conditions of Receipt
Sample I.D. No. and Description Containers for each sample may be combined on one line) Date	Tito Balance International Int	AªOH Zuych HCi HSz0¢	ीटर <i>भ</i>	
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TUNPOILIS I K-I-1-16				
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Terhanonuns 3 6	7			
Possible Hazard Identification	Sample Disposal			assessed if samples are retained
mmable 🔲 Skin Irritant 📃 Poison B	Unknown	Disposal By Lab	Months	longer than 1 month)
	Other.	nts (Spe		
111 L	Date Time	1. Received By		Date
2. Relinquished By	1	2. Received By		Date
3. Relinquished By	Date	3. Received By		Date Time
Comments	-			
DISTRIBUTION: WHITE - Returned to Client with Report. CANARY - Stays with the Sample; PINK - Field Copy	th the Sample; PINK - Field Copy			

Page  $\int of l$ 

# DAILY FIELD ACTIVITY REPORT

Client Name:	Project Number:
Project Name: TCAAP ESTEP2015	
Contractor:	Arrival Time: <u>8:35</u>
Weather: <u>Cloudy</u>	
V Time Development Deine	
Time Breakdown: Drive: W	Vork: Standby:
Onsite S'35 Am Location and Description of Activities:	
$O[\mathcal{U}]$	
Equipment Head on President	
Equipment Used on Project:	
······	
······································	
Activity Summary and General Remarks:	.her
13.89/tdeptn to U	vate Toc
V	
1) 34.81ft Bottomon	well TOC softbottom
(2) 34,98 ft Batton g	will TOC Soft battom
28517-DC 40 1	well TOC softbottom well TOC Softbattom riddle wellsereen
	uddu warshur
14aal = 1 pour 1	volume 21 pt water
Puysle - DNA 7	f
Duiz - KNA	preservativi
D. Clemson Somplie	IA2 = 01U117 b-2-16
- Clemson Somplia	
10:27 H Samples	PNNL (each [Liter]
TCNAP (	214117 Samples 1-4
10:30 3 Samples C	Lenson <u>EAS #1, IN2#2, 192#3</u>
Technician Signature: (~ 100 mil each	$-3$ $TB_{+} = 1B_{+} = 2$ , $1B_{+} = 3$
Technician Signature:	MJORPHIN TCAAPIOUILY DNA 1000
on 10:34 DNA & Samples	microhial TCAAPIOUII7 DNA 1000
SOML 10:49 KNH	Insights TCHAPIONIT RNA
C:\Admin\Forms\Daily Field Activity Report.doc	Samples from WIEDEMEIER
C:\Admin\Forms\Daily Field Activity Report.doc	will & ASSOCIATES

Proje	ect Na	ame:	STC	P 20	1584	TCI	9AP		COC N	umber:	·
Sam	ple Co	ollected	by: <u>Jo</u>	hNW	ilsm.	Roch	wa vali	lsn	Well II Date of	Collection	117
	JIPME										
			t:								
-	-	Equipme									
		Equipme									
	-	t Decont		<u></u>	Per Wa	vrk Plan _	Alconox W	Vach w	th Triple	Dince and	Isopropyl Alcohol Rinse
Lqui	pinen			<u> </u>			ent Calibra		ui inpi		<u>Isopropyr Alconor Kinse</u>
		Ea	uipment/l	Model		Equipm		Numbe	r		Date Calibrated
					tor			520 AA			
YSI 556 Multi Parameter Meter HACH DR 890 Colorimeter						0301	520 AA				
HACH DR 890 Colorimeter N/A							N/A				
<u>FIEL</u> Ambi	FIELD PARAMETERS         Ambient Air Temperature (°F):       60         Weather Conditions:										
Sampling Depth (ft): Pump Inlet@					_			-	ner PVC cas	ing	
Flo	w	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pH	ORP	Water
me		rate		9:27	Purged	(°C)	(µS/cm)	(mg/L	· ·	(mV)	Description/Comments
(gall	ons)	/min	tt to water	Time 9	(Gallons)						
			13.89	0	0						
				1:44							
				4:47	<u></u>						
				8:01	3						
				10:46	<u>    4                                </u>				_		
				13:30					_		
				16:24 19:11	<u> </u>	10.33	.456	1. 1.1	7.16	233.7	A A A A A A A A A A A A A A A A A A A
				22:11	8	10.29	1453	6.44 6.31		289.5	coloress, no tur
				25:04	9	10.18		6.51			
				28:02	10		455	5.94	6.10	2 262.8	
				30:55	<u> </u>	10:53	.458	5.51		248,4	
				33:50	12	10.63				- 243.5	
				36:54	/3	10.65		5.12	. 6.93	245.6	
		≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
				L				· · · · · · · · · · · · · · · · · · ·			······
D.O	. mg/l	Filtered Alk mg/l	Non Filtered	Filtered Fe2+	Filtered Fe2+ mg/l	Non Filtered Fe2+ mg/l	Filtered Mangane		Filtered anganese	Non Filtered Manganese	
	metrix isual)	Hach	Alk mg/l Hach	mg/l Hach	Chemetrix (Visual)	Hach	mangane mg/l Hach	с	mg/l hemetrix Visual)	mg/l Hach	Comments

# **PURGE INFORMATION**

Starting Flow meter Reading:	Ending Flow meter Reading:	Flow Rate:
Total Volume Purged: 1401 Purg	ed Dry (Y/N): <u>N</u> Micro purged (	Y/N): <u>M</u> _Minimal purged (Y/N):
	Initial Depth to Water (feet) $13.8$	9 Depth to bottom of well (feet)34,95
Controller settings: Pressure (psi)		(sec.)
Casing Volume Calculation (gallons): 2" well = $0.17 \text{ x}$	WCT 4" well = 0.66 x WCT 6" well = 1.47 x WCT	Where WCT = Water Column Thickness (feet)

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Page 1 of 2

#### **GROUNDWATER PURGE AND SAMPLING FORM - Continued**

Project Name: <u>ESTCP 201584 TCAAP</u> Sample Collected by: <u>JOHN Wilson / Barbara Wilson</u> Date of Collection: <u>6 - 2 -16</u>

Flow Meter (gallons)	Flow rate _/min	Depth to water	Time	Volume Purged (Gallons)	Temp (°F)	Sp.Cond µS/cm	DO (mg/L)	pН	ORP (mV)	Water Description/Comments
			39:5	14	10.107	1462	4.71	6.98	243.8	
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	> 40 < 200				. 100/	100/				
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	



Page \_ 1 of \_ 1

# DAILY FIELD ACTIVITY REPORT

Client Name:	Project Number:
Project Name: TCAAP ESTCP 201584 Contractor:	Date: $6 - 2 - 16$ Arrival Time: $11/10$
Weather: Partly Sunny	
Time Breakdown: Drive: Work: II'. 10 or of Activities: Location and Description of Activities: OIUII9	
Equipment Used on Project:	· · ·
Activity Summary and General Remarks:	
21:35 betterney will	ter TOC TOC
Purge Volume = 10gal Set Tubing at 16ft 5	Thefor TUC
182#1,2,3 Clemson	TCAAP OIU119
13: 02 3 Samples PNNL TCAAP 13: 02 3 Samples Clemson TCAA 13:12DW 2 Samples Microbia Insight 13:21 RNR	DIUILY Samples 1-4 (11 each) POIULY 132#1,2,3 (2100m Leach) 5 TCAAPOIULY 1-DNA: 1-RNA presence 1000mL 1000ml
finisks preizing 12:35	
12:40 Fe2t 0.10mg/L.	
	· · · · · · · · · · · · · · · · · · ·
Technician Signature:	Date:
C:\Admin\Forms\Daily Field Activity Report.doc	WIEDEMEIER & ASSOCIATES

			GNU	UNDWA	ILKFU	KGE AN	D SAM	FLING	<b>FUKIVI</b>	
Project N	ame: <u>E</u>	STCP	2015	584 -	TCAA	-P		COC Nu		
Project N Sample C	ollected	oy: Joh	nW:	Ism/boc	borai	loon	V I	Vell ID: Date of C	OIUI Collection	19 : 6-2-16
EQUIPM										
Purging E		t٠								
Sampling										
Filtering										
0			on:	Per Wo	ork Plan –	Alconox V	Vash wit	n Triple I	Rinse and I	sopropyl Alcohol Rinse
-1-1						ent Calibra		<u></u>	timbe und I	
	Eq	uipment/I	Model			Serial	Number			Date Calibrated
YSI 556 Multi Parameter Meter						05C1	520 AA			
HACH DR 890 Colorimeter					-					N/A
		<u> </u>		I					I	
FIELD PAI Ambient Ai	<u>KAMETER</u> ir Temperat	<u>.S</u> ture (°F):	63°			Weather Co	onditions			
Sampling D	epth (ft):	Pump I	nlet@	· · ·					er PVC casi	ng
Flow				Volume					r	-
meter	Flow rate	Depth to	Time	Volume Purged	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	pH	ORP (mV)	Water Description/Comments
(gallons)	/min	water	12:10	(Gallons)		(µ0/em)	(		(	Description/Comments
		6.12	0.0	0				l		
			3:17		9.3	.599	1.89	6.71	2223	light ala
			4:3	23	8.88	.657	1.39	6.67	2241	light color
			6:54	- <u>3</u>	8.64	.750	1.16	6.65	2247	light color
			11:09	4	0.50	.841	.90 .81	6.68	2365	ho color
			13:10	6	8.55	.856	173	6.71	227.3	no color
			15:13	1	8.49	.882	·H	6.72	233,9	1
			17:16	8	8.47	1864	182	6.73		
			19:23	9	8.58	.864	.88	6.74	230.1	
			21:28	10	8.59	.862	197	6.76	226.3	
			22,41		ant (le	t b. la	.96 NO TO	6.77	2232	Y
				<u> </u>	par ve	1 Lien	10 10	ř		
					· · · · · · · · · · · · · · · · · · ·					
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
					I					
D.O. mg/l Chemetrix	≥40 ≤200 Filtered Alk mg/l	Non Filtered	Filtered Fe2+	Filtered Fe2+ mg/l	±10% Non Filtered Fe2+ mg/l	d Filtered Manganes	Fil se Man	tered ganese	Non Filtered Manganese	
D.O. mg/l Chemetrix (Visual)	Filtered			Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered	d Filtered Manganes mg/l	se Fil Fil Se Man r Che	tered ganese ng/l metrix	Non Filtered Manganese mg/l	Comments
Chemetrix	Filtered Alk mg/l	Filtered Alk mg/l	Fe2+ mg/l	Fe2+ mg/l Chemetrix	Non Filtered Fe2+ mg/l	d Filtered Manganes	se Fil Fil Se Man r Che	tered ganese	Non Filtered Manganese	Comments

# **PURGE INFORMATION**

Starting Flow meter Reading:	Ending Flow meter Reading:	Flow Rate:
Total Volume Purged: 10.668 Purged	Dry $(Y/N)$ : <u>M</u> Micro purged $(Y/N)$ :	Minimal purged (Y/N):
Casing Inner Diameter (inches) 4 In Tubing inner diameter 40 (in) Tubin Controller settings: Pressure (psi) Dia	nitial Depth to Water (feet) (0, 12 D ng & Pump Volume(ml)	

Casing Volume Calculation (gallons): 2" well = 0.17 x WCT 4" well = 0.66 x WCT 6" well = 1.47 x WCT

Where WCT = Water Column Thickness (feet)

WEDEMEIER

& ASSOCIATES

Icasing = 10gal Volume

 $D: \label{eq:constraint} D: \label{eq:constraint} D: \label{eq:constraint} D: \label{eq:constraint} THWA \label{eq:constraint} Admin \label{eq:constraint} Forms - Field \label{eq:constraint} Groundwater \label{eq:constraint} Purge and \label{eq:constraint} Sampling \label{eq:constraint} Forms - Field \label{eq:constraint} Sampling \label{eq:constraint} Sampling \label{eq:constraint} Sampling \label{eq:constraint} D: \label{eq:constraint} THWA \label{eq:constraint} Admin \label{eq:constraint} Sampling \label{eq:constrain$ 

STL-1124 (0001)       Client       Client       Project Manager         Client       Control       Client       Project Manager         Address       Control       Control       Control         Control       Control       Control       Control         Control       Control       Control       Control       Control         ContractPurchase Order/Duote No.       ContractPurchase Order/Duote No.       Matrix         Sample I.D. No. and Description       Date       Time       Address         Contacts for each sample may be combined on one line)       Date       Time       Control         T       T       Control       Control       Control       Control         ContractPurchase Order/Duote       Control       Control       Control       Control       Control         ContractPurchase Order/Duote       Control       Control       Control       Control </th <th>Containers &amp; Containers &amp; Containers &amp; Ana Preservatives Preserv</th> <th>Date Date Lab Number Analysis (Attach list if more space is needed)</th> <th>Chain of Custody Number <b>Page</b> <i>of of conditions of Receipt</i></th>	Containers & Containers & Containers & Ana Preservatives Preserv	Date Date Lab Number Analysis (Attach list if more space is needed)	Chain of Custody Number <b>Page</b> <i>of of conditions of Receipt</i>
Sol CCOLL     D     Telephone Number (       ess     CCOLL     State     Zp Code       State     Zp Code     State (     State (       CCL     State     Zp Code     State (       State     Zp Code     State (     State (       CCL     State (     State (     State (       Tactic H H P CULUE     N     Date (     Time (       CL     N     State (     State (       Sample ID. No. and Description     Date (     N       Time italiners for each sample may be combined on one line)     Date (       CL     CL     State (       CL     CL     State (       CL     CL     State (	ax Number ax Number D Contact P C Co	Lab Number Attach list if re space is needed)	Page of of Conditions of Receipt
State     Zip Code     State     Zip Code     State     State <th>b Contact CC Contact CC Containers &amp; Preservatives HNU03 HNU</th> <th>re space is needed)</th> <th>Special Instructions/ Conditions of Receipt</th>	b Contact CC Contact CC Containers & Preservatives HNU03 HNU	re space is needed)	Special Instructions/ Conditions of Receipt
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Date Time Air Aurous	+/ ]		
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Same & 6-2			
Sample 2 6-3 Sample 1 6-5			
Sauge 1 6-60	<u>د</u>		4 
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Clung Sander	<u> </u>		
	1	(A fee may be as	sessed if samples are retained
🕡 Non-Hazard 🛛 Flammable 🗌 Skin Irritant 🔲 Poison B 🔲 Unknown 🔲 Return To Client	Disposal By Lab 🛛 Archive For	Months longer than 1 mo	longer than 1 month)
squired 48 Hours 7 Davs 14 Davs 21 Davs 00ther	QC Requirements (Specify)		
	1. Received By		Date
	2. Received By		Date
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Chain of Custody Record		SEVERN TRENT Severn Tren	SEVERN STL TRENT Severn Trent Laboratories, Inc.	<b>STL Denver</b> 4955 Yarrow Street Arvada, CO 80002	
STL-4124 (0901)					
Client Client Client Client Client	Project Manager	e lemeir r	2  0910 2  0-2-16	Chain of Custody Number 345883	
	Telephone Number (Area Code)/Fa		,	Page of /	
	ntact	Lab Contact	ed is		l
	Carrier/Waybill Number	Davidreeuna	Э.) 	Special Instructions/	
rchase Orde/Outor No.	Matrix	Containers & Preservatives	L 64	Conditions of Receipt	
Sample I.D. No. and Description (Containers for each sample may be combined on one line)	IioS ibeS	Langes Langer HOBN HOBN HOBN HOBN	75 M		I
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Possible Hazard Identification	Sample Disposal	t Disposal By Lab Archive For	Months	(A fee may be assessed if samples are retained longer than 1 month)	
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2. Relinquished By	Date	2. Received By		Date Time	
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DISTRIBUTION: WHITE - Returned to Client with Report: CANARY - Stays with the Sample; PINK - Field Copy

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	Knoxville, TN 865-573-8188 www.microbe.	<b>se Ch</b> e More No Ac	(%)		RDEG (Toluene Monooxygenase)										1	ple.
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INVOICE TO: (For Invoices paid by a third party it is imperative that all information be provided) Name: ・ ノルレビ科 デ州 (Company: Address:	email: Phone: Fax:	Purchase Order No. Subcontract No. MI Quote No.	l raw data(15% surcharge) □ Microbial Insights L □ All other available EDDs (5% surcharge) 22 9400 (0-00 on 5.500 on 5.51 M.51 A452 bound	Analyses	SON						╈	╋			Rece	It is vital that chain of custody is filled out correctly & that all relative information is provided. Failure to provide sufficient and/or correct information regarding reporting, invoicing & analyses requested information may result in delays for which MI will not be liable.
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REPORT TO: Name: Company: Address:		Project Manager: Project Name: Project No.:	. <b>'pe:</b>	Inde	Climboratory Use Only										Relinquished by:	
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Purging	Equipmen	t:		HMA	1 45	35	May	15	ins 5	and
*	g Equipmer		-					-		
-	ent Decont		on:	Per Wo				Triple	Rinse and	Isopropyl Alcohol Rinse
-	Ea	uipment/	Model		Equipm	ent Calibrat Serial	Number			Date Calibrated
2-1		Multi Para		ter			520-AA			
	НАСН	DR 890 C	colorimete	er						N/A
Ambient	ARAMETER Air Temperat Depth (ft):				_	Weather Co Reference I			er PVC cas	sing
Flow meter (gallons)	Flow rate /min	Depth to water	Time	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comments
11:30.	Phe	i to	b1@	-25	fut	for a	Guili	brat	ters up	Kyo Teny
-12:30	AF	ter	Zero	mu	Soul	le M	atri	- 10	gaind	Sustern
	read	: 2	8,49	below	2 Top	d F	VC	8 à	Sinch	1 moveus
	me	sare	Ve	alue	dr.	29,65	BTO	e wi	th	unter -
	leve	e1	Prob	e	/					
0	Begin	Equ	ipmes	st Ca	librat	tion	0	an	et 5	X10=3 ST
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
	A 11 /1	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach		e Man n Cher	ered ganese gg/l netrix sual)	Non Filtered Manganese mg/l Hach	Comments
D.O. mg/ Chemetriz (Visual)					1					
Chemetri: (Visual) PURGE	INFORM low meter		10	=5, Endin		Long neter Read	ing:		Flow Rat	e:
Chemetric (Visual) PURGE Starting F Total Volu	low meter ume Purge	Reading	: Pur	Endin ged Dry (`	ng Flow r Y/N):	neter Read Micro	purged (	Y/N):	Min	e: imal purged (Y/N): ottom of well (feet) 97 Z9, 6

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	Project Na Sample C	ame:	by: T	F-	-Man	h Fe	ever	V	/ell ID	umber: Collection	
-	EQUIPM Purging E Sampling Filtering I Equipmer	quipmen Equipme Equipmen	ent:			nrk Plan -	Alconox W	Vach with	Triple	Rinse and	Isopropyl Alcohol Ring
			ammatic	/11	101 110		ent Calibrat		mpie	Trinoe una	
		Eq	uipment/N	Model			Serial	Number			Date Calibrated
			Multi Para				05C1	520 AA			
		HACH	DR 890 C	olorimete	er						N/A
	FIELD PAF Ambient Ai Sampling D	r Temperat	ture (°F):_	nlet@		_	Weather Co Reference I			ner PVC cas	ing
	Flow meter (gallons)	Flow rate /min	Depth to water	Time	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comme SI Units
fg .	~ Rive	111	114 1	Dow	10	1 to	linin				Calif 1 Sette
w	pun	- 1100		EDDW		3	1021-1				0= 60,586
felve	Ru	1/4	aliol	u	p 1	\$ 14	=/m	5			SE-3 = 1160,53
Ipriv	Ru	n 2	Jeali	b /	upon	ing -	7 ft/	min			
						±10%	±10%	±10%	±0.2	±10mv	
L	D.O. mg/l Chemetrix (Visual)	≥40 ≤200 Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach		se Filt Man The	ered ganese Ig/l netrix sual)	Non Filtered Manganese mg/l Hach	Comments
	PURGE I tarting Flo			:	Endin	ng Flow m	neter Read	ling:		Flow Rate	e:
	-		-								mal purged (Y/N):
С	asing Inne	er Diamet	ter (inche	es)		Depth to	Water (fee	et)	I		ottom of well (feet)_



Page 2 of 2

						IRGE AN	D SAMI	PLING	FORM	
Project N	lame: E	STEP	- 201	584 -	TL1-	TAP		OC Nu		107
Sample C	Collected	by:					D	ate of C	Collection	n: 6/2/16
EQUIPM	IENT	hunner	tic	Suscer	tibili	ty 1	reasu	rent		
Purging I	Equipmen	t: H	MA-1	4535		-/				
Sampling	Equipme	ent:			20182	2		25 ml		
-	Equipmen			A		2000				
Equipme	nt Decont	aminatio	on:	Per W				Triple F	Rinse and	Isopropyl Alcohol Rinse
_	E	• • • • •			Equipm	ent Calibra				D. t. C. Phys. 1
-		uipment/					Number			Date Calibrated
		Multi Para DR 890 C				0501	.520 AA			N/A
	ПАСН	DR 890 C	olorimet	er		1	-			IN/A
Ambient A	RAMETER ir Tempera Depth (ft):	ture (°F):_	75 nlet@			Weather C Reference	onditions: Point: <u>To</u>	Sun op of inne	er PVC cas	sing Cloud y
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pH	ORP	Water
meter	rate	to		Purged	(°C)	(µS/cm)	(mg/L)		(mV)	Description/Comments
(gallons)	/min	water	rrive	(Gallons)	1-102					
	13:4	3 4	libra	ting t	PC	P(Zero)	ŧ s	-X 10"	3 51	Units
									101	e.A.
						031	units	-	610	cps
						5E-	RSTL	uik -	= 11	68,2700
				A .0	- 11.					
	15 Ru	m	TCA	AP C	111-	102 L	own -	- Cali	61	7 tt/mm
	Zank	mh	100	PAP (	qui	102 0	tp -	1an		Fight
	- 1		1							
	1001	cours	an	x 00	to.	to fu	t by			
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
			L Ellerer d	L Filtered	L Mar Ellere	d I Tiltered	Tella	ered	Non Filtered	
D.O. mg/l Chemetrix	Filtered Alk mg/l	Non Filtered Alk mg/l	Filtered Fe2+ mg/l	Filtered Fe2+ mg/l Chemetrix	Non Filtere Fe2+ mg/l		se Mang		Non Filtered Manganese mg/l	Comments
(Visual)	Hach	Hach	Hach	(Visual)	Hach	Hach	Cher	netrix sual)	Hach	Comments
DUDODU	DIEODI	ATION	-	1.01	1 - 11	· 68' 4	ml			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	INFORM			-			/			
Starting Flo	ow meter	Reading	:	Endi	ng Flow 1	meter Read	ling:		Flow Rat	e:
Total Volu	me Purge	d:	Pur	ged Dry (	Y/N):	Micro	purged (	Y/N):	Min	imal purged (Y/N):
Casing Inn	er Diame	ter (inch	es) 2'	Initial	Depth to	Water (fee	et) 15,7	22 D	epth to b	ottom of well (feet) 24, b
Tubing inn Controller	er diamet	er	_(in) ]	ubing &	Pump Vo	olume	(ml)			
Casing Volume	e Calculation (	gallons): 2"	well = 0.17	x WCT 4" w	$ell = 0.66 \times W$	VCT 6" well = $1$	.47 x WCT		Where WC	T = Water Column Thickness (feet)
Stille	the p	Top of	P	that C	Casily	-2.6	feet	ag s b	elow	App of uital wiedemeier
	_	Eizku	p=	- 2,48	'R	26	1			
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	E	CTA			IEKPU	KGE AN				
Project N	ame: Fa	siap	2019	87				OC Nu		1=106
Sample C	Collected 1	by: TH	wh	lark	Ferr	ey	D	ate of (	Collectio	<b>n = 106</b> on: <u>6/2/16</u>
EQUIPM	ENT			p	~/	-				
Purging I	Equipmen	it: <u>H</u>	MA	-45	55					
Filtering	g Equipme Equipment									
Equipme			on:	Per We	ork Plan –	Alconox V	Vash with	Triple	Rinse and	d Isopropyl Alcohol Rinse
					Equipm	ent Calibra				
	-	uipment/ Multi Para		ator			Number 520 AA			Date Calibrated
-		DR 890 C	12			0301	.320 AA			N/A
					Got	Tral	t1)-	15.2	ZFE	hac
FIELD PA Ambient A	ir Tempera				Sec	Weather C			510	995
Sampling I					-	Reference	Point: To	op of inn	er PVC ca	asing
Flow meter (gallons)	Flow rate /min	Depth to water	Time	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comments
(guilding)	an	ve a	0	1u-10	16 R	~ 1	1:22	-		
	Zer	vering	Reg	- 14:	30	2				
	100	Crity			17.	A				
	7	pol /	nade	it.	te.	25122	1.29	5		
	H	tting	120	mp cq	uniono	n 14	422			
	Start	Calib	ratin	· W	14:	50	1.01			
		•		52.	35	1187	23 CP	5		
	Ram	- 7	100	P all	1-101	100.1	h Du		P. 1-1-	1 SI ft lunder
	Runt	22	TCA	APO	24-11	DG UD	Rui	12	Calib	) -> att/min
	Run	3=	TCA	AP O	±10%	<u>el Dej</u> ±10%	±10%	±0.2	±10mv	il -> 15 At/inth
	≥40 ≤200 Rum	4-	TO	AAP	810%			Run	2 (4)	1 > 1 = Ft/man
D.O. mg/l Chemetrix	Filtered Alk mg/l	Non Filtered	Filtered Fe2+	Filtered Fe2+ mg/l	Non Filtere Fe2+ mg/l		Filto Mang	ered	Non Filtered Manganese	
(Visual)	Hach	Alk mg/l Hach	mg/l Hach	Chemetrix (Visual)	Hach	mg/l Hach	Chen	g/l netrix sual)	mg/l Hach	Comments
	20	he,	Q	15:05						
PURGE	NFORM	ATION		Tool	Leng	th	4.70	1		
Starting Flo	ow meter	Reading							Flow Ra	ite:
Total Volu	me Purge	d:	Pur	ged Dry (	Y/N):	Micro	purged (	Y/N):	Mi	nimal purged (Y/N):
Casing Inne Tubing inn Controller	er diamet	er	_(in) T	ubing & l	Pump Vo	lume	(ml)			bottom of well (feet) <u>29.0</u> 3
	Calculation (	gallons): 2."	well = $0.17$	x WCT 4" we	$ell = 0.66 \times W$	CT 6" well = 1	.47 x WCT		Where W	CT = Water Column Thickness (feet)
Тор	d'i	Meta Pvc	Lassing)	sing =	- 4.05	ft ag ft be	S low to	opog	Stuk	Casingsal
	Stick	eup.	= 2	.871	fr		,	V		
D:\TH			-	Sampling Form.doc		Page 1 of	1			& ASSOCIATES

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& ASSOCIATES

## DAILY FIELD ACTIVITY REPORT

Client Name: Project Name: <u>ESTOP 2016 XM</u> Contractor: Weather: Partly Cloudy		Project Number: Date: <u>6-3-16</u> Arrival Time:	)
Time Breakdown: Drive:	Work:	Standby:	
Location and Description of Activities: TCAAP 01U108 Set Sample Fulle of 27	Sapth to 1 Sant belie	ude 13.95 fe m TOC	ut below TOC
Equipment Used on Project:			
Activity Summary and General Remarks:			· · · · · · · · · · · · · · · · · · ·
		· · · · · · · · · · · · · · · · · · ·	
	· · · · · · · · · · · · · · · · · · ·		
Technician Signature:		_ Date:	<b>~</b>

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Project N	ame:_E	STOP	2015	84				COC Nu	mber:	
Sample C	Collected	by:	skn L	Vitro	~160	er bour	<b>-</b> ]	Well ID: Date of (	OIL Collectio	108 n:_6-3-16
EQUIPM	FNT	-				LU.	loon			
Purging H										
	· ·									
Filtering	Equipme	nt:								
Equipmen	nt Decont	aminati	on:	Per W	ork Plan –	Alconox W	Vash wit	h Triple	Rinse and	Isopropyl Alcohol Rinse
	_				Equipm	ent Calibra	tion			
	Eq	uipment/	Model			Serial	Numbe	r		Date Calibrated
	YSI 556	Multi Para	ameter Me	eter		05C1	520 AA			-
	HACH	DR 890 (	Colorimete	er						N/A
FIELD PA	RAMETER	s								
Ambient A			64			Weather C	onditions	:		
Sampling D	epth (ft):	Pump I	nlet@			Reference	Point:	<u>Fop of inn</u>	er PVC ca	sing
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pH	ORP	Water
meter	rate	to	9:54	Purged	(°C)	(µS/cm)	(mg/L)		(mV)	<b>Description/Comments</b>
(gallons)	/min	water	<u> </u>	(Gallons)						light
			6:35		10.59	.535	2.38	5,53	342.1	Color brown / gro
			11:34	2	10.61	.520	1.79		278.0	Color light gray
			16:42	3	10.62	. 500	1.36	6.79	264-	1 no color
			21:46	4	10.62	1485	1.15			
			26:50	5	10.66	.476 .475	1.02	6.45		
			27.06	7	10.64	.468	.86			ho color
								_		
					<u>†</u>					
								1		
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
	L Dikess I	<u> </u>		<b>1 1 1</b>					· · · · · · · · · · · · · · · · · · ·	
D.O. mg/l Chemetrix	Filtered Alk mg/l	Non Filtered	Filtered Fe2+	Filtered Fe2+ mg/l Chemetrix	Non Filtered Fe2+ mg/l	Manganes	se Ma	nganese	Non Filtered Manganese	
(Visual)	Hach	Alk mg/l Hach	mg/l Hach	(Visual)	Hach	mg/l Hach	Ch	mg/l emetrix 'isual)	mg/l Hach	Comments
								isual)		
			1							
<u>PURGE I</u>						_				
Starting Flo					-	neter Read			-	
Total Volur	ne Purge	d:	Purg	ged Dry	Y/N):N	Micro	purged	(Y/N):_	<u>N</u> Min	imal purged (Y/N):
Casing Inne	r Diamet	er (inche	es) 🎏	Initial I	Depth to '	Water (fee	et) <b>13.9</b>	5 D	epth to h	ottom of well (feet)
Tubing inne	er diamet	er <u> 740</u> 5	<u>) (</u> in) T	ubing & F	oump Vol	ume	(ml)		10 U	
Controller s	ettings: F	Pressure_		Discharg				(see	c.)	

Casing Volume Calculation (gallons): 2" well = 0.17 x WCT 4" well = 0.66 x WCT 6" well = 1.47 x WCT

Where WCT = Water Column Thickness (feet)



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& ASSOCIATES

#### DAILY FIELD ACTIVITY REPORT

Client Name: Project Name:		Project Number: Date: $6-3-16$
Contractor:		Arrival Time: 18;46
Time Breakdown: Drive:	Work:	Standby:
Location and Description of Activ		
Equipment Used on Project:		
Activity Summary and General Re	Diotito Wa	to 12.25 pt 27 yt Toc from
	·····	•
		· · · · · · · · · · · · · · · · · · ·
Technician Signature:		Date:
		- M-

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Project Na	ame: E	STC	P 201	584-	TCAA	7		COC Nu		
Sample C	ollected 1		la l	DiDan	$\sim$		۱ ۲	Well ID:		<u>115</u> ion: <u>6-3-16</u>
				10400			I		Joneen	ιοπ. <u>03-γφ</u>
EQUIPM										
Purging E										
Filtering l										
Equipmer	nt Decont	aminatio	on:	Per Wo	ork Plan –	Alconox W	ash wit/	h Triple	Rinse ar	nd Isopropyl Alcohol Rins
					Equipm	ent Calibrat	tion			
	Eq	uipment/	Model			Serial	Number			Date Calibrated
ľ	YSI 556	Multi Para	meter Me	ter		05C1	520 AA			
	HACH	DR 890 C	olorimete	r						N/A
FIELD PAF Ambient Ai Sampling D	r Temperat	ture (°F):_	η <sub>0</sub>			Weather Co Reference I	onditions Point: <u>1</u>	Part	er PVC	aidy / light rain
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pH	ORI	
meter	rate	to		Purged	(°C)	(µS/cm)	(mg/L)	<b>F</b>	(mV	
(gallons)	/min	water	11:00	(Gallons)						
				<u> </u>	9.79	-395	1.56		2386	
			3:42		9.79	.395	1.56	7.42		
			6:10	2	9.72	,393	1.37	7.39		
			8:21	34	9.82 9.84	393	1.15	7.40	232	9 no color
			12:45	5	9.87	,394 ,394	1.03	7.41	228.	
			15:17	6	9.91	.396	. 91	7.41	220.	
			17.57	7	9.93	. 399	-81	7,40		
			20:16	8	9.99	.402	,82	7.40		
			23:00	9	9.99	1402	.75	7.39	2251	
			25:31	10	10.05	.405	167	7.39	225.	
			28:14	11	10.02	.403	. 68	7.38		
			30:39 33:14	12	9.9 9	1405	• 71	7.38		
	> 40 < 200				9.99 +10%	14/1	.66	7.37		
	≥40 ≤200		35:44	14	10-03	<u> </u>	158	7.35	225	6 no alor
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filterec Fe2+ mg/l Hach	Filtered Manganes mg/l Hach	e Mar r Che	ltered nganese ng/l emetrix isual)	Non Filter Manganes mg/l Hach	
<u>PURGE I</u>	NFORM.	<u>ATION</u>				finis	hed	Per	gin	311:37
tarting Flo	w meter	Reading	:	Endir	ng Flow n	neter Read	ing:		Flow R	Rate:
otal Volur	ne Purge	d:	Pur	ged Dry (	Y/N): <u>N</u>	Micro ]	purged	(Y/N):	<u>N_</u> м	inimal purged (Y/N):
Casing Inne Tubing inne Controller s	er diamet	er_V40	D(in)T	ubing & F	Pump Vol	lume	(ml)		-	bottom of well (feet)
Casing Volume			_	-				,	/	WCT = Water Column Thickness (fo



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#### **DAILY FIELD ACTIVITY REPORT**

Client Name: Project Number: Client Name: Project Name: ES TCP DO1584 Plattishingh Date: 6-6-16Contractor: NY Arrival Time: 8815 Weather: Work: \_\_\_\_\_ Standby: \_\_\_\_ Time Breakdown: Drive: Location and Description of Activities: 14402-006 MW-02-006 Equipment Used on Project: Activity Summary and General Remarks: Deptu to water Deptug will 9:26 Plenson MW-02-006 Ø. # AI PNNL Plattobulg MW-02-006 Sampl 9:10 q 9:31 Plattsburgh MW-02-006 DNAI HM M Technician Signature: Date: 9:50 Pletts burgh MW-02-006 RNAI 400 MLS mecrobial IL 300 mLS. IL 300 mLS. WEDEMEIER & ASSOCIATES C:\Admin\Forms\Daily Field Activity Report.doc

Sample (	Collected	by:						Da	te of (	Collecti	ion:	$2 - \infty 6$ 6 - 6 - 16
EQUIPM	<u>IENT</u>											
Purging I	Equipmen	ıt:										
	g Equipme				· · · · · · · · · · · · · · · · · · ·							
	Equipme											
Equipme	nt Decont	taminatic	on:	Per We				with 7	<u><b>Triple</b></u>	Rinse ar	nd Is	sopropyl Alcohol Rin
					Equipmo	ent Calibra						
	-	uipment/N				Serial						Date Calibrated
		Multi Para				05C1	520 A	4A				
	HACH	DR 890 C	olorimete	er								N/A
Ambient A	RAMETER ir Tempera Depth (ft):		<u>63</u>			Weather C Reference	onditi	ons:	for	les Mes	<u>  u</u>	Jindy
			<u> </u>				-					
Flow meter (gallons)	Flow rate /min	Depth to water	Time	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)		0 ;/L)	рН	ORF (mV		Water Description/Comme
				-3-		$\sim$	-			-	-	
				<u> </u>	1475	,824	. 4	.2	10.65		77	Clean NFA
·					10.1	10-1	47		(216)		9	Sdur
											$\rightarrow$	
										ļ		
					┥────┤							
					1					<u> </u>	-	
	≥40 ≤200				±10%	±10%	±1(	)%	±0.2	±10mv	/	
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach	Filtered Manganes mg/l Hach	se	Filtere Mangan mg/l Chemet (Visua	nese l trix	Non Filter Manganes mg/l Hach		Comments
					.29							
PURGE	NFORM	<u>ATION</u>	· · · ·		1.25 m	g/L_	I		<u> </u>		<b>I</b>	
otal Volu	me Purge	d: <u>1.5</u>	<u>ga</u> lPur	ged Dry (	Y/N):	Micro	purg	ed (Y	/N):_[	<u> </u>	inin	nal purged (Y/N):_
asing Inn	er Diamet	er (inche er V/( $\wedge$ 1	(in) T	Initial	Depth to Y	Water (fee	et)	<u>m1)</u>	D	epth to	bot	tom of well (feet)_



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# DAILY FIELD ACTIVITY REPORT

			Project Number:
Project Name: EST Contractor: Weather:	1) 201584 ¥	attsbugh	Date: <u>6-6-16</u> Arrival Time: <u>11', 10</u>
Time Breakdown:	Drive:	Work:	Standby:
Location and Descript M w - 02			
Equipment Used on Pr	oject:		
Activity Summary and	General Remarks:	16.74	F17 TO C
Depth	well	25.8	sout bottom
Set T	ube Jo Vel 3.5	gul for	Josing Veluen
11:52 Plattel	aurgh Mu	-02	Samples PNI 2 3 (11)
12:01	mw	-02	I A 2 # 1 7 I A 2 # 2 7 Clemo
			IA2#3_1~100 M
12:16 DNA RNA			1000 mL June
12:16 DNA RNA	MW-02 MW-02		1000 mL J Ins

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Project N Sample C <u>EQUIPM</u> Purging E Sampling						<u></u>		_Da	ate of C	Collecti	)-02-019 on: <u>6-6-16</u>
Purging E	quipmen	it: <u>PE</u>	<u>sta</u>	t(L	Phon	<u>р</u>					· · · · · · · · ·
Filtering	Equipme	nt: $\checkmark$	VIA	PSIC	pat la	n Mil	as	Y XX	ia	Cicil	to Sampta
Equipmen	nt Decont	aminatio	on:	Per Wo	ork Plan –	Alconox V	/ash w	vith	Triple F	Rinse ar	nd Isopropyl Alcohol Rinse
						ent Calibra					
		uipment/l				Serial					Date Calibrated
		Multi Para				05C1	520 A.	A			
	НАСН	DR 890 C	olorimete	er	N/A						
FIELD PAR Ambient Ai Sampling D	ir Tempera	 ture (°F):_	nlet@			Weather Co Reference				er PVC o	casing
Flow meter (gallons)	Flow rate /min	Depth to water		Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/l		рН	ORP (mV)	
		1	<u>}</u>	0	12.33		1.3		7.08		
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Casing Volume Calculation (gallons): 2" well = 0.17 x WCT 4" well = 0.66 x WCT 6" well = 1.47 x WCT Where WCT = Water Column Thickness (feet)



Page 1 of \_\_\_\_\_

Chain of Custody Record	SEVERN STL TRENT Sorres, Inc.	<b>STL Denver</b> 4955 Yarrow Street <b>Inc.</b> Arvada, C0 80002
Client Todd Michellor Project Manager (X) i pd p Mi	CLARIER Date Co-16	16 Chain of Gustpork Number 2
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Project Na	me: E	STLA	1-6	lattsb	man		C(	OC Nun	nber:	2-00/2		
					'		W	ell ID:	MW-0	2-006		
Sample Co	ollected b	y:(	WK	HN		-	Da	ale of C	onection	6/0/10-		
EQUIPM	ENT	0	16	~								
EQUIPMI Purging E	quipmen	t:	ane	/								
Sampling Filtering I			1									
Equipmer			on:	Per Wo	ork Plan –	Alconox W	Vash with	Triple F	Rinse and I	sopropyl Alcohol Rinse		
					Equipme	ent Calibra	tion	-				
	Eq	uipment/N	Model				Number			Date Calibrated		
	YSI 556 1	Multi Para	meter Me	eter		05C1	520 AA					
	HACH	DR 890 C	olorimete	er						N/A		
FIELD PAR												
Ambient Ai			alat@			Weather C			er PVC casi	ing		
Sampling D				X7.1	Term		DO	pH	ORP	Water		
Flow meter	Flow rate	Depth to	Time	Volume Purged	Temp (°C)	Sp.Cond (µS/cm)	(mg/L)	pn	(mV)	Description/Comments		
(gallons)	/min	water		(Gallons)								
		ti	13	Well	11/11	144	firet	- 01	P t	hat was		
		- la -	0 p		mo	ond	1	A		- mater		
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		20	botte	\$ th	en t	tahs-fer	red t	F Sei	matry	Contained with		
	≥40 ≤200			-	±10%	±10%	±10%	±0.2	±10mv	a peristaltic pu		
D.O. mg/l	Filtered	Non	Filtered Fe2+	Filtered Fe2+ mg/l	Non Filtered Fe2+ mg/l				Non Filtered			
Chemetrix (Visual)	Alk mg/l Hach	Filtered Alk mg/l Hach	mg/l Hach	Chemetrix (Visual)	Hach	mg/l	m	g/l netrix	Manganese mg/l	Comments		
		Thuch	Indell			Hach	(Vis	ual)	Hach			
			1									
PURGE I	NFORM	ATION										

# Starting Flow meter Reading: Ending Flow meter Reading: Flow Rate: Total Volume Purged: Purged Dry (Y/N): Micro purged (Y/N): Minimal purged (Y/N): Casing Inner Diameter (inches) Initial Depth to Water (feet) 33.45 Depth to bottom of well (feet) Tubing inner diameter (in) Tubing & Pump Volume (ml) Controller settings: Pressure (psi) Discharge (sec.) Recharge (sec.)

Casing Volume Calculation (gallons): 2" well = 0.17 x WCT 4" well = 0.66 x WCT 6" well = 1.47 x WCT

Where WCT = Water Column Thickness (feet)



	Collected 1			lattsbu JTU	)'		D	Vell ID:	<i>MW</i> . Collectio	-02-032 n: 6/6/16
EQUIPM Purging I Sampling	ENT Equipmen Equipme	t: <u>H</u>	MA	-453	25		_			
	Equipmen								1	
Equipme	nt Decont	aminatio	n:	Per Wo		and the second se		Triple 1	Rinse and	Isopropyl Alcohol Rinse
					Equipm	ent Calibra				
-	-	uipment/N			-		Number			Date Calibrated
		Multi Para	-			- <u>45C1</u>	520 AA			<b>N</b> 1/A
	HACH	DR 890 C	otorimeto		- 1		-	An	1.1	N/A
	RAMETER ir Temperat Depth (ft):		USe nlet@	ed 7	-ft/v	Weather Co Reference	onditions:	Priv	1 000	ing breetyn;
Flow meter (gallons)	Flow rate /min	Depth to water	Time	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comments
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ye-run	pu	11 1	1P -	= 11	i.	11 /	11	40	11	11 11 11 11
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	≥40 ≤200			10100	±10%	±10%	±10%	±0.2	±10mv	
	D'14 1	N	T'l 1				1 T°14			
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filterer Fe2+ mg/l Hach		e Mang m Cher	ered ganese g/l netrix sual)	Non Filtered Manganese mg/l Hach	
PURGE	NFORM	ATION	Ca	liblatica	n 2	Ze	10 =	681	\$20	SCAS
Starting Flo										
	er Diamet	er (inche er	es) (in) T	Initial I Tubing & P	Depth to Pump Vo	Water (fee lume	t) <u>/5</u> (ml)	20D	epth to b	nimal purged (Y/N):
Casing Volume	Calculation (	vallons): 2"	well = $0.17$	x WCT 4" wel	l = 0.66  x W	CT 6" well = 1	47 x WCT		Where WO	CT = Water Column Thickness (fee
Be	low 51	rach .	Cov	er -	Zero	Sond	L@	60	und .	Surpres

# DAILY FIELD ACTIVITY REPORT

(	Client Name:				Project Number:	
I C	Project Name: Contractor:	ESTEP Pla 201584	ittsburgh		Date: $6 - 7 - 16$ Arrival Time: $8,55$	
	Weather:		air Part	Eg Sunny		
]	Гіme Breakdo	58°F wn: Drive	•	Work:	Standby:	
т	ocation and I	Description of	Activities			
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_	32PL	TWIS				
-						
- T	Faviament I la	ad an Draigati				
1	Equipment Us	ed on Project:				
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-			Ļ	<b>7</b>		
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10: -	is plat	15 burger	32PL TU	12 KNH	1000 m L I morght	<u> </u>
-						
5	Fechnician Sig	gnature:			Date:	
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					<b>.</b>	



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Project Name: E	STOP	101584	4 Plaz	Hsbul	<u>zh</u>		COC Nu		The
Sample Collecte	d by: <u>5</u>	WIR	SWITI	ىر		ע נ	Vell ID: Date of (	<u>32 Pl</u> Collecti	<u>-TWIZ</u> on: <u>6-7-16</u>
<u>EQUIPMENT</u> Purging Equipm									
Sampling Equip				<u> </u>					
Filtering Equipm	ent:								
Equipment Deco	ntaminati	on:	Per Wo		Alconox V ent Calibra		<u>n Triple</u>	Rinse an	d Isopropyl Alcohol Rinse
	Equipment/	Model		Equipin		Number			Date Calibrated
	6 Multi Para		ter			520 AA			
	H DR 890 C					1520 AA			N/A
FIELD PARAMET	rature (°F):_	580			Weather C	onditions:	Je	shty	Cain Partly Sunny
Sampling Depth (ft)		· · · ·				Point: <u>1</u>	op of inn	er PVC c	
Flow Flow meter rate (gallons) /min	Depth to water	Time <b>G: 24</b>	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	
(gunono)			0	12.03	.214	9.49	6.91	141.6	<b>,</b>
		1:28	·2	11.22		9.38	5.25	255.8	
		4:19	40	0.85	.227	9.21	4.73	298-0	
		7:45	20	1).11 11.39	·27 -227	9.02	4.95	294.	
		(* , <b>p</b> *	2.0	<u> </u>					s berg su jux un
	·	Stop	spei 9	• 36					
≥40 ≤200	)			±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l Filtered Chemetrix Alk mg (Visual) Hach		Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filterer Fe2+ mg/l Hach		se Man n Che	tered ganese ng/l metrix isual)	Non Filtere Manganes mg/l Hach	
				0.00					
PURGE INFOR	MATION								······
Starting Flow met	er Reading	<u>.                                    </u>	Endir	ng Flow r	neter Read	ling:		Flow R	ate:
Total Volume Pur	ged: Jan	ℓ Pur	ged Dry (	Y/Ø	Micro	purged (	Y/Ø:_	Mi	nimal purged (YA).
Taging Innon Diam		``							
Cubing inner diam Controller settings	eter (inch eter <u>0</u> , [つ	es)(in) T	Initial ] ubing & I	Depth to Pump Vo	Water (fee lume	et) <u>  3</u> (ml)	(se	epth to	bottom of well (feet) $16.8$

WEDEMEIER

& ASSOCIATES

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Page \_\_\_\_ of \_\_\_\_

# DAILY FIELD ACTIVITY REPORT

	Client Name: Project Number:
	Project Name: ESTEP 201584 Plottsburgh Date: 6-7-16
	Contractor: Arrival Time: 10:35
	Weather:
	Time Breakdown:   Drive:   Work:   Standby:
	Location and Description of Activities: 64°F Mostly Cloudy 35PLT13
	Equipment Used on Project: <u>Greofech Pemp</u> YSI 556 MPS HACH DR 890 Calorimeter
	Activity Summary and General Remarks: Deptn to Water 10.35ft
	Sand at 24.25 pt BTOC (Base & well Set Tube at 17 pt BTOC for sampling Ignl = 3 casing volumes
11:30	Protteburgh 35PTL13 Semples PNNL 24 3 4
11:43	Plattsburgh 35PTLB IB2 #1 2 Clemson
12100	Prottsburgh 35PTL13 DNA 1000 ml ? Microbial Prottsburgh 35PTL13 RNH 1000 mL Tusight
	Technician Signature: Date:
	C:\Admin\Earme\Daily Field Activity Report doc & ASSOCIATES

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-

Project Name:			C	OC Nu	mber:	- <b>T</b> + 2
Sample Collected by: <u>JwlBwlT</u> <u>EQUIPMENT</u> Purging Equipment: <u>Geotoph Pon</u>	$\omega$		W D	/ell ID: ate of (	35P	$\frac{1}{10} \frac{1}{10} \frac$
FOLIPMENT						
Purging Equipment: Exects of Dismi	<b>P</b>					
Sampling Equipment:	1					
Filtering Equipment:						
· · · · · · · · · · · · · · · · · · ·	/ork Plan – A	lconox W	ash with	Triple 1	Rinse and	Isopropyl Alcohol Rinse
-	Equipmen			-		
Equipment/Model		Serial 1	Number			Date Calibrated
YSI 556 Multi Parameter Meter		05C15	520 AA			6-7-14
HACH DR 890 Colorimeter		-				N/A
FIELD PARAMETERS					L	
Ambient Air Temperature (°F): <u>64</u>	V	Veather Co	, nditions <sup>,</sup>	Pai	they S	unny ( Cloredy
Sampling Depth (ft): Pump Inlet@	F	Reference P	oint: <u>To</u>	op of inn	er PVC cas	sing
Flow Flow Depth Time Volume	Temp S	Sp.Cond	DO	pH	ORP	Water
meter rate to Purged		(µS/cm)	(mg/L)	P	(mV)	Description/Comments
(gallons) _/min water (0:17 (Gallons)			_			
Back out to much bisz .5	14.97		2.91	7,33		
Back ofto too much birz .5 drawdown 11608 1.9		536	6.27 4.78	6.93	85.2	lear, fount prove
Lower Tubika ~ 1 116:00 1.		538	2.28			
19:11 2.0				6.84	58.3	lear, colorless
24:57 2.5	12.3/ .	540	1.58	7.11	45.4	clear, colobro
Stopped 11:17						
≥40 ≤200	±10%	±10%	±10%	±0.2	±10mv	
					L	
D.O. mg/l Filtered Non Filtered Filtered Chemetrix Alk mg/l Filtered Fe2+ Fe2+ mg/l	Non Filtered Fe2+ mg/l	Filtered Manganese	Filte Mang	ered anese	Non Filtered Manganese	
Chemetrix         Grad Chemetrix         Mach         Alk mg/l         mg/l         Chemetrix           (Visual)         Hach         Hach         Hach         Hach         (Visual)	Hach	mg/l	m Chen	g/l netrix	mg/l	Comments
		Hach	(V15	sual)	Hach	
	0,00					
PURGE INFORMATION						
Starting Flow meter Reading: End	ing Flow me	ter Readi	ng:		Flow Rat	e:
Total Volume Purged: 2. Soul Purged Dry	÷					
Casing Inner Diameter (inches) Initial	Depth to W	ater (feet	10.3	5 D	epth to be	ottom of well (feet)24.2
Tubing inner diameter (in) Tubing &	T	· · · · · · · · · · · · · · · · · · ·				

Casing Volume Calculation (gallons): 2" well = 0.17 x WCT 4" well = 0.66 x WCT 6" well = 1.47 x WCT

Where WCT = Water Column Thickness (feet)



Severn Trent Laboratories, Inc.	Arvada, CO 80002
1 Date 10-7-16	Chain of Custody Number 348476
Lab Number	APage / of /
Analysis (Attaci more space is n	
	Subject Instructions.
)1 fri	Conditions of Receipt
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	<i>3</i> 4.
7	
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	accord if camples are related
Archive For Months longer than 1 m	(A rec rial be assessed in samples are relation to the former of the for
	Date
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	alysis (Attach list if e space is needed) Anonths longer than 1 i

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DISTRIBUTION: WHITE - Returned to Client with Report; CANARY - Stays with the Sample; PINK - Field Copy

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Chain of Custody Record			SEVERN TRENT Severn Tren	<b>SEVERN</b> TRENT <b>STL</b> Severn Trent Laboratories, Inc.	STL Denver 4955 Yarrow Street Arvada, CO 80002	Street 0002
STL4124 (0901)						
	Project Manager		Je.	Date 19-7-16	Chain of Custody Number	<sup>34</sup> Number 4
Address Antonia La Dr.	Telephone Number (A	er (Area Code)/Fax Number	ber 1 999	Lab Number	Pade	of
State Zip Code	Site Contact		-	Analysis (Attach list if more space is needed)		
Project Name and Location (State)	Carrier/Waybill Number	Imber Land	4.ac			ial Instructions/
ContractPurchase Order/Quote No.		Matrix CC	Containers &		Cond	Conditions of Receipt
Sample I.D. No. and Description (Containers for each sample may be combined on one line)	Time Air suoaupA	tosth rossh rossh rossh ross ross ross ross	Н изон изон ног ног ног			
Plattshurah 32 PLTW1250000 10-7-16	04:6		4	· · · · · · · · · · · · · · · · · · ·		
1			<u>ن</u>			
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Durther with 32 PLTWID Someth V	>		7			
Platuburah 35PTL 13 Samelel 16-7-16	11:30 1		ن. بر ا			
Sanule 2	<b>و</b>			£-		
	4		 			
	$\rightarrow$			Ċ		
Tim Bland DIWIH 6-7-16	7			· · · · · · · · · · · · · · · · · · ·		
8591-21-5 L						
n mmable	Sample Unknown Re	Sample Disposal  Return To Client Dis	Disposal By Lab	Months	(A fee may be assessed if samples are retained longer than 1 month)	are retained
Required		-	Spe	and the second		
1. Relinquished By     1. Ualys     1.4 Ualys     2.1 Ualys		h	1. Received By		Date	Time
~racin() andrax	9-1-16	15:03				
2. Relinquished By	Date	Time 2. Re	2. Received By		Date	Time
3. Relinquished By	Date	Time 3. Re	3. Received By		Date	Time
Comments	_	_				_
DISTRIBUTION: WHITE - Returned to Client with Report; CANARY - Stays with the Sample; PINK - Field Copy	's with the Sample; PINK	- Field Copy				

	Chain of Custody Record	• •	SEVERN TRENT Severn Tren	SEVERN STL TRENT SQUERN Trent Laboratories, Inc.	<b>STL Denver</b> 4955 Yarrow Street Arvada, CO 80002	
	STI-4124 (0901)					
Ц	Client Control TALIO Larman	5	e lemeror	Date 101-7-16	Chain of Custody Number 348478	8
1	Address OC I Provide and A		ode)/Fax Num	MULTU LO CA	Page of	
		Site Contact		Analysis (Attach-list ti more space is needed)		
ĺ.	Project Name and Location (State)		17010 1000 1		Snee a Instru	nstructions/
д Г	Contract/Purchase Odder/Quote No.	NG Matrix	Containers & Preservatives		Condinus of	s of Receipt
r	Sample I.D. No. and Description (Containers for each sample may be combined on one line)	Date	NªOH ZUYC( NªOH HCI HNO3 HSO4 HSO5			- (g - 
Part	+ - +	× 7	1.01.0	- A MANA		
Pla.		6-7-16 10:15 4				
	THE					
Pla	Platishiral 35 PTL 13 DNA 1000	10-7-16 12:00 V			*	
Da.	35 PTLI3 KNA IDED	6-7-16 12:10 4				
		-				
		32				
				*		
				- Marga		-
	Identification	Sample Disposal	lient Disposal Bv Lab DArchive For	Months	(A fee may be assessed if samples are retained longer than 1 month)	led
			OC Requirements (Spe			
	Part         Part <th< td=""><td>s 21 Days Other</td><td>F-N1 Received Bv</td><td></td><td>, Date , Time</td><td>e</td></th<>	s 21 Days Other	F-N1 Received Bv		, Date , Time	e
		91-1	122			
	2. Relinquished By	1	2. Received By		Date	Ð
	3. Relinquished By	Date	3. Received By		Date	Ð
,	Comments					
Ý	3. DISTRIBUTION: WHITE - Returned to Client with Report: CANARY - Stays with the Sample; PINK - Field Copy	ANARY - Stays with the Sample: PINK - Field Co	Хdo			

REPORT TO:			-		Z :	INVOICE TO:	Ö		nvoices	(For Invoices paid by a third party it is imperative that all information be provided)	y a thiro	l party	tt is imp	erative	that al	ll inforn	nation	be pro	vided)														
Name: Company: Address:	δ×.	140 140 144 144	N N T S S T		Ϋ́ŬĂ	Name: Company: Address:													111		<b>1</b>	515 R	10515 Research Dr	<b>crobial</b> insights	Q	lir.	ist	5	ş				
	- 107 - 285 2057 - 401 -	05 tai	11 e. W.	122	프 프 프	email: Phone: Fax:															778 ¥	Knoxville, TN 3 865-573-8188 www.microbe.	Knoxville, TN 37932 865-573-8188 www.microbe.com	7932 om									
Project Manager: Project Name: Project No.: Report Type: EDD type:	PLATE PSOF ALENTED		C C Haghts Levi	Purchase Order No. Subcontract No. MI Quote No. el III raw data(15% surcharge) □ Microbial Insights L	Pu Su MI 5% surchi	Purchase Order Subcontract No. MI Quote No. charge) D. M	Order Inct No. No.	No.	Insigh		Shed	vel IV (25% surcharge) Snecify FDD Tyne:	charge)				J J J J J J J J J J J J J J J J J J J	ehen	Please I Mo	terpr	etive D	ease ( ] Mo ] No (15%)	Please Check One: Description Additiona (15%)	s 🔆 🗖	samp Histo	llow des orical	Inter	to follow Samples Historical Interpretive (35%)	e (35°	(%			·
ontact us wi	Please contact us with any questions about the analyses or filling out the COC at (865) 573-8188 (9:00 am to 5:00 pm EST, Sample Information Analyses	or filling out th	ne COC at (865)	573-8188 (9:0	00 am to	to 5:00 pm E Analyses	EST, I	CI HH	After h		nail: cu ease	sele	rservic ct the	e@mii targ	crobe.	com	sm/c	tene													1.30		
M ID	Sample Name	Date Sampled	bəlqms2 əmiT	XiteM	PLFA	SON	QuantArray Chlor	QuantArray Petro DHC (Dehalococcoides)	DHC Functional genes	DHBt (Deµalobacter)	DHG (Dehalogenimonas)	DSM (Desulturomonas)	DSB (Desuffitobacterium)	EBAC (Total) SRB	(Sulfate Reducing Bacteria-APS)	MGN (Methanogens)	(srigorionaria) MMB	OWWS	DNF (Dentrifiers-nirS and nirK) AOB	(ammonia oxidizing bacteria)	PM1 (MT8E aerobic)	RNO (Toluene Monooxygenase)	PHE (Phenol Hydroxylase)		BSSA	(Toluene-Anaerobic)	add. qPCR: RNA	*(noitqO noisearqx∃)	neuto	Other: 			
	Plath Jun als					╞		-			,	5					<u> </u>			Î	-	┝			-	┢─	┢	┢		_	_		
	1 < 1 /	10-7-716	ه ۱۵:۵۲	A.C.			$\vdash$	<u> </u>	ļ					┢		ᡟ─		┥──	17	* *	┢								$\vdash$	┢		Jine	
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	10	a	-	67 17					_				+	+		+	+	+	_	+	-		_		+	+	-	+	+	-	<u>- 2</u>	7.4.2.21	1
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Relinquished by:	the base of A Jun	Low				Rece	Received by:	ž				_	Date																				
			It is vital that chain of custody is filled out correctly & that all relative information is provided.	It is vital that chain of custody is	hat chair	n of custo	ody is f	filled or	ut corre	filled out correctly & that all relative information is provided.	that all	relativ	e infor	mation	is pro	vided.			4-14-1		1										1		

r = 7 - 7 - 7Failure to provide sufficient and/or correct information regarding reporting, involcing & analyses requested information may result in delays for which MI will not be liable. r = 10 - 7

GROUNDWATEH	<b>PURGE AND</b>	SAMPLING FORM
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Project N	lame: E	STOP	P - P	latts	burg	KOL AN		OC Nu	imber:	
Sample C				ITTO	11					-02-17 n: 6/7/16
		oj. <u> </u>	m		0			ure or .	comoono.	
EQUIPM Purging I	<u>IEN I</u> Equipmer	nt. 1	in	1-4	452	5				
Sampling			11001	1	52	2				
Filtering										
Equipme			on:	Per We	ork Plan -	Alconox V	Vash with	Triple	Rinse and	Isopropyl Alcohol Rinse
	in Decen					ent Calibra	and the second			
	Eq	uipment/	Model			Serial	Number	3		Date Calibrated
		Multi Para		eter		0501	520 AA	-		in the second second
	HACH	DR 890 C	olorimete	er						N/A
				-	-					s- mary s
FIELD PA	ir Tempera					Weather C	anditions:	Unio	work	St Rain Breeze
Sampling I	*		nlet@		_	Reference	Point: To	op of inn	ner PVC ca	sing
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pH	ORP	Water
meter	rate	to	Time	Purged	(°C)	(µS/cm)	(mg/L)	pir	(mV)	Description/Comments
(gallons)	/min	water		(Gallons)						
13	39	Zer	0 700	I TO	Surfa		~~~			
13:	He tar	TCOL	Stopp	da.	41.8	f ft	BGS			
17 .	55 Da	he de	1 A	Wath		Citho	Bulli			
151	IS Pla	Calil	atter	~ 1	Fero=	E TO	561			
			1 million		SE-	3=11	52,10	1		
14:0		Ruh	1	PLIS	Punt	Galibi	Dow	2		2 1 2 11 1 1 1
	Downe	28,5 ft	minz	PLTS	Runl	Down	Calib 1	M	10-07-0	1 5t-16, tto
	MDQ	0.5 40	anin =	PITC	Rund	110	12,02	mw.	-07-171	7 6-7-16
	ST	teel	lasin	y int	erfer	s near	Surla	ul	aving	to start
-	Run	20	10	bas	25	tart i	rith	Probe	101	a' bgs
		Run	-2 =	D-PLI	K Ru	n2	Down	la	Ab1	11W-02-017-6-1-1-
-	>10 <200	Rue	-2 =	E PLI	±10%	±10%	±10%	±0,2	±10my	MW-02-017. 6-+
	≥40 ≤200				1070	1070	1076	10.2	±10mV	
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l	Filtered Fe2+ mg/l	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filterer Fe2+ mg/l Hach		se Mang	ered ganese g/l netrix	Non Filtered Manganese mg/l	Comments
(visual)		Hach	Hach	(*15444)		Hach	(Vis		Hach	
					1					
PURGE	INFORM	ATION	54	rickup	= 2	64' 51	Measu	u pr	in Zer	o up 2.045
Starting Flo	ow meter	Reading		Endir	ng Flow n	neter Read	ling:		Flow Rat	te:
Total Volu	me Purge	d:	Pur	ged Dry (	Y/N):	Micro	purged (	Y/N):	Min	imal purged (Y/N):
	er Diame	ter (inche	es) 7	Initial	Depth to	Water (fee	t) 33.4	12 D	epth to b	ottom of well (feet) 44/60
Casing Volume									Where WC	T = Water Column Thickness (feet)

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Page  $\_$  of  $\_$ 

#### DAILY FIELD ACTIVITY REPORT

Client Name:	Project Number:
Project Name: ESTCP 201584	Date: $6 - 8 - 16$ Arrival Time: $9:30 \text{ Arry}$
Contractor:	Arrival Time: 7:30 Am
Weather: Cloudy + Calm	-
Time Breakdown: Drive: Wo	rk: Standby:
Location and Description of Activities:	
EPA-165 (124 Crea	mery Road)
	1 /
·	
Equipment Used on Project:	
Activity Summary and General Remarks:	
21.40	
Samples collected: Hopen	well EPA-(65 1) PNN
	11 11 11 3 [ ] ita
	11 11 11 4 1 Late
10:56	
Hopewell EPA-165 JEAI	<u>#1</u>
	<u>#2</u> #3
	н 5
11:02	
Hopewell EPA-165 DNA	1000mL
11:0'7 RNA	LOOD preserved
;	
Technician Signature:	Date:
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Sample C	Collected	by:					D	ate of (	Collectio	065 0n: <u>6/8/16</u>
EQUIPM	<u>ENT</u>									<b>,</b>
Purging E	Equipmen	t:								
Sampling	Equipme	ent:								
Filtering	Equipmer	nt:								
						Alconox V	Vash with	Triple 1	Rinse and	d Isopropyl Alcohol Rinse
						ent Calibra				
	Eq	uipment/	Model			Serial	Number			Date Calibrated
	YSI 556	Multi Para	ameter Me	ter		05C1	520 AA			
	HACH	DR 890 C	Colorimete	er						N/A
FIELD PA	RAMETER ir Temperat	<u>.S</u> hure (°E):	62°	1 F		Weather C	anditional	Clo	udv	
Sampling D	Depth (ft):	Pump I	nlet@			Reference	Point; <u>T</u>	op of inn	er PVC ca	
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pH	ORP	Water
meter	rate	to	102.06	Purged	(°C)	(µS/cm)	(mg/L)		(mV)	Description/Comments
(gallons)	/min	water		(Gallons)						
			2:41		145	.666	6.63	1 117	220	5 Clear us color
			5:31	12	10.94		593	5.90	247.8	
			8:04	3	10.85	1669	5.79	5.81	247.3	
			10:39	4	10.84	.671		5.84	242.	
			13:19	<u> </u>	10.86		5.69		235.	
			15:58	<u>_6</u>	10.87	,673	5,72	6.01	230.	
			18:40		10.86 10.83	1673 1672	5.74	1.7	225.	
			<u>~</u> [• µ0	0	10:00	101-	2012	6.09		
		e								
		Jin	cohed	1 [0:	22					
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
	240 5200				10/0	10/0	10/0	10.2	10111	
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach	Filtered Manganes mg/l Hach	se Mang m Cher	ered ganese g/l netrix sual)	Non Filterec Manganese mg/l Hach	
					0.00					
	NFORM.									
arting Flo	w meter	Reading	;	Endin	ıg Flow n	neter Read	ling:		Flow Ra	ate:
tal Volu	ne Purge	d:	Pur	ged Dry (	Y/N):	Micro	purged (	Y/N):	Mi	nimal purged (Y/N):
sing Inne bing inne	er Diamet	er (incher er .17	es) <u>4</u> " (in) T	Initial I ubing & F	Depth to Pump Vol	Water (fee lume	et) <b>\$/3</b> . (ml)	<u>40</u> D	epth to l	bottom of well (feet) $\frac{29.92}{29.92}$
ontroller s	settings: H	ressure	(psi)	Discharg	e (sec.) I	Recharge_	()	(see	c.)	3



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Page \_\_\_\_ of \_\_\_\_

# DAILY FIELD ACTIVITY REPORT

.

	Client Name: Project Name: ESTCP 201584 Contractor: Weather: 58° F Light Rour	Project Number: Date: $6 - 8 - 16$ Arrival Time: 13: 50
	ŭ	Standby:
	Location and Description of Activities: EPA 15D 162 Creamony Rd Hopewrld Junctim NY	45-55 screenentenal?
	Equipment Used on Project:	
	Activity Summary and General Remarks: Deptr to Wale 19. Botton Well 45. Screened Friterval 45	9 ft 2 ft -55 ft? per Deanna Cutt iches TOC TO ground surface
	flash moented well 8.5 m	iches TOC TO ground surface
14:50	Hopewill EPA-15D Sample 1 2 3 4	J PNNL
15:00	Hopewell EPA-15D TTL A2#1 #2 #3	Zelenson
15:10 15:16	Hopewall EPA-15D DNA 10000	I microbial J Insight
	Technician Signature:	Date:

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<u>EQUIPM</u>		0. <u></u>	DIDU	5/DC			D	ate of C	Collectio	A-15D 1676 n: 6-8-16
Purging H										
Filtering Equipment				Der W.		A 1		T.:.1.	D:	1.1.1.1.1.
Equipme	in Decom	ammatic	<u> </u>	Per wo		nt Calibra		Triple	kinse and	l Isopropyl Alcohol Rin
	Ea	uipment/I	Model		Equipme		Number			Date Calibrated
	-	Multi Para		ter			520 AA			
		DR 890 C								N/A
L										
FIELD PA	RAMETER	<u>(85</u>	58			Weather C		y.	ht	20111
Sampling L	Depth (ft):	Pump I	nlet@			Reference				
Flow	Flow	Depth	Time	Volume	 Temp	Sp.Cond	DO	pH	ORP	Water
meter	rate	to	14:18	Purged	(°C)	(μS/cm)	(mg/L)		(mV)	Description/Comme
(gallons)	/min	water	סיודו	(Gallons)			10 11 0			
			4.17	0	13.07	<u>,337</u> ,646	13,42	7.21	89.7	Clean Hard
			7:57	2		<u>.678</u>	4.33		147.9	Clear hocal
			11:43	2 3	11.06	1710	3.85	7.07	154.3	Chen No colo bi
		15:28		46	11.05	1730	3.82		158.4	<b>y</b>
			19:08	6	11.04	1743	4.14	6.95	163.0	Clean slightbro
				7						
	······	Ston	and	14:42			ļ		·	
		Pret	pes	14140	,					
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l Chemetrix	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach	Filtered Mangane mg/l Hach	se Mang m Cher	ganese g/l netrix	Non Filtered Manganese mg/l Hach	Comments
(Visual)					0.00		(VI:	sual)	Hach	
						1	1			1



10

	collected l		i	Hope			w D	ate of	Collectio	v-16D on: <u>6-8-16</u>
- QUIPM	ENT	•								
		t:								
ampling	Equipme	ent:								
quipmei	nt Decont	aminatic	on:	Per Wo				Triple	Rinse and	d Isopropyl Alcohol Rinse
	Fa	uipment/I	Model		Едигрие	ent Calibrat	Number			Date Calibrated
		Multi Para		eter			520 AA			Date Camprated
		DR 890 C				0501	5207111			N/A
mbient A	RAMETER ir Temperat Depth (ft):	 ture (°F):_	62°	F		Weather Co Reference I	onditions:	Cl	oudy per PVC c	+ Calm
Flow meter gallons)	Flow rate /min	Depth to water	Time	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comments
									_	
							· .			
	- 40 - 200				100/	100/	100/	10.2		
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach	Filtered Manganes mg/l Hach	e Mang m Chen	ered ganese g/l netrix sual)	Non Filtered Manganese mg/l Hach	
URGE I	NFORM	ATION								
rting Flo	w meter	Reading	:	Endin	g Flow n	neter Read	ing:		Flow Ra	ate:
sing Inne	er Diamet	er (inche	$\frac{1}{(in)}$	Initial I	Depth to	Water (fee	$t) \frac{13}{(m^{1})}$	44' I	Depth to l	nimal purged (Y/N):
ntroller s	settings: I	Pressure	(m) 1 (psi)	) Discharg	e (sec.) H	Recharge	(m)	(s	ec.)	4
				x WCT 4" we		-				CT = Water Column Thickness (feet

 $\neg \uparrow$ 

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Chain of Custody Record	SEVERN TRENT STL	STL Denver 4955 Yarrow Street
STL-4124 (0901)	Severili ficilit Labol atolies, ilic.	Arvada, cu ouuuz
1 Wirdemeier - ESTCP Project Managor Wirel	emeier Date 8-16	Chain of Custody Number 052
ess 309 Согона С. Г. Soz-670-	79 DN NL	Page   of
800135	Analysis (Attach list if more space is needed)	
etter NPL Site CarrierMaybill Number		
1)		Special instructions/ Conditions of Receipt
+OSZH Sejdu() IIOS Snoenby IIV	E H	
6-8-16 10:40		
1		
Hepeweel EPH-165 Sample 3 6-8-16 1	7	
I	7	
topewallEVA-15D Samples 6-8-16 M:50 V		
	7	
Hopewal EPH-15D Semple 3 6-8-16		
1 tip cur ( E 2A - 15 D S angle 4 6- 8-16 4 4		
Turp Werk		
DIWENCE 16-16 36-8-9 10-10 14 WILL	7	
Tossiue nazaru identiincairon UK Non-Hazard	Archive For Months	(A fee may be assessed if samples are retained longer than 1 month)
Required           48 Hours         7 Days         14 Days         21 Days         Other	Specify)	
wilson		Date
Date		Date Time
3. Relinquished By Date Time 3. Received By		Date Time
Comments		
DISTRIBUTION: WHITE - Returned to Client with Report: CANARY - Stays with the Sample; PINK - Field Copy		

STL-4124 (0901)							
ES 101-1021 WIELEMEIEL	ef Project Manager	Wied	emeier	in	0-8-9-16	C	Chain of Custody Number 324051
309 COLONADO DE	Telep	(Area Code)/f	6	op v. O	Lab Number	ã	Page _/ of
City Service and 20135	Site Co		Lab Contact		Analysis (Attach list if more space is needed)		
	aybill		Freedman				
Contract Purchase Registrade No. 1410 CLUCI DU CLUOR		Matrix	Containers & Preservatives	Tu			Special Instructions/ Conditions of Receipt
Sample I.D. No. and Description (Containers for each sample may be combined on one line) Date	snoənb∀	səJdu∩ I!ºS	NªOH Zuvc\ NªOH HCI HCI HCI HCI	<del>ऽ</del> ऽम्			
the word EPA-165 TI A1#1 6-8-16	10:56 1	ł		7			
a				7			
4 pervelo EPA-16571A1#3 6-8-16	P + A			7			
HEDEWUL EPA TISDIL A241 6.8-16 15:00	6 15300 10			$\iota$			
496 curde F7A + 15 DTL A2#2/6-2+16	6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			7			
1-2-2-41 EDH -15 D-# H2 H2 16-8-16	e +			7			
Possible Hazard Identification	Unknown	Sample Disposal	Disposal By Lab	Archive For	(A fee may Months longer than	be assesse 1 month)	(A fee may be assessed if samples are retained longer than 1 month)
Pequired	Days Dother		Spe		1		
bara Wilson	Date 6-8-16	Time   (6;   0	1. Received By			2	Date
]	Date	Time	2. Received By				Date
3. Relinquished By	Date	Time	3. Received By			,	Date
Comments							

DISTRIBUTION: WHITE - Returned to Client with Report; CANARY - Stays with the Sample; PINK - Field Copy

	•		Severn Tre	Severn Trent Laboratories, Inc.	Arvada, CO 80002
STL-4124 (0901)				· · · ·	
ESTOP-Tadd Windemeier		Project Manager	Niedemerer	Date (0-8-16	Chain of Custody Number 324053
309 Corada Dr		Telephone Number (Area	Area Code)/Fax Number 3 - 6 70 - 7 999		, Hace / of /
Sector 10 State Zp Code	0	Site Contact	Lab Contact	1= 7	<b>(</b>
T	to Carr	liq			
Contract Purchase Order Olote No. 1760 CUC COULDU	el gui ete	O Matrix	Containers & Preservatives		Special instructions, Conditions of Receipt
Sample I.D. No. and Description (Containers for each sample may be combined on one line)	Date Time	lioS InoeupA NoeupA	HOPN VVVC MBOH HOI HAI Sold Floce		
HEDULUCLEEPH-IES DNH m2 6-	6-8-16 11:02	, , , , , ,		1 A ARCH	
	6-8-10 11:07	7 1			
HapewoellEDA -15D DNA 6-	6-8-16 15:10	7			
RNA	6-8-16 15:16	7			
1000ML					
,					
Possible Hazard Identification		Sample Disposal	ient Discoved Bull ab		(A fee may be assessed if samples are retained
Required	Í	]	OC Requirements (Spe	CINIOM	
] 48 Hours 🛛 7 Days 🔲 14 Days	21 Days     Other				
1. Holinguished By DOG (U. R. C. A. U. ), L. D. D.		Date Date Date Date Date Date Date Date			Date
2. Relinquished By	Date	Time	2. Received By		Date
3. Relinquished By	Date	Time	3. Received By		Date Time

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DISTRIBUTION: WHITE - Returned to Client with Report: CANARY - Stays with the Sample; PINK - Field Copy

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Failure to provide sufficient and/or correct information regarding reporting, invoicing & analyses requested information may result in delays for which MI will not be liable.

6-2-0 10:01

Project N	ame: C	JTCI	HN	Hopen	sell		V	COC Nur Vell ID: Date of C	ERA	
DOLUDI							L		oncent	. <u> </u>
Purging I	Equipmen	t: HN	IA-	4535	>	1				
Sampling	Equipme	ent:								
Filtering Equipment		and the second s	n:	Per Wo	ork Plan –	Alconox V	Wash with	n Triple H	Rinse and	d Isopropyl Alcohol Rin
						ent Calibra				
	-	uipment/N					Number	-		Date Calibrated
		Multi Para				05C	1520 AA			N1/A
			olorimet	er						N/A
FIELD PAL Ambient A						Weather C	onditions			
Sampling I			nlet@		_	Reference			er PVC ca	asing
Flow meter (gallons)	Flow rate /min	Depth to water	Time	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Commo
	11:20	Zen	7001	Depth	\$ 10	wer ju	TO U	en	Zer	veda Groud
	11:36	TOO	lib	Wat	Fen	っこっ	0.53	2		
					SE	-3 = 1	105.8	6	A	Speed 8+4
	11:40	Run	r.H.	HPWL	EPAL	4160	un	Calib	/	n u
		1ca	~							
		1/15	8 784							
	≥40 ≤200	1			±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach		se Man n Che		Non Filtered Manganese mg/l Hach	
			-			Malia	1000			
PURGE	NFORM	ATION		7001 R	eads	79.09	505	5	TICK	4P=5"
Starting Flo	ow meter	Reading		Endin	g Flow r	neter Read	ling:	]	Flow Ra	ate:
Total Volu	me Purge	d:	Pur	ged Dry (	Y/N):	Micro	purged (	(Y/N):	Mii	nimal purged (Y/N):_
Casing Inne Tubing inn Controller	er diamet	er	_(in) ]	Tubing & P	ump Vo	lume	(ml)			bottom of well (feet)
Casing Volume		gallons): 2"	well $= 0.17$	x WCT 4" wel						CT = Water Column Thickness

mm

	E	CAT D	11.		/		C	OC Nu	mber:	
Project Na	me: <u>E</u>	SILP	- 401	sewell	$\frac{1}{10000000000000000000000000000000000$					
Sample Co	ollected b	y: JF	tw		Date of Collection: 6876					
EQUIPMI Purging E	quipmen	t:	MA	453	-5					
Sampling	Equipme	ent:								
Filtering H Equipment			n:	Per Wo	ork Plan –	Alconox W	ash with	Triple	Rinse and	Isopropyl Alcohol Rinse
	it Decom				Equipmo	ent Calibrat	ion			
	Eq	uipment/I	Model				Number			Date Calibrated
	YSI 556 1	Multi Para	meter Me	ter		05C1	520 AA			27/4
	НАСН	DR 890 C	olorimete	r						N/A
FIELD PAR Ambient Ai Sampling D	r Temperat	ture (°F):_	nlet@		_	Weather Co Reference I	onditions: Point: <u>T</u>	Chor op of inn	er PVC cas	6001 ~ 650 ing
Flow meter	Flow rate	Depth to	Time	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comments
(gallons)	<u>/min</u>	water 157	Star	t = A	2A 20	en to	ott	06	voud	Surfur
	11	:58	Run		WL	Runl	EAA	165	Down	Calib 1 6-8-1
	12	101	Run	1 11	PWL	Run 1	EPI	165	4.P	Calls 6-51.
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach	Filtered Manganes mg/l Hach	e Mang m Cher	ered ganese g/l netrix sual)	Non Filtered Manganese mg/l Hach	Comments
PURGE I			Stil	Endin	= 4	$T_{CC} = L$	Vota tinc	Ste	B65 Flow Rate	= Tush m
		-								mal purged (Y/N):
sing Inne	r Diamet	er (inche	es) 4"	Initial I	Depth to		t) 13,4			ottom of well (feet)
ontroller s	ettings: F	Pressure	(psi)	Discharg	e (sec.) I	Recharge_				
ising Volume	Calculation (	gallons): 2"	well = $0.17$	WCT 4" wel	$1 = 0.66 \times W($	T 6" well = 1	47 x WCT		Where WC7	$\Gamma = $ Water Column Thickness (feet)

Page 1 of \_\_\_\_\_ n



Project N	ame:	STLA	- He	pewell	COC Number:					
									EPA	
Sample C	ollected	by:	100				D	ate of (	Collection	: 6-8-16
EQUIPM	ENT		. 1 -	457-	C					
Purging E	Equipmen	t:/	uH =	453 -	2					
Sampling	Equipme	ent:					-	-		
Filtering							-			
Equipmen	nt Decont	aminatio	on:	Per Wo				Triple	Rinse and I	sopropyl Alcohol Rinse
	14		_		Equipme	ent Calibrat	ion			
	-	uipment/I				Serial	Number			Date Calibrated
	¥SI 556	Multi Para	meter Me	eter		05C15	520 AA			
	HACH	DR 890 C	olorimete	er						N/A
FIELD PAI Ambient Ai Sampling D	ir Tempera Depth (ft):	ture (°F): Pump In				Weather Co Reference P	oint: To		_	
Flow meter (gallons)	Flow rate _/min	Depth to water	Time	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comments
Time	15.	38	Zen	1001	to	sound	1 Se	rfor	n	and a D
15:5	7 50	nac	goe	dor	in	TU Y	-0×8	4 6	the	Hitting Botton
15 -	16	dis	4 70	atto	Gam	1100	9-1	-: -:		
15:	55	Cal	That	tour 1	2	en =	75.0	65		Down Sper
		Cr				5E-3	=1	133	2,69	git telmin
										up Spird
										8. Ftt/min
	244									
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10my	
	240 5200									
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach	Filtered Manganese mg/l Hach	Mang m Cher	ered ganese g/l netrix sual)	Non Filtered Manganese mg/l Hach	Comments

#### PURGE INFORMATION

Starting Flow meter Reading:	Ending Flow n	neter Reading:	Flow Rate:
Total Volume Purged:	Purged Dry (Y/N):	Micro purged (	· · · · · · · · ·
	<u>4</u> Initial Depth to in) Tubing & Pump Vol (psi) Discharge (sec.) F	lume (ml)	9 Depth to bottom of well (feet) $42-2$ (sec.)
Controller settings: Pressure	_(psi) Discharge (sec.) F	kecharge	(sec.)

Casing Volume Calculation (gallons): 2" well = 0.17 x WCT 4" well = 0.66 x WCT 6" well = 1.47 x WCT

Where WCT = Water Column Thickness (feet)



Sample C EQUIPM							D	ate of C	Collection	6-8-16
Purging I	Equipmen	t: H	MA	- 45-	3-5					
Sampling	Equipme	ent:								
Filtering				-						
Equipmen	nt Decont	aminatio	on:	Per Wo				Triple I	Rinse and I	sopropyl Alcohol Rinse
-		•			Equipmo	ent Calibra				Date Calibrated
-	-	uipment/ Multi Para		Rom			Number 520 AA			Date Calibrated
-		DR 890 C				0001	320 AA	-		N/A
L	HACH	DK 890 C	Colorimete	#						IN/A
FIELD PAL Ambient A Sampling D	ir Temperat	ture (°F):_			_	Weather Co Reference	-		er PVC casi	ng
Flow meter (gallons)	Flow rate /min	Depth to water	Time	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comments
(8)	17;	25 7	Pero	Tool				1.1/2		
	17:	28-10	ol r	lits 1	lotton	a.	26.05	C id	TA	
	17	:40	pl m	pattan	- Equ	ili brat	ing in	With 2.25	lemp	
	- / /	110	Callo	M	-	SE.	3 =	1140	2.52	4
	17:43		Run	1 Don HP	WL E	PAZIS	pown	Cali	1-6-8-1	6 pown spy 8,5 mi
	17:47		P	HE	HPWI		15 UP		1 1 1 1	1115 1057
	17.99		Run	1 yp	UNFW C	EFAL	Sup	cang	1-68-11	e up spin ost
						1				
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l	Filtered	Non	Filtered	Filtered	Non Filtered	Filtered	Filt	ered	Non Filtered	
Chemetrix (Visual)	Alk mg/l Hach	Filtered Alk mg/l Hach	Fe2+ mg/l Hach	Fe2+ mg/l Chemetrix (Visual)	Fe2+ mg/l Hach	Manganes mg/l Hach	se Mang m Chen	ganese g/l netrix sual)	Manganese mg/l Hach	Comments
PURGE	INFORM	ATION	F	lush.	Noun	t To	0=	8.2	5" B	s
			:	Endir	ng Flow n	neter Read	ling:		Flow Rate	:
		-								
Starting Flo		d:	Pur	ged Dry (	Y/N:	Micro	purged (	Y/N):	IVIIIII	mal purged (Y/N):



GROUNDWATER	<b>PURGE AND</b>	SAMPLING	FORM

			GRU	UNDWA	IEKPU	KGE AN	U SAIVII	LING	FURM		
Project N	ame: E	STCK	- H	peure	11			OC Nu			
				1	7	Well ID: EPAZIO					
Sample C	ollected	by: 7/	YWI	TTU	Well ID: $EPA > ID$ Date of Collection: $6 - 8 - 16$						
EQUIPM	ENT	, ,		11	2-5						
Purging F	quipmen	t:	MH	- 453	5						
Sampling	Equipme	ent:									
Filtering I				D IV	1 . D1	A 1	7 1 11	T 1 1	D' 1	T 141 1 1D'	
Equipmer	nt Decont	aminatio	on:	Per Wo		ent Calibra		Triple	Rinse and	Isopropyl Alcohol Rinse	
-	Fa	uipment/	Model		Equipm		Number			Date Calibrated	
		Multi Para		Tar			520 AA	-		Date Calibrateu	
		DR 890 C					520 mm			N/A	
	IIACH	DK 890 C	olormiete							N/A	
FIELD PAR											
Ambient Ai Sampling D						Weather Co Reference			er DVC ca	sing	
		-							-		
Flow meter	Flow rate	Depth to	Time	Volume Purged	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	pH	ORP (mV)	Water Description/Comments	
(gallons)	/min	water		(Gallons)	(0)	(µs/em)	(		(	Description/Comments	
		17:5	32	en Ta	21						
			Used	Caliba	attan	from	70	ZD			
	12	54	Start	- Pow	Da	un h	nle +	an	Dura	1	
	110	9-1	Juana	nill	. AUG	on o	1.1		Run		
		Ru	us por	HPW.	LEP	A210	Down	Cali	61-6	-8-16 Down Spul	
	17:50	:0) Ru	n IUP/	HPW	EA	PAZIK	o up	10	h c	and as the	
			/								
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	9	
D.O. mg/l	Filtered	Non	Filtered	Filtered	Non Filtered			ered	Non Filtered		
Chemetrix (Visual)	Alk mg/l Hach	Filtered Alk mg/l	Fe2+ mg/l	Fe2+ mg/l Chemetrix (Visual)	Fe2+ mg/l Hach	Manganes mg/l	m	g/l netrix	Manganese mg/l	Comments	
(visual)		Hach	Hach	(Visual)		Hach		sual)	Hach		
PURGE I	NFORM	ATION	TO	ic is	IInc	h BG	ら三	> Fla	igh A	iaunt	
Starting Flo					-				Flow Rat		
				85				-		imal purged (Y/N):	
Casing Inne								D	epth to b	ottom of well (feet) 37.2	
Fubing inne								(			
Controller s	-			-			and the second	(se			
Casing Volume	Calculation (	gallons): 2"	well = 0.17	x WCT 4" wel	l = 0.66  x W	CT 6" well = 1.	47 x WCT		Where WC	T = Water Column Thickness (feet)	



Page <u>|</u> of <u>|</u>

& ASSOCIATES

#### DAILY FIELD ACTIVITY REPORT

	Client Name: Project Name: <u>ESTCP 20 1574</u> Hopewalf Contractor: Weather: <u>60° F Mostly</u>	Project Number: Date: Arrival Time:
	Time Breakdown: Drive: Work:	Standby:
	Location and Description of Activities: EPA 12 Shallow	
	Equipment Used on Project:	
10:15		28.60 - 0. 28) = 28.32pt INL Liter
0:30	Hopewall EPAIDSTIL BI # 12 (1) TH BI # 2 TH BI # 3	MISON - 100 ml
	Background Hopciocle EPA125 ~ 150	mL
10:43 10:50	HopewellEPA 125 DNA 1000mL & 9m HopewellEPA 125 RNA 1000mL J	ucrobial (Nomenal 500 = naght 510mL both nalgene 500 Berkas mL
	Technician Signature:	Date:
		WIEDEMEIER

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C:\Admin\Forms\Daily Field Activity Report.doc

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GROUNDWATER	PURGE AND	SAMPLING FORM

Project N	lame: E	STCI	2019	584 H	opeur	<u>ol</u>	C	OC Nu	mber:	- 12 S n: 6/9/14
Sample (	Collected 1	hv. Tr	NB	$\frac{1}{1}$	ITC.		V D	Vell ID:	Collectio	-125
		<u> </u>	/////	~			D		concetto	n. <u> </u>
EQUIPM Purging E		t٠								
•••	· ·	-								
Filtering										······································
					ork Plan –	Alconox V	Vash with	Triple	Rinse and	Isopropyl Alcohol Rinse
				· · · · ·	Equipm	ent Calibra	tion			
	Eq	uipment/	Model			Serial	Number			Date Calibrated
	YSI 556	Multi Para	ameter Me	eter		05C1	520 AA			
	HACH	DR 890 C	Colorimete	er ·						N/A
FIELD PAL Ambient A Sampling D	ir Temperat	 ture (°F):_	(00 <sup>0</sup> nlet@			Weather Concept	onditions:_ Point:	MOS op of inn	Hy Cl er PVC ca	ordy
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	- pH	ORP	Water
meter (gallons)	rate /min	to water	9:58	Purged (Gallons)	(°C)	(μS/cm)	(mg/L)	pn	(mV)	Description/Comments
				0	12.23	.970	10.89	7.19	242.6	
			4:35	<u> </u>	10.62	1.01	6.81	6.70	271.8	
			6:17	പ്പയ	10.55	1.009	6.77	6.76	269.8	
			10:30	4	10.53	1.004	6.72	6.61	270.9	
		Sto	ened	10:00						
		210	pro	10:00	¶		· · · · · · · · · · · · · · · · · · ·			
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
								I		
D.O. mg/l Chemetrix	Filtered Alk mg/l	Non Filtered	Filtered Fe2+ mg/l	Filtered Fe2+ mg/l Chemetrix	Non Filtered Fe2+ mg/l	Manganes	e Mang	ganese	Non Filtered Manganese	Commonte
(Visual)	Hach	Alk mg/l Hach	Hach	(Visual)	Hach	mg/l Hach	Cher	g/l netrix sual)	mg/l Hach	Comments
	1				0.00					
L					10.00					
<u>PURGE I</u> Starting Flo			•	Endin	ng Flow n	neter Read	ling:		Flow Rat	te:
otal Volu	me Purge	d: <u>4</u>	Pur	ged Dry (	Y/(S):	Micro	purged (	Y/Ø):	Min	imal purged (Y/SP?
Casing Inne	er Diamet	er (inch	es) 4	Initial	Depth to	– Water (fee	t) 10.4	ריי, ת`∕	enth to h	ottom of well (feet) 28.32
Tubing inne Controller	er diamete settings: F	er <u>11</u> Pressure	(in) T (psi)	ubing & F Discharg	Pump Vol	lume Recharge	(ml)	ر ا	c.)	ottom of well (feet) $28.32$
						-		-		
All	purg	E W	oter	Conta - Plan	ineriza	ed in	5 qp	llon	Doj	T = Water Column Thickness <u>(feet)</u> - Appruvee 28.3 SAL
Con	tainer	per			ur ···	- 1				<b>₩</b>
D:\THV	VA\Admin\Forms -	Field\Groundwa	ater Purge and S	ampling Form.doc	Р	age 1 of _				

Page \_\_\_\_ of \_\_\_\_

# **DAILY FIELD ACTIVITY REPORT**

	Client Name: Project Number: Project Number: Project Name: ESTCP 201584 Hopewell Date: 6-9-16 Contractor: Arrival Time: 13:22 Weather: Ce7°F Mostlyclear/Survey	
	Time Breakdown: Drive: Work: Standby:	
	Location and Description of Activities: <u>FPH 10 S</u>	
	Equipment Used on Project: 	
	Activity Summary and General Remarks: Depth to water 2021t BTOC Depth Well 30-4 · 28/t correction sensor toottom probe Distance Toc and ground surface 6.2 inches	
14:20	Hopewelf EPA 105 Sample 2 4 PINNI Hopewell EPA 105 Sample 2 4 PINNI Hopewell EPA 105 Sample 3 1 Jitu Hopewel EPA 105 Sample 4 + 1 Trip Slank (1 hiter)	
14:33	Hopewell EPA 105 TH B2#1 Clemson Hopewell EPA 105 TH B2#2 Hopewell EPA 105 TH B2#3 Bashground Hopewell EPA 105~10 Thechground Hopewell Bashground Hopewell EPA 105~10 Thechground Hopewell EPA 15D	
14:41	Hopewell EPAIDS DNA 6000mL EPAID Extra 6 Hopewell EPAIDS DNA 6000mL Extra 6 Hopewell PAIDS NA 6000mL preserved ~150m	L
	Technician Signature: Date:	



N:\Admin\Forms - Field\Daily Field Activity Report.doc

Project N	ame: E	STCP	2015	84	Hope	well	C	COC Nu	mber:	10.6
Sample C	Collected I	oy: JL	NIBU	otto	1DC		C	ate of (	Collection	- 105 n: 6-9-16
EQUIPM		-		•						
Purging E		t:								
Sampling										
Filtering										
Equipmen	nt Decont	aminatio	on:	Per W				<u>Triple</u>	Rinse and	Isopropyl Alcohol Rinse
					Equipmo	ent Calibra			1	
		uipment/					Number			Date Calibrated
			ameter Me			05C1	520 AA			
	HACH	DR 890 C	Colorimete	r						N/A
FIELD PAL Ambient A Sampling D	ir Temperat	ure (°F):_	<u>67</u>		<u></u>	Weather C	onditions:	Mo	stly (	lear Summy
			· · · · · ·	N/- I				<b>T</b>		
Flow meter (gallons)	Flow rate /min	Depth to water	Time 13:55	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comments
				0	12.19		5.55	6.74	95.7	clear no color
			3:00	2	10.68	·620 .712	4,79 5.49		133,4	clear no Celon
			7:31	<u> </u>	9.87	1756	5.75	6.38	179.1	chear no color,
			9:49	ų.	9.82	.771	5.86	6.31	172.8	
			sto	mat	14:0	>-1				
·····			and	μ <b>ρ</b> ω						
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l Chemetrix	Filtered Alk mg/l Hach	Non Filtered Alk mg/l	Filtered Fe2+ mg/l	Filtered Fe2+ mg/l Chemetrix	Non Filtered Fe2+ mg/l Hach	Filtered Mangane mg/l	se Man	tered ganese ng/l	Non Filtered Manganese mg/l	Comments
(Visual)	Thach	Hach	Hach	(Visual)		Hach		metrix sual)	Hach	
PURGE I	ow meter	Reading								
otal Volu	me Purge	d: <u>4</u>	Pur	ged Dry (	Y/🕅):	Micro	purged (	Y/ <b>(\$∲)</b> :	Min	imal purged (YA):
Casing Inne Subing inne Controller S	er Diamet er diamet	er (incher er <u>17</u>	$\underbrace{\begin{array}{c} \text{es} \underline{4} \\ \underline{-(\text{in}) T} \\ (\text{nsi}) \end{array}$	Initial ubing & I	Depth to T Pump Vol	Water (fee ume	et) <u>9,0</u> (ml)	<u><b>2</b></u> D	epth to b	ottom of well (feet) <u>84.6</u>
Casing Volume	-			-		-			, ,	T = Water Column Thickness (feet)

•

Mitchenter Francis Manage Lo Dr Francis Manage Lo Dr Francis Manage State Backas State Conflict Mitchenter State Backas State Conflict Mitchenter State Backas State Conflict Mitchenter Front Lo Contact Marker Manage Contact Mitchenter Providenter Providenter Providenter Mitchenter	
Telephone Number     Telephone Number     Telephone Number       Floc     Floc     Floc     Floc       Floc	
Role     Stie Contact     Analysis (Attach list if hore space is needed)       Image: State in the image is contact     Image: State in the image is needed)       Image: State in the image is contact     Image: State in the image is needed)       Image: State in the image is contact     Image: State in the image is needed)       Image: State in the image is contact     Image: State in the image is contact       Image: State in the image is contact     Image: State in the image is contact       Image: State in the image is contact     Image: State in the image is contact       Image: State in the image is contact     Image: State in the image is contact       Image: Image: State in the image is contact     Image: State in the image is contact       Image: Image: Image: Image is contact     Image: Image is contact       Image: Image: Image: Image is contact     Image: Image is contact       Image: Image: Image: Image is contact     Image: Image is contact       Image: Im	910-1
Date Time Matrix Containers & Matrix Containers & Matrix Containers & Matrix Containers & Contai	
Date Time Date Date Date Date Date Date Date Dat	Special Instructions/ Conditions of Receipt
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	
mable 🗌 Skin Irritant 🗌 Poison B 🔲 Unknown 📙 Return To Client 📔	may be assessed if samples are retained than 1 month)
dequirements (Specify)           48 Hours         7 Days         21 Days         Other	
U. C. U. J. D. Date Time 1. Received By Date Date	Date
Date Time 2. Received By	Date
thed By 3. Received By Date Time 3. Received By Date	Date
Comments	
DISTRIBUTION: WHILE - Hetumed to Client with Report. CANARY - Stays with the Sample. PINK - Field Copy	

DISTRIBUTION: WHITE - Returned to Client with Report: CANARY - Stays with the Sample; PINK - Field Copy

-1 - Wig Pol

Chain of		SEV TR	TRENT STL		STL Denver	~ - -
Custody Record		Sever	Severn Trent Laboratories, Inc.	ttories, Inc.	4955 Yarrow Street Arvada, CO 80002	ureet 002
STL-4124 (0901) Cliant			2			
ESTOP-TOdd Wliedemeier	Project Manager NIA	alemeier	1.1 6-24	10-9-16	Chain of Custody Number 342283	Number 000
SOJ COPARACO DE	Telephone Number (Area Code)/Fax Number	ellFax Number 999		Lab Number	Page	of /
Sechlia Rate Za code	Site Confact	David Flepdurch	Analy more :	Analysis (Attach list if more space is needed)	       	
Cation (State) NPLS the	11		(1)			/ <u></u>
Contractifunctiast Order/Quote No. Hep CULLECT Desice	Lov Matrix	Containers & Preservatives	Lfre		Conditio	opecial instructions/ Conditions of Receipt
Sample I.D. No. and Description (Containers for each sample may be combined on one line) Date	Time beac inos	HO <sup>E</sup> N Zu <sup>y</sup> o <mark>U</mark> HO <sup>E</sup> N HO HOO3 HOO3 HOSZH	נשינ			
91-6-9	10130		1			
田 81#2	7		7			
Hopewold EPA-125 181 #3 6-9-16	7		7			
#1 6-9-16	H:33 V		7			
Hepewell EPAIOS IL 82 #2 6-9-16	2		1			
Hopewell FPA105 The #3 6-9-16	7		7			
Kachground Hesewere PHIDS 6-9-16	× ⊥ ⊥ ↓	ía –				
Than you bank ground the well EM 165 14	HIS V EX	के		2		
Ture you land grownal lequererer 15D 14	14:50 . V EX4	xtra 6				
n mmable 🔤 Skin Irritant 🔤 Poison B	Sample Disposal		chive For Months		(A fee may be assessed if samples are retained longer than 1 month)	e retained
Required ] 48 Hours	Other	CC Requirements (Specify)				
"a Withor	Pate 9-16 Time: 18	1. Received By			Date	Time
2. Relinquished By	Date	2. Received By			Date	Time
3. Relinquished By	Date	3. Received By			Date	Time
Comments					_	

DISTRIBUTION: WHITE - Returned to Client with Report: CANARY - Stays with the Sample: PINK - Field Copy

Name: Company:				144		Name: Company: Address:	¥															Ĭ	5	<b>crobial</b> insights	ġ.	lin	Sić	T.	\$	
uuress.		9.5 17 17			-	scalling															6 Z	515 Rt	10515 Research Dr Knowille TN 37032	Dr (03)						
email:					ي ر.	remail:															86	865-573-8188	8188							
Phone: Fax:						Phone: Fax:		1			ar ,										Š	w.mic	www.microbe.com	ш						
Project Manager:					<u>ب</u>	Purchase Order No.	s Orde	No.		1							4	4	I		ā	ease C	Please Check One:	Sne:						
Project Name:						Subcontract No.	ract Nc	l I c			i -										ப	] Moi	re san	□ More samples to follow	to foll	MO				
Project No.:					-	MI Quote No.	No.														Ц	No	Additi	No Additional Samples	ampl	es				
Report Type: EDD type:	<ul> <li>☐ Standard (default)</li> <li>☐ Microbial</li> <li>☐ Microbial Insights Standard (default)</li> </ul>	☐ Microb ndard (defau	Microbial Insights Level III raw data(15% surcharge)     ird (default)	∦ III raw dat: □ All c	raw data(15% surcharge) □ Microbial Insights L □ All other available EDDs (5% surcharge)	harge) ailable [		dicrob (5% :	ial Insi surche	Microbial Insights Level IV (25% surcharge) s (5% surcharge) Špecify EDD Type	vel IV Spe	el IV (25% surcharge) Specify EDD Type:	ırchargı JD Typ	l œ_e)			dmo	□ Comprehensive Interpretive(15%)	sive II	nterpi	etive(	15%)			Histo	rical I	Historical Interpretive (35%)	retive	(35%	~
	Sample Information Analyses CENSUS: Please select the target organ	ation				Analyses	es	0	ËNS:	US: F	leas	e sele	sct th	le tar	get c	rgar	lism	CÉNSUS: Please select the target organism/gene												
(Auc) sen (Aussunger)	Sample Name	Date Sampled	bəlqms2 əmiT	xittsM	PLFA	SON	QuantArray Chlor	QuantArray Petro	DHC Functional genes	DHBt (Dehalobacter)	DHG (Dehalogenimonas)	DSM (Desulfuromonas)	DSB (Desulfitobacterium)	EBAC (Total)	SRB (Sulfate Reducing Bacteria-APS)	MGN (Methanogens)	(sriqotionsriteM) 80M	OMMS	DNF (Dentrifiers-nirS and nirK) AOB	(ammonia oxidizing bacteria)	PM1 (MTBE aerobic)	RODEG (Toluene Monooxygenase)	PHE (Phenol Hydroxylase)	NAH (Иарthalene-аегоріс)	ASSA	add. qPCR: add. qPCR:	АИЯ	(Expression Option)* Othe∷	Other:	Other:
		S.	th)					-	<u> </u>		5		<b>ب</b> و ر ب					4	. 1		-					_				
	T TH LES DNH	6-1		G.A.					<u>}</u>	/ 						5	Ė.	-					 							
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Relinquished by:		Ų.				Rec	Received by:	;; p					Date															8.		

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# IDWATED DUDGE AND CAMPLING EO

				UNDWA		RGE AN	U SAMI	PLING	FORM	
Project N	lame: E	STCI	5-1	Hopewe	11			COC Nu		
							V	Vell ID:	EPA	-125 n: 6/9/16
Sample C	Collected 1	by:	HU I	1 DM	C		D	Date of (	Collection	n: 6/9/16
EQUIPM	IENT	1.								
				4535						
	Equipme									
-	Equipmen			D W	1 D1	A 1	17 1	T. 1. 1. 1	D:1	T
Equipme	nt Decont	aminatio	on:	Per wo		ent Calibra		i I riple	kinse and	Isopropyl Alcohol Rinse
-	Ea	uipment/I	Model		Equipin		Number			Date Calibrated
	-	Multi Para		eter			520 AA			
	HACH	DR 890 C	olorimet	er						N/A
	RAMETER	C								
Ambient A	ir Temperat	ture (°F):	62	0		Weather C	onditions:	11	par a	Breezy /Lool
Sampling I	Depth (ft):	Pump I	nlet@			Reference	Point: T	op of inn	er PVC cas	sing
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pH	ORP	Water
meter (gallons)	rate /min	to water		Purged (Gallons)	(°C)	(µS/cm)	(mg/L)		(mV)	Description/Comments
(ganons)	11:13	Zen	Too		ver in	to u	atri-	2Tm	Read	28A8' bas@
			tom	of ho	e					
	11:27	- la	si bia	Eing	1001	Zen	=	8	97.4	66
						50		- //	rori	•
	11:36	Run	1	HAML	EP1	1251	Down	Rint	lalih	16-9-16
-										
	11:40	RIN	1	HOWL	ED	A125	UD	Runi	Calib 1	Ran probe
					r		1		1	up & down, at
										approx 8'/Min
										-6-1-16
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l	Filtered	Non	Filtered	Filtered	Non Filtered				Non Filtered	
Chemetrix (Visual)	Alk mg/l Hach	Filtered Alk mg/l	Fe2+ mg/l	Fe2+ mg/l Chemetrix (Visual)	Fe2+ mg/l Hach	Manganes mg/l	n	ganese ng/l metrix	Manganese mg/l	Comments
(*15001)		Hach	Hach	(		Hach		sual)	Hach	
			-			144	10		100	
PURGE	INFORM.	ATION	Flu	sh M	Ount	100	15 0	6" K	365	
arting Flo	ow meter	Reading	:	Endin	g Flow n	neter Read	ling:		Flow Rat	e:
					-					imal purged (Y/N):
	-									ottom of well (feet)
ibing inn	er diamet	er	(in) T	Tubing & F	Pump Vo	lume	(ml)	D	opui to b	
				) Discharg				(see	c.)	
sing Volum	e Calculation (	gallons): 2"	well = 0.17	x WCT 4" wel	$ll = 0.66 \times W$	CT 6" well = $1$	.47 x WCT		Where WC	T = Water Column Thickness (feet)



Project N Sample C <u>EQUIPM</u> Purging F	ollected h	w. Th	w/	DMC	- n		C W D	OC Nu /ell ID:	EPA	-120 n: 6-9-16
FOLIPM	FNT	. <u>.</u>		<u>.</u>	-		D	ate of c	Joneetion	
Purging F	Equipmen	t:	+MA	- 45.	3-5					
Sampling	Equipme	ent:								
Filtering					1.01		7 1 1.1	m ' 1 1	D: 1	Y 141 1 1D'
Equipmen	nt Decont	aminatic	on:	Per W		Alconox V ent Calibra		Triple	Rinse and	Isopropyl Alcohol Rinse
	Eq	uipment/I	Iodel		Equipm		Number			Date Calibrated
	-	Multi Para		eter		05C1	520 AA	-		
	HACH	DR 890 C	olorimete	er						N/A
FIELD PAI	RAMETER	S	-							
Ambient A			1.0			Weather C			DUC	
Sampling D					_	Reference		-		-
Flow meter (gallons)	Flow rate /min	Depth to water	Time	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comments
(ganons)	11:50	Zero	Too	to	april	& Su	fuce			
	11:52	Ry	21	HOWL	EDA	120 7	Jown	Run	1 Cali	41 1/9/1/
	11.76	2							1 Call	
	11:58	Kus	nl	HPWI	LEPA	120	upp	kun	Cal	6 9 6
										RATE
										APPROX 8 /min
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l	Filtered	Non	Filtered Fe2+	Filtered Fe2+ mg/l	Non Filtered Fe2+ mg/l			ered	Non Filtered	
Chemetrix (Visual)	Alk mg/l Hach	Filtered Alk mg/l Hach	mg/l Hach	Chemetrix (Visual)	Hach	Mangane mg/l	m Cher	g/l netrix	Manganese mg/l	Comments
		Them	Theon			Hach	(Vis	sual)	Hach	
			EI	uch. A	rount	TOC	0	= ic	6" B	65
PURGE I										
-		-			-	neter Read				
								~		imal purged (Y/N):
ubing inn	er diamet	er	(in) T	ubing &	Pump Vo	Water (fee lume Recharge_	(ml)			ottom of well (feet) 3.92 BTOC
										T = Water Column Thickness (feet)
asing volume	e Calculation (		wen = $0.17$	x wc1 4 W	en = 0.00  x W	CT 6" well = 1	HAWCI		where we	water Column Thickness (leet)
		44.2								

& ASSOCIATES

Project N	ame: E	STCA	~ Ho	Dewell				OC Nu		<u> </u>
Sample C	collected	by: TH	V/A	mc			D	ate of (	Collection	5 6-9-16
EQUIPM Rurging E Sampling	Equipmen			<u>53-5</u>		SN	555	4		
Filtering 1										
Equipmen			n.	Per Wo	rk Plan_	Alconox V	Vach with	Triple	Rinse and I	Isopropyl Alcohol Rinse
Lquipinei	In Decom	ammane		101 00		ent Calibra		mpie	Itilise and I	sopropyrmeonormise
	Ea	uipment/I	Model		-1-1-		Number			Date Calibrated
	-YSI 556	-		eter			520 AA			
		DR 890 C	~							N/A
	HACH	010000	oroninieu							
FIELD PAI Ambient Ai Sampling D	ir Tempera	ture (°F):_			_	Weather C Reference			er PVC casi	ing
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pH	ORP	Water
meter	rate	to		Purged	(°C)	(µS/cm)	(mg/L)		(mV)	Description/Comments
(gallons)	/min	water	200	(Gallons)		<i>c</i> ,				speid a 8-to/m
		15:40	Zero Rui		march .	Serfue	215 1	2.24	1161	10-9-16
		15:46	Ru	n li	D HD		4215	110 (	alibi	6-9-16
		10 10			14	·P	10			
		15:57		2=>0			PA21	SDO	won Calib	
			Run	2 40	-> /	HANL	EPAZ	24	p Cali	61 6-9-16
			-							
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filterer Fe2+ mg/l Hach		se Mang m Cher	ered ganese g/l netrix sual)	Non Filtered Manganese mg/l Hach	Comments
			Ī-	Fun	Mai	int T	TOG :	= 6	2" R.	50
PURGE I	NFORM	AHON		ur Ju	11100	1116 1		0,		2
tarting Flo	ow meter	Reading	:	Endin	g Flow r	neter Read	ling:		Flow Rate	2:
otal Volu	me Purge	d:	Pur	ged Dry (	(/N):	Micro	purged (	Y/N):	Mini	mal purged (Y/N):
Casing Inne	er Diamer er diamet	ter (inche	es) <u>4</u> (in) T	Initial I Tubing & P	Depth to Pump Vo		et) <u>9, 1</u> (ml)	<u>02</u> 0	epth to bo	ottom of well (feet)
	-			-						= Water Column Thickness (fast)
Casing Volume	Powe	(gallons): 2"	well = 0.17	x WCT 4" wel	I = 0.66 x W	CT 6" well = 1	.47 x WC1		where wC1	T = Water Column Thickness (feet)
		Field Correct	ater Duran and	Sempling Form doc	T	Page 1 of				

Project	lame: E	STCK	) - H	spenel	1		C	OC Nu	mber:	
<b>a</b> 1 <b>a</b>		+	1110	Inno					EPH	
	Collected 1	by:	huj	Dia	-		D	ate of (	Collection	n: 6-9-16
EQUIPM	I <u>ENT</u> Equipmen	· bl	11 A-	457-	C	Kar	En I	Al.	10.0	6754
Sampling	g Equipmen	nt:	ил	~	>	arr	·u /	van	BUL	3331
	Equipmen				1000					
-	nt Decont		on:	Per Wo	ork Plan –	Alconox W	ash with	Triple	Rinse and	Isopropyl Alcohol Rinse
					Equipm	ent Calibrat	tion			
	-	uipment/I					Number			Date Calibrated
		Multi Para				05C1	520 AA			
	HACH	DR 890 C	olorimete	er						N/A
	RAMETER									
	ir Temperat Depth (ft):		nlet@		-	Weather Co Reference I			er PVC cas	ving
Flow		-	Time	Volume	Toma		DO		-	Water
meter	Flow rate	Depth to	Time	Volume Purged	Temp (°C)	Sp.Cond (µS/cm)	(mg/L)	pH	ORP (mV)	Description/Comments
(gallons)	/min	water	4	(Gallons)		1				
	14:00	tero	100,	Tept	5 Our	1.101	part +	2	Sailibe	ate TRansA
	11-01	-00		1001	101.00	per p		-		the map
	TOOL H	ITS GI	TOM	AIME	ASURE	2 DEPTH	OK5	3.02	fbgs	anon Spiel
	15.4	p 00	1101	an	200	E-3	= 00	151	1	
own	15:20	Ru	n1	HPWL	EPA	DO DO	un R	unic	alibi	6-9-16
	15:4	+ Ru	n/	HPWI	EPI	4 100 4	P Ru	610	alib 1	6-9-16
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach		e Mang	anese g/l netrix	Non Filtered Manganese mg/l Hach	Comments
	INFORM									Mount
			-		-	neter Read				
	-		10							imal purged (Y/N):
ubing inn	er diamet	er	(in) T	ubing & P	ump Vo	Water (fee lume Recharge	(ml)			ottom of well (feet) <u>54</u>
						CT 6" well = 1.				T = Water Column Thickness (feet)
	()			Lines						

# COOLINDWATED DUDCE AND SAMDUNC FORM

			GRU	UNDWA	IEKPU	KGE ANI	J SAIVII	PLING	FURM	
Project N	ame: <u>E</u>	STOP	-Ho	pewel	/			COC Nu		
Sample C	ollected	hu. TH	WITT	W			V	Vell ID	EPA-	190
FOLIDM	ENIT						L	ale of	Conection	1. 6-10-10
EQUIPM Purging E	<u>EN I</u> Cauipmen	t: HA	NA -	453 =	5					
Sampling	Equipme	ent:								
Filtering										
Equipmen	nt Decont	aminatio	on:	Per Wo				n Triple	Rinse and	Isopropyl Alcohol Rinse
	Fa	uipment/	Model		Equipmo	ent Calibrat	Number			Date Calibrated
		Multi Para		eter		05C1				Date Cambrateu
		DR 890 C								N/A
FIELD PAI Ambient Ai Sampling D	r Tempera	ture (°F):_	nlet@	3	_	Weather Co Reference I	onditions: Point: T	<u>Chu</u> op of int	n \$	Breezy
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pH	ORP	Water
meter (gallons)	rate /min	to water		Purged (Gallons)	(°C)	(µS/cm)	(mg/L)		(mV)	Description/Comments
			09:35	Zero	Tool	to yre	und S	rfac	1	
			69:37	2 Iog	1 15	- Wa	the j	F C	quili.	brat joc
			Dais	3 6	liho	et to.	1 9	Zer	20 =	65 F
					2110	- un	5E	-3	=112	81
			01.59	Run 1 -	HPU	UL ER	4-191	Dou	Rund	(alib + 6-10-1)
		/	0.00	Part	/ np		7		- Mart	and a note
-										Speed up a
										down ris for
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l	Filtered	Non	Filtered	Filtered	Non Filtered		1	tered	Non Filtered	
Chemetrix (Visual)	Alk mg/l Hach	Filtered Alk mg/l Hach	Fe2+ mg/l Hach	Fe2+ mg/l Chemetrix (Visual)	Fe2+ mg/l Hach	Manganes mg/l Hach	m Cher	ganese ng/l metrix sual)	Manganese mg/l Hach	Comments
PURGE I	NFORM	ATION								

Starting Flow meter Reading:	Ending Flow meter Reading:	Flow Rate:	
Total Volume Purged: P	'urged Dry (Y/N): Micro purg	ed (Y/N):Minimal purged (Y/N):	,
Casing Inner Diameter (inches) Tubing inner diameter // (in) Controller settings: Pressure(p	) Tubing & Pump Volume(1	$\frac{23,7'B}{\text{ml}} \xrightarrow{\text{BFC}} \text{Brock}$ $\frac{13,7'B}{\text{ml}} \xrightarrow{\text{BFC}} \text{Brock}$	7
Casing Volume Calculation (gallons): 2" well = 0	0.17  x WCT 4" well = 0.66  x WCT 6" well = 1.47  x V	WCT Where WCT = Water Column Thickness (feet)	
4915 28		***	
48,87	Page 1 of	WEDEMEIER & ABBOCIATES	

GROUNDWATER PURGE AND SAMPLING FORM
-------------------------------------

SN/ 5554

Project Name: ESTCP-Hopewell

Sample Collected by: THU/JTW

COC Number: Well ID: <u>EPA-195</u> Date of Collection: <u>b-10-16</u>

N/A

EQUIPMENT

24.80

128

Rurging Equipment: HMA -453 -5

Sampling Equipment:

Filtering Equipment:

 Equipment Decontamination:
 Per Work Plan – Alconox Wash with Triple Rinse and Isopropyl Alcohol Rinse

 Equipment Calibration
 Date Calibrated

 Value
 Serial Number
 Date Calibrated

 VSI 556 Multi Parameter Meter
 05C1520 AA
 05C1520 AA

HACH DR 890 Colorimeter

FIELD PARAMETERS

Ambient Air Temperature (°F): 66 Sampling Depth (ft): Pump Inlet@ Weather Conditions: <u>Gear, Gol & Brezzy</u> Reference Point: Top of inner PVC casing

Flow meter (gallons)	Flow rate /min	Depth to water	Time	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comments
Down	~	Run1 Runt	h	En Tu AWL DW1	EPA-	Star 195 Down	r Ru Ru Run	114	elib f	6-10-16
			100	r Dead	5 2	5,26,	a Re	ttor	~	Down & up sport 27.7
Awn hp		Run	24	HPWL HPWL	EPA	-195 -195	Баш	Run	un Z 2 C	Calib 1 6-10-
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	

D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach	Filtered Manganese mg/l Hach	Filtered Manganese mg/l Chemetrix (Visual)	Non Filtered Manganese mg/l Hach	Comments
			-						

# PURGE INFORMATION TOX IS 6" below Grown Surface => Flush mount

Starting Flow meter Reading:	Ending Flow meter Readi	ng: Flow Rate:	
		· · · · · · · · · · · · · · · · · · ·	nal purged (Y/N):
Tubing inner diameter 4 (in) Tubi	Initial Depth to Water (feet ng & Pump Volume ischarge (sec.) Recharge	) <u>23,56</u> Depth to bot _(ml) _(sec.)	tom of well (feet) <u>24</u> 55 BTOC
Controller settings. Tressure(psi) Di	isenarge (see.) Reenarge_	(500.)	

Casing Volume Calculation (gallons): 2" well = 0.17 x WCT 4" well = 0.66 x WCT 6" well = 1.47 x WCT

Where WCT = Water Column Thickness (feet)



Project N	ame: FS	TCP-	Hope	aver .				OC Nu		
Sample C	collected 1	by: TH	W/J	TW			W D	ell ID: ate of C	EPA - 8	6-10-16
	<u>ENT</u> Equipmen	t:/	/	-453	-5					
Filtering	Equipmen	nt:								
Equipmen	nt Decont	aminatio	on:	Per Wo		Alconox V ent Calibra		Triple I	Rinse and I	sopropyl Alcohol Rinse
	Ea	uipment/N	Iodel		Eduihu		Number			Date Calibrated
	-	Multi Para		eter			520 AA			
	HACH	DR 890 C	olorimete	er						N/A
FIELD PAI	RAMETER	S				1.2 3. 5	23.2			
Ambient A Sampling D	ir Temperat	ture (°F):_	nlet@		_	Weather Concerne		op of inne	er PVC casi	ing
Flow meter (gallons)	Flow rate /min	Depth to water	Time	Volume Purged (Gallons)	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comments
		10:50	2	ero Ta	21	To 61	ound	Suy	mer	
			Did	not v	by	brite E	stee	from 2	1 mat Could	Well because not Rind
			ave	a wit	hout	Marin	Stul	Pjei	es a	Structure
Down	Ru	nl	HPW	L EPA	1-80	Davi	Rue	10	1151	6-10-16
up	Ri	en l	HPU	L EP,	4-80	Lip	Ru	nl	Calibi	6-10-16
				Terl	Rend	A Bot	ton	æ	81.78	'RG'S
Runz	HA	WLE	PA-	RA D	own	Run Z	Cali	hI	10-10	Speed ~ sttlenten
Runz	LKK	TWI A	DA-	sn l	1P	Run Z	- Ca	libl	6-10	16
	≥40 ≤200		, ,,	1.0	±10%	±10%	±10%	±0.2	±10mv	16
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filterer Fe2+ mg/l Hach		se Mang m Chen	ered anese g/l netrix sual)	Non Filtered Manganese mg/l Hach	Comments
								_		
PURGE I	NFORM	ATION	Flu	sh ma	not t	et a	- BO	ST	DC = 0	0.6 BGS
Starting Flo	ow meter	Reading	:	Endin	g Flow r	neter Read	ling:	]	Flow Rate	2:
Total Volu	me Purge	d:	Pur	ged Dry ()	(/N):	Micro	purged (	Y/N):	Mini	mal purged (Y/N):
Casing Inne Tubing inne Controller	er Diamet er diamet	ter (inche er 4	es)(in) T	Initial I Tubing & P	Depth to Sump Vo	Water (fee lume	et) <u>[3,00</u> (ml)	Broch	epth to bo	ottom of well (feet) <u>82,72</u> BTOL
Casing Volume	Calculation (	gallons): 2"	well = 0.17	x WCT 4" wel	l = 0.66 x W	CT 6" well = 1	.47 x WCT		Where WCT	" = Water Column Thickness (feet)
-	STOT L	F110		Come line French	T	Page 1 of				

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EQUIPMENT         Parging Equipment:	Date Calibrated N/A C casing P Water
EQUIPMENT         Parging Equipment:         Sampling Equipment:         Grittering Equipment:         Grittering Equipment:         Grittering Equipment:         Grittering Equipment:         Grittering Equipment:         Equipment Decontamination:       Per Work Plan – Alconox Wash with Triple Rinse         Equipment Calibration         Equipment/Model       Serial Number         YSI 556 Multi Parameter Meter       OSCI520 AA         HACH DR 890 Colorimeter         Weather Conditions:         CHELD PARAMETERS         Ambient Air Temperature (°F):       Weather Conditions:         Grittering Equipment to         Meeter       Sp.Cond       DO       pH       OI         Matter Colspan="2">Colspa="2">Colspa= Colspa= Colspa="2">Colspan="2" <t< td=""><td>and Isopropyl Alcohol Rinse Date Calibrated N/A Casing Water Water</td></t<>	and Isopropyl Alcohol Rinse Date Calibrated N/A Casing Water Water
Purging Equipment:       Image: Arrow of the second s	Date Calibrated N/A Casing Water Water
Sampling Equipment:         Cluipment Decontamination:       Per Work Plan – Alconox Wash with Triple Rinse         Equipment Calibration         Equipment Calibration         Equipment Calibration         Vist 556 Multi Parameter Meter       OSC1520 AA         HACH DR 890 Colorimeter         Weather Conditions:         TELD PARAMETERS         Weather Conditions:         Top of inner PV/         Reference Point:       Top of inner PV/         Flow       Per Work Plan – Alconox Wash with Triple Rinse         Mision All PACH DR 890 Colorimeter         ''IELD PARAMETERS         Weather Conditions:         Top of inner PV/         Reference Point:       Top of inner PV/         Gallons)       /// M         /// M       OD       Purged       (°C)       (%C)       Mach       //// M         Image: Colspan="2">Mage: Colspan="2">Mage: Colspan="2">Mage: Colspan="2"         Image: Colspan= 2 <th< td=""><td>Date Calibrated N/A Casing Water Water</td></th<>	Date Calibrated N/A Casing Water Water
Per Work Plan – Alconox Wash with Triple Rinse         Equipment Calibration         Equipment/Model       Serial Number         YSI 556 Multi Parameter Meter       05C1520 AA         HACH DR 890 Colorimeter	Date Calibrated N/A Casing Water Water
Equipment Calibration         Equipment/Model       Serial Number         YSI 556 Multi Parameter Meter       05C1520 AA         HACH DR 890 Colorimeter       05C1520 AA         IELD PARAMETERS       Weather Conditions:         ampling Depth (ft):       Pump Inlet@         Flow       Flow         rate       0         gallons)	Date Calibrated N/A Casing Water Water
YSI 556 Multi Parameter Meter       05C1520 AA         HACH DR 890 Colorimeter       IELD PARAMETERS         Ambient Air Temperature (°F):	C casing P Water
HACH DR 890 Colorimeter         IELD PARAMETERS         unbient Air Temperature (°F):	C casing P Water
IELD PARAMETERS         Ambient Air Temperature (°F):	C casing P Water
Ambient Air Temperature (°F):	P Water
Flow meter       Flow rate       Depth to       Time to       Volume Purged (Gallons)       Temp (°C)       Sp.Cond ( $\mu$ S/cm)       DO ( $mg/L$ )       pH       OI (mg/L)         (gallons)       _/min       water	P Water
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	
D.O. mg/l Chemetrix (Visual) Hach Kiltered Hach Kiltered Hach Kiltered Hach Kiltered Hach Kiltered Fe2+ mg/l Hach Kiltered Fe2+ mg/l Hach Kiltered Fe2+ mg/l Hach Kiltered Fe2+ mg/l Hach Kiltered Fe2+ mg/l Hach Kiltered Hach Kiltered Fe2+ mg/l Hach Kiltered Hach Kiltered Kiltered Hach Kiltered	
D.O. mg/l Chemetrix (Visual) Hach Kiltered Hach Kiltered Hach Kiltered Hach Kiltered Hach Kiltered Fe2+ mg/l Hach Kiltered Fe2+ mg/l Hach Kiltered Fe2+ mg/l Hach Kiltered Fe2+ mg/l Hach Kiltered Fe2+ mg/l Hach Kiltered Hach Kiltered Fe2+ mg/l Hach Kiltered Hach Kiltered Kiltered Hach Kiltered	
D.O. mg/l Chemetrix (Visual) Hach Hach Non Filtered Fe2+ mg/l Hach Hach Hach Hach Hach Hach Hach Hach	
D.O. mg/l Chemetrix (Visual) Hach Hach Filtered Hach Hach Hach Hach Hach Hach Hach Hach	
D.O. mg/l Chemetrix (Visual) Hach Hach Filtered Hach Hach Hach Hach Hach Hach Hach Hach	
D.O. mg/l Chemetrix (Visual) Hach	1 contraction of the second se
D.O. mg/l Chemetrix (Visual) Hach	
D.O. mg/l Chemetrix (Visual) Hach Hach Filtered Hach Hach Hach Hach Hach Hach Hach Hach	
D.O. mg/l Chemetrix (Visual) Hach Hach Filtered Hach Hach Hach Hach Hach Hach Hach Hach	
D.O. mg/l Chemetrix (Visual) Hach Hach Filtered Hach Hach Hach Hach Hach Hach Hach Hach	
Chemetrix (Visual)     Alk mg/l Hach     Filtered Alk mg/l Hach     Fe2+ mg/l Hach     Fe2+ mg/l Chemetrix (Visual)     Fe2+ mg/l Hach     Manganese mg/l Hach     Manganese mg/l (Visual)	nv
PURGE INFORMATION Stickup => Steel Casing = 3' Abo TOP of AVC Lasing = 0.1 to	ese Comments
arting Flow meter Reading: Ending Flow meter Reading: Flow	ve Ground Surp of below Steel Cast Rate: "Top of PVCC astru
tal Volume Purged: Purged Dry (Y/N): Micro purged (Y/N): I	1 10
sing Inner Diameter (inches) 2 Initial Depth to Water (feet) 1714 Depth to bing inner diameter (in) Tubing & Pump Volume (ml)	o bottom of well (feet).37
ntroller settings: Pressure(psi) Discharge (sec.) Recharge(sec.) using Volume Calculation (gallons): 2" well = 0.17 x WCT 4" well = 0.66 x WCT 6" well = 1.47 x WCT Where	
Two Inch wen Not Fluch Mounted	WCT = Water Column Thickness (feet)

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	E	STLP	-			JRGE AN				
Project N	Name:	Rat		Indust	vial C	lient.	ZN-1 c	COC NI	umber:	
Sample (	Collected	by: T	HU)	WZN	)		V D	Vell ID	Collection	-60 :6-12-16
FOLIPM	IENT		/	- 453 -			D	ale of	concetion	10
Purging	Equinmen	t. H	MA-	-43-	-5					
Sampling	g Equipme	ent:	2.011	192						
	Equipmen									······································
-	ent Decont		on:	Per W	ork Plan -	- Alconox V	Vash with	Triple	Rinse and	sopropyl Alcohol Rinse
						ent Calibra		mpie	Temse und I	
	Eq	uipment/	Model			Serial	Number			Date Calibrated
	YSI 556	Multi Para	meter M	eter		- 05C1	520 AA			10-17-110
	НАСН	DR 890 C	olorimet	er						6-12-16 N/A
Ambient A	RAMETER for Temperation Depth (ft):	ture (°F):_				Weather C			er PVC casi	
Flow meter (gallons)	Flow rate	Depth to	Time	Volume Purged	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comments
(ganons)	/min	water	Para	(Gallons)	ta C	David	Sin	- 1	-	
	15	25	Tool	in 1	Vath	Juni	2000			
	17:49	Cali	grai	n 1	7	ero -	- 10	1.74	16	
						SE-	3 -	112	8,4	
	17049	Rus	17	MTSU	Mw.	81 De	Up	Run Run	1 Cali	16-12-16 1616-12-16
		¥	Sono	e No	ht. C	Q the	Way	r to	TD	Down /inp
										Speed fe
										28,3 min
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach		e Mang m Chen	ered ganese g/l netrix sual)	Non Filtered Manganese mg/l Hach	Comments
PURGE	INFORM	ATION	Flush	h Monit	T=> TO	2-	.45	Ft	BG	
Starting Flo	ow meter	Reading		Endin	ng Flow r	neter Read	ing:		Flow Rate	:
Total Volu	me Purge	d:	Pur	ged Dry (	Y/N):	Micro	ourged (	Y/N):	Minin	mal purged (Y/N):
l ubing inn	er diamete	er	(1n) 1	ubing & F	ump vo	Water (fee lume Recharge	(ml)			ttom of well (feet)
Casing Volume	e Calculation (	allone): 2"		-		CT 6" well = 1				= Water Column Thickness (feet)
Set .	Bour		9	7.00 L.287	•					-
DITI	WALA denial Factor	Field/Convert	Durante	Section From 1	p	Page 1 of				

Project Name:

Industrial Client Il-COC Number:

Sample Collected by:

Well ID:  $\underline{MW} = 6.5$ Date of Collection:  $\underline{6} = 12 - 10$ 

EQUIPMENT

Purging Equipment:

Sampling Equipment:

Filtering Equipment:

Equipment Decontamination:\_

GIMA 453-5

Per Work Plan - Alconox Wash with Triple Rinse and Isopropyl Alcohol Rinse

E	quipment Calibration	
Equipment/Model	Serial Number	Date Calibrated
YSI 556 Multi Parameter Meter	0 <del>5C</del> 1520 AA	672-16
HACH DR-890 Colorimeter		N/A

#### FIELD PARAMETERS

Ambient Air Temperature (°F):\_\_\_\_\_ Sampling Depth (ft):\_\_\_Pump Inlet@ Weather Conditions:\_\_\_\_\_ Reference Point:\_\_\_\_Top of inner PVC casing

Flow meter	Flow rate	Depth to	Time	Volume Purged	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comments
(gallons)	/min	water	1	(Gallons)			~	1		
			18:1	4 FCV	o ta	01 20	610	und	Sul	ad a second s
						1	-		- pr	
	P	1 1						0		
	Min	1 Por	in	MISU	nu	UBSDO	with	Kim	1 Ca	161 - 6-12-1
	Kar	1	AP	MTG	1 M	WBS	up	Run	1 6	all 6-12-
	1.000	~ (							tr A	(A)
								-	& UP	Spill fr
							NDA	M		A Siland
							100			10 09.000
									0	
					1	10	10	$\bigcirc$	DIT	A Hdy
				Cool k	Dail	$  \rangle$	K	0	Dan	n of non
				001	ear			-		/
					_					
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	

D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach	Filtered Manganese mg/l Hach	Filtered Manganese mg/l Chemetrix (Visual)	Non Filtered Manganese mg/l Hach	Comments
									1.1

PURGE INFORMATION	Tush Man	TOC=.57	Ft BGS
Starting Flow meter Reading:	Ending Flow me	ter Reading: Flo	ow Rate:
Total Volume Purged: H			Minimal purged (Y/N):
Casing Inner Diameter (inches) Tubing inner diameter(in Controller settings: Pressure()	1) Tubing & Pump Volur	me (ml)	th to bottom of well (feet) 17,22
Casing Volume Calculation (gallons): 2" well = (	0.17 x WCT 4" well = 0.66 x WCT	6" well = 1.47 x WCT	Where WCT = Water Column Thickness (feet)

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	E	STCP	GRO	UNDWA	TER PU	RGE AN	D SAMI	PLING	FORM		
Project N	ame:			Torhus	Wicel	Client	iv.k	OC Nu	mber:		
Sample C			a)	WZ	$\wedge$		V	Vell ID:	Mu		
		by:	MV.				U	ate of C	Collection	- In 1	1
EQUIPM Purging F	<u>ENT</u> Equipmen	+ ()	MA	~ 45	3-5				L	6-12-1	Y
Sampling	Equipment	ent								~	
Filtering											
Equipmen			on:	Per Wo	ork Plan –	Alconox V	ash with	Triple I	Rinse and I	sopropyl Alcohol Rinse	
					Equipm	ent Calibra	tion				
		uipment/					Number			Date Calibrated	
		Multi Para				05C1	520 AA				
	НАСН	DR 890 C	colorimete	er						N/A	
FIELD PAI											
Ambient Ai Sampling D						Weather Co			er PVC casi	ng	
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pH	ORP	Water	٦
meter	rate	to	Thire	Purged	(°C)	(µS/cm)	(mg/L)	pii	(mV)	Description/Comments	
(gallons)	/min	water	12	(Gallons)	Test	te	60				-
		18	1.78	Ferd	1001	-W	Din	n s	enford		-
	. 10	1		, shere	/			2	1 1	1917 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
Down	- <u>"</u> Ku	n	M	TSV,	un-	6 p	own	Ru	1 4	1191 6-12-7	4
110	Ru	m)	M	TOD	MI	-10	10	Run	1 14	tit 1 6-17-1	
Cip		.,									7
								Dal		1	-
							39	- A	Þ	Marzn / MA	
				1	tou	<del>110 (4</del>	25	171	A	Chaid -	-
		( ~	mal	- 50	1.4		BO	55		altel.	
			00							you Imin	
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv		
D.O. mg/l Chemetrix	Filtered Alk mg/l Hach	Non Filtered Alk mg/l	Filtered Fe2+ mg/l	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach	Filtered Manganes mg/l	e Mang m		Non Filtered Manganese mg/l	Comments	
(Visual)		Hach	Hach	(visual)		Hach		sual)	Hach		
PURGE I	NFORM	ATION	St	Flush	Ma	m	TOC =	0.5	ft B	TECHES	
Starting Flo										-	
										mal purged (Y/N):	
Casing Inne	er Diamet	er (inch	(29	Initial	Depth to	Water (fee	t) 17.4	* 4 D	enth to bo	ttom of well (feet)	33
I ubing nun	el ulamet	ei	(111) 1	uoning oc r	ump vo	luine	(mn)				
Controller s	settings: l	Pressure	(psi)	) Discharg	e (sec.) l	Recharge_		(sec	c.)		
Casing Volume	Calculation (	gallons): 2"	well = 0.17	XWGT 4" we	$ll = 0.66 \times W_{0}$	CT 6" well = 1	47 x WCT		Where WCT	= Water Column Thickness (feet)	
	nn	31		to							
	281	2K	-	40						AVE	
		2		$\mathcal{M}$							
DUTIN	VA\Admin\Eo	E alert	tar Durne and G	Campling Form day	р	age 1 of				& ASBOCIATES	

THWA\Admin\Forms -	Field	Groundwater	Purge	and	Sampling	Form	do

Sample	Collected	by: Th	m/u	VZD			V D	Vell ID	Collecti	и-6мр) on: 6-12-16
						· · · · · · · · · · · · · · · · · · ·				
Purging	<u>MENT</u> Equipmer	nt:	MA	- 453	~ 5					
Samplin	g Equipm	ent:								
	g Equipme			D W	1 11			<b>T</b> : 1	D.:	
Equipm	ent Decon	laminatio	on:	Per We		Alconox W		Triple	Rinse an	d Isopropyl Alcohol Rinse
	Eq	uipment/I	Model		Equipino		Number			Date Calibrated
		Multi Para		eter			520 AA	_		(0=0-1/0
	НАСН	DR 890 C	olorimet	er						N/A
FIELD P	ARAMETER	25								
Ambient	Air Tempera	ture (°F):_				Weather Co	onditions:			
Sampling	Depth (ft):	Pump In	nlet@			Reference I	Point: To	op of ini	ner PVC c	asing
Flow meter	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pН	ORP	
(gallons)	rate _/min	to water		Purged (Gallons)	(°C)	(µS/cm)	(mg/L)		(mV)	Description/Commen
			15:98		Fen 1	Tra	raid	Surp	ect	
			15:49	Start	Kint	Down	2			
		2								
Pa	pn	Rui		M	M	W-CM	n Da	on i	Run 1	Alib1 6-12-16
		p UV		MT	pu n	14-61	*D 6	P	unt	Galer 0-12
			1	<u>a</u> 1	$\hat{\boldsymbol{D}}$					1.4
		Q	56	21.1						Down/up
		1000			+					Sper II
										(int)
	≥40 ≤200			-	±10%	±10%	±10%	±0.2	±10mv	
	Filtered	Non	Filtered	Filtered	Non Filtered	Filtered	Filt	ered	Non Filtere	d
D.O. mg/	Alk mg/l	Filtered Alk mg/l	Fe2+ mg/l	Fe2+ mg/l Chemetrix (Visual)	Fe2+ mg/l Hach	Manganes mg/l	m	anese g/l netrix	Manganese mg/l	Comments
Chemetrix	Hach		Hach	(visual)	1	Hach		ual)	Hach	
0		Hach			+	Ilden				
Chemetriz (Visual)	Hach								7	
Chemetriz (Visual)	Hach			in Mo	nt		= ,5	71	ft 1	365
Chemetrin (Visual) PURGE	Hach	ATION	Flus			TOC				
Chemetrix (Visual) PURGE arting F	Hach INFORM	ATION Reading	Flus	Endin	ng Flow m	TOC neter Read	ing:		Flow Ra	ate:
Chemetrix (Visual) PURGE arting F	Hach INFORM	ATION Reading	Flus	Endin	ng Flow m	TOC neter Read	ing:		Flow Ra	ate:
Chemetriz (Visual) PURGE arting F otal Volu asing Ini Jbing ini	Hach INFORM low meter ume Purge ner Diamet ner diamet	ATION Reading d: ter (inche	<i>Flus</i> Pur es)(in) T	Endin ged Dry (` Initial I `ubing & F	ng Flow m Y/N): Depth to Y Pump Vol	TDC neter Read Micro p Water (fee hume	ing: purged ( t)(ml)	Y/N): 7 Z	Flow Ra Mi Depth to 1	
Chemetriz (Visual) PURGE arting F otal Volu asing Ini ubing im- ontroller	Hach INFORM low meter ume Purge her Diamet her diamet	ATION Reading d: ter (inche er Pressure_	Flus 	Endin ged Dry (` Initial l `ubing & F ) Discharg	ng Flow m Y/N): Depth to V Pump Vol ge <u>(</u> sec.) F	TOC neter Read Micro p Water (fee uume Recharge	ing: ourged ( t)_ <u>12,4</u> (ml)	Y/N): 17 D	Flow Ra Mi Depth to 1 ec.)	ate: nimal purged (Y/N):
Chemetriz (Visual) PURGE arting F otal Volu asing Ini ubing im- ontroller	Hach INFORM low meter ume Purge ner Diamet ner diamet	ATION Reading d: ter (inche er Pressure_	Flus 	Endin ged Dry (` Initial l `ubing & F ) Discharg	ng Flow m Y/N): Depth to V Pump Vol ge <u>(</u> sec.) F	TOC neter Read Micro p Water (fee uume Recharge	ing: ourged ( t)_ <u>12,4</u> (ml)	Y/N): 17 D	Flow Ra Mi Depth to 1 ec.)	ate:
Chemetriz (Visual) PURGE arting F otal Volu asing Ini ubing im- ontroller	Hach INFORM low meter ume Purge her Diamet her diamet	ATION Reading d: ter (inche er Pressure_	Flus 	Endin ged Dry (` Initial l `ubing & F ) Discharg	ng Flow m Y/N): Depth to V Pump Vol ge <u>(</u> sec.) F	TOC neter Read Micro p Water (fee uume Recharge	ing: ourged ( t)_ <u>12,4</u> (ml)	Y/N): 17 D	Flow Ra Mi Depth to 1 ec.)	ate: nimal purged (Y/N):

5

t

	E	STOP	GRO	UNDWA	TER PU	RGE AN	D SAMI	PLING	FORM	
Project N	Vame:			Indust	vial	Clicut,	TN-10	OC Ni	umber:	
Sample (	Collected						V	Vell ID	Collection	MD-12-16
FOLIDA	ENT									
Purging ]	Equipmen	it: H	nA 4	53-5						
Sampling	gEquipme	ent:								
0	Equipme						_			
Equipme	nt Decont	taminatio	on:	Per W				Triple	Rinse and	Isopropyl Alcohol Rinse
					Equipm	ent Calibra				
		uipment/					Number			Date Calibrated
	YSI 556					05C1	520 AA	-		6-12-16
	HACH	DR 890 (	olorimete	er						N/A
	RAMETER									
	ir Tempera Depth (ft):					Weather Co Reference			ner PVC cas	ing
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pH	ORP	Water
meter	rate	to		Purged	(°C)	(µS/cm)	(mg/L)	-	(mV)	Description/Comments
(gallons)	/min	water	-6	(Gallons)	Tool				+	
		1	9:58	Tal	plin	Water	to	to	xilibre	ti
			5415		1:1	- 1	7	2	~ 1	127
		10	1215	- Ca	liber	um /	E	FE	-3 2	1124.56
							_	SE		
Pou	m	Run	1	MIS	V M	WSM	DO	win	Runt	Calip/ 6-12-1
- Up		Run	-	MT	pv 1	1W-87	4 <u>0</u>	UP	Man (	Calibl E-12-16
			7							
			/							Speed = 9thingin
										1000 100
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l	Filtered	Non	Filtered	Filtered	Non Filtered	Filtered	Filt	ered	Non Filtered	T
Chemetrix	Alk mg/l Hach	Filtered Alk mg/l	Fe2+ mg/l	Fe2+ mg/l Chemetrix	Fe2+ mg/l Hach	Manganes mg/l	m	ganese g/l	Manganese mg/l	Comments
(Visual)	Tiach	Hach	Hach	(Visual)		Hach		netrix sual)	Hach	
PURGE	INFORM	ATION	CIUL	Morus	TOC -	0,41	365			
									Flow Rat	e:
_		-								
lotal Volu	me Purge	d:	Pur	ged Dry (	Y/N):	IVIIcro	purgea (	1/N):	Mini	mal purged (Y/N):
Casing Inn	er Diamer	ter (inch	es)	Initial	Depth to	Water (fee	$(m^{1})$	B_D	bepth to be	ottom of well (feet)
Controller	settings:	er Pressure	(1n) (nsi	) Discharg	pe (sec.)	Recharge	(IIII)	(se	ec.)	
	0					CT 6" well = 1.				r = Water Column Thickness (feet)
					5.00 A M					
		0.0	33							
		1	2,9							***
			1		_					WIEDEMEIER

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	2	STOP				RGE AN				
Project N	lame:		A.F.	Inclu	strial	Clieut	Juk	OC Nu	mber:	n: 6-12-16
Sample (	Collected	by:	FIL	121	NZ	n	V	Vell ID:		10-95 MW-95
EQUIPM		oy	00-		10	<u>~</u>	L	ale of v	Conection	1.0-12-10
Purging I	Equipmen	t: HA	(A )	453-	-5					
Sampling	g Equipme	ent:								
Filtering	Equipme	nt:								
Equipme	nt Decont	aminatio	on:	Per We		the second se		Triple	Rinse and	Isopropyl Alcohol Rinse
	E		I		Equipm	ent Calibra				D ( C III ) I
	-	uipment/I Multi Para		atan			Number			Date Calibrated
		DR 890 C				0501	520 AA			N/A
			olorimen							IN/A
FIELD PA	RAMETER ir Tempera					Weather	anditionau			
Sampling I						Weather C Reference			er PVC cas	sing
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pH	ORP	Water
meter	rate	to		Purged	(°C)	(µS/cm)	(mg/L)	P	(mV)	Description/Comments
(gallons)	/min	water	42-	(Gallons)	Tral	ter	round	10	tack	
				200	1001	14-5	paule	24	Tan	
Rou	n	10	/	10-	101	1. 1 6	CA		IP 1	15h C (2)-24
Jun In	100	Ran	1	M	SV.	anu-8	2500	on	Rm 1	200 1 6-17-TU
		RAV			pv_	10 cm	1	-	ran	
								-		
							6			110/ Omina
				711	Dall	$ \rightarrow $	0, 1	h	1	Shul
				1001	Ferr		The	and		aft/
					-		0			ng imon
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtere Fe2+ mg/l Hach		se Man T Che	ered ganese ng/l metrix sual)	Non Filtered Manganese mg/l Hach	Comments
L				1		11-1	DE	S		
PURGE	INFORM	ATION	Mus	n 10	002	1451	RO			te:
Starting Flo	ow meter	Reading		Endir	ng Flow 1	neter Read	ling:		Flow Rat	te:
Fotal Volu	me Purge	d:	Pur	ged Dry (	Y/N):	Micro	purged (	Y/N):_	Min	imal purged (Y/N):
Casing Inn Fubing inn	er Diame er diamet	ter (inche	es)(in) ]	L Initial	Depth to Pump Vo	Water (fee lume Recharge_	et)_ <b>[3,4</b> (ml)	1 <u>7</u> D	epth to b	ottom of well (feet) <u>191</u> 34
	-					'CT 6'' well = 1				T = Water Column Thickness (feet)
casing volum	Calculation (	Banons): 2	· 5	12. 4	– 0.00 X W	CI V Well-1	ATTA HUI		in nore fre	
			19.8	RY			2			
				28						***
			500	34						WIEDEMEIER
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	É	STLA	GRO	UNDWA	TER PL	RGE AN	D SAMI	PLING	FORM	
Project N	ame:	14		Indust	vial .	client	IN-K	OC Ni	umber:	
Sample C	Collected		1				V	Vell ID	Collection	1-8 : 6-12-16
FOLIDM	ENT						D		concetion	
Purging I	Equipmen	it: H	MAI	153-4	Ŝ					
Sampling	Equipme	ent:								
Filtering										
Equipmen	nt Decont	aminatio	on:	Per Wo		Alconox V ent Calibra		Triple	Rinse and	Isopropyl Alcohol Rinse
	Ea	uipment/I	Model		Equipm		Number			Date Calibrated
		Multi Para		eter			520 AA			6-12-110
	HACH	DR 890 C	olorimet	er						N/A
FIELD PA										
Ambient A Sampling D		· · · -				Weather Co Reference			ner PVC cas	ing
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pН	ORP	Water
meter (gallons)	rate /min	to water		Purged (Gallons)	(°C)	(µS/cm)	(mg/L)		(mV)	Description/Comments
		20:	51 :	Zaro	Tal	to 6	Tomp	Su	infarr	
Down		Runt	7	ATTSI	2	MW-8	Da.	110	Runl	Calib 1 (0-12-46
up		Runt	-)	MISI		mw-4	Up		Runt	Calib1 6-12-4
						0				
					A	E Co	K			
				$\left \right $	61-	X	m		11-	
				A		R	$\partial$	5.	43	
						Ē	/ '			
								-		
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtere Fe2+ mg/l Hach		e Mang m Cher	ered ganese g/l netrix sual)	Non Filtered Manganese mg/l Hach	Comments
PURGE I	NFORM	ATION	Ausi	4 7	TOC =	-0.3'	BES			e:
Starting Flo	ow meter	Reading	Nov	Endir	ng Flow r	neter Read	ing:	·	Flow Rate	e:
										mal purged (Y/N):
Casing Inne	er Diamet	ter (inche	(in)	Initial	Depth to	Water (fee	(ml)	2 <u>9</u> D	Depth to be	ottom of well (feet) 426
Controller	settings: I	Pressure	(psi	) Discharg	ge (sec.)	Recharge_	(1111)	(se	ec.)	
Casing Volume	e Calculation (	gallons): 2"	well = 0.17	x WCT 4" we	ell = 0.66 x W	CT 6" well = $1$	47 x WCT		Where WC1	T = Water Column Thickness (feet)
Ć	Ð	49	54	2						***
DITT	VA) A desire Ear	FO	.26	) Samelina Er J	F	Page 1 of				

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## DAILY FIELD ACTIVITY REPORT

	Client Name: Project Name: <u>ESTCP 2015 84 Tooele</u> Date: <u>7-25-16</u> Contractor: Weather: <u>81°F</u> Clear Meather: <u>81°F</u> Clear	
	Time Breakdown:   Drive:   Work:   Standby:	
	Location and Description of Activities: Let 25 pulled <del>Activities</del> D20 pulled <del>Activities</del>	10 leve
	Equipment Used on Project:	
	Activity Summary and General Remarks: Slightly turked water	
	Liter Semples 2. Approsleeve 2.2 Eisthoret headspore 3 2	10:4 <b>0</b> 10:55
100 mL 100 mL 100 m	Climson Toolele D-20 TV AI #1 Hydrosleevel TV AI #2 Hydrosleeve 2+3 I liter Bottle From Hydrosleeve 2+3	10:42 11:00 0:43
	Microbial Insights Toolle D-20 Hours 2414ers 11:20RNA HOUL Hydrostavez (1:44 270mL ( 2414ers DNA 500 + 500mL Hydrostavez 10:44	
	Technician Signature: Date:	
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# **GROUNDWATER PURGE AND SAMPLING FORM**

Samplin	Collected <u>AENT</u> Equipmer g Equipmer Equipme	nt: <u>//</u>			Peris	taltiz		ate of C		-0 1: <u>7<del>1</del>25/16</u>
Equipme	ent Decon	taminatio	on:	Per Wo	ork Plan –	Alconox V	Vash with	Triple I	Rinse and	Isopropyl Alcohol Rinse
		•			Equipm	ent Calibra				
		uipment/ Multi Para		ton			Number 520 AA			Date Calibrated
		DR 890 C				0301	520 AA			N/A
Ambient A	ARAMETER Air Tempera Depth (ft):	<u>RS</u> .ture (°F):_		-		Weather C Reference			er PVC cas	
Flow meter (gallons)	Flow rate _/min	Depth to water	Time	Volume Purged	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP (mV)	Water Description/Comments
		11:03		Liters		1411	774	7.16	1835	clean
		11.00		A		1,146	7.21	1.10	18-25	Ceal
			12:05	Kigd	17.0	1430	7.87	7.41	161	12-15
			12:07		16.52	1417	7.60	7.04	179	
	≥40 ≤200				±10%	±10%	±10%	±0.2		
	240 5200	l			±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach	Filtered Manganes mg/l Hach	m Chen		Non Filtered Manganese mg/l Hach	Comments
			ļ						la the s	A 12 16.
	<u>INFORM</u>		•	Endin	g Flow n	een <u>–</u> neter Read	68،5 ing:	۲۲ ا ا	Flow Rate	Bue of Saver 88, e:
	ow meter	Reading					1.0		Mini	
tarting Fl otal Volu asing Inn ubing inn	me Purge	d: ter (inche er_	Purg es)_41 (in) T	Initial I ubing & P	Depth to V Pump Vol	Water (fee ume	t) <u>67.0</u> (ml)	<u>68</u> De	epth to bo	mal purged (Y/N):

Page \_\_\_\_ of \_\_\_\_

## DAILY FIELD ACTIVITY REPORT

	Client Name:	Project Number:	
	Project Name: ESTCP201584 Tooele	Date: $\frac{1}{-25-16}$	
	Contractor: Weather: <u>-&amp;/</u> Cleave	Arrival Time: <u>ターイ</u> 「 エレジア	<u></u>
·	960	•	
	Time Breakdown: Drive: Work:	Standby:	-
	Location and Description of Activities:		
	Well 2000 pulled wel	l Logger	
	Debblos in weller		
	Equipment Used on Project:		
	Depth to water 6 7.38 -	TOC to water	
			<u> </u>
	Activity Summary and General Remarks:		
	· · · · ·		
2:26	PNNL Topele D23 Samplel		(+5/
			HS2
	3		HSZ HS3
	<del>4</del>		
2:2	Clemson Toole D23 JX A2 1		H5/
	<u> </u>		HS2 HS3
	Extra water 160mi Seriem bret	tle	HS3
	2:35 DNA LOOOML Hadro	cleant	
•	2:00 RNA 150 ML Hydro		
	Technician Signature:	Date:	
		٨L	L
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		_				RGE AN		PLINO	G FORM	
Project N	ame:	Twel	e A	Irmy	Supor 1	~	С	OC N	umber:	
- <b>J</b>		Γ	- 11	1.1500			W			3 7/25/16
Sample C	collected	by:/	H	Wiea	lineill		D	ate of	Collection	: 7/25/16
									0	•
Purging E	Equipmen	.t:	100	Sleve	4 H	er#sta	iltic	/	ump	
Sampling	Equipme	ent:	-						/	
Filtering Equipment				Den W/	aule Dian			Tuinle	D:	I
	It Decom	ammatic	<u></u>	Perwo		ent Calibra		Triple	Rinse and	Isopropyl Alcohol Rinse
	Eq	uipment/l	Model				Number			Date Calibrated
	YSI 556	 Multi Para	meter Me	eter		05C1	520 AA			
	HACH	DR 890 C	olorimete	er						N/A
FIELD PAI	RAMETER	S								
Ambient A	ir Tempera	ture (°F):	96	2		Weather C	onditions:	Hor	BIEZ	y & Clear
Sampling D	epth (ft):	Pump I	nlet@ -	200 ft	<u>BT</u> AC	Reference	Point: <u>T</u>	op of in	ner PVC cas	ing
Flow meter	Flow rate	Depth to	Time	Volume Purged	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	рН	ORP	Water
(gallons)	/min	water		(Gallons)		(µs/em)	(mg/L)		(mV)	Description/Comments
						18,770	2122	7.11	233	
						19,240	1.88	7.05	21	
	····· ·									
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
						I	L			
D.O. mg/l Chemetrix	Filtered Alk mg/l	Non Filtered	Filtered Fe2+	Filtered Fe2+ mg/l	Non Filtered Fe2+ mg/l	Manganes	se Mang	ered ganese	Non Filtered Manganese	
(Visual)	Hach	Alk mg/l Hach	mg/l Hach	Chemetrix (Visual)	Hach	mg/l Hach	Cher	g/l netrix sual)	mg/l Hach	Comments
			NF							
			0.0	<u> </u>						
<u>PURGE I</u>										
										e:
Total Volur	ne Purge	d:	Purg	ged Dry (	Y/N):	Micro	purged (	Y/N):_	Mini	mal purged (Y/N):
Casing Inne	er Diamet	er (inche	es)	Initial I	Depth to	Water (fee	et)	I	Depth to be	ottom of well (feet)
l'ubing inne	er diamet	er	(in) T	ubing & F	Pump Vo	lume	(ml)	1.		
Controller s										
Casing Volume	Calculation (	ganons): 27	wen = 0.1/:	x wui 4" we	u = 0.00 x W	$CI \circ Well = 1$	.47 x wCT		where WCI	Γ = Water Column Thickness (feet)



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INVOICE TO: (For Invoices patcing a third party it is imperative that all information be provided)	Sausartar Curr POBOX, 1206	March C - 74831	ichar @ Saradar Lawer, Com email:		er: Purchase Order No.	Subcontract No.		e: * *	act us with any questions about the analyses or filling out the COC at (865) 573-8188 (9:00 am to 5:00 pm EST, M-F). After hours en	Sample Information         Analyses         CENSUS: Please select the target organism/gene	d d d d d d d d d d d d d d d d d d d	Sugara Sampler Sugara Sampler	Tople DDDNA 7-25-16 and 1 1 1 Web Dha Shart 12 1	Des 1212 1 25 16 90	7-25-16	10 10 31 3 2 MAY 7-26-16	Toolo D23 DNA7-45 10 02		lished by: Darcharcer With and Received by: Date 1-25-16	It is vital that chain of custody is filled out correctly & that all relative information is novvided
REPORT TO:	Name: Company: Address:		email: Phone:	Fax:	Project Manager:	Project Name:	Project No.:	Report Type: T	Please contact u:		*	Laboratory Use C							Kelinquished by:	

Failure to provide sufficient and/or correct information regarding reporting, invoicing & analyses requested information may result in delays for which MI will not be liable.

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Sample and the second second second

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Custody Record			Se	evern Trent La	Severn Trent Laboratories, Inc.		Arvada, CO 80002
STL-4124 (0901) Client		Project Manager	1 e Merce F		Date / / / //	Chain of Custody Number 310485	ov Number 0485
a Comunda F		Area	Number		Lab Number No. 10 Log. (	t Page	of
State	Zip Code Site	Site Contact	Lab Contact			1 ·	
e and Location (State)		Carrier/Waybill Number					
Contract/Purchase Order/Quote No.	(ft@/)	Matrix	Containers & Preservatives			Cond	Special Instructions/ Conditions of Receipt
Sample I.D. No. and Description (Containers for each sample may be combined on one line)	Date Time	IIOS PAS snoanby JIV	sendruc ()2ACI 2ACI 2ACI 2ACI 2ACI 2ACI 2ACI 2ACI		<b>5</b>		
	1-35 16 121-	·			1 (1) X		
ch h-zo řah	2						
TEAFLE D-20 KNH	1-21 1611.20	μ μ					
(C D-20 LNA	1-21 16 11.4	ų   1					
nsomtwelle D-23 KNH	1-28-16 B :COM						
DOOLTASELE D. 23 D.N.H.	I RY IL Store	7					
	W. S. W.					τ.	
	~						
dentification					-	A fee may be assessed if samples are retained	are retained
Turn Around Time Required			OC Requirements (Specify)	Decify)		(111)011	
			1. Received By			Date	Time
2. Relinquished By	Date		Y 2. Received By			Date	Time
3. Relinquished By	Date	e Time	3. Received By			Date	Time
Comments						_	
DISTRIBUTION: WHITE - Returned to Client with Report: CANARY - Stays with the Sample: PINK - Field Copy	CANARY - Stays with the S	ample; PINK - Field Cop					
							733

Chain of								SE' TR	S E V E R N T R E N T		ST		-		STL Denver 4955 Yarrow Street	v Street
Custody Record								Seve	Severn Trent Laboratories, Inc.	ent L	abor	atori	es, li	лс.	Arvada, CO 80002	80002
	ļ	Project Manage	nager							ett :	Date	1		110	Chain of Cust	Chain of Custody Number
ED ICK ICALO MIKUTANEIC	-	l ( ) (	Mimbe	Telephone Number (Area Code) (Eav Number	1 + - 1 + - 1 + - + 1 + + + + + + + + +	Number	-			, I	ta l	Mumbe			<b>)</b>	70+01
209 CORCHARD Dr	<u> </u>		3		5 C	1		199		c As		ê le n		$\sim 0$	Page /	of /
State Zip Code	N.	Site Contact			Lab C	Lab Contact	j. Li	ab Contact	ر 1 م	י ד גי	Vnalysis ore spi	Analysis (Attach list if more space is needed)	h list if eeded)			
and Location (State)		Carrier/Waybill Number	vbill Nu	nber	4	ر د				1 30					<u> </u>	/occitor retrict
			Má	Matrix	ļ	Cont	Containers & Preservatives	& es		Lim						Conditions of Receipt
Sample I.D. No. and Description Date (Containers for each sample may be combined on one line)	e Time	م Air	snoənb∀	ioS.	∩ubres.	EONH #OSTH	HO®N IOH	\oans HO <sub>E</sub> N								
Travele has IN AIHI 11-51	16		7							7					-	
L SAL HAS			<i>t.</i>							7						
1. 841 AVI 02-1			3.							2						
1 - Transfer to the second state of the	angelage - 1 Philippe		7							7						
Toole D-23 MH2#1 4-51	16		ć							Ż						
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Possible Hazard Identification			Sample	Sample Disposal		Disposal By Lab	sal Bv I		Archive For	For	2	Months	(A fee n tonger t	nay be a han 1 m	(A fee may be assessed if samples are retained longer than 1 month)	ss are retained
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dBy (Alice (1) (1)		Date	2	Time []:5(		1. Received By	ved By								Date	Time
2. Relinquished By		Date		Time		2. Received By	ved By								Date	Time
3. Relinquished By		Date		Time		3. Received By	ved By				2		-		Date	Time
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DISTRIBUTION: WHITE - Returned to Client with Report, CANARY - Stays with the Sample: PINK - Field Copy

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Possible Hazard Identification	Sample Disposal	Disposal Bv Lab	Archive For	(A fee may be a Months longer than 1 m	(A fee may be assessed if samples are retained longer than 1 month)	retained
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18y UN USA	1-16 5:300	1. Received By A			Date	Time
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DISTRIBUTION: WHITE - Returned to Client with Report: CANARY - Stays with the Sample; PINK - Field Copy

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MAGNETIC SUSCEPTIBILITY MEASURE	MENT FORM SONDE
MAGNETIC SUSCEPTIBILITY MEASURE	LIMENT FORM - SOMDE
PROJECT NAME: JOOCLE HIMY NEDOT	_
Well ID: 0-20	7/2/16
Sample Collected by: THWIEdemeill	_Date of Collection:
SAMPLING EQUIPMENT HMA - 935 -5	

]	Equipment Calibration	
Equipment/Model	Serial Number	Date Calibrated
HNA-453-5	555-4	7/25/16

EQUIPMENT DECONTAMINATION: <u>Alconox Wash, Double Rinse, and Isopropyl Alcohol Spray</u>

CALIBRATION RESULTS
Ambient Air Temperature $(^{O}F)^{a'}$ : <u>7</u> Weather Conditions: <u><i>Olew</i></u>
Groundwater Temperature $(^{O}F)^{a'}$ :
Time Probe Inserted into Ambient Groundwater (Minimum = 20 Minutes):
Calibration Standards (Include Units): Low: <u>High 5E-354</u> UnitES
Time of Calibration: The 13:20
Time of Calibration:       The IS: W         Calibration Results (Include Units):       Low:       230       High       1326.4
Casing Inner Diameter (inches) 4 <sup>4</sup> Borehole Diameter (Inches)
Initial Depth to Water (feet) $69.68716$ Depth to bottom of well (feet) $-90^{\circ}BTOC$
Screened Interval, If Known (Include Datum) <u>68-88</u> Ft bqp
Depth Measured by Sonde <u>6917 ft bg</u> (Include Units)
Reference Point: Top of inner PVC casing or BGS Specify:

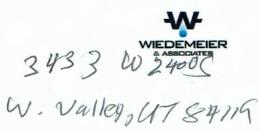
Run Number	Calibration Number	Up Versus Down	Winch Speed (specify Units)	Comments
0		Mur	9 Et/mile	worked Great
1	1	ILA	9 ft/min	
		- /		

Notes:

a/ The greater the difference between the groundwater temperature and the ambient temperature at the surface where the sonde will be calibrated, the longer the sonde should be allowed to equilibrate because the sonde is very sensitive to temperature.

D:\THWA\Admin\Forms - Field\Magnetic Susceptibility Measurement Form.doc

Page 1 of 1



Zilt

PROJECT NAME: Typele Army Dupot	_
Well ID: $D-23$	11.116
Sample Collected by: TH Wiele Mciel	Date of Collection: 7/25/12
SAMPLING EQUIPMENT	

	<b>Equipment Calibration</b>	
Equipment/Model	Serial Number	Date Calibrated
1-1 MA -453-5	5554	7/25/10
EQUIPMENT DECONTAMINATION:	Alconox Wash, Double Rinse, and I	sopropyl Alcohol Spray
CALIBRATION RESULTS		
Ambient Air Temperature ( <sup>O</sup> F) <sup>a/</sup> : <u>98</u>	Weather Condit	ions: Clear, BREZY
Groundwater Temperature ( <sup>o</sup> F) <sup>a/</sup> :	7.	
Time Probe Inserted into Ambient Ground	water (Minimum = 20 Minutes):	16.20
Time Probe Inserted into Ambient Ground Calibration Standards (Include Units): Lo	ow: <u>G</u> High FE	-3 ST Units
Time of Calibration: $12 - 20$		
Calibration Results (Include Units): Low:	Z30 High	1326,4
Casing Inner Diameter (inches) 4 1/		
Initial Depth to Water (feet) 67.38	Depth to bottom of well (feet)	
Screened Interval, If Known (Include Datu		
Depth Measured by Sonde 212	fr by S (Include Units)	
Reference Point: Top of inner PVC cas	ing or BGS, Specify:	

Run Number	Calibration Number	Up Versus Down	Winch Speed (specify Units)	Comments
1	1	Down	9 ft/sec	
1	1	40	9 ft/Sec	
		1		

Notes:



# Page <u>1</u> of <u>1</u>

& ASSOCIATES

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#### DAILY FIELD ACTIVITY REPORT

Client Name: Project Number: _	
Project Name: ESTCP 201584 Toole Date: 1-26	
Contractor: Arrival Time: _	200
Weather: 78°F Clear	
Time Breakdown: Drive: Work: Standby:	
Location and Description of Activities: $D \gtrsim 5$	
Set Hydrosleere at 185	
Depth to water 87.42 pt ??	
Equipment Used on Project:	
Activity Summary and General Remarks:	
PNNL	
8:35 Tooele D25 Samplel 11	HSI
g'05 Toole Das Sample 2 11	HS2
9:05 Touche D25 Sample 3 11	++52 H 53
9:17 Toucle D25 Sumple 4 IL	H S3
2:40 Clemson	
Toole IKBI # 1 100mL	HS/
9:07 TRI # 2 100mL	
9100 JUBI # 3 100mL	jłsz
4: 11:50 Am 160mil extra collected	#
8.46 mearobeal Insights	HSI
8:50 RNA 900mL	Hel
0.30 KINT JOOWIE	p <:
* note added 8-2-16	
Technician Signature: Date:	
Date.	



		T					ND SAM	IPLING	FORM	
Project N	Name:	<u> 00el</u>	C H	rmy SHWJ	Depo	L		COC Ni	umber:	
Sample (	Collected	by T	TINK	RHIAL	THU	$\mathcal{N}$		Well ID	<u>_</u>	25 pn:_7-26-16
		. Uy	100/1	51100	1.00			Date of (	Collectio	on: <u>1-26-16</u>
EQUIPM Purging	<u>IEN I</u> Fauinme	nt:  -	Inda	deile.						
Sampling	g Equipme	nent:	. yo			<u> </u>				
Filtering	Equipme	ent:	···········	<u></u>						
Equipme				Per W	'ork Plan -	- Alconox V	Wash wit	h Triple	Rinse and	I Isopropyl Alcohol Rinse
					Equipm	ent Calibra	ation			
		quipment/					l Number	•		Date Calibrated
		Multi Para				05C	1520 AA			
L		I DR 890 (	olorimet	er				· · · · · · · · · · · · · · · · · · ·		N/A
FIELD PA Ambient A										
Sampling I	Depth (ft):_	Pump I	nlet@			Weather C Reference			er PVC ca	sina
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO		-	
meter	rate	to		Purged	(°C)	sp.conu (μS/cm)	(mg/L)	рН	ORP (mV)	Water Description/Comments
(gallons)	/min	water	0.12	(Gallons)			6.0			-
		87.42	9:21		1	4945 4776	5.69	7.13		<u></u>
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						······································				
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/1	Filtered	Non	Filtered	Filtered	Non Filtered	Filtered	I Fil	ered N	Non Filtered	······
Chemetrix (Visual)	Alk mg/l Hach	Filtered Alk mg/l	Fe2+ mg/l	Fe2+ mg/l Chemetrix (Visual)	Fe2+ mg/l Hach	Manganes mg/l	n	ganese g/l	Manganese mg/l	Comments
( ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (		Hach	Hach	(Visuar)		Hach		netrix sual)	Hach	
				<u> </u>	0.0					
<u>PURGE I</u>	NFORM	ATION			X					
Starting Flo	w meter	Reading		Endin	ig Flow n	neter Read	ing:	F	Flow Rat	e:
										imal purged (Y/N):
Tubing inne	er diamet	er	(in) T	ubing & P	Pump Vol	ume	(ml)			ottom of well (feet)
Controller s	ettings: H	Pressure_	(psi)	Discharg	e (sec.) F	Recharge_	` /	(sec	.)	
Casing Volume	Calculation (	gallons): 2" v	well = $0.17$	x WCT 4" wel	ll = 0.66 x WC	T 6" well = 1.	<b>47 x</b> WCT		Where WC	Γ = Water Column Thickness (feet)

Hydro Sleeple @ 185 BTOC



# DAILY FIELD ACTIVITY REPORT

Page \_\_\_\_ of \_\_\_\_

& ASSOCIATES

те. Ге		
Client Name: Project Name: EsTCP 201584 Too-ele	Project Number:	<u></u>
Contractor:	Date: <u>7-26-16</u> Arrival Time: <u>12:2</u>	5
Weather: <u>93</u> Clear	·	
Time Breakdown: Drive: Work:	Standby:	_
Location and Description of Activities:		
well D19		
Equipment Used on Project: 142.5 to	TOC	
	•	
Activity Summary and General Remarks:		
PNNL		
		<u> #s /</u>
<b>9</b>		HS ?
		HS
Clemon		
TWR 2.# 2		HS
		HS
Unerrobal Insight		
13:06 DNA 1000ML		<u> </u>
15:10 KNW 800m C		170
Technician Signature:	Date:	
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	-	

a **a** 2011 a 20

			GRO	UNDWA	TER PU	RGE AN	D SAM	PLING	FORM	
Project N	ame: 10	Soel	e Ar	ma I	) epot		C	COC Nu	mber:	
			•		•		v	Vell ID:	$: \overline{\mathcal{T}}$	19
Sample C	Collected	by: <u>5</u> L	vlTl	NBU	<u>о</u>		I	Date of O	Collection	19 n: 7-26-16
EQUIPM	ENT		. <b>.</b>							
Purging E Sampling	Equipmen	t:	Her	drosle	eve					
Sampling	Equipme	ent:	. 0							
Filtering	Equipmen	nt:								
Equipmer	nt Decont	aminatio	on:	Per Wo	ork Plan –	Alconox V	Vash with	<u>n Triple</u>	Rinse and	Isopropyl Alcohol Rinse
					Equipm	ent Calibra	tion			
	Eq	uipment/	Model			Serial	Number			Date Calibrated
	YSI 556	Multi Para	meter Me	eter		05C1	520 AA			
	HACH	DR 890 C	colorimete	er						N/A
FIELD PAI	RAMETER	S							•	
Ambient A	ir Tempera	ture (°F):	93			Weather C	onditions:	C	ear	
Sampling D	Depth (ft):	Pump I	nlet@			Reference	Point: <u>T</u>	op of inn	ner PVC ca	sing
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pH	ORP	Water
meter	rate	to		Purged	(°C)	(µS/cm)	(mg/L)		(mV)	Description/Comments
(gallons)	/min	water		(Gallons)				-		
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	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	•
D.O. mg/l	Filtered	Non	Filtered	Filtered	Non Filtered	I Filtered	- Fil	tered	Non Filtered	
Chemetrix	Alk mg/l	Filtered Alk mg/l	Fe2+ mg/l	Fe2+ mg/l Chemetrix	Fe2+ mg/l	Mangane	se Man	ganese ng/l	Manganese	Comments
(Visual)	Hach	Hach	Hach	(Visual)	Hach	mg/l Hach	Che	metrix isual)	mg/l Hach	Comments
					0.0					· · ·
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<u>PURGE I</u>	NFORM	ATION		* • .						
Starting Flo	w meter	Reading	•	Endir	ng Flow n	neter Read	ling:		Flow Ra	te:
										imal purged (Y/N):
Lasing Inne	er Diamet	er (inche	$\frac{(in) T}{}$	Initial I	Depth to	Water (fee	(ml)	<u> </u>	bepth to b	ottom of well (feet)
Controller s	settings: I	Pressure	(msi)	) Discharo	e (sec.)	Recharge	(IIII)	(se	c.)	
Casing Volume										T = Water Column Thickness (feet)
Susing volume		5anon3). 2		A 11 CI + WC		ci o well-l	TT A WUI		where we	T - water Column Thickness (Ieel)



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	Chain of Custody Bocord	STL	<b>STL Denver</b> 4955 Yarrow Street
		Severn Irent Laboratories, Inc.	Arvada, CO 80002
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	Telephone Number (Area Code)/Fax	()	Page of /
	State Zip Code Site Contact Lab Contact	Analysis (Attach list if more space is needed)	
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	Contract/Purchase Order/Quote No.	<u>fre</u>	Conditions of Receipt
	Sample I.D. No. and Description     Date     Time     Advisor     Advisor     Advisor       (Containers for each sample may be combined on one line)     Date     Time     Air     Air     Air		
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	5 TU BU #2 7-26-16		
	Torre Dar TV B1#3 7-26-16 9:20 V		
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	53 # 317-3		
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DISTRIBUTION: WHITE - Returned to Client with Report; CANARY - Stays with the Sample; PINK - Field Copy

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Indication       Image: Sample Disposal       Image: Sample Disposal         Imable       Sample Disposal       Sample Disposal         Imable       Sample Disposal       Sample Disposal         Imable       Sample Disposal       Disposal By Lab       Image: Claim Annual Disposal By Lab       Image: Claim Annual Annua Annual Annual Annua Annual Annual Annual Annua Annual Annual An							
Initiation       Sample Disposal       (A fee may be assessed if samples are retained         Flammable       Skin Irritant       Poison B       Unknown       Return To Client       Disposal By Lab       Archive For       Months       (A fee may be assessed if samples are retained         Required       0C Requirements (Specify)       0C Requirements (Specify)       Date       Ime       Date       Ime         1       1       1       Received By       1       Received By       Date       Ime       Date       Ime         1       Date       Ime       2       Received By       2       Received By       Date       Ime       Ime       Date       Ime       <							
Required       OC Requirements (Specify) $48$ Hours $7$ Days $21$ Days $0$ Other $48$ Hours $7$ Days $21$ Days $0$ Date $14$ Hours $7$ Days $21$ Days $0$ Date $14$ Hours $7$ Days $14$ Date $1$ Received By $16$ ( $1$ ) $10$ Date $1$ me $2$ Received By $16$ ( $1$ ) $10$ Date $1$ me $2$ Received By $16$ ( $10$ ) $10$ Date $1$ me $2$ Received By $10$ Date $10$ ( $10$ ) $10$ Date $1$ me $3$ Received By $10$ Date $1$ me	Identification	Unknown	ient	1	1	assessed if samples a	e retained
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Date Time 3. Received By Date		Date	┥ ──	2. Received By		Date	Time
	. Relinquished By	Date	Time	3. Received By		Date	Time

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$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	POLONIA DC 303-670 Telephone Number (Area Code)/Fax Number	N N	Page /
Project Manual Andread (Sum)       Contraction of the analysis (Sum)       Contractin	State Zip Code Stite Contact	Analysis (Attach list if more space is needed)	
Consistencies & The formation of the for	territy (1.0 1.0 1.0 0.0 0 Carrier/Waybill Number 1.0 0.1 0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1		Connict Instructions
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Possible Hazard Identification       Sample Disposal       Sample Disposal       Constraint (A fee may be assessed if samples are retained and time and time are are are are are are are are are ar			
Turn Around Time Required       Other       Date       Time         1       Relinquished By       I       Pate       Time       1. Received By       Date       Time         2. Relinquished By       I       I       2. Received By       2. Received By       Date       Time         3. Relinquished By       I       I       2. Received By       2. Received By       Date       Time         3. Relinquished By       I       I       I       I       I       I       I       I       I         3. Relinquished By       I       I       Bate       I       I       Bate       I	Sample Disposal       Mable Skin Irritant       Poiscon R       Linknown       Raturn To Client       Disposal By Lab	Months	ssessed if samples are retained onth)
Let rous     1 todas     1 todas     1 todas     1 todas       1. Reinquished By     1. Received By     1. Received By     1. Received By       2. Reinquished By     1. Action 1     1. Received By       2. Reinquished By     1. Received By     1. Received By       3. Reinquished By     1. Received By     1. Received By		*.	
Date Time 2. Received By Date Date Date Date 3. Received By Date Date Date Date Date Date Date Date			Time
Date 3. Received By	1039 U WOW   1-2 (c-16 10:22)		
	Date Time		

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DISTRIBUTION: WHITE - Returned to Client with Report: CANARY - Stays with the Sample: PINK - Field Copy

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PROJECT NAME: Toget Army Depot	_	
Well ID: $D-25$		
Sample Collected by: THW JTW	Date of Collection:	7/26/17
SAMPLING EQUIPMENT		

	Equipment Calibration	
Equipment/Model	Serial Number	Date Calibrated
HMA-453-5	5554	7/26/17
EQUIPMENT DECONTAMINATION:	Alconox Wash, Double Rinse, and Is	sopropyl Alcohol Spray
CALIBRATION RESULTS Stickut	1 = 2.85 Eeva	Tool 09:46
CALIBRATION RESULTS       Stickus         Ambient Air Temperature (°F) <sup>a/</sup> :       83         Groundwater Temperature (°F) <sup>a/</sup> :       71         Time Probe Inserted into Ambient Groundwater Groun	Weather Condition	ons: Ptly Cloudy
Groundwater Temperature ( <sup>O</sup> F) <sup>a/</sup> :		Strivet
Time Probe Inserted into Ambient Groundw	ater (Minimum = 20 Minutes):	9:52 aut a
Calibration Standards (Include Units): Low		
Time of Calibration: $\sim 10^{\circ}.2^{\circ}$	3	4-70
Calibration Results (Include Units): Low:	23014 High	445
Casing Inner Diameter (inches)	Borehole Diameter (Inche	s)
Casing Inner Diameter (inches) 4 Initial Depth to Water (feet) 87.42	Depth to bottom of well (feet)	- 145
Screened Interval, If Known (Include Datum	n)	
Depth Measured by Sonde	(Include Units)	
Reference Point: Top of inner PVC casin	g or BGS, Specify:	

Run Number	Calibration Number	Up Versus Down	Winch Speed (specify Units)	Con	mments
i	1	Down	9,5 ft/min	and the second s	
1	Y	UP		in the second se	14
		/			
	alt is		~		

Notes:

a/ The greater the difference between the groundwater temperature and the ambient temperature at the surface where the sonde will be calibrated, the longer the sonde should be allowed to equilibrate because the sonde is very sensitive to temperature.



Page 1 of 1

PROJECT NAME: Tracele Army Depot		
Well ID: $D - Iq$	- 1 121	
Sample Collected by: THW/J FW	_Date of Collection: 7/20/16	
SAMPLING EQUIPMENT MMA - 53-5		
Equipment Calibration		

	Equipment Canoration	
Equipment/Model	Serial Number	Date Calibrated
HMA - 553-5	5554	7/26/16
-	Alconox Wash, Double Rinse, and Iso	propyl Alcohol Spray
CALIBRATION RESULTS Sticky	p 2,76 ~ 14:0	B Prode in war
Ambient Air Temperature ( <sup>o</sup> F) <sup>a/</sup> : 93	Weather Condition	B Prode in when ns: Claur, Breezy )
Groundwater Temperature ( <sup>O</sup> F) <sup>a/</sup> :		
Time Probe Inserted into Ambient Groundw	vater (Minimum = 20 Minutes):	400 hours
Calibration Standards (Include Units): Low	w: 205, Phigh	

Calibration Standards (Include Units): Low: 205, Time of Calibration: 14:44

Calibration Results (Include Units): Low:	High		
Casing Inner Diameter (inches) 4"	Borehole Diameter (Inches)_	•	
Initial Depth to Water (feet) 142.5 BJC Dept	h to bottom of well (feet)	167.07 TOC	
Screened Interval, If Known (Include Datum)			

Depth Measured by Sonde \_\_\_\_\_ (Include Units)

Reference Point: Top of inner PVC casing or BGS, Specify:

Run Number	Calibration Number	Up Versus Down	Winch Speed (specify Units)	Comments
1		Down	1) ft/pin	
(		UP	10 ft/min	
			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
				100
		-		

Notes:

Page <u>/</u> of <u>/</u>

& ASSOCIATES

1

## DAILY FIELD ACTIVITY REPORT

Client Name: Project Name: <u>Hill Ar</u> Contractor: Weather: <u>40°</u> F	FB ESTCF C	201584 learfield UT	Project Number: Date: 7-27 Arrival Time: <u></u>	
Time Breakdown: D	rive:	Work:	Standby:	
Location and Description	n of Activities: 20143	We	ll 0 <del>4243</del>	
		2	110-043	
Equipment Used on Proj	ect:	10.:	55 pt depter to Below topes	water
Activity Summary and C $P_{IN} NL$ $V > 0 \le Hill AFB U =$ V > 07 V > 09	U#35mp			
10:12 Clemson Hill AFB Web. 10:13 10:14		2		
10:15 Microbia DNA 10:20 RNA		n C		
Technician Signature:			Date:	<b>₩</b>

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## **GROUNDWATER PURGE AND SAMPLING FORM**

Project N	lame: <u>Hi</u>	U AFE	3 E	STCP 2	01584	yield UT	(	COC Nu	mber:	
Somalo (	<sup>1</sup> ollootod	here T	21-	nlkin	Clea	field	. 1	Well ID:		110-043 n: 7-27-16
		by: <u> </u>	0110	lpw			L	Date of (	Collection	n: <u>7-2+-16</u>
EQUIPM	<u>IENT</u>		,	0 '	- A A A -	2				
Purging H	Equipmer	1t: <u>G-ee</u>	tech	Peri	Taltee	Pan	φ			
Sampling										
Filtering										
Equipmen	nt Decon	taminati	on:	Per W	ork Plan –	Alconox V	Vash witl	n Triple	Rinse and	Isopropyl Alcohol Rinse
				······································		ent Calibra				
	Eq	uipment/	Model			Seria	Number			Date Calibrated
	YSI 556	Multi Para	ameter M	eter		05C1	1520 AA			
	HACH	DR 890 C	Colorimete	er			٩.			N/A
FIELD PAI	RAMETER	25				117	<u> </u>			
Ambient A	ir Tempera	ture (°F):	70	Clea	rfeld.	, UT Weather C	nnditions:	el	and set a	
Sampling D	Depth (ft):	Pump I	nlet@			Reference	Point: T	op of inn	er PVC ca	sing
Flow	Flow	Depth	Time	Volume						
meter	rate	to	Time	Purged	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/L)	pH	ORP (mV)	Water
(gallons)	/min	water		(Gallons)		(µo/cm)	(		(mV)	Description/Comments
			9:23		~	(		1	·	
			9:25	.750	15.73	1996	7.84	6.26	211.2.	· ·
			9.27		1587	1012	4.2	6.32	207.7	
			9.29	2	15.87	938	3.1	6.5	199.9	
			9.31	3	15.9	910	1.85	10.6	1953	
			9.34	4	15:77	966	3,10	6.64		
			9,36	<b>4</b> 4	N-68	1023	2.5	6.65	187.3	
			9:39	uped 9:	اربطا	1075	1.17	6.7	183.0	
			9.41	1	15.75		1.65	6.81	179.4	
			9.44	2	15.4	1099	1.52	6.83		
			9.47	23	15.4	1104	2.45	6.86	176.9	
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
	<b>D</b> <sup>1</sup> <b>1</b>				· · · · · · · · · · · · · · · · · · ·				L	
D.O. mg/l Chemetrix	Filtered Alk mg/l	Non Filtered	Filtered Fe2+	Filtered Fe2+ mg/l	Non Filtered Fe2+ mg/l	Filtered Manganes			Non Filtered Manganese	
(Visual)	Hach	Alk mg/l Hach	mg/l Hach	Chemetrix (Visual)	Hach	mg/l	m	ng/l netrix	mg/l	Comments
						Hach		sual)	Hach	
					0.0					
PURGE I	NFORM	ATION								
				<b>D</b> 1!	<b>.</b>		•	-		
tarting FIO	w meter	Reading	·	Endin	ig Flow n	neter Read	ing:		Flow Rat	e:
otal Volun	ne Purge	d:	Purg	ged Dry (	Y/N):	Micro ]	purged (	Y/N):	Mini	imal purged (Y/N):
										ottom of well (feet)
uoing inne	er alamete	er	(1n)	ubing & F	'ump Vol	ume	(ml)			
Controller s	ettings: F	ressure_	(ps1)	Discharg	ge <u>(</u> sec.) F	kecharge_		(sec	:.)	

Casing Volume Calculation (gallons): 2" well = 0.17 x WCT 4" well = 0.66 x WCT 6" well = 1.47 x WCT

Where WCT = Water Column Thickness (feet)



# **GROUNDWATER PURGE AND SAMPLING FORM - Continued**

Project Name: Hill AFB ESTCP 2015P4	Well ID: 5 U10-043
Sample Collected by: <u>Jultulk</u>	Date of Collection: $7 - 27 - 16$

Flow Meter	Flow			Volumo	Tomm	En Cond		~TT		Water
	rate	Depth to	Time	Volume Purgod	Temp	Sp.Cond	DO (mg/I)	pH	ORP	Water
(gallons)	/min	water		Purged (Gallons)	(°F)	µS/cm	(mg/L)		(mV)	Description/Comments
(ganons)	/111111	water	9.51	(Ganons)						
			9.54	1	15.18	1177	1.20	1 91	172.0	
·				2	15.27	1135	100	6174	172.9 172.6 168.5	
			9.57	3	1521	1133	0.85	6.12	112.6	
			10:00	3	1531	1158	, 75	6.78	16813	
			10:00		$\Lambda(\mathcal{F})$	1145	1 ()	7.0	168.2	
									•	
					-	· · ·		•		· · · · · · · · · · · · · · · · · · ·
									4	
						•				
		-								
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	



Page \_\_\_\_\_ of \_\_\_\_\_

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#### DAILY FIELD ACTIVITY REPORT

	Client Name:	Project Number: Date: $\frac{7-27-16}{27-16}$
	Project Name: Hill APB ESTCP 201584	Date: 7-27-16
	Contractor:	Arrival Time: <u>/3/10</u>
	Weather: 70° F Clear	
	Time Breakdown: Drive: Work:	Standby:
	Location and Description of Activities:	110-025
	14,45 pt Depth to wate	4 Loon TOC
	11.5 gal prenging	Stat 32/
		Graen I
	Equipment Used on Project:	200.
	Activity Summary and General Remarks:	
	PNNL	
15:03		
7	ఫ	
il –		
K		
14		
22	1	
00	2	
1	DNA 100	>>>
15:27	RN # Loc	
		D ML
	Technician Signature:	Date:
		WIEDEMEIER
	N:\Admin\Forms - Field\Daily Field Activity Report.doc	

#### **GROUNDWATER PURGE AND SAMPLING FORM**

Project N	ame:	LLAF	n Es	TCP 20	1584			COC Nu		
Sample C	Collected	by: <u>Tư</u>	JJW	IBW			V [	Vell ID: Date of (	<u> </u>	-025 : <u>7-27-16</u>
EQUIPM	ENT									
Purging H	<u>Eauipmen</u>	t: 6	esto	ah F	) orin	talte	A. Po	m		
Sampling	Eauipme	m			y na	- auto		-11		
Filtering										
Equipme			on:	Per Wo	ork Plan –	- Alconox V	Vash with	Triple	Rinse and I	sopropyl Alcohol Rinse
	52 A					ent Calibra				
	Eq	uipment/	Model			Serial	Number			Date Calibrated
	YSI 556	Multi Para	ameter Me	eter		05C1	520 AA			
	HACH	DR 890 C	Colorimete	er						N/A
FIELD PA Ambient A			90			Weather C	onditions:	C	eve	
Sampling D	Depth (ft):	Pump I	nlet@			Reference	Point: <u>T</u>	op of inn	er PVC casi	ng
Flow	Flow	Depth	Time	Volume	Temp	Sp.Cond	DO	pH	ORP	Water
meter	rate	to		Purged	(°C)	(µS/cm)	(mg/L)	-	(mV)	<b>Description/Comments</b>
(gallons)	/min	water		(Gallons)						
			13:46		1. I.C.	772-	7.54	6.95	-178.2	also Cutture
			13:50	elis	18.22	984	20.13		-18.2	odor-Salfur
			1359	2	18.61	12/4		6.97		
		_	14:09	2.5	19.06	1347	2.12	7.09	-167.1	
			14:15	3_				•		
			14:25	3,5				~ 0		
			14,30	4.0	20.10	1493	1.27	1.28	-32.7	
			14,58	40	18,98	1454	0.31	7.13	~35.0	
			4:3	5.0	19.04	11155	0.30	7.11	-61.4	
					17.04	1433	10.51	1-16	~46.7	
				6.00	18.87	1453	0,29		-51-5	
							0101	7.17	000	
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/l Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtere, Fe2+ mg/l Hach		se Man; rr Chei	ered ganese ng/l netrix sual)	Non Filtered Manganese mg/l Hach	Comments
						\$				

#### **PURGE INFORMATION**

Starting Flow meter Reading:	Ending Flow me	ter Reading:	Flow Rate:
Total Volume Purged:	Purged Dry (Y/N):	_ Micro purged (Y/N):_	Minimal purged (Y/N):
	Initial Depth to W in) Tubing & Pump Volu (psi) Discharge (sec.) Re	me(ml)	Depth to bottom of well (feet)

Casing Volume Calculation (gallons): 2" well = 0.17 x WCT 4" well = 0.66 x WCT 6" well = 1.47 x WCT

Where WCT = Water Column Thickness (feet)



<b>33 et</b>	24056	<b></b>	netruotione/	Conditions of Receipt									etained		Time	Time	Time	
<b>STL Deriver</b> 4955 Yarrow Street Arvada, CO 80002	Chain of Custody Burghod, 056	Page /		Condition									(A fee may be assessed if samples are retained longer than 1 month)		Date	Date	Date	
<b>STL</b> aboratories, Inc.	Date 1 - 3 7 - 16 Lab Number	Analysis (Attach list if more space is needed)				The second secon						x	(A fee may be a Months longer than 1 m	T to the second				
SEVERN STL TRENT Severn Trent Laboratories, Inc.						- Daga					-2							
S E V T R Sever	12			Containers & Preservatives	HO <sup>E</sup> N /ɔʉuz HO <sup>E</sup> N IOH EONH								Disposal By Lab	å	1. Received By	2. Received By	3. Received By	
•	J N ber (Area Coo	0.20		Matrix	IIOS IIOS IPOS Snoonby		1						Sample Disposal		L 110:00	Time	. Time 3.	
	Project Manager	1	CarrierWi		Time	16/10:15	02:01 91-7C-1	1 2: 31 71-66-6	-				Unknown S			Date	Date	
	demel	Zip Code			ine) Date	4 7-27-1610:15							 Poison B				-	
Chain of Custody Record	C D		Project Name and Location (State)	Contract/Purchase Order/Quote No.	Sample I.D. No. and Description (Containers for each sample may be combined on one line)	HIND EHO-OHS DNH	HILLHED UNO-045 RNH	HUNTE LID-005 RNA					Possible Hazard Identification	equired 48 Hours 7 Days	1)100	lished By	3. Relinquished By	Comments

DISTRIBUTION: WHITE - Returned to Client with Report; CANARY - Stays with the Sample; PINK - Field Copy

100

Chain of Custody Record				SEVEKN TRENT evern Trent L	Severn Trent Laboratories, Inc.	<b>STL Denver</b> 4955 Yarrow Street Arvada, CO 80002
ESTUPTODD Whelemere	L	Project Manager M , 4	l'edeneier		91-t.C. to	Chain of Custody Number 054
309				6	TN NN ME	
1, a state Zap Code	891	Site Contact	Brach Lee		Analysis (Attach list if more space is needed)	
Project Name and Location (State)	Carris	Carrier/Waybill Number				Conciel Instructions/
Contract/Purchase Order/Quote No.		Matrix	Containers & Preservatives	725 74		Conditions of Receipt
line)	Date Time	lioS bəS suoənpA	N <sup>3</sup> OH Zuye( N <sup>3</sup> OH HCI HCI HNO3 HSZO¢	18 13		
Hill AFB U. 10-043 5ample/ 7.3	27 16 10:05	4		11		
Hill MFBUID-043 Sample 2	1 10:01	3		11		
HALARD UN0-043 Sample 3	10:08			11		
HITTRUD 043 Sanaly V	r 10:09			4		
0						
HillHEB WID - 035 Sand 1 -	27-16 IS:03			7		
HILLE ULD. 025 Jenule 2	15.07	Ĺ.				
HILHED K10-025 Sampt 3	6:1			11		
Hild His Uro-025 Sander 1	15:16	7		7		
TJ D K ( ex ( DT W # 7 1 3	27-16 11:00	1		7		
Possible Hazard Identification 12 Non-Hazard	son B 🗌 Unknown	Sample Disposal	ort Disposal Bv Lab	Archive For	(A fee may be as: Months Tomer than 1 mon	(A fee may be assessed if samples are retained
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DISTRIBUTION: WHITE - Returned to Client with Report: CANARY - Stays with the Sample; PINK - Field Copy

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Matrix         Containers & Preservatives         After Preservatives         After Preservatives     <	$\frac{1}{2}$	0153	Carrier/W			Jaro i (	I Flow	- The second		ore space	is needec			
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DateTime1. Received ByDate $(7 - 2.7 - 1 - 1 / b)$ $(1 / b)$ 2. Received ByDateDateTime2. Received ByDateDateTime3. Received ByDate	Q Q	21 Day				OC Req	urements (Sp	secify)			1.5.5			
Time 2. Received By Date Date Time 3. Received By Date Date		1		91		1. Recei	ved By						Date	Time
Time 3. Received By			Date		ne	2. Recei	/ed By						Date	Time
			Date	_ <u>1</u>	ne	3. Recei	/ed By						Date	Time
	ith Donort: CA	DISTRIBUTION: WHITE Behimed to Client with Bonod: CAMABV State with the Second of DIMY Fil	- the Cample.	UNIN D						-				

DISTRIBUTION: WHITE - Returned to Client with Report: CANARY - Stays with the Sample; PINK - Field Copy

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PROJECT NAME: Hill AFB Well ID: Q U10-043

Sample Collected by: THW

Date of Collection: 7/27/16

SAMPLING EQUIPMENT

	Equipment Calibration	
Equipment/Model	Serial Number	Date Calibrated
HMA-453-5	5554	7127/16
		1.0
EQUIPMENT DECONTAMINATION:	Alconox Wash, Double Rinse, and Is	opropyl Alcohol Spray
CALIBRATION RESULTS	A -	a IV.Ly
Ambient Air Temperature (°F) <sup>a/</sup> : 87	Weather Condition	ms: Clew & Not
Groundwater Temperature ( <sup>O</sup> F) <sup>a/</sup> :		11/
Time Probe Inserted into Ambient Ground	dwater (Minimum = 20 Minutes):	1:45
Calibration Standards (Include Units): L	ow:	-3
Time of Calibration: 11"10		
Calibration Results (Include Units): Low	Z13.37 High /	55500
Casing Inner Diameter (inches)		
Initial Depth to Water (feet) 10,55 ft	Depth to bottom of well (feet)	6.38 ft has
Screened Interval, If Known (Include Dat	um)	
Depth Measured by Sonde	(Include Units)	
Reference Point: Top of inner PVC cas	sing or BGS, Specify:	

Run Number	Calibration Number	Up Versus Down	Winch Speed (specify Units)	Comments
/	/	Hown	9 ft/min	
1	)	up	9 ft/min	
1				
		1.1		

Notes:



PROJECT NAME:	Hid	AFB	-	0410
Well ID: () () -	025	1		
Sample Collected by	TUCI		-	

\_\_\_\_\_Date of Collection: 7-27-16

SAMPLING EQUIPMENT

Equipment Calibration							
Equipment/Model	Serial Number	Date Calibrated					
1-1MA - 453-5	5554	7/27/16					
EQUIPMENT DECONTAMINATION:	Alconox Wash, Double Rinse, and Isopro	pyl Alcohol Spray					
CALIBRATION RESULTS		a Kin					
Ambient Air Temperature ( $^{\circ}F$ ) <sup>a/</sup> : <u>(10)</u> Weather Conditions: <u>Clear &amp; Hot</u>							
Groundwater Temperature ( <sup>O</sup> F) <sup>a/</sup> :		11					
Time Probe Inserted into Ambient Groundwater (Minimum = 20 Minutes): $\frac{16.04}{10.04}$							
Calibration Standards (Include Units): Lo	ow: D High SEA3	•					
16.7.5							
Time of Calibration: <u>10709</u> Calibration Results (Include Units): Low: <u>224,375 High</u> 1281.87 Casing Inner Diameter (inclus)							
Casing inner Diameter (inches)							
Initial Depth to Water (feet) 14,45 Depth to bottom of well (feet) 41.87 bg 5							
Screened Interval, If Known (Include Datu	um)						
Depth Measured by Sonde (Include Units)							
Reference Point: Top of inner PVC casing or BGS, Specify:							

Run Number	Calibration Number	Up Versus Down	Winch Speed (specify Units)	Comments
H		Down	10 ft/min	D'dist Run Started w/ AF
1	1	UP	10 felmin	
2	1	Down	10 ft/min	
2	1	Up	12 ft/min	
		/	, .	

Notes:



PROJECT NAME: WILL AFB OU-10	
Well ID: 410-051	-1-7/16
Sample Collected by: FHW/JTW	Date of Collection: $\frac{1}{1}$
SAMPLING EQUIPMENT	

	Equipment Calibration	
Equipment/Model	Serial Number	Date Calibrated
HMA-453-5	5554	+127/16
		1.0
EQUIPMENT DECONTAMINATION:	Alconox Wash, Double Rinse, and Iso	propyl Alcohol Spray
CALIBRATION RESULTS		
Ambient Air Temperature ( <sup>O</sup> F) <sup>a/</sup> :	Weather Condition	ns: CIEar & Vlot
Groundwater Temperature ( <sup>O</sup> F) <sup>a/</sup> :		
Time Probe Inserted into Ambient Groundy	water (Minimum = 20 Minutes):	103 hours
Callbert's Chardende (Instate Instate)	a mat SE-C	> IVAN COLIN
Time of Calibration: <u>Could</u> <u>uot</u> <u>c</u> Calibration Results (Include Units): Low:	alibrate because of To	austornator a
Calibration Results (Include Units): Low:_	Statut, usa fich	6 Cla head 1
Casing Inner Diameter (inches) 4/1	Borehole Diameter (Inches)	10 F-5 S
Initial Depth to Water (feet)	Depth to bottom of well (feet)	Calib
Screened Interval, If Known (Include Datu	m)	fin
Depth Measured by Sonde	(Include Units)	
Reference Point: Top of inner PVC casi	ng or BGS, Specify:	
		-

Run Number	Calibration Number	Up Versus Down	Winch Speed (specify Units)	Comments
	1 -	UP	15 Ftmin	

Notes:



Page \_\_\_\_ of \_\_\_\_ **DAILY FIELD ACTIVITY REPORT** Project Number: Date: 7-28-16Arrival Time: 8:00Client Name: Project Name: ESTOP 201584 Hill APR Contractor: 68° F Clear Weather: Work: Standby: Time Breakdown: Drive: Location and Description of Activities: Description of Activities: 72.83ft Depth To water from TOC UO-019 2gol purge water well U10 - 019Equipment Used on Project: Griendios Pump 215Hz for pump Activity Summary and General Remarks: PNNL Hill AFB 410-019 Sample 1 Jeratid Usaarahd 10:29 2 340 porta 11:20 collection filled 11:00 portes 9:50 <u>Clomoon</u> 9:52 Nill AFB 410-019 IBI#1 9:55 #2 #3 Microbial Insights DNA 300+300 10;14 RNA 300 +300 10:22 10:18 Date: Technician Signature: \_\_\_\_\_ 0.69 with black ASSOCIATES

N:\Admin\Forms - Field\Daily Field Activity Report.doc

			GRO	UNDWA	TER PU	RGE AN	D SA	MPLING	FORM	
Project N	ame: <u>F</u>	STCI	> 20	1584	Hi	I AFE	3	_COC Nu	mber:	
Sample Collected by: Tw/Jw/B								<u> 110 -</u>	10 -019 ection: 7 -28 - 16	
		wibi				_Date of C	Collection			
EQUIPM Purging E Sampling	<u>EN I</u> Cauipmer	nt: G	nun	1100	Puna	2				
Sampling	Equipm	ent:		0						
Filtering	Equipme	nt:								
Equipmer	nt Decon	taminatio	on:	Per W		<u>Alconox V</u> ent Calibra		vith Triple	Rinse and	Isopropyl Alcohol Rinse
	Eq	uipment/	Model		Equipm		Numb	er		Date Calibrated
		Multi Para		eter			520 A			
	HACH	DR 890 C	olorimete	er						N/A
FIELD PAI	RAMETER	<u> </u>							, <u>, , , , , , , , , , , , , , , , </u>	
Ambient Ai						Weather C				
Sampling D								Top of inn		
Flow meter	Flow rate	Depth to	Time	Volume Purged	Temp (°C)	Sp.Cond (µS/cm)	DO (mg/l		ORP (mV)	Water Description/Comments
(gallons)	/min	water	and	(Gallons)	( 0)	(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	(8			Description/Comments
		9:35	43 43		22.98	1325	610	7.42	-143.4	
		9:45			23.4	1.0005	P.0		-59.8	
	<u> </u>				2308	.007	7.4	C R.12	-51.7	
	··					<u> </u>				
						·				
	≥40 ≤200				±10%	±10%	±10%	±0.2	±10mv	
					-1070		11070			
D.O. mg/l Chemetrix (Visual)	Filtered Alk mg/l Hach	Non Filtered Alk mg/i Hach	Filtered Fe2+ mg/l Hach	Filtered Fe2+ mg/l Chemetrix (Visual)	Non Filtered Fe2+ mg/l Hach	Filtered Manganes mg/l Hach			Non Filtered Manganese mg/l Hach	Comments
		1								
PURGE I	NFORM	ATION			•		<b></b>	·····•		
			•	Endin	ng Flow m	neter Read	ling	1	Flow Date	e:
Total Volun	ne Purge	d:	Purg	ged Dry (	Y/N):	Micro	purgeo	d (Y/N):	Mini	mal purged (Y/N):
Casing Inne Tubing inne Controller s	r Diamet r diamet	er (inche er	es)(in) T	Initial I ubing & F	Depth to Y Pump Vol	Water (fee ume	et)_ <b>1</b> 3 (m	1) 7,82 D	epth to bo	ottom of well (feet)

Casing Volume Calculation (gallons): 2" well = 0.17 x WCT 4" well = 0.66 x WCT 6" well = 1.47 x WCT

Where WCT = Water Column Thickness (feet)



Chain of Custody Record	•	•		SEVERN TRENT Severn Tren	RN NT Trent La	SEVERN TRENT STL Severn Trent Laboratories. Inc.		<b>STL Denver</b> 4955 Yarrow Street Arvada, CO, 80002	et 2
STL-4124 (0901)									1
ESTOP TO JU Wirdemeier	Project Manager	Whie	dem	emeier		Date 28-16	e	Chain of Custod Number 1	291
	Telephone Number (Area Code)/Fax Number	IL (Area Code)/Fa	V.Number	7999	6	JN WW L		Page /	of
$\frac{\operatorname{clip}}{\operatorname{Cr}} + \frac{1}{\operatorname{Cr}} + \frac{1}{\operatorname{Cr}} + \frac{\operatorname{State}}{\operatorname{Cr}} + \frac$	Site Contact	$\frac{1}{1}$	tab Contact	 ນ	An	Analysis (Attach list if more space is needed)		 	
cation (State) Surver C	1	mber						Snecial II	structions/
urchase Order/Quote No.	W	Matrix	Containers & Preservatives	s &	7 70			Condition	Conditions of Receipt
Sample I.D. No. and Description (Containers for each sample may be combined on one line) Date	snoenby	Serdi Soil	HCI EONH HISCH	HOEN HOEN	, <del>Ĝ</del>	· · · · · · · · · · · · · · · · · · ·			
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Drup & and DIWH \$ 1-38.4 13	12:40								
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e Required 1 / Days 1 / Days 2 / Da			OC Requirements (Specify)	ğ					
Mara Will or	Pare & -16	Time , 1/4	1. Received By					Date	Time
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3. Relinquished By	Date	Time	3. Received By		- - - -			Date	Time
Comments									

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DISTRIBUTION: WHITE - Returned to Client with Report: CANARY - Stays with the Sample; PINK - Field Copy

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uote No.	Conditions	Receipt
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7-28-10:09 L		
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20 1.11 #F.S. 11 10 - 019 RNA 1-28-10 10:18		
HIII 123-16 ANA 1-23-16		
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DISTRIBUTION: WHITE - Returned to Client with Report. CANARY - Stays with the Sample: PINK - Field Copy

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Chain of			SEVERN TRFNT	RN STL	STL Deriver	
Custody Record			Severn	∎ <b>ਦ</b> 2	4955 Yarrow Street Arvada, CO 80002	
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uote No.		Matrix	Containers & Preservatives	J() =	Conditions of Receipt	
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Hill AFBUID OLA VBI#3		7				
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dentification		Sample Disposal	Disnocal By Lab	Months	(A fee may be assessed if samples are retained longer than 1 month)	
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	Date		2. Received By		Date	
3. Relinquished By	Date	Time	3. Received By		Date	
Comments						

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DISTRIBUTION: WHITE - Returned to Client with Report: CANARY - Stays with the Sample; PINK - Field Copy

## MAGNETIC SUSCEPTIBILITY MEASUREMENT FORM - SONDE

PROJECT		2-019	HIL AFB	<u>-04-10</u>			
	410-019	()			21 111		
Sample Col	lected by:	THU		Date of Collect	ion: <u> </u>		
SAMPLIN	G EQUIPMENT						
			Easting and Calib				
	E	M. 1.1	Equipment Calib		Dete Calibrated		
	Equipment/		Seria	ll Number	Date Calibrated		
- /	IMA - 45.	53	5.55 F				
EQUIPME	NT DECONTA	MINATION:	Alconox Wash, D	ouble Rinse, and Isopro	pyl Alcohol Spray		
CALIBRA	TION RESULT	<u>S</u>			1 F.		
Ambient A	ir Temperature (	<sup>(0</sup> F) <sup>a/</sup> : <u>90</u>		Weather Conditions:_	Hot & Sunny		
		( <sup>O</sup> F) <sup>a/</sup> :			/		
Time Probe Inserted into Ambient Groundwater (Minimum = 20 Minutes): 12:00							
Calibration	Standards (Incl	ude Units): Lo	w:	High 5E-	3		
Time of Ca	libration:			in Well			
Calibration	Results (Includ	e Units): Low:_	Retural	in Well High			
Casing Inne	er Diameter (inc	thes) 2"	Boreho	le Diameter (Inches)			
			Depth to botto	m of well (feet)			
Screened In	nterval, If Know	n (Include Datu	m)				
Depth Mea	sured by Sonde			(Include Units)			
Reference I	Point: Top of	finner PVC casi	ng or BGS, Specif	y:			
Run	Calibration	Up Versus	Winch Speed	Con	nments		
Number	Number	Down	(specify Units)				
	Got	retus	al a a	= 27' BGS	> - Probe		
	Would	d 60	No FU	reher			

Notes:

a/ The greater the difference between the groundwater temperature and the ambient temperature at the surface where the sonde will be calibrated, the longer the sonde should be allowed to equilibrate because the sonde is very sensitive to temperature.



Page 1 of 1

Gu-2

- E-3 Calibration

MAGNETIC SUSCEPTIBILITY MEASUREMENT FORM - SONDE

PROJECT NAME: MILLAFB - 402-43		
Well ID: $U2 - 043$		2/20/11
Sample Collected by: THW/BHW	Date of Collection:	7/01/10
SAMPLING EQUIPMENT		

**Equipment Calibration** Serial Number **Date Calibrated** Equipment/Model 4 55 515 EQUIPMENT DECONTAMINATION: Alconox Wash, Double Rinse, and Isopropyl Alcohol Spray CALIBRATION RESULTS Weather Conditions: Clean & Warm Ambient Air Temperature (°F)<sup>a/</sup>: 82 Groundwater Temperature (<sup>O</sup>F)<sup>a/</sup>: Time Probe Inserted into Ambient Groundwater (Minimum = 20 Minutes): 0905Calibration Standards (Include Units): Low: High Time of Calibration: 09:25 Calibration Results (Include Units): Low: High Casing Inner Diameter (inches) 4<sup>11</sup> Borehole Diameter (Inches) Initial Depth to Water (feet) 41.30 BT Depth to bottom of well (feet) 61.88 RTOC Casing Inner Diameter (inches) 4 1/ Screened Interval, If Known (Include Datum) Depth Measured by Sonde \_\_\_\_\_ (Include Units) Reference Point: Top of inner PVC casing or BGS, Specify:

Run Number	Calibration Number	Up Versus Down	Winch Speed (specify Units)	Comments
	1	Davin	10 ft hui	
	1	INP	(1) ft/mil	$\sim$
		0.1	,	
				i'

Notes: Stickup = 3'

a/ The greater the difference between the groundwater temperature and the ambient temperature at the surface where the sonde will be calibrated, the longer the sonde should be allowed to equilibrate because the sonde is very sensitive to temperature.



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# APPENDIX C DATA COLLECTED USING THE DOWNHOLE MAGNETIC SUSCEPTIBILITY SONDE

				3-Up/Down Average Sonde Data		01U103-Uj	o/Down Ave	erage Sonde Data		Data not used for core data versus son data analysis because no core data
Depth	Elevation	Mag Susc (10e-3 SI		Sonde Data		Depth	Elevation	Mag Susc		
(ft bgs)	feet amsl	units)	(m3/kg)			ft bgs	feet amsl	10e-3 SI un	m3/kg	
	904						904			
3.54	900.46	1.43	8.40E-07			4.45		0.480648	2.83E-07	
3.64	900.36	1.28	7.51E-07	Mean	7.26499E-07	4.55		0.693829		
3.76	900.24	1.13	6.65E-07	Standard Error	2.1558E-08	4.65		0.917049	4.62E-07	
3.86	900.14	1.10	6.44E-07	Median	7.49526E-07	4.75			5.9E-07	
3.96 4.06	900.04 899.94	1.15 1.24	6.78E-07 7.30E-07	Mode Standard Deviation	#N/A 1.01116E-07	4.85 4.95			6.78E-07 7.68E-07	
4.00	899.84	1.24	7.71E-07	Sample Variance	1.02245E-14	4.95			7.93E-07	
4.10	899.75	1.10	6.47E-07	Kurtosis	-0.716024798	5.15			8.12E-07	
4.36	899.65	0.85	4.98E-07	Skewness	-0.352777309	5.25			8.04E-07	
4.46	899.55	0.77	4.51E-07	Range	3.50579E-07	5.35				
4.56	899.45	0.73	4.30E-07	Minimum	5.40591E-07	5.45			8.06E-07	
4.66	899.35	0.83	4.90E-07	Maximum	8.91171E-07	5.55			8.49E-07	
4.76	899.25	1.08	6.38E-07	Sum	1.5983E-05	5.65				
4.86	899.15	1.26	7.41E-07	Count	22	5.75			8.38E-07	
4.96	899.05	1.36	7.99E-07	Confidence Level(95.09	4.48324E-08	5.85			9.06E-07	
5.05	898.95	1.41	8.29E-07			5.95	898.05	1.47332	8.99E-07	
5.15	898.85	1.21	7.12E-07			6.05	897.95	1.42182	8.42E-07	
5.25	898.75	1.18	6.92E-07			6.15			8.46E-07	
5.35	898.65	1.20	7.06E-07			6.25	897.75	1.51648	8.57E-07	
5.45	898.55	1.21	7.11E-07			6.35	897.65	1.57219	8.62E-07	
5.55	898.45	1.30	7.67E-07			6.45	897.55	1.56796	9E-07	
5.65	898.35	1.28	7.54E-07			6.54	897.46	1.41391	8.56E-07	
5.75	898.25	1.16	6.84E-07			6.64	897.36	1.42215	8.21E-07	
5.85	898.15	1.07	6.29E-07			6.74	897.26	1.33314	8.12E-07	
5.95	898.05	1.01	5.91E-07			6.84				
6.05	897.95	1.04	6.11E-07			6.94			8.86E-07	
6.15	897.85	1.07	6.30E-07			7.04			9.06E-07	
6.25	897.75	1.09	6.42E-07			7.14			9.61E-07	
6.35	897.65	1.18	6.93E-07			7.24			9.41E-07	
6.45	897.55	1.23	7.23E-07			7.34				
6.55	897.45	1.16	6.85E-07			7.44				
6.65	897.35	1.11	6.51E-07			7.54			9.98E-07	
6.75	897.25	1.04	6.12E-07			7.64			1E-06	
6.85	897.15 897.05	1.07 1.12	6.30E-07			7.74			8.87E-07	
6.95 7.05	897.05	1.12	6.56E-07 6.77E-07			7.84 7.94			9.51E-07 1.17E-06	
7.15	896.85	1.15	6.82E-07			8.04			1.44E-06	
7.25	896.75	1.15	6.78E-07			8.14			1.57E-06	
7.35	896.65	1.15	7.15E-07			8.24			1.43E-06	
7.45	896.55	1.31	7.73E-07			8.34			1.15E-06	
7.55	896.45	1.37	8.03E-07			8.44			1.19E-06	
7.65	896.36	1.55	9.11E-07			8.54			1.37E-06	
7.75	896.26	1.57	9.25E-07			8.64			1.57E-06	
7.85	896.16	1.53	8.98E-07			8.74			1.47E-06	
7.95	896.06	1.47	8.63E-07			8.84			1.16E-06	
8.05	895.96	1.50	8.84E-07			8.94	895.06	1.58058	9.57E-07	
8.15	895.86	1.51	8.90E-07			9.04	894.96	1.68537	9.51E-07	
8.25	895.76	1.47	8.62E-07			9.14	894.86	1.67791	9.99E-07	
8.34	895.66	1.45	8.53E-07			9.24	894.76	1.71596	1.01E-06	
8.44	895.56	1.49	8.77E-07			9.34	894.66	1.60963	9.44E-07	
8.54	895.46	1.66	9.75E-07			9.44	894.56	1.70857	9.69E-07	
8.64	895.36	1.84	1.08E-06			9.54	894.46	1.80175	1.03E-06	
8.74	895.26	2.16	1.27E-06			9.64			1.15E-06	
8.84	895.16	2.52	1.48E-06			9.74	894.26	2 04164	1.22E-06	

01U106-U	p/Down Averag	-		Data not used for core data versus sonde data analysis because no core data
		Sonde Data	1	
	Elevation	Mag Susc	Mag Susc	
Depth (ft b	feet amsl	10e-3 SI Ur	(m3/kg)	
	897			
3.59	893.41	1.207055	7.1E-07	
3.68	893.32	1.258857	7.41E-07	
3.7775	893.2225	1.23356	7.26E-07	
3.8775	893.1225	1.15295	6.78E-07	
3.9775		1.068423	6.28E-07	
4.0775	892.9225	1.090918	6.42E-07	
4.1775		1.242143	7.31E-07	
4.2775		1.163678	6.85E-07	
4.3775		1.157335	6.81E-07	
4.4775		1.187938	6.99E-07	
4.5775		1.259565	7.41E-07	
4.6775		1.291185	7.6E-07	
4.7775			7.01E-07	
4.8775		1.012743	5.96E-07	
4.9775		1.049575	6.17E-07	
5.0775		1.223816	7.2E-07	
5.1775 5.2775		1.439368 1.38539	8.47E-07 8.15E-07	
5.3775			7.89E-07	
		1.255335	7.38E-07	
5.4775		1.167253	6.87E-07	
5.6775			6.66E-07	
5.7775		1.076042	6.33E-07	
5.875			6.7E-07	
5.975			7.27E-07	
6.075		1.354895	7.97E-07	
6.17		1.305548	7.68E-07	
6.27	890.73	1.202698	7.07E-07	
6.37	890.63	1.161978	6.84E-07	
6.47	890.53	1.292398	7.6E-07	
6.57	890.43	1.402328	8.25E-07	
6.67	890.33	1.399908	8.23E-07	
6.77	890.23	1.255638	7.39E-07	
6.87	890.13	1.08594	6.39E-07	
6.9675	890.0325	1.062202	6.25E-07	
7.0675				
7.1675			9.86E-07	
7.2675			9.88E-07	
7.3675		1.347172	7.92E-07	
7.4675			6.86E-07	
7.5675			6.73E-07	
7.6675		1.391038	8.18E-07	
7.7675		1.589943	9.35E-07	
7.8675 7.9675			8.94E-07 7.94E-07	
7.9675 8.0675			7.94E-07 7.56E-07	
8.1675		1.350325	7.94E-07	
8.1675		1.438048	7.94E-07 8.46E-07	
8.2675		1.514485	8.46E-07 8.91E-07	
8.4675			9.11E-07	
8.5675			1.03E-06	
8.6675		1.909728	1.03L-00	
8.7675			1.36E-06	
8.8675		2.707195	1.59E-06	

			01U10	-Up/Down Average 01U	J103-Up	/Down Ave	erage	
				Sonde Data			Sonde Data	
Depth	Elevation	Mag Susc (10e-3 SI	Mag Susc	Dep	oth	Elevation	Mag Susc	Mag S
(ft bgs)	feet amsl	units)	(m3/kg)	ft bg	gs	feet amsl	10e-3 SI un	m3/kg
8.94	895.06	2.83	1.66E-06		9.83	894.17	2.21544	1.27
9.04	894.96	3.03	1.79E-06		9.93	894.07	2.19798	1.25
9.14	894.86	3.17	1.86E-06		10.03	893.97	2.60981	1.45
9.24	894.76	3.29	1.93E-06		10.13	893.87	2.77126	1.59
9.34	894.66	3.28	1.93E-06		10.23	893.77	2.99766	1.67
9.44	894.56	3.17	1.87E-06		10.33	893.67	3.58869	1.92
9.54	894.46	3.03	1.78E-06		10.43	893.57	4.27703	2.3
9.64	894.36	2.73	1.60E-06		10.53	893.47	4.70673	2.61
9.74	894.26	2.39	1.41E-06		10.63	893.37	4.87341	2.82
9.84	894.16	2.30	1.35E-06		10.73	893.27	4.90963	2.85
9.94	894.06	1.93	1.13E-06		10.83	893.17	5.23835	2.99
10.04	893.96	1.77	1.04E-06		10.93	893.07	5.52384	3.12
10.14	893.86	1.84	1.08E-06		11.03	892.97	5.21488	3.15
10.24	893.76	1.97	1.16E-06		11.13	892.87	4.16713	2.76
10.34	893.66	2.16	1.27E-06		11.23	892.77	3.349	2.2
10.44	893.56	2.44	1.43E-06		11.33	892.67	3.21972	1.94
10.54	893.46	2.63	1.55E-06		11.43	892.57	3.36543	1.95
10.64	893.36	2.44	1.44E-06		11.53	892.47	3.4792	1.99
10.74	893.26	2.17	1.28E-06		11.63	892.37	3.51432	2.02
10.84	893.16	2.12	1.25E-06		11.73	892.27	3.52001	2.08
10.94	893.07	2.12	1.25E-06		11.83	892.17	3.54907	2.09
11.04	892.97	1.96	1.15E-06		11.93	892.07	3.328	2.04
11.14	892.87	2.00	1.18E-06		12.03	891.97	3.14544	1.95
11.24	892.77	1.85	1.09E-06		12.13	891.87	2.74459	1.72
11.34	892.67	1.78	1.05E-06		12.23	891.77	2.84109	1.66
11.44	892.57	1.85	1.09E-06		12.33	891.67	2.67204	1.61
11.54	892.47	1.89	1.11E-06		12.43	891.57	2.37711	1.45
11.63	892.37	1.73	1.02E-06		12.53	891.47	2.26109	1.37
11.73	892.27	1.62	9.54E-07		12.63	891.37	2.19227	1.31
11.83	892.17	1.79	1.05E-06		12.73	891.27	2.24014	1.29
11.93	892.07	2.07	1.22E-06		12.83	891.17	2.28678	1.34
12.03	891.97	2.07	1.22E-06		12.93	891.07	2.35715	1.34
12.13	891.87	1.86	1.09E-06		13.03	890.97	2.3284	1.35
12.23	891.77	1.69	9.95E-07		13.12	890.88	2.65483	1.44
12.33	891.67	1.67	9.85E-07		13.22	890.78	2.67784	1.52
12.43	891.57	1.98	1.16E-06		13.32	890.68	2.56585	1.52
12.53	891.47	2.19	1.29E-06		13.42	890.58	2.45715	1.49
12.63	891.37	2.25	1.32E-06		13.52	890.48	2.69079	1.49
12.73	891.27	2.30	1.35E-06		13.62	890.38	2.96561	1.67
12.83	891.17	1.89	1.11E-06		13.72	890.28	3.02152	1.77
12.93	891.07	1.69	9.95E-07		13.82	890.18	2.985	1.81
13.03	890.97	1.79	1.05E-06		13.92	890.08	2.99111	1.78
13.13	890.87	1.93	1.14E-06		14.02	889.98	3.14266	1.83
13.23	890.77	2.24	1.32E-06		14.12	889.88	2.84281	1.77
13.33	890.67	2.33	1.37E-06		14.22	889.78	2.96113	1.79
13.43	890.57	2.04	1.20E-06		14.32	889.68	2.70255	1.66
13.53	890.47	1.82	1.07E-06		14.42	889.58	2.60823	1.59
13.63	890.37	1.71	1.01E-06		14.52	889.48	2.43819	1.5
13.73	890.27	1.76	1.04E-06		14.62	889.38	2.44788	1.39
13.83	890.17	1.79	1.05E-06		14.72	889.28	2.65017	1.53
13.93	890.07	2.00	1.18E-06		14.82	889.18	2.73359	1.59
14.03	889.97	2.10	1.23E-06		14.92	889.08	2.76265	1.62
14.13	889.87	2.03	1.19E-06		15.02	888.98	2.85017	1.65
14.23	889.78	1.96	1.15E-06		15.12	888.88		1.63
14.33	889.68	1.95	1.15E-06		15.22	888.78		1.67

Data not used for core data versus sonde data analysis because no core data	01U106-Up/Down #	lverage		Data not used for core data versus sonde data analysis because no core data
		Sonde Data		
	Elevation	n Mag Susc N	/lag Susc	
	Depth (ft b feet ams	l 10e-3 SI Ur (i	m3/kg)	
		.0325 2.939788	1.73E-06	
		.9325 2.97879	1.75E-06	
			1.74E-06	
			1.72E-06	
			1.67E-06 1.73E-06	
		.5375 2.93278 87.44 3.404518	2E-06	
			2.49E-06	
		87.24 5.098695	3E-06	
			3.35E-06	
	9.96 8	87.04 6.026765	3.55E-06	
	10.06 8	86.94 6.15785	3.62E-06	
	10.16 8	86.84 6.397345	3.76E-06	
			3.72E-06	
			3.44E-06	
			3.05E-06	
			2.73E-06	
		.3425 4.135508 .2425 3.741238	2.43E-06	
		.1425 3.40371	2.2E-06 2E-06	
		.0425 3.062145	1.8E-06	
			1.78E-06	
			1.76E-06	
			1.75E-06	
	11.3575 885	.6425 2.90165	1.71E-06	
	11.4575 885	.5425 3.02226	1.78E-06	
	11.5575 885	.4425 3.269503	1.92E-06	
			1.94E-06	
			1.92E-06	
			1.87E-06	
			1.94E-06	
		.9425 3.425793 .8425 3.570158	2.02E-06 2.1E-06	
			2.05E-06	
			1.99E-06	
			2.02E-06	
			2.11E-06	
			2.18E-06	
	12.7525 884	.2475 3.78951	2.23E-06	
	12.85 8	84.15 3.848253	2.26E-06	
			2.22E-06	
			2.26E-06	
			2.12E-06	
			1.97E-06	
		83.65 3.237218 83.55 3.286855	1.9E-06 1.93E-06	
			2.03E-06	
			2.16E-06	
			2.05E-06	
		.1525 3.139878	1.85E-06	
	13.9475 883	.0525 3.051408	1.79E-06	
	14.0475 882	.9525 3.082045	1.81E-06	
	14.1475 882	.8525 3.337795	1.96E-06	
			2.11E-06	
	14.3475 882	.6525 3.952903	2.33E-06	

			011110	Up/Down Average	011102-11-	/Down Ave	rage	
			01010	onde Data	010103-01	DOWINAVE	Sonde Data	
epth	Elevation	Mag Susc (10e-3 SI	Mag Susc		Depth	Elevation	Mag Susc	
t bgs)	feet amsl	units)	(m3/kg)		ft bgs	feet amsl	10e-3 SI un	m3/kg
.43	889.58	1.99	1.17E-06		15.32	888.68	2.67412	1.6
.53	889.48	2.01	1.18E-06		15.42	888.58	2.69669	1.58
1.63	889.38	2.02	1.19E-06		15.52	888.48	2.61423	1.55
1.73	889.28	1.96	1.15E-06		15.62	888.38	2.62533	1.53
4.83	889.18	1.87	1.10E-06		15.72	888.28	2.47808	1.47
4.93	889.08	1.89	1.11E-06		15.82	888.18		1.5
5.02	888.98	2.01	1.18E-06		15.92	888.08		1.59
5.12	888.88	2.01	1.19E-06		16.02	887.98		1.55
5.22	888.78	2.02	1.19E-06		16.12	887.88		1.54
5.32	888.68	1.96	1.15E-06		16.22	887.78		1.65
5.42	888.58	1.95	1.15E-06		16.32	887.68		1.58
5.52	888.48	1.98	1.16E-06		16.42	887.58		1.51
5.62	888.38	2.04	1.20E-06		16.51	887.49		1.62
5.72	888.28	2.03	1.19E-06		16.61	887.39		1.51
5.82	888.18	1.85	1.09E-06		16.71	887.29		1.42
5.92	888.08	1.84	1.08E-06		16.81	887.19		1.49
6.02	887.98	1.87	1.10E-06		16.91	887.09		1.63
6.12	887.88	1.93	1.13E-06		17.01	886.99		1.72
6.22	887.78	1.89	1.11E-06		17.11	886.89		1.76
6.32	887.68	1.94	1.14E-06		17.21	886.79		1.83
6.42	887.58	1.99	1.17E-06		17.31	886.69		1.86
5.52	887.48	2.05	1.21E-06		17.41	886.59		1.92
5.62	887.38	2.06	1.21E-06		17.51	886.49		2.08
5.72	887.28	2.08	1.22E-06		17.61	886.39		2.13
5.82	887.18	1.89	1.11E-06		17.71	886.29		2.12
6.92	887.08	1.73	1.02E-06		17.81	886.19		2.3
7.02	886.98	1.62	9.53E-07		17.91	886.09		2.42
7.12	886.88	1.54	9.05E-07		18.01	885.99		2.4
7.22	886.78	1.54	9.06E-07		18.11	885.89		2.51
7.32	886.68	1.60	9.39E-07		18.21	885.79		2.6
7.42	886.58	1.73	1.02E-06		18.31	885.69		2.52
7.52	886.49	1.66	9.75E-07		18.41	885.59		2.55
7.62	886.39	1.55	9.12E-07		18.51	885.49		2.5
7.72	886.29	1.52	8.95E-07		18.61	885.39		2.36
7.82	886.19	1.51	8.89E-07		18.71	885.29		2.14
7.92	886.09	1.43	8.42E-07		18.81	885.19		1.90
8.02	885.99	1.31	7.68E-07		18.91	885.09		1.92
8.12	885.89	1.22	7.18E-07		19.01	884.99		1.94
8.22	885.79	1.10	6.48E-07		19.11	884.89		1.86
8.31	885.69	1.17	6.88E-07		19.21	884.79		1.79
8.41	885.59	1.25	7.35E-07		19.31	884.69		1.83
8.51 8.61	885.49 885.39	1.38 1.34	8.10E-07 7.90E-07		19.41 19.51	884.59 884.49		1.93
								1.89
8.71	885.29	1.30	7.64E-07		19.61	884.39		1.77
8.81	885.19	1.30	7.65E-07		19.71	884.29		1.79
8.91	885.09	1.30	7.65E-07		19.8 19.9	884.2		1.7
9.01	884.99	1.18	6.96E-07				2.80979	1.67
9.11	884.89	1.13	6.66E-07		20.0		2.75557	1.62
9.21	884.79	1.02	6.00E-07		20.1		2.53151	1.56
9.31	884.69	0.96	5.62E-07		20.2			1.33
9.41	884.59	0.92	5.41E-07		20.3	883.7		1.09
9.51	884.49	0.95	5.60E-07		20.4	883.6		9.9
9.61	884.39	1.14	6.73E-07		20.5	883.5		8.1
9.71	884.29	1.37	8.07E-07		20.6	883.4	1.57533	8.02
9.81	884.19	1.40	8.24E-07		20.7	883.3	2.23732	1 11

Data not used for core data versus sonde				
data analysis because no core data	01U106-U	o/Down Averag	ge	
			Sonde Data	a
		Elevation	Mag Susc	Mag Susc
	Depth (ft b	feet amsl	10e-3 SI Ur	(m3/kg)
	14.4475	882.5525		2.46E-06
	14.5475		4.402348	2.59E-06
	14.6475		4.701538	2.77E-06
	14.7475	882.2525		2.77E-06
	14.8475	882.1525	4.575168	2.69E-06
	14.9475	882.0525	4.401035	2.59E-06
	15.0475	881.9525	4.210525	2.48E-06
	15.1475	881.8525	3.905058	2.3E-06
	15.2475	881.7525	3.691598	2.17E-06
	15.3475	881.6525	3.596823	2.12E-06
	15.4475	881.5525	3.472525	2.04E-06
	15.5475	881.4525	3.353383	1.97E-06
	15.6475	881.3525	3.3768	1.99E-06
	15.7475		3.569745	2.1E-06
	15.845		3.460983	
	15.945		3.208193	
	16.045		3.088508	
	16.14		3.210473	
	16.24	880.76		
	16.34	880.66		
	16.44	880.56		
	16.54		2.517965	1.48E-06
	16.64	880.36	2.29173 2.420195	1.35E-06
	16.74 16.84		2.532918	
	16.9375		2.519855	1.49E-00
	17.0375	879.9625		
	17.1375	879.8625		
	17.2375		2.203953	1.3E-06
	17.3375	879.6625		1.33E-06
	17.4375		2.249393	1.32E-06
	17.5375	879.4625		
	17.6375	879.3625	2.033548	1.2E-06
	17.7375	879.2625	2.0178	1.19E-06
	17.8375	879.1625	2.319903	1.36E-06
	17.9375	879.0625	2.53814	1.49E-06
	18.0375	878.9625	2.58663	1.52E-06
	18.1375	878.8625	2.407258	1.42E-06
	18.2375	878.7625	2.209005	1.3E-06
	18.3375	878.6625	2.102103	1.24E-06
	18.4375	878.5625	2.092245	1.23E-06
	18.5375	878.4625	2.140738	1.26E-06
	18.6375		2.014035	1.18E-06
	18.7375		1.920538	1.13E-06
	18.8375		1.987418	1.17E-06
	18.9375		1.994328	1.17E-06
	19.0375		1.900065	1.12E-06
	19.135		1.832578	1.08E-06
	19.235		1.849745	1.09E-06
	19.335		1.726545	1.02E-06
	19.4325		1.693728	9.96E-07
	19.53	877.47	1.746948	1.03E-06
	19.63	877.37	1.770128	1.04E-06
	19.73	877.27		1.11E-06
	19.83	877.17	2.143335	1.26E-06



Data not used for core data versus sonde data

analysis because no core data

			01U108-Up/Down Average Sonde Data	01U103-L	p/Down Ave	-	_
Depth	Elevation	Mag Susc		Depth	Elevation	Sonde Data Mag Susc	
it (a a a )	factored	(10e-3 SI units)	(	ft has	factorial	10 - 2 61	
t bgs) 19.91	feet amsl 884.09	1.48	(m3/kg) 8.70E-07	ft bgs 20.	feet amsl 8 883.2	10e-3 SI un 2.51899	1.41E-
20.01	883.99	1.48	8.91E-07	20.			1.41L-
20.11	883.89	1.47	8.66E-07	20.			1.67E-
0.21	883.79	1.47	8.68E-07	21.			1.71E
0.31	883.69	1.41	8.32E-07	21.			1.93E
0.41	883.59	1.37	8.04E-07	21.			2.11E
0.51	883.49	1.43	8.39E-07	21.			2.35E
0.61	883.39	1.53	9.00E-07	21.		4.22991	2.44E
0.71	883.29	1.47	8.65E-07	21.	5 882.4	3.88979	2.41E
0.81	883.19	1.45	8.54E-07	21.	7 882.3	3.88912	2.28E
0.91	883.10	1.50	8.84E-07	21.	8 882.2	3.47377	2.14E
1.01	883.00	1.51	8.86E-07	21.			1.86E
1.11	882.90	1.56	9.19E-07	2			1.498
1.21	882.80	1.49	8.76E-07	22.		2.10066	1.28
1.31	882.70	1.41	8.31E-07	22.			1.16
1.41	882.60	1.44	8.50E-07	22.			9.88
1.51 1.61	882.50 882.40	1.44 1.36	8.45E-07 7.97E-07	22. 22.		1.71899 1.64889	9.97E 9.48E
1.01	882.40 882.30	1.36	7.33E-07	22.6	881.3		9.48
1.70	882.30	1.25	6.80E-07	22.0	881.4		1.08
1.90	882.20	1.10	7.45E-07	22.7	881.2		1.08
2.00	882.00	1.27	7.64E-07	22.8	881.1		1.22
2.10	881.90	1.30	7.31E-07	23	881		1.22
2.20	881.80	1.24	7.23E-07	23.09	880.91		1.16
2.30	881.70	1.23	7.23E-07	23.07			1.26
2.40	881.60	1.25	7.44E-07	23.2		2.49341	1.47
2.50	881.50	1.32	7.77E-07	23.3			1.56
2.60	881.40	1.37	8.07E-07	23.4	9 880.51	3.04569	1.73
2.70	881.30	1.30	7.64E-07	23.5	9 880.41	2.78508	1.72
2.80	881.20	1.29	7.60E-07	23.6	9 880.31	2.73985	1.66
2.90	881.10	1.35	7.92E-07	23.7	9 880.21	2.9866	1.67
3.00	881.00	1.34	7.86E-07	23.8			1.81
3.10	880.90	1.25	7.36E-07	23.9			1.87
3.20	880.80	1.24	7.31E-07	24.0			1.95
3.30	880.70	1.75	1.03E-06	24.1			1.89
3.40 3.50	880.60 880.50	2.54 2.93	1.49E-06 1.73E-06	24.2 24.3			1.66I 1.54I
3.50 3.60	880.50	2.93	1.79E-06	24.3			1.54
3.70	880.40	3.11	1.83E-06	24.4			1.51
3.80	880.20	3.32	1.95E-06	24.6			1.40E
				24.7			1.32E
				24.8			1.24E
				24.9	9 879.01	2.07776	1.27
				25.0	9 878.91	2.2094	1.278
				25.1	9 878.81	2.51304	1.376
				25.2			1.58
				25.3			1.528
				25.4			1.46
				25.5			1.78
			core samples was	25.6			2.31
tained	trom sample	es collected	from 18 to 20 ft bgs	25.7			2.31
				25.8			2.11
				25.9 26.0			1.72
				26.0			1.020

Ave	rage		Data not used for core data versus sonde data analysis because no core data	01U106-
	Sonde Data	a		
n	Mag Susc			
	0	0		
sl	10e-3 SI un	m3/kg		Depth (f
3.2	2.51899	1.41E-06		19.9
3.1	2.67494	1.5E-06		20.
383		1.67E-06		20.:
2.9		1.71E-06		20.
2.8		1.93E-06		20.32
2.7	3.84495	2.11E-06		20.42
2.6	4.13059	2.35E-06		20.52
2.5	4.22991	2.44E-06		20.62
2.4	3.88979	2.41E-06		20.72
2.3	3.88912	2.28E-06		20.82
2.2	3.47377	2.14E-06		20.92
2.1	2.91726	1.86E-06		21.02
382		1.49E-06		21.12
1.9		1.28E-06		21.22
1.8		1.16E-06		21.32
1.7	1.59202	9.88E-07		21.42
1.6		9.97E-07		21.52
1.5		9.48E-07		21.62
1.4				21.72
1.3		1.08E-06		21.82
1.2		1.2E-06		21.92
1.1	2.15377	1.22E-06		22.02
881	2.04817	1.2E-06		22.12
.91	2.0514	1.16E-06		22.22
.81				22.32
.71				22.4
.61		1.56E-06		22.5
.51		1.73E-06		22.6
.41		1.72E-06		22.72
.31		1.66E-06		22.
.21		1.67E-06		22.
.11		1.81E-06		23.
.01				23.
.91		1.95E-06		23. 23.
.81 .71		1.89E-06 1.66E-06		23.
.61		1.54E-06		23.
.51		1.6E-06		23.61
.41		1.51E-06		23.71
.31		1.40E-06		23.81
.21		1.32E-06		23.91
.11		1.24E-06		24.0
.01		1.27E-06		24.0
.91		1.27E-06		
.81		1.37E-06		
.71		1.58E-06		
.61		1.52E-06		
.51		1.46E-06		
.41				
.31		2.3E-06		
.21		2.31E-06		
.11		2.1E-06		

)1U106-Ur	)/Down Averag	7e		Data not used for core data versus sonde dat analysis because no core data
	, 2011, 10010	Sonde Dat	a	
Elevation Mag Susc Mag Susc				
Depth (ft b	feet amsl	10e-3 SI Ur	(m3/kg)	
19.93	877.07	2.2667	1.33E-06	
20.03	876.97	2.14875	1.26E-06	
20.13	876.87	1.794165	1.06E-06	
20.23	876.77	1.778	1.05E-06	
20.3275	876.6725	1.938043	1.14E-06	
20.4275	876.5725	2.154988	1.27E-06	
20.5275	876.4725	2.198868	1.29E-06	
20.6275	876.3725	2.073553	1.22E-06	
20.7275	876.2725	1.861893	1.1E-06	
20.8275	876.1725	1.82471	1.07E-06	
20.9275	876.0725	1.872613	1.1E-06	
21.0275	875.9725	1.872003	1.1E-06	
21.1275	875.8725	1.782183	1.05E-06	
21.2275	875.7725	1.603388	9.43E-07	
21.3275	875.6725	1.454033	8.55E-07	
21.4275	875.5725	1.308413	7.7E-07	
21.5275	875.4725	1.209915	7.12E-07	
21.6275	875.3725	1.368525	8.05E-07	
21.7275	875.2725	1.587058	9.34E-07	
21.8275	875.1725	1.77742	1.05E-06	
21.9275	875.0725	1.84797	1.09E-06	
22.0275	874.9725	1.873	1.1E-06	
22.1275	874.8725	2.077095	1.22E-06	
22.2275	874.7725	2.53255	1.49E-06	
22.3275	874.6725	2.871793	1.69E-06	
22.425	874.575	2.870698	1.69E-06	
22.525	874.475	2.812058	1.65E-06	
22.625	874.375	2.97499	1.75E-06	
22.7225	874.2775	3.403308	2E-06	
22.82	874.18	3.784135	2.23E-06	
22.92	874.08	3.792553	2.23E-06	
23.02	873.98	3.6507	2.15E-06	
23.12	873.88	3.309258	1.95E-06	
23.22	873.78	3.222525	1.9E-06	
23.32	873.68	3.058803	1.8E-06	
23.42	873.58	2.93435	1.73E-06	
23.52	873.48	2.90729	1.71E-06	
23.6175	873.3825	2.962745	1.74E-06	
23.7175	873.2825	3.018993	1.78E-06	
23.8175	873.1825	2.976043	1.75E-06	
23.9175	873.0825	2.4902	1.46E-06	
24.005	872,995	2.400035	1.41E-06	



			01U108
Depth	Elevation	Mag Susc	Mag Susc
Deptil	2.000	(10e-3 SI	ining suse
(ft bgs)	feet amsl	units)	(m3/kg)

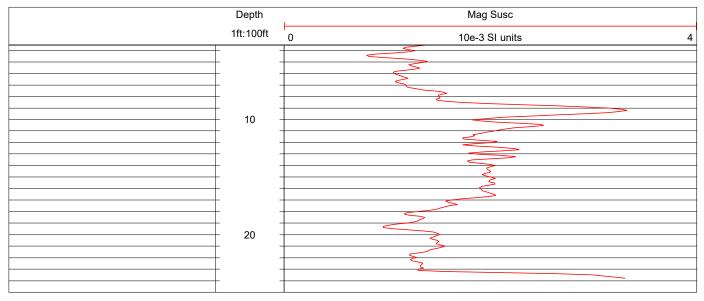
01U103-Up	)/Down Ave	rage		Data not used for core data versus sonde data analysis because no core data
		Sonde Dat	a	-
Depth	Elevation	Mag Susc	Mag Susc	
ft bgs	feet amsl	10e-3 SI ur	nm3/kg	
26.29	877.71	2.47884	1.61E-06	
26.39	877.61	2.58309	1.51E-06	
26.48	877.52	2.79943	1.58E-06	
26.58	877.42	2.69549	1.62E-06	
26.68	877.32	2.61643	1.55E-06	
26.78	877.22	2.86318	1.61E-06	
26.88	877.12	3.01221	1.7E-06	
26.98	877.02	2.89905	1.75E-06	
27.08	876.92	2.2708	1.48E-06	
27.18	876.82	0.945118	9.04E-07	

01U106-Up/Down Aver	rage	Data not used for core data versus sonde data analysis because no core data
	Sonde Data	
Elevation	Mag Susc Mag Susc	
Depth (ft b feet amsl	10e-3 SI Ur (m3/kg)	

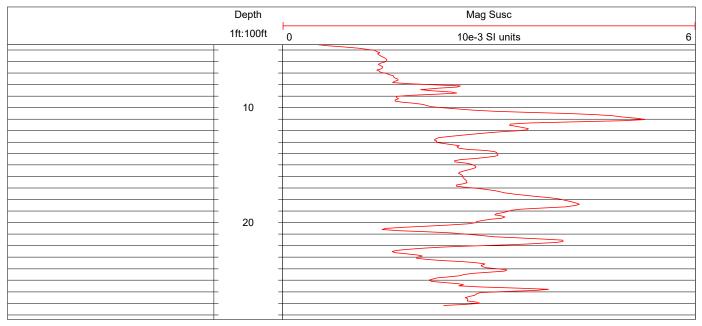
		TOOL HMA-453-S CALIBRATION DATE/TIME 5/31/16 12:15 CALIBRATION STANDARDS 0 and 5E-3 SI Units CALIBRATION RESULTS Not Recorded
PROJECT	ESTCP 201584	REMARKS
LOCATION	Former Twin Cities Army Ammunition Plant	
WELL	O1U108	
LOGGER	THW	Tool bottomed out at 23.82 feet BGS.
DATE	May 31, 2016	

	epth	Mag Susc
1ft	:100ft	0 10e-3 SI units 4
	10	
	20	

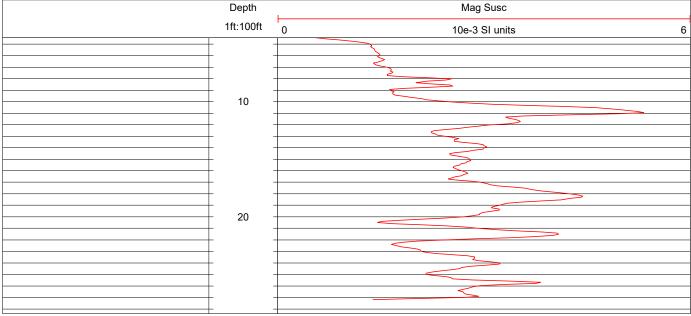
		TOOLHMA-453-SCALIBRATION DATE/TIME5/31/1612:15CALIBRATION STANDARDS0 and 5E-3 SI UnitsCALIBRATION RESULTSNot Recorded
PROJECT	ESTCP 201584	REMARKS
LOCATION	Former Twin Cities Army Ammunition Plant	
WELL	01U108	
LOGGER	THW	Tool bottomed out at 23.82 feet BGS
DATE	5/31/16	



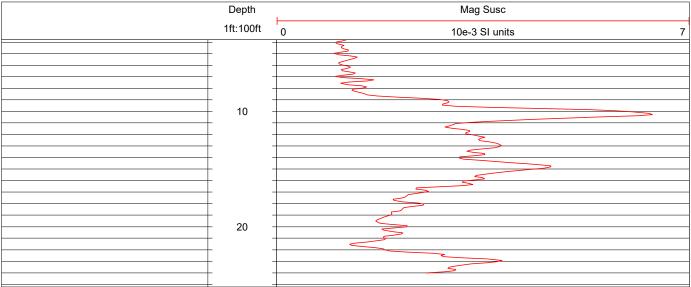
		TOOL HMA-453-S CALIBRATION DATE/TIME 6/2/16 - 12:30 CALIBRATION STANDARDS 0 and 5E-3 SI Units CALIBRATION RESULTS Zero = 60.6, 5E-3 = 1160.53 cps
PROJECT	ESTCP ER-201584	REMARKS
LOCATION	TCAAP, Shoreview, MN	
WELL	O1U-103 Down - Calib 1	
LOGGER	Todd Wiedemeier	
DATE	June 2, 2016	



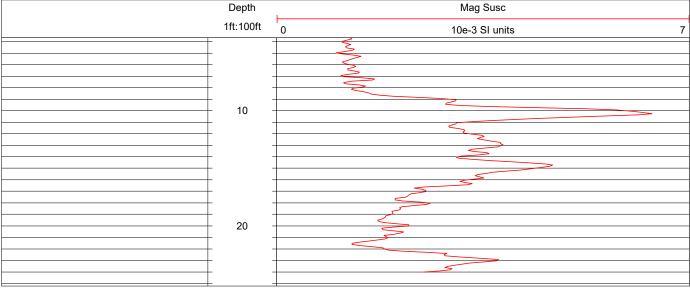
		TOOLHMA-453-SCALIBRATION DATE/TIME6/2/16 - 12:30CALIBRATION STANDARDS0 and 5E-3 SI UnitsCALIBRATION RESULTSZero = 60.6, 5E-3 = 1160.53 cps
PROJECT	ESTCP ER-201584	REMARKS
LOCATION	TCAAP, Shoreview, MN	
WELL	O1U-103 Up Calibration 1	
LOGGER	Todd Wiedemeier	
DATE	June	
	Denth	Mag Suga



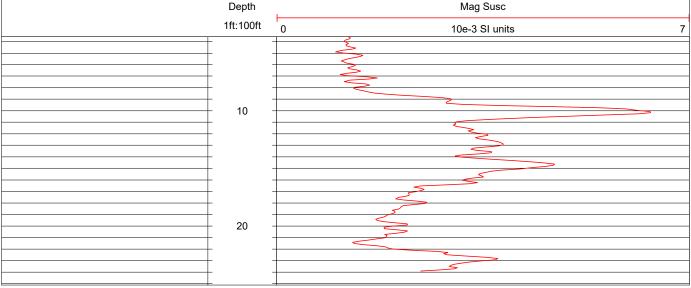
		TOOL HMA-453-S CALIBRATION DATE/TIME 6/2/16 14:50 CALIBRATION STANDARDS 0 and 5E-3 SI Units
& ASSO		CALIBRATION RESULTS $0 = 56.91$ , 5E-3 = 1187.23 cps
PROJECT	ESTCP ER-201584	REMARKS
LOCATION	TCAAP, Shoreview, MN	
WELL	O1U-106 - Down - Run 1 - Calib 1	
LOGGER	Todd Wiedemeier	
DATE	June 2, 2016	
·		



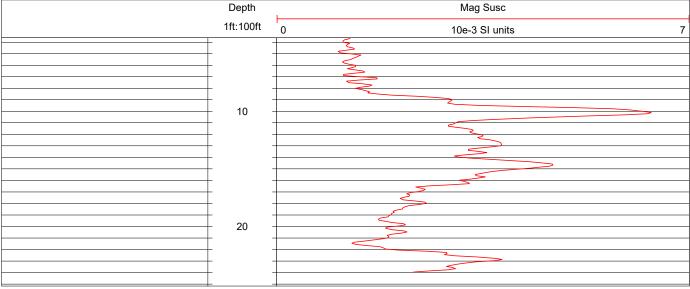
		TOOLHMA-453-SCALIBRATION DATE/TIME6/2/16 - 14:50CALIBRATION STANDARDS0 and 5E-3 SI UnitsCALIBRATION RESULTS0 = 56.91, 5E-3 = 1187.23 cps
PROJECT LOCATION WELL LOGGER DATE	ESTCP ER-201184 TCAAP, Shoreview, MN O1U-106 - Down - Run 2 - Calib 1 Todd Wiedemeier June 2, 2016	REMARKS
	Denth	Mag Suga



		TOOLHMA-453-SCALIBRATION DATE/TIME6/2/16 14:50CALIBRATION STANDARDS0 and 5E-3 SI UnitsCALIBRATION RESULTS0 = 56.91, 5E-3 = 1187.23 cps
PROJECT LOCATION WELL LOGGER DATE	ESTCP ER-201584 TCAAP, Shoreview, MN O1U-106 - Up - Run 1 - Calib 1 Todd Wiedemeier June 2, 2016	REMARKS
	Depth	Mag Susc



		TOOLHMA-453-SCALIBRATION DATE/TIME $6/2/16 - 14:50$ CALIBRATION STANDARDS0 and 5E-3 SI UnitsCALIBRATION RESULTS $0 = 56.91, 5E-3 = 1187.23 \text{ cps}$
PROJECT LOCATION WELL LOGGER DATE	ESTCP ER-201184 TCAAP, Shoreview, MN O1U-106 - Up - Run 2 - Calib 1 Todd Wiedemeier June 2, 2016	REMARKS
	Depth	Mag Susc



					MW-02-0	30 Run 2 Up	and Down			
Top of riser elevation (feet)	MV	V-02-017 Rur	n 2 Up and Down - Average	Top of riser elevation (feet)		Average				
250.44				229.55						
Elevation	Depth	Mag Susc	Mag Susc		Depth	Mag Susc	Mag Susc			
		10e-3 SI				10e-3 SI				
feet amsl	ft bgs	units	m3/kg	feet amsl	ft bgs	units	m3/kg			
241.85	8.59	2.08	1.23E-06	226.02	3.53	2.69	1.58E-06	Mean 190 to 220 feet		1.2E-06
241.75	8.69	2.07	1.22E-06	225.92	3.63	2.62	1.54E-06	Sample Standard Deviation		3.7E-07
241.65	8.79	2.01	1.18E-06	225.81	3.74	2.51	1.48E-06			
241.55	8.89	2.11	1.24E-06	225.71	3.84	2.34	1.37E-06	Mean	1.18151E-06	
241.45	8.99	2.04	1.20E-06	225.61	3.94	2.27	1.34E-06	Standard Error	2.15102E-08	
241.35	9.09	2.03	1.19E-06	225.51	4.04	2.24	1.31E-06	Median	1.07027E-06	
241.25	9.19	2.01	1.18E-06	225.415	4.135	2.18	1.29E-06	Mode Standard Deviation	#N/A	
241.15	9.29	2.07	1.22E-06	225.315	4.235	2.17	1.28E-06	Standard Deviation	3.73807E-07	
241.05	9.39	2.18	1.28E-06	225.215	4.335	2.13	1.25E-06	Sample Variance	1.39732E-13	
240.95	9.49	2.04	1.20E-06	225.115	4.435	2.25	1.32E-06	Kurtosis	-0.162552451	
240.85	9.59	1.90	1.11E-06	225.015	4.535	2.17	1.28E-06	Skewness	0.743357621	
240.75	9.69	1.88	1.11E-06	224.915	4.635	2.27	1.34E-06	Range	1.66179E-06	
240.65	9.79	1.87	1.10E-06	224.815	4.735	2.28	1.34E-06	Minimum	6.0655E-07	
240.56	9.88	1.77	1.04E-06	224.715	4.835	2.33	1.37E-06	Maximum	2.26834E-06	
240.46	9.98	1.74	1.02E-06	224.615	4.935	2.39	1.40E-06	Sum	0.000356815	
	10.085	1.94	1.14E-06	224.515	5.035	2.29	1.35E-06	Count	302	
240.255		1.75 1.85	1.03E-06	224.415	5.135	2.26	1.33E-06	Confidence Level(95.0%)	4.23294E-08	
240.155		1.85	1.09E-06	224.315	5.235 5.335	2.19	1.29E-06			
240.055 239.955	10.385	1.95	1.13E-06 1.17E-06	224.215 224.115	5.335 5.435	2.05 2.07	1.21E-06 1.22E-06			
239.855		2.04	1.20E-06	224.115	5.535	2.07	1.22E-00 1.25E-06			
239.755		2.04	1.23E-06	223.915	5.635	2.12	1.26E-06			
239.655		2.10	1.23E-06	223.815	5.735	2.14	1.23E-06			
239.555		2.09	1.24E-06	223.715	5.835	1.95	1.15E-06			
239.455		2.10	1.20E-06	223.615	5.935	1.82	1.07E-06			
239.355		1.98	1.17E-06	223.515	6.035	1.85	1.09E-06			
239.255		1.81	1.06E-06	223.415	6.135	1.86	1.09E-06			
239.155		1.64	9.64E-07	223.315	6.235	1.84	1.08E-06			
239.055		1.59	9.38E-07	223.215	6.335	1.87	1.10E-06			
238.955		1.53	9.01E-07	223.115	6.435	1.93	1.13E-06			
238.855		1.51	8.91E-07	223.015	6.535	1.95	1.15E-06			
238.755		1.60	9.39E-07	222.915	6.635	1.96	1.15E-06			
238.655		1.81	1.06E-06	222.815	6.735	2.07	1.22E-06			
238.555		2.00	1.18E-06	222.715	6.835	2.06	1.21E-06			
238.455		2.35	1.38E-06	222.62	6.93	2.27	1.33E-06			
238.355		2.57	1.51E-06	222.52	7.03	2.30	1.36E-06			
238.255		2.85	1.67E-06	222.42	7.13	2.31	1.36E-06			
238.155		2.92	1.72E-06	222.32	7.23	2.24	1.32E-06			
238.055	12.385	2.75	1.62E-06	222.22	7.33	2.13	1.25E-06			
237.955		2.45	1.44E-06	222.12	7.43	2.01	1.18E-06			
237.855	12.585	2.06	1.21E-06	222.025	7.525	1.91	1.12E-06			
237.755	12.685	1.51	8.91E-07	221.925	7.625	1.94	1.14E-06			
237.655	12.785	1.11	6.54E-07	221.825	7.725	1.90	1.12E-06			



					MW-02-0	)30 Run 2 Up	and Down
Top of riser elevation (feet)	MW	/-02-017 Rui	n 2 Up and Down - Average	Top of riser elevation (feet)		Average	
250.44				229.55			
Elevation	Depth	Mag Susc 10e-3 SI	Mag Susc		Depth	Mag Susc 10e-3 SI	Mag Susc
feet amsl	ft bgs	units	m3/kg	feet amsl	ft bgs	units	m3/kg
237.555	12.885	0.84	4.95E-07	221.725	7.825	2.01	1.18E-06
237.46	12.98	0.77	4.51E-07	221.625	7.925	2.17	1.28E-06
237.36	13.08	0.83	4.90E-07	221.525	8.025	2.22	1.30E-06
237.26	13.18	0.86	5.06E-07	221.425	8.125	2.12	1.25E-06
237.165	13.275	0.89	5.22E-07	221.325	8.225	2.18	1.28E-06
237.065	13.375	0.99	5.82E-07	221.225	8.325	2.06	1.21E-06
236.965	13.475	1.07	6.28E-07	221.125	8.425	1.94	1.14E-06
236.865	13.575	1.28	7.54E-07	221.025	8.525	1.68	9.88E-07
236.765	13.675	1.54	9.05E-07	220.925	8.625	1.58	9.31E-07
236.665	13.775	1.73	1.01E-06	220.825	8.725	1.47	8.64E-07
236.565	13.875	1.89	1.11E-06	220.725	8.825	1.50	8.84E-07
236.465	13.975	1.99	1.17E-06	220.625	8.925	1.60	9.42E-07
236.365	14.075	1.95	1.15E-06	220.525	9.025	1.68	9.88E-07
236.265	14.175	1.90	1.12E-06	220.425	9.125	1.69	9.95E-07
236.165	14.275	1.83	1.08E-06	220.325	9.225	1.77	1.04E-06
236.065	14.375	1.75	1.03E-06	220.225	9.325	1.75	1.03E-06
235.965	14.475	1.74	1.02E-06	220.125	9.425	1.72	1.01E-06
235.865	14.575	1.74	1.02E-06	220.025	9.525	1.72	1.01E-06
235.765	14.675	1.64	9.65E-07	219.925	9.625	1.66	9.77E-07
235.665	14.775	1.69	9.96E-07	219.825	9.725	1.61	9.47E-07
235.565	14.875	1.63	9.58E-07	219.725	9.825	1.57	9.24E-07
235.465	14.975	1.59	9.37E-07	219.625	9.925	1.61	9.45E-07
235.365	15.075	1.49	8.78E-07	219.525	10.025	1.68	9.86E-07
235.265	15.175	1.39	8.20E-07	219.425	10.125	1.72	1.01E-06
235.165	15.275	1.38	8.10E-07	219.33	10.22	1.79	1.05E-06
235.065	15.375	1.34	7.88E-07	219.23	10.32	1.80	1.06E-06
234.965	15.475	1.30	7.65E-07	219.13	10.42	1.80	1.06E-06
234.865	15.575	1.32	7.78E-07	219.03	10.52	1.74	1.02E-06
234.765	15.675	1.39	8.16E-07	218.93	10.62	1.82	1.07E-06
234.665	15.775	1.40	8.22E-07	218.83	10.72	1.80	1.06E-06
234.565	15.875	1.43	8.39E-07	218.735	10.815	1.80	1.06E-06
234.465	15.975	1.38	8.14E-07	218.635	10.915	1.72	1.01E-06
234.365	16.075	1.30	7.66E-07	218.535	11.015	1.69	9.93E-07
234.265	16.175	1.29	7.58E-07	218.435	11.115	1.67	9.80E-07
234.165	16.275	1.29	7.57E-07	218.335	11.215	1.72	1.01E-06
234.07	16.37	1.27	7.49E-07	218.235	11.315	1.73	1.02E-06
233.97	16.47	1.31	7.72E-07	218.135	11.415	1.82	1.07E-06
233.875	16.565	1.28	7.51E-07	218.035	11.515	1.94	1.14E-06
233.075	16.665	1.37	8.05E-07	217.935	11.615	2.03	1.20E-06
233.775	16.765	1.57	9.02E-07	217.835	11.715	1.99	1.17E-06
233.075	16.865	1.53	8.92E-07	217.835	11.815	1.90	1.17E-00
233.373	16.965	1.70	1.00E-06	217.635	11.915	1.90	1.06E-06
233.475	17.065	1.70	1.05E-06	217.535	12.015	1.71	1.00E-00
233.375	17.005	1./3	1.052.00	217.335	12.015	1./1	1.001-00



					MW-02-0	30 Run 2 Uj	o and Down
Top of riser elevation (feet) 250.44	MV	V-02-017 Ru	n 2 Up and Down - Average	Top of riser elevation (feet) 229.55		Average	
Elevation	Depth	Mag Susc 10e-3 SI	Mag Susc		Depth	Mag Susc 10e-3 SI	Mag Susc
feet amsl	ft bgs	units	m3/kg	feet amsl	ft bgs	units	m3/kg
233.275	17.165	1.98	1.16E-06	217.42	12.13	1.62	9.54E-07
233.175	17.265	1.94	1.14E-06	217.335	12.215	1.62	9.52E-07
233.075	17.365	2.01	1.18E-06	217.235	12.315	1.55	9.11E-07
232.975	17.465	1.89	1.11E-06	217.135	12.415	1.63	9.58E-07
232.875	17.565	1.68	9.86E-07	217.035	12.515	1.74	1.03E-06
232.775	17.665	1.57	9.26E-07	216.935	12.615	2.07	1.22E-06
232.675	17.765	1.41	8.30E-07	216.835	12.715	2.27	1.34E-06
232.575	17.865	1.32	7.74E-07	216.735	12.815	2.51	1.48E-06
232.475	17.965	1.28	7.51E-07	216.635	12.915	2.56	1.51E-06
232.375	18.065	1.26	7.41E-07	216.535	13.015	2.50	1.47E-06
232.275	18.165	1.31	7.68E-07	216.435	13.115	2.71	1.59E-06
232.175	18.265	1.36	8.01E-07	216.32	13.23	2.90	1.70E-06
232.075	18.365	1.41	8.28E-07	216.235	13.315	3.04	1.79E-06
231.975	18.465	1.40	8.21E-07	216.135	13.415	2.86	1.68E-06
231.875	18.565	1.38	8.10E-07	216.04	13.51	2.50	1.47E-06
231.775	18.665	1.36	8.01E-07	215.94	13.61	2.42	1.42E-06
231.675	18.765	1.40	8.24E-07	215.84	13.71	2.56	1.50E-06
231.575	18.865	1.38	8.12E-07	215.74	13.81	2.75	1.62E-06
231.475	18.965	1.35	7.93E-07	215.64	13.91	2.84	1.67E-06
231.375	19.065	1.31	7.68E-07	215.54	14.01	2.76	1.63E-06
231.275	19.165	1.24	7.30E-07	215.445	14.105	2.64	1.56E-06
231.175	19.265	1.28	7.55E-07	215.345	14.205	2.57	1.51E-06
231.075	19.365	1.38	8.10E-07	215.245	14.305	2.54	1.49E-06
230.975	19.465	1.38	8.09E-07	215.145	14.405	2.66	1.56E-06
230.875	19.565	1.38	8.12E-07	215.045	14.505	2.64	1.55E-06
230.78	19.66	1.33	7.83E-07	214.945	14.605	2.57	1.51E-06
230.68	19.76	1.28	7.54E-07	214.845	14.705	2.70	1.59E-06
230.585	19.855	1.23	7.23E-07	214.745	14.805	2.60	1.53E-06
230.485	19.955	1.17	6.87E-07	214.645	14.905	2.62	1.54E-06
230.385	20.055	1.16	6.83E-07	214.545	15.005	2.47	1.45E-06
230.285	20.155	1.19	6.99E-07	214.445	15.105	2.47	1.45E-06
230.185	20.255	1.16	6.82E-07	214.345	15.205	2.39	1.41E-06
230.085	20.355	1.18	6.96E-07	214.245	15.305	2.39	1.40E-06
229.985	20.455	1.22	7.17E-07	214.145	15.405	2.34	1.38E-06
229.885	20.555	1.30	7.65E-07	214.045	15.505	2.23	1.31E-06
229.785	20.655	1.33	7.82E-07	213.945	15.605	2.09	1.23E-06
229.685	20.755	1.33	7.84E-07	213.845	15.705	2.01	1.18E-06
229.585	20.855	1.38	8.11E-07	213.745	15.805	1.82	1.07E-06
229.485	20.955	1.45	8.51E-07	213.645	15.905	1.81	1.07E-06
229.385	21.055	1.61	9.46E-07	213.545	16.005	1.83	1.08E-06
229.285	21.155	1.60	9.41E-07	213.445	16.105	1.86	1.10E-06
229.185	21.255	1.65	9.72E-07	213.345	16.205	1.83	1.08E-06
229.085	21.355	1.56	9.20E-07	213.245	16.305	1.75	1.03E-06



					MW-02-0	30 Run 2 Uj	o and Down
Top of riser elevation (feet) 250.44	MV	/-02-017 Ru	n 2 Up and Down - Average	Top of riser elevation (feet) 229.55		Average	
Elevation	Depth	Mag Susc 10e-3 SI	Mag Susc		Depth	Mag Susc 10e-3 SI	Mag Susc
feet amsl	ft bgs	units	m3/kg	feet amsl	ft bgs	units	m3/kg
228.985	21.455	1.43	8.43E-07	213.145	16.405	1.66	9.78E-07
228.885	21.555	1.44	8.47E-07	213.045	16.505	1.64	9.62E-07
228.785	21.655	1.38	8.12E-07	212.945	16.605	1.61	9.45E-07
228.685	21.755	1.41	8.27E-07	212.845	16.705	1.66	9.74E-07
228.585	21.855	1.43	8.41E-07	212.745	16.805	1.68	9.89E-07
228.485	21.955	1.43	8.41E-07	212.65	16.9	1.82	1.07E-06
228.385	22.055	1.50	8.80E-07	212.55	17	1.82	1.07E-06
228.285	22.155	1.63	9.58E-07	212.45	17.1	1.88	1.10E-06
228.185	22.255	1.70	1.00E-06	212.35	17.2	1.92	1.13E-06
228.085	22.355	1.55	9.10E-07	212.25	17.3	1.91	1.12E-06
227.985	22.455	1.29	7.57E-07	212.15	17.4	1.92	1.13E-06
227.885	22.555	1.17	6.87E-07	212.055	17.495	1.99	1.17E-06
227.785	22.655	1.16	6.85E-07	211.955	17.595	2.07	1.22E-06
227.685	22.755	1.24	7.32E-07	211.855	17.695	2.12	1.25E-06
227.585	22.855	1.28	7.53E-07	211.755	17.795	2.06	1.21E-06
227.49	22.95	1.14	6.70E-07	211.655	17.895	1.94	1.14E-06
227.39	23.05	0.91	5.35E-07	211.555	17.995	1.94	1.14E-06
227.29	23.15	0.86	5.06E-07	211.455	18.095	2.00	1.18E-06
227.195	23.245	0.88	5.21E-07	211.355	18.195	2.10	1.24E-06
227.095	23.345	0.86	5.04E-07	211.255	18.295	2.18	1.28E-06
226.995	23.445	0.85	5.03E-07	211.155	18.395	2.23	1.31E-06
226.895	23.545	0.84	4.91E-07	211.055	18.495	2.29	1.35E-06
226.795	23.645	0.75	4.42E-07	210.955	18.595	2.25	1.33E-06
226.695	23.745	0.75	4.43E-07	210.855	18.695	2.17	1.28E-06
226.595	23.845	0.79	4.64E-07	210.755	18.795	2.17	1.28E-06
226.495	23.945	0.71	4.20E-07	210.655	18.895	2.15	1.26E-06
226.395	24.045	0.70	4.14E-07	210.555	18.995	2.33	1.37E-06
226.295	24.145	0.71	4.17E-07	210.455	19.095	2.46	1.45E-06
226.195	24.245	0.70	4.12E-07	210.355	19.195	2.53	1.49E-06
226.095	24.345	0.68	3.99E-07	210.255	19.295	2.44	1.43E-06
225.995	24.445	0.61	3.57E-07	210.155	19.395	2.41	1.41E-06
225.895	24.545	0.66	3.87E-07	210.055	19.495	2.44	1.44E-06
225.795	24.645	0.59	3.49E-07	209.955	19.595	2.52	1.48E-06
225.695	24.745	0.54	3.15E-07	209.855	19.695	2.56	1.50E-06
225.595	24.845	0.54	3.20E-07	209.755	19.795	2.52	1.48E-06
225.495	24.945	0.52	3.08E-07	209.655	19.895	2.41	1.41E-06
225.395	25.045	0.32	2.74E-07	209.555	19.995	2.43	1.43E-06
225.295	25.145	0.47	2.79E-07	209.455	20.095	2.55	1.50E-06
225.195	25.245	0.47	2.74E-07	209.36	20.19	2.33	1.45E-06
225.095	25.345	0.50	2.97E-07	209.26	20.19	2.45	1.44E-06
224.995	25.445	0.50	3.33E-07	209.16	20.39	2.55	1.50E-06
224.895	25.545	0.62	3.64E-07	209.06	20.35	2.62	1.54E-06
224.795		0.74	4.36E-07	208.96	20.59	2.49	1.46E-06
224.795	23.043	0.74		200.50	20.33	2.75	1.401 00



op of riser elevation (feet) 250.44	MW	/-02-017 Rui	a 2 Up and Down - Average	Top of riser elevation (feet) 229.55		30 Run 2 Uj Average	
levation	Depth	Mag Susc 10e-3 SI	Mag Susc		Depth	Mag Susc 10e-3 SI	Mag Susc
eet amsl	ft bgs	units	m3/kg	feet amsl	ft bgs	units	m3/kg
224.695	25.745	0.77	4.55E-07	208.86	20.69	2.44	1.44E-06
224.595	25.845	0.81	4.76E-07	208.765	20.785	2.20	1.30E-06
224.495	25.945	0.88	5.20E-07	208.665	20.885	2.05	1.21E-06
224.395	26.045	0.87	5.10E-07	208.565	20.985	2.05	1.20E-06
224.295	26.145	0.83	4.86E-07	208.465	21.085	2.02	1.19E-06
224.195	26.245	0.84	4.96E-07	208.365	21.185	2.12	1.25E-06
224.1	26.34	0.82	4.82E-07	208.265	21.285	2.13	1.26E-06
224	26.44	0.81	4.74E-07	208.165	21.385	2.07	1.22E-06
223.905	26.535	0.85	5.02E-07	208.065	21.485	1.89	1.11E-06
223.805	26.635	0.85	4.98E-07	207.965	21.585	1.77	1.04E-06
223.705	26.735	0.95	5.57E-07	207.865	21.685	1.70	1.00E-06
223.605	26.835	0.98	5.76E-07	207.765	21.785	1.73	1.02E-06
223.505	26.935	0.98	5.76E-07	207.665	21.885	1.66	9.74E-07
223.405	27.035	0.98	5.78E-07	207.565	21.985	1.63	9.60E-07
223.305	27.135	0.98	5.74E-07	207.465	22.085	1.60	9.44E-07
223.205	27.235	0.90	5.32E-07	207.365	22.185	1.68	9.87E-07
223.105	27.335	0.85	5.03E-07	207.265	22.285	1.73	1.02E-06
223.005	27.435	0.85	4.97E-07	207.165	22.385	1.71	1.01E-06
222.905	27.535	0.81	4.77E-07	207.065	22.485	1.52	8.93E-07
222.805	27.635	0.81	4.74E-07	206.965	22.585	1.46	8.58E-07
222.705	27.735	0.84	4.95E-07	206.865	22.685	1.49	8.76E-07
222.605	27.835	0.85	4.98E-07	206.765	22.785	1.55	9.14E-07
222.505	27.935	0.85	5.00E-07	206.665	22.885	1.53	8.99E-07
222.303	28.035	0.84	4.95E-07	206.565	22.985	1.43	8.42E-07
222.305	28.135	0.84	4.91E-07	206.465	23.085	1.33	7.84E-07
222.305	28.235	0.84	4.73E-07	206.365	23.185	1.33	8.10E-07
222.205	28.235	0.80	4.68E-07	206.265	23.285	1.38	8.10E-07
222.005	28.435	0.91	5.33E-07	206.165	23.385	1.42	8.33E-07
221.905	28.535	0.91	5.46E-07	206.07	23.48	1.57	9.22E-07
221.905	28.635	0.95	5.63E-07	205.97	23.48	1.57	9.22E-07 9.02E-07
221.805	28.735	0.98	5.77E-07	205.87	23.68	1.55	9.02E-07 8.29E-07
221.703	28.835	0.98	5.78E-07	205.87	23.08	1.41	8.29E-07
221.605	28.835	0.98	5.76E-07	205.67		1.46	8.58E-07 8.66E-07
221.505	28.935			205.67	23.88 23.98		8.66E-07 8.28E-07
221.405	29.035 29.135	0.95 0.90	5.57E-07 5.29E-07	205.57	23.98	1.41 1.32	7.75E-07
	29.135						7.92E-07
221.205	29.235 29.335	0.89	5.24E-07	205.375	24.175	1.35	7.92E-07
221.105		0.79	4.63E-07	205.275	24.275	1.29	
221.005	29.435	0.79	4.67E-07	205.175	24.375	1.32	7.78E-07
220.905	29.535	0.79	4.64E-07	205.075	24.475	1.37	8.07E-07
220.81	29.63	0.78	4.57E-07	204.975	24.575	1.46	8.60E-07
220.71	29.73	0.70	4.09E-07	204.875	24.675	1.46	8.60E-07
220.61	29.83	0.63	3.71E-07	204.775	24.775	1.42	8.36E-07

					MW-02-0	30 Run 2 Up	and Down
Top of riser elevation (feet)	MV	V-02-017 Ru	n 2 Up and Down - Average	Top of riser elevation (feet)		Average	
250.44	Donth	Mag Succ	MagSuga	229.55	Donth	Mag Succ	Mag
Elevation	Depth	10e-3 SI	Mag Susc		Depth	10e-3 SI	Mag Susc
feet amsl	ft bgs	units	m3/kg	feet amsl	ft bgs	units	m3/kg
220.415	30.025	0.57	3.38E-07	204.575	24.975	1.42	8.34E-07
220.315	30.125	0.53	3.12E-07	204.475	25.075	1.39	8.20E-07
220.215	30.225	0.56	3.30E-07	204.375	25.175	1.41	8.27E-07
220.115	30.325	0.52	3.07E-07	204.275	25.275	1.28	7.52E-07
220.015	30.425	0.64	3.76E-07	204.175	25.375	1.29	7.61E-07
219.915	30.525	0.67	3.96E-07	204.075	25.475	1.29	7.61E-07
219.815	30.625	0.68	3.99E-07	203.975	25.575	1.30	7.67E-07
219.715	30.725	0.75	4.39E-07	203.875	25.675	1.28	7.51E-07
219.615	30.825	0.78	4.61E-07	203.775	25.775	1.25	7.34E-07
219.515	30.925	0.98	5.76E-07	203.675	25.875	1.21	7.13E-07
219.415	31.025	1.17	6.88E-07	203.575	25.975	1.26	7.39E-07
219.315	31.125	1.34	7.91E-07	203.475	26.075	1.26	7.43E-07
219.215	31.225	1.49	8.74E-07	203.375	26.175	1.12	6.58E-07
219.115	31.325	1.58	9.32E-07	203.275	26.275	1.11	6.53E-07
219.015	31.425	1.89	1.11E-06	203.175	26.375	1.13	6.65E-07
218.915	31.525	2.20	1.29E-06	203.075	26.475	1.17	6.90E-07
218.815	31.625	2.49	1.46E-06	202.975	26.575	1.26	7.42E-07
218.715	31.725	2.49	1.47E-06	202.875	26.675	1.38	8.11E-07
218.615	31.825	2.41	1.42E-06	202.775	26.775	1.35	7.95E-07
218.515	31.925	2.27	1.34E-06	202.67	26.88	1.40	8.21E-07
218.415	32.025	2.20	1.30E-06	202.58	26.97	1.42	8.33E-07
218.315	32.125	2.14	1.26E-06	202.48	27.07	1.45	8.52E-07
218.215	32.225	2.20	1.29E-06	202.38	27.17	1.47	8.63E-07
218.115	32.325	2.09	1.23E-06	202.28	27.27	1.43	8.39E-07
218.015	32.425	1.99	1.17E-06	202.18	27.37	1.42	8.34E-07
217.915	32.525	1.78	1.05E-06	202.085	27.465	1.45	8.53E-07
217.815	32.625	1.58	9.30E-07	201.985	27.565	1.43	8.40E-07
217.715	32.725	1.55	9.14E-07	201.885	27.665	1.37	8.04E-07
217.615	32.825	1.67	9.85E-07	201.785	27.765	1.33	7.82E-07
217.52	32.92	1.66	9.75E-07	201.685	27.865	1.25	7.36E-07
217.42	33.02	1.60	9.41E-07	201.585	27.965	1.27	7.50E-07
217.32	33.12	1.65	9.70E-07	201.47	28.08	1.23	7.22E-07
217.225	33.215	1.49	8.76E-07	201.385	28.165	1.16	6.83E-07
217.125	33.315	1.49	8.77E-07	201.285	28.265	1.04	6.13E-07
217.025	33.415	1.58	9.28E-07	201.185	28.365	1.03	6.08E-07
216.925	33.515	1.66	9.77E-07	201.085	28.465	1.03	6.07E-07
216.825	33.615	1.65	9.69E-07	200.985	28.565	1.06	6.22E-07
216.725	33.715	1.85	1.09E-06	200.885	28.665	1.11	6.54E-07
216.625	33.815	1.97	1.16E-06	200.785	28.765	1.19	6.99E-07
216.525	33.915	2.19	1.29E-06	200.685	28.865	1.22	7.19E-07
216.425	34.015	2.25	1.32E-06	200.585	28.965	1.27	7.45E-07
216.325	34.115	2.57	1.51E-06	200.485	29.065	1.39	8.19E-07
216.225	34.215	2.58	1.52E-06	200.385	29.165	1.45	8.51E-07



					MW-02-0	30 Run 2 Uj	o and Down
Top of riser elevation (feet) 250.44	MW	/-02-017 Ru	n 2 Up and Down - Average	Top of riser elevation (feet) 229.55		Average	
Elevation	Depth	Mag Susc 10e-3 SI	Mag Susc		Depth	Mag Susc 10e-3 SI	Mag Susc
feet amsl	ft bgs	units	m3/kg	feet amsl	ft bgs	units	m3/kg
216.125	34.315	2.74	1.61E-06	200.285	29.265	1.46	8.56E-07
216.025	34.415	2.72	1.60E-06	200.185	29.365	1.44	8.45E-07
215.925	34.515	2.50	1.47E-06	200.085	29.465	1.44	8.47E-07
215.825	34.615	2.36	1.39E-06	199.985	29.565	1.41	8.32E-07
215.725	34.715	2.20	1.29E-06	199.885	29.665	1.39	8.15E-07
215.625	34.815	2.18	1.28E-06	199.785	29.765	1.34	7.90E-07
215.525	34.915	2.14	1.26E-06	199.685	29.865	1.33	7.83E-07
215.425	35.015	1.98	1.16E-06	199.585	29.965	1.36	8.03E-07
215.325	35.115	1.78	1.05E-06	199.485	30.065	1.29	7.56E-07
215.225	35.215	1.64	9.67E-07	199.39	30.16	1.33	7.84E-07
215.125	35.315	1.53	8.97E-07	199.29	30.26	1.34	7.89E-07
215.025	35.415	1.47	8.67E-07	199.19	30.36	1.33	7.82E-07
214.925	35.515	1.51	8.90E-07	199.09	30.46	1.34	7.89E-07
214.825	35.615	1.47	8.64E-07	198.99	30.56	1.37	8.07E-07
214.725	35.715	1.35	7.95E-07	198.89	30.66	1.30	7.65E-07
214.625	35.815	1.39	8.15E-07	198.795	30.755	1.30	7.63E-07
214.525	35.915	1.39	8.19E-07	198.695	30.855	1.37	8.04E-07
214.425	36.015	1.36	8.00E-07	198.595	30.955	1.46	8.59E-07
214.325	36.115	1.38	8.15E-07	198.495	31.055	1.57	9.26E-07
214.225	36.215	1.37	8.08E-07	198.395	31.155	1.70	9.99E-07
214.13	36.31	1.28	7.50E-07	198.295	31.255	1.70	1.00E-06
214.03	36.41	1.32	7.75E-07	198.195	31.355	1.76	1.03E-06
213.935	36.505	1.33	7.81E-07	198.095	31.455	1.74	1.02E-06
213.835	36.605	1.28	7.52E-07	197.995	31.555	1.75	1.03E-06
213.735	36.705	1.23	7.26E-07	197.895	31.655	1.68	9.88E-07
213.635	36.805	1.37	8.07E-07	197.795	31.755	1.67	9.83E-07
213.535	36.905	1.42	8.35E-07	197.695	31.855	1.74	1.02E-06
213.435	37.005	1.49	8.74E-07	197.595	31.955	1.77	1.04E-06
213.335	37.105	1.50	8.80E-07	197.495	32.055	1.76	1.04E-06
213.235	37.205	1.51	8.91E-07	197.395	32.155	1.80	1.06E-06
213.135	37.305	1.53	8.98E-07	197.295	32.255	1.74	1.03E-06
213.035	37.405	1.54	9.03E-07	197.195	32.355	1.77	1.04E-06
212.935	37.505	1.55	9.10E-07	197.095	32.455	1.80	1.06E-06
212.835	37.605	1.56	9.18E-07	196.995	32.555	1.84	1.08E-06
212.735	37.705	1.56	9.18E-07	196.895	32.655	1.75	1.03E-06
212.635	37.805	1.62	9.54E-07	196.795	32.755	1.73	1.02E-06
212.535	37.905	1.55	9.13E-07	196.695	32.855	1.64	9.66E-07
212.435	38.005	1.49	8.77E-07	196.595	32.955	1.64	9.66E-07
212.335	38.105	1.46	8.58E-07	196.495	33.055	1.64	9.63E-07
212.235	38.205	1.42	8.35E-07	196.395	33.155	1.52	8.94E-07
212.135	38.305	1.29	7.56E-07	196.295	33.255	1.56	9.18E-07
212.035	38.405	1.25	7.92E-07	196.195	33.355	1.58	9.29E-07
211.935		1.39	8.18E-07	196.095	33.455	1.75	1.03E-06
211.555	50.505	1.55	0.102 07	190.099	55.455	1.75	1.032 00



Top of riser elevation	(feet) 250.44	MW	/-02-017 Rui	n 2 Up and Down - Average	Top of riser elevation (feet) 229.55	MW-02-0	30 Run 2 Up Average	and Down
Elevation	200111	Depth	Mag Susc 10e-3 SI	Mag Susc		Depth	Mag Susc 10e-3 SI	Mag Susc
feet amsl		ft bgs	units	m3/kg	feet amsl	ft bgs	units	m3/kg
	211.835	38.605	1.62	9.53E-07	196	33.55	1.86	1.09E-06
	211.735	38.705	1.82	1.07E-06	195.9	33.65	1.90	1.12E-06
	211.635	38.805	2.00	1.17E-06	195.8	33.75	1.94	1.14E-06
	211.535	38.905	2.11	1.24E-06	195.7	33.85	2.05	1.20E-06
	211.435	39.005	2.12	1.25E-06	195.6	33.95	2.13	1.25E-06
	211.335	39.105	2.16	1.27E-06	195.505	34.045	2.21	1.30E-06
	211.235	39.205	2.21	1.30E-06	195.405	34.145	2.16	1.27E-06
	211.135	39.305	2.16	1.27E-06	195.305	34.245	2.19	1.29E-06
	211.035	39.405	1.97	1.16E-06	195.205	34.345	2.22	1.31E-06
	210.935	39.505	1.88	1.11E-06	195.105	34.445	2.27	1.33E-06
	210.84	39.6	1.82	1.07E-06	195.005	34.545	2.32	1.37E-06
	210.74	39.7	1.71	1.00E-06	194.905	34.645	2.28	1.34E-06
	210.64	39.8	1.68	9.87E-07	194.805	34.745	2.29	1.35E-06
	210.545	39.895	1.71	1.01E-06	194.705	34.845	2.36	1.39E-06
	210.445	39.995	1.67	9.82E-07	194.605	34.945	2.44	1.43E-06
	210.345	40.095	1.63	9.57E-07	194.505	35.045	2.50	1.47E-06
	210.245	40.195	1.66	9.77E-07	194.405	35.145	2.54	1.50E-06
	210.145	40.295	1.63	9.60E-07	194.305	35.245	2.62	1.54E-06
	210.045	40.395	1.64	9.63E-07	194.205	35.345	2.70	1.59E-06
	209.945	40.495	1.68	9.88E-07	194.105	35.445	2.81	1.65E-06
	209.845	40.595	1.65	9.68E-07	194.005	35.545	2.80	1.65E-06
	209.74	40.7	1.67	9.82E-07	193.905	35.645	2.81	1.65E-06
					193.805	35.745	2.89	1.70E-06
					193.705	35.845	2.90	1.71E-06
					193.605	35.945	2.83	1.67E-06
					193.505	36.045	2.82	1.66E-06
					193.405	36.145	2.66	1.57E-06
					193.305	36.245	2.68	1.58E-06
					193.205	36.345	2.64	1.55E-06
					193.105	36.445	2.62	1.54E-06
					193.005	36.545	2.60	1.53E-06
					192.905	36.645	2.62	1.54E-06
					192.805	36.745	2.72	1.60E-06
					192.71	36.84	2.75	1.62E-06
					192.61	36.94	2.77	1.63E-06
					192.51	37.04	2.80	1.65E-06
					192.41	37.14	2.80	1.65E-06
					192.31	37.24	2.92	1.72E-06
					192.21	37.34	2.99	1.76E-06
					192.115	37.435	2.98	1.75E-06
					192.015	37.535	3.00	1.76E-06
					191.915	37.635	3.08	1.81E-06
					191.815	37.735	3.20	1.88E-06



Top of riser elevation (feet) 250.44	MV	V-02-017 Ru	n 2 Up and Down - Average	Top of riser elevation (feet) 229.55	MW-02-0	30 Run 2 Up Average	and Down
Elevation	Depth	Mag Susc 10e-3 SI	Mag Susc		Depth	Mag Susc 10e-3 SI	Mag Susc
feet amsl	ft bgs	units	m3/kg	feet amsl	ft bgs	units	m3/kg
	-		-	191.715	37.835	3.27	1.92E-06
				191.615	37.935	3.28	1.93E-06
				191.515	38.035	3.28	1.93E-06
				191.415	38.135	3.33	1.96E-06
				191.315	38.235	3.33	1.96E-06
				191.215	38.335	3.37	1.98E-06
				191.115	38.435	3.47	2.04E-06
				191.015	38.535	3.48	2.05E-06
				190.915	38.635	3.67	2.16E-06
				190.815	38.735	3.86	2.27E-06
				190.715	38.835	3.73	2.20E-06
				190.615	38.935	3.53	2.07E-06
				190.515	39.035	3.38	1.99E-06
				190.415	39.135	3.49	2.05E-06
				190.315	39.235	3.74	2.20E-06
				190.215	39.335	3.69	2.17E-06
				190.115	39.435	3.60	2.12E-06
				190.015	39.535	3.37	1.98E-06
				189.915	39.635	3.10	1.83E-06
				189.815	39.735	3.30	1.94E-06
				189.715	39.835	3.38	1.99E-06
				189.615	39.935	3.58	2.11E-06
				189.515	40.035	3.43	2.02E-06
				189.42	40.13	3.20	1.88E-06
				189.32	40.23	3.06	1.80E-06
				189.22	40.33	3.30	1.94E-06
				189.12	40.43	3.51	2.06E-06
				189.02	40.53	3.49	2.05E-06
				188.92	40.63	3.43	2.02E-06
				188.825	40.725	3.29	1.93E-06
				188.725	40.825	3.29	1.94E-06
				188.625	40.925	3.52	2.07E-06
				188.525	41.025	3.64	2.14E-06
				188.425	41.125	3.54	2.08E-06
				188.325	41.225	3.62	2.13E-06
				188.225	41.325	3.51	2.07E-06
				188.125	41.425	3.47	2.04E-06
				188.025	41.525	3.45	2.03E-06
				187.925	41.625	3.30	1.94E-06
				187.825	41.725	3.14	1.85E-06
				187.725	41.825	3.14	1.85E-06
				187.625	41.925	3.06	1.80E-06
				187.525	42.025	3.05	1.79E-06



op of riser elevation (feet) 250.44	MV	V-02-017 Ru	n 2 Up and Down - Average	Top of riser elevation (feet) 229.55	MW-02-0	30 Run 2 Up Average	and Dowi
levation	Depth	Mag Susc 10e-3 SI	Mag Susc	223.35	Depth	Mag Susc 10e-3 SI	Mag Susc
eet amsl	ft bgs	units	m3/kg	feet amsl	ft bgs	units	m3/kg
				187.425	42.125	2.90	1.70E-06
				187.325	42.225	2.84	1.67E-06
				187.225	42.325	2.83	1.66E-06
				187.125	42.425	2.78	1.64E-06
				187.025	42.525	2.82	1.66E-06
				186.925	42.625	2.81	1.65E-06
				186.825	42.725	2.90	1.71E-06
				186.725	42.825	3.00	1.77E-06
				186.625	42.925	3.12	1.83E-06
				186.525	43.025	3.15	1.86E-06
				186.425	43.125	3.19	1.88E-06
				186.325	43.225	3.25	1.91E-06
				186.225	43.325	3.39	2.00E-06
				186.125	43.425	3.49	2.05E-06
				186.03	43.52	3.41	2.01E-06
				185.93	43.62	3.33	1.96E-06
				185.83	43.72	3.06	1.80E-0
				185.73	43.82	2.91	1.71E-0
				185.63	43.92	2.91	1.72E-0
				185.535	44.015	2.92	1.72E-0 1.74E-0
				185.435	44.015	2.30	1.64E-0
				185.335	44.215	2.78	1.55E-0
				185.235	44.215 44.315	2.65	
							1.50E-0
				185.135	44.415	2.61	1.54E-0
				185.035	44.515	2.72	1.60E-0
				184.935	44.615	2.60	1.53E-0
				184.835	44.715	2.47	1.45E-0
				184.735	44.815	2.34	1.38E-0
				184.635	44.915	2.23	1.31E-0
				184.535	45.015	2.14	1.26E-0
				184.435	45.115	1.98	1.17E-0
				184.335	45.215	1.97	1.16E-0
				184.235	45.315	1.85	1.09E-06
				184.135	45.415	1.74	1.03E-06
				184.035	45.515	1.70	9.99E-07
				183.935	45.615	1.62	9.50E-07
				183.835	45.715	1.71	1.01E-06
				183.735	45.815	1.66	9.78E-07
				183.635	45.915	1.73	1.02E-06
				183.535	46.015	1.78	1.05E-06
				183.435	46.115	1.82	1.07E-06
				183.335	46.215	1.76	1.04E-06
				183.235	46.315	1.88	1.10E-06



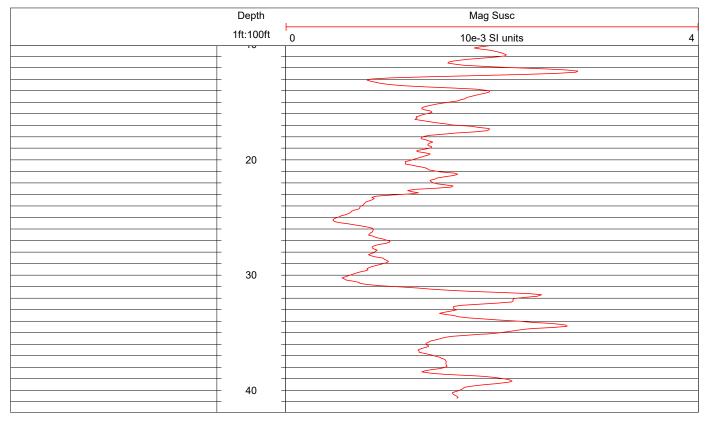
op of riser elevation (feet) 250.44	MM	V-02-017 Ru	n 2 Up and Down - Average	Top of riser elevation (feet) 229.55	IVI VV-02-0	30 Run 2 Up Average	and Down
levation	Depth	Mag Susc 10e-3 SI	Mag Susc	229.55	Depth	Mag Susc 10e-3 SI	Mag Susc
eet amsl	ft bgs	units	m3/kg	feet amsl	ft bgs	units	m3/kg
	•			183.135	46.415	1.92	1.13E-06
				183.035	46.515	2.03	1.19E-06
				182.935	46.615	2.04	1.20E-06
				182.835	46.715	2.04	1.20E-06
				182.74	46.81	1.96	1.15E-06
				182.64	46.91	2.00	1.18E-06
				182.54	47.01	1.99	1.17E-06
				182.44	47.11	1.84	1.08E-06
				182.34	47.21	1.70	1.00E-06
				182.24	47.31	1.64	9.64E-07
				182.145	47.405	1.63	9.58E-0
				182.045	47.505	1.65	9.72E-0
				181.945	47.605	1.63	9.59E-0
				181.845	47.705	1.50	8.82E-0
				181.745	47.805	1.55	9.11E-0
				181.645	47.905	1.58	9.29E-0
				181.545	48.005	1.70	1.00E-0
				181.445	48.105	1.83	1.08E-0
				181.345	48.205	1.73	1.02E-0
				181.245	48.305	1.68	9.90E-0
				181.145	48.405	1.72	1.01E-0
				181.045	48.505	1.87	1.10E-0
				180.945	48.605	2.07	1.22E-0
				180.845	48.005	2.16	1.27E-0
				180.745	48.805	2.10	1.27E-0
				180.743	48.805	2.09	1.23E-0 1.20E-0
				180.545	48.903	2.03	1.20E-0 1.26E-0
				180.345	49.005	2.14	1.28E-0
				180.345	49.105	2.18	1.25E-0
				180.245	49.205	2.13	1.25E-0
				180.243	49.303	1.94	1.19E-0
				180.045	49.505	1.82	1.07E-0
				179.945	49.605	1.79	1.05E-0
				179.845	49.705	1.75	1.03E-0
				179.745	49.805	1.83	1.08E-06
				179.645	49.905	1.99	1.17E-0
				179.545	50.005	1.55	9.12E-07
				179.45	50.1	2.08	1.22E-06
				179.35	50.2	2.12	1.25E-06
				179.25	50.3	2.15	1.27E-06
				179.15	50.4	2.21	1.30E-06
				179.05	50.5	2.27	1.33E-06
				178.95	50.6	2.22	1.31E-0



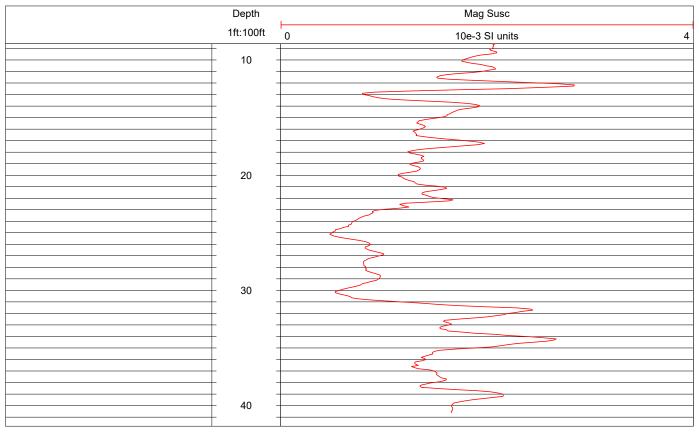
Top driser elevation (field)         WW-U-U-U-Wardage         Top driser elevation (field)         Average           10-31         223.51         223.51         10-35						MW-02-0	30 Run 2 Up	and Down
Elevation       Depth       Mag Sus Mag Sus 10:-3 (10:-3)       Depth 10:-3 (10:-3)       Mag Sus 10:-3 (10:-3)         feet amsl       ft bgs       units       m3/kg       (10:-3)       (10:-3)       (10:-3)       (10:-3)         feet amsl       ft bgs       units       m3/kg       (10:-3)       (10:-3)       (10:-3)       (10:-3)       (10:-3)         feet amsl       ft bgs       units       m3/kg       (10:-3) <td></td> <td>MV</td> <td>V-02-017 Rui</td> <td>n 2 Up and Down - Average</td> <td></td> <td></td> <td>Average</td> <td></td>		MV	V-02-017 Rui	n 2 Up and Down - Average			Average	
10e-3 Si         10e-3 Si           feet amsl         ft bgs         units         m3/kg         feet amsl         ft bgs         units         m3/kg           feet amsl         ft bgs         units         m3/kg         feet amsl         ft bgs         units         m3/kg           feet amsl         ft bgs         units         m3/kg         feet amsl         ft bgs         units         m3/kg           feet amsl         ft bgs         units         m3/kg         feet amsl         ft bgs         units         m3/kg           feet amsl         ft bgs         units         m3/kg         feet amsl         ft bgs         units         ft bgs         124-06           178.55         50.095         2.00         1.22E-06         178.655         51.095         2.07         1.22E-06           178.55         51.095         1.19         1.07E-06         178.055         51.095         1.08         1.07E-06           177.055         51.595         1.71         1.01E-06         177.755         51.995         1.08         1.06E-06           177.755         51.995         1.08         1.06E-06         177.755         51.995         1.08         1.06E-06           177.755					229.55			
178.855         50.955         2.16         1.27E-06           178.755         50.795         2.10         1.24E-06           178.655         50.995         2.08         1.22E-06           178.555         50.995         2.08         1.22E-06           178.555         51.995         2.07         1.22E-06           178.355         51.195         2.07         1.22E-06           178.355         51.295         1.99         1.17E-06           178.355         51.295         1.99         1.17E-06           178.055         51.495         1.81         1.07E-06           177.855         51.995         1.72         1.01E-06           177.855         51.995         1.72         1.01E-06           177.755         51.995         1.75         1.03E-06           177.755         51.995         1.75         1.03E-06           177.755         51.995         1.84         1.08E-06           177.755         51.995         1.84         1.08E-06           177.755         52.995         1.03         1.06E-06           177.755         52.995         1.00         1.18E-06           177.055         52.995         1.	Elevation	Depth	-	Mag Susc		Depth	-	Mag Susc
178.755       50.795       2.10       1.24E-06         178.655       50.895       2.12       1.25E-06         178.655       50.995       2.07       1.22E-06         178.455       51.095       2.07       1.22E-06         178.355       51.295       1.195       1.20         178.355       51.295       1.395       1.18       1.11E-06         178.355       51.395       1.38       1.11E-06         178.055       51.495       1.38       1.11E-06         177.055       51.955       1.72       1.01E-06         177.055       51.955       1.75       1.03E-06         177.655       51.895       1.75       1.03E-06         177.655       51.995       1.80       1.06E-06         177.655       51.995       1.80       1.06E-06         177.655       52.995       1.80       1.06E-06         177.655       52.995       1.80       1.06E-06         177.655       52.995       2.00       1.18E-06         176.055       52.995       2.00       1.18E-06         176.055       52.995       2.00       1.20E-06         176.655       52.995       2.00 <td>feet amsl</td> <td>ft bgs</td> <td>units</td> <td>m3/kg</td> <td>feet amsl</td> <td>ft bgs</td> <td>units</td> <td>m3/kg</td>	feet amsl	ft bgs	units	m3/kg	feet amsl	ft bgs	units	m3/kg
178.655       50.895       2.12       1.25E-06         178.555       50.095       2.08       1.22E-06         178.455       51.095       2.07       1.22E-06         178.355       51.195       2.07       1.22E-06         178.355       51.395       1.18       0.17E-06         178.255       51.395       1.88       1.11E-06         178.055       51.495       1.81       1.07E-06         178.055       51.95       1.71       1.01E-06         177.055       51.95       1.72       1.03E-06         177.755       51.955       1.75       1.03E-06         177.755       51.955       1.75       1.03E-06         177.755       51.955       1.80       1.06E-06         177.755       52.055       1.80       1.08E-06         177.755       52.055       1.80       1.06E-06         177.255       52.055       1.80       1.08E-06         177.255       52.055       1.80       1.08E-06         177.055       52.495       2.00       1.18E-06         177.055       52.495       2.00       1.20E-06         176.655       52.955       2.06       1.20E-06					178.855	50.695	2.16	1.27E-06
178.555       50.955       2.08       1.22E-06         178.455       51.095       2.07       1.22E-06         178.455       51.295       1.99       1.27E-06         178.255       51.295       51.295       1.99       1.17E-06         178.155       51.395       1.88       1.10F-06         177.855       51.695       1.71       1.01E-06         177.855       51.695       1.72       1.03E-06         177.755       51.995       1.75       1.03E-06         177.655       51.995       1.84       1.08E-06         177.555       51.995       1.84       1.08E-06         177.555       51.995       1.84       1.08E-06         177.555       52.995       1.98       1.13E-06         177.555       52.995       1.98       1.13E-06         177.555       52.995       1.98       1.12E-06         176.755       52.995       2.05       1.20E-06         176.755       52.995       2.05       1.20E-06         176.655       52.995       2.05       1.20E-06         176.655       52.995       2.05       1.20E-06         176.655       52.995       1.92					178.755	50.795	2.10	1.24E-06
178.455       51.095       2.07       1.22E-06         178.355       51.195       1.195       1.176-06         178.155       51.395       1.88       1.11E-06         178.055       51.495       1.81       1.07E-06         177.055       51.695       1.72       1.01E-06         177.755       51.695       1.72       1.01E-06         177.755       51.695       1.75       1.03E-06         177.755       51.895       1.75       1.03E-06         177.755       51.995       1.84       1.00E-06         177.755       51.995       1.84       1.00E-06         177.755       52.995       1.84       1.00E-06         177.455       52.095       1.84       1.00E-06         177.355       52.195       1.91       1.13E-06         177.455       52.395       2.00       1.18E-06         177.055       52.495       2.05       1.20E-06         176.655       52.595       2.06       1.21E-06         176.655       52.995       2.06       1.21E-06         176.64       52.91       2.07       1.22E-06         176.655       52.995       1.92       1.13E-0					178.655	50.895	2.12	1.25E-06
178.355       51.195       2.07       1.22E-06         178.255       51.295       1.99       1.17E-06         178.155       51.395       1.485       1.81         178.055       51.595       1.71       1.01E-06         177.855       51.695       1.72       1.01E-06         177.855       51.695       1.72       1.03E-06         177.755       51.795       1.75       1.03E-06         177.755       51.995       1.75       1.03E-06         177.755       51.995       1.84       1.08E-06         177.455       52.095       1.80       1.06E-06         177.355       52.195       1.98       1.16E-06         177.355       52.295       1.98       1.12E-06         177.455       52.295       1.98       1.12E-06         177.355       52.395       2.00       1.18E-06         176.055       52.495       2.05       1.20E-06         176.645       52.995       1.92       1.12E-06         176.55       52.995       2.05       1.21E-06         176.55       52.995       1.92       1.12E-06         176.55       52.995       1.92       1.12E-06 <td></td> <td></td> <td></td> <td></td> <td>178.555</td> <td>50.995</td> <td>2.08</td> <td>1.22E-06</td>					178.555	50.995	2.08	1.22E-06
178.255       51.295       1.99       1.17E-06         178.155       51.395       1.88       1.11E-06         178.055       51.595       1.325       1.326         177.955       51.595       1.72       1.01E-06         177.855       51.695       1.72       1.01E-06         177.855       51.695       1.75       1.03E-06         177.655       51.895       1.75       1.03E-06         177.655       51.995       1.84       1.08E-06         177.455       52.095       1.80       1.06E-06         177.255       52.295       1.89       1.16E-06         177.255       52.295       1.98       1.16E-06         177.255       52.495       1.98       1.16E-06         177.255       52.495       1.98       1.16E-06         177.255       52.495       2.05       1.20E-06         176.855       52.695       2.03       1.20E-06         176.655       52.995       1.03       1.20E-06         176.555       52.995       2.05       1.21E-06         176.555       52.995       2.05       1.21E-06         176.555       52.995       1.92       1.13E-06					178.455	51.095	2.07	1.22E-06
178.155       51.395       1.88       1.11E-06         178.055       51.495       1.81       1.07E-06         177.955       51.695       1.72       1.01E-06         177.855       51.695       1.72       1.01E-06         177.855       51.695       1.72       1.01E-06         177.755       51.995       1.75       1.03E-06         177.655       51.995       1.84       1.08E-06         177.455       52.095       1.80       1.06E-06         177.355       52.195       1.91       1.3E-06         177.455       52.095       1.80       1.06E-06         177.355       52.295       1.98       1.16E-06         177.55       52.295       1.98       1.16E-06         177.55       52.495       2.00       1.3E-06         176.55       52.95       2.06       1.21E-06         176.55       52.95       2.06       1.21E-06         176.55       52.95       1.02       1.3E-06         176.55       52.95       1.02       1.3E-06         176.55       52.95       1.02       1.21E-06         176.55       52.95       1.02       1.3E-06					178.355	51.195	2.07	1.22E-06
178.055       51.495       1.81       1.07E-06         177.955       51.595       1.71       1.01E-06         177.855       51.695       1.72       1.03E-06         177.755       51.795       1.35       1.37         177.655       51.895       1.75       1.03E-06         177.755       51.995       1.84       1.08E-06         177.455       52.095       1.80       1.06E-06         177.355       52.195       1.91       1.13E-06         177.155       52.395       1.90       1.84       1.06E-06         177.355       52.395       1.91       1.13E-06         177.155       52.395       1.93       1.61E-06         177.555       52.495       1.93       1.21E-06         176.555       52.595       2.06       1.21E-06         176.555       52.995       2.06       1.21E-06         176.555       52.995       2.00       1.32E-06         176.555       52.995       1.92       1.32E-06         176.555       52.995       1.92       1.32E-06         176.555       53.095       2.00       1.32E-06         176.455       53.095       2.00					178.255	51.295	1.99	1.17E-06
177,955       51.595       1.71       1.01E-06         177,855       51.695       1.72       1.01E-06         177,855       51.795       1.75       1.03E-06         177,555       51.995       1.84       1.08E-06         177,555       52.095       1.80       1.06E-06         177,555       52.095       1.98       1.16E-06         177,555       52.495       1.98       1.16E-06         177,555       52.495       2.00       1.18E-06         177,555       52.495       2.05       1.20E-06         176,655       52.695       2.03       1.20E-06         176,655       52.995       2.06       1.21E-06         176,655       52.995       1.92       1.13E-06         176,655       52.995       1.92       1.13E-06         176,655       52.995       1.92       1.13E-06         176,655       53.095       1.92       1.13E-					178.155	51.395	1.88	1.11E-06
177.855       51.695       1.72       1.01E-06         177.755       51.795       1.75       1.03E-06         177.655       51.895       1.75       1.03E-06         177.555       51.995       1.84       1.08E-06         177.455       52.095       1.91       1.13E-06         177.355       52.195       1.91       1.13E-06         177.155       52.295       1.92       1.13E-06         177.155       52.395       2.00       1.18E-06         177.055       52.495       2.05       1.20E-06         177.055       52.495       2.05       1.20E-06         176.855       52.695       2.06       1.21E-06         176.855       52.695       2.06       1.21E-06         176.64       52.91       2.07       1.22E-06         176.455       52.995       2.06       1.21E-06         176.455       53.095       2.00       1.13E-06         176.455       53.095       2.00       1.13E-06         176.455       53.095       2.00       1.13E-06         176.455       53.295       1.92       1.13E-06         176.455       53.295       1.92       1.13E-06					178.055	51.495	1.81	1.07E-06
177.755       51.795       1.75       1.03E-06         177.655       51.895       1.75       1.03E-06         177.555       51.995       1.84       1.08E-06         177.455       52.095       1.80       1.06E-06         177.355       52.195       1.91       1.13E-06         177.255       52.295       1.98       1.16E-06         177.255       52.495       2.05       1.20E-06         177.055       52.495       2.05       1.20E-06         176.755       52.595       2.06       1.21E-06         176.755       52.695       2.06       1.21E-06         176.64       52.91       2.07       1.22E-06         176.555       52.995       1.92       1.13E-06         176.555       52.995       1.92       1.13E-06         176.455       53.095       2.00       1.13E-06         176.555       52.995       1.92       1.13E-06         176.555       53.295       1.92       1.13E-06         176.16       53.39       2.00       1.13E-06         176.16       53.495       1.92       1.13E-06         176.16       53.497       1.01E-06					177.955	51.595	1.71	1.01E-06
177.65551.8951.751.03E-06177.55551.9951.841.08E-06177.45552.0951.801.06E-06177.35552.1951.911.13E-06177.25552.2951.981.16E-06177.15552.4952.051.20E-06176.55552.5952.061.20E-06176.65552.6952.031.20E-06176.75552.952.061.21E-06176.6452.912.071.22E-06176.55552.9951.921.13E-06176.55552.9951.921.13E-06176.55552.9951.921.13E-06176.55552.9951.921.13E-06176.55553.1951.921.13E-06176.55553.2951.921.13E-06176.55553.2951.921.13E-06176.25553.2951.921.13E-06176.25553.2951.921.13E-06176.16553.392.001.18E-06176.16553.392.011.18E-06176.16653.392.011.18E-06176.16653.392.011.18E-06176.16653.492.071.21E-06176.16653.492.071.21E-06176.16653.492.071.21E-06176.16653.492.071.21E-06176.16653.492.071.21E-06176.16653.492.071.21E-06					177.855	51.695	1.72	1.01E-06
177.55551.9951.841.08E-06177.45552.0951.801.06E-06177.35552.1951.911.13E-06177.25552.2951.981.16E-06177.15552.3952.001.18E-06177.05552.4952.051.20E-06176.95552.5952.061.21E-06176.75552.6952.031.20E-06176.75552.7952.061.21E-06176.64552.912.071.22E-06176.45552.951.921.13E-06176.35553.0951.921.13E-06176.35553.0951.921.13E-06176.25553.2951.921.13E-06176.25553.2951.921.13E-06176.25553.2951.921.13E-06176.25553.2951.921.13E-06176.25553.2951.921.13E-06176.25553.2951.921.13E-06176.25553.2951.921.13E-06176.25553.2951.971.16E-06176.1653.392.011.18E-06176.0653.492.071.21E-06					177.755	51.795	1.75	1.03E-06
177.45552.0951.801.06E-06177.35552.1951.911.13E-06177.25552.2951.981.16E-06177.15552.3952.001.18E-06177.05552.4952.051.20E-06176.95552.5952.061.21E-06176.85552.6952.031.20E-06176.64552.0952.061.21E-06176.64552.912.071.22E-06176.45552.9951.021.13E-06176.35553.0952.001.18E-06176.45553.0951.021.13E-06176.25553.1951.921.13E-06176.25553.0951.021.13E-06176.16153.392.011.18E-06176.16153.392.011.18E-06176.0653.492.071.21E-06					177.655	51.895	1.75	1.03E-06
177.35552.1951.911.13E-06177.25552.2951.981.16E-06177.15552.3952.001.18E-06177.05552.4952.051.20E-06176.95552.5952.061.21E-06176.85552.6952.031.20E-06176.6452.912.071.22E-06176.65552.9551.921.13E-06176.55552.9551.921.13E-06176.35553.0952.001.18E-06176.25553.2951.921.13E-06176.25553.2951.921.13E-06176.25553.2951.921.13E-06176.16153.392.011.18E-06176.16653.392.011.18E-06176.16653.492.071.21E-06176.16653.492.071.21E-06176.16653.492.071.21E-06					177.555	51.995	1.84	1.08E-06
177.255       52.295       1.98       1.16E-06         177.155       52.395       2.00       1.18E-06         177.055       52.495       2.05       1.20E-06         176.955       52.695       2.03       1.20E-06         176.855       52.695       2.03       1.20E-06         176.755       52.795       2.06       1.21E-06         176.64       52.91       2.07       1.22E-06         176.655       52.995       1.92       1.13E-06         176.455       53.095       2.00       1.18E-06         176.355       53.195       1.92       1.13E-06         176.355       53.195       1.92       1.13E-06         176.255       53.295       1.92       1.13E-06         176.255       53.295       1.92       1.13E-06         176.255       53.295       1.92       1.13E-06         176.16       53.39       2.01       1.18E-06         176.16       53.39       2.01       1.18E-06         176.06       53.49       2.07       1.21E-06					177.455	52.095	1.80	1.06E-06
177.15552.3952.001.18E-06177.05552.4952.051.20E-06176.95552.6952.031.20E-06176.75552.7952.061.21E-06176.6452.912.071.22E-06176.55552.9951.921.13E-06176.45553.0952.001.18E-06176.55553.1951.921.13E-06176.65553.2951.921.13E-06176.16653.392.011.18E-06176.66653.492.071.21E-06					177.355	52.195	1.91	1.13E-06
177.05552.4952.051.20E-06176.95552.5952.061.21E-06176.85552.6952.031.20E-06176.75552.7952.061.21E-06176.6452.912.071.22E-06176.45552.9951.921.13E-06176.45553.0952.001.18E-06176.25553.2951.921.13E-06176.16153.392.011.18E-06176.06153.492.071.21E-06					177.255	52.295	1.98	1.16E-06
176.95552.5952.061.21E-06176.85552.6952.031.20E-06176.75552.7952.061.21E-06176.6452.912.071.22E-06176.55552.9951.921.13E-06176.45553.0952.001.18E-06176.25553.2951.921.13E-06176.16653.392.011.18E-06176.6653.4952.011.18E-06176.0653.492.071.21E-06					177.155	52.395	2.00	1.18E-06
176.855       52.695       2.03       1.20E-06         176.755       52.795       2.06       1.21E-06         176.64       52.91       2.07       1.22E-06         176.555       52.995       1.92       1.13E-06         176.455       53.095       2.00       1.18E-06         176.555       53.195       1.92       1.13E-06         176.255       53.295       1.97       1.16E-06         176.166       53.39       2.01       1.18E-06         176.066       53.49       2.07       1.21E-06					177.055	52.495	2.05	1.20E-06
176.75552.7952.061.21E-06176.6452.912.071.22E-06176.55552.9951.921.13E-06176.45553.0952.001.18E-06176.35553.1951.921.13E-06176.25553.2951.971.16E-06176.1653.392.011.18E-06176.0653.492.071.21E-06					176.955	52.595	2.06	1.21E-06
176.6452.912.071.22E-06176.55552.9951.921.13E-06176.45553.0952.001.18E-06176.35553.1951.921.13E-06176.25553.2951.971.16E-06176.1653.392.011.18E-06176.0653.492.071.21E-06					176.855	52.695	2.03	1.20E-06
176.555       52.995       1.92       1.13E-06         176.455       53.095       2.00       1.18E-06         176.355       53.195       1.92       1.13E-06         176.255       53.295       1.97       1.16E-06         176.16       53.39       2.01       1.18E-06         176.06       53.49       2.07       1.21E-06					176.755	52.795	2.06	1.21E-06
176.45553.0952.001.18E-06176.35553.1951.921.13E-06176.25553.2951.971.16E-06176.1653.392.011.18E-06176.0653.492.071.21E-06					176.64	52.91	2.07	1.22E-06
176.355       53.195       1.92       1.13E-06         176.255       53.295       1.97       1.16E-06         176.16       53.39       2.01       1.18E-06         176.06       53.49       2.07       1.21E-06					176.555	52.995	1.92	1.13E-06
176.25553.2951.971.16E-06176.1653.392.011.18E-06176.0653.492.071.21E-06					176.455	53.095	2.00	1.18E-06
176.1653.392.011.18E-06176.0653.492.071.21E-06					176.355	53.195	1.92	1.13E-06
176.06 53.49 2.07 1.21E-06					176.255	53.295	1.97	1.16E-06
					176.16	53.39	2.01	1.18E-06
175.95 53.6 2.05 1.20E-06					176.06	53.49	2.07	1.21E-06
					175.95	53.6	2.05	1.20E-06



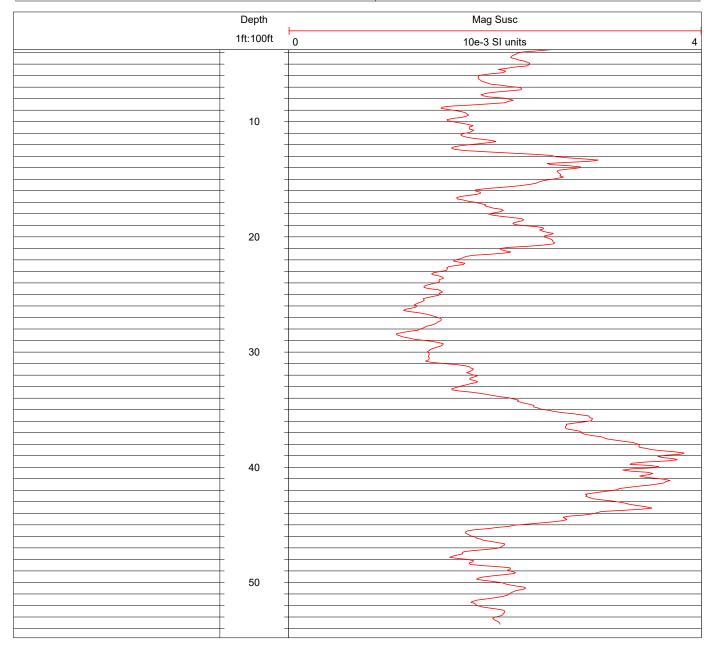
WIEDEMEIER & ASSOCIATES		TOOLHMA-453-SCALIBRATION DATE/TIME6/6/16 - 13:55CALIBRATION STANDARDS0 and 5E-3 SI UnitsCALIBRATION RESULTSZero = 70.56, 5E-3 = 1152.19 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Former Plattsburgh AFB	
WELL	MW-02-017 - Down - Run 2	
LOGGER	Todd Wiedemeier	Run 1 - Down had erronous data so Run 1 not used.
DATE	June 6, 2016	



		TOOLHMA-453-SCALIBRATION DATE/TIME6/6/16 - 13:55CALIBRATION STANDARDS0 and 5E-3 SI UnitsCALIBRATION RESULTSZero = 70.56, 5E-3 = 1152.19 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Former Plattsburgh AFB	
WELL	MW-02-017	
LOGGER	Todd Wiedemeier	
DATE	June 6, 2016	

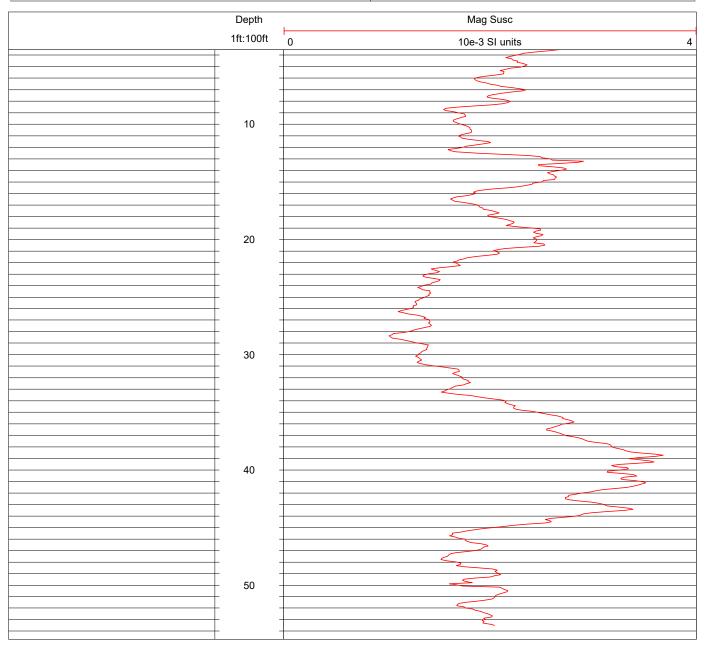


		TOOLHMA-453-SCALIBRATION DATE/TIME6/6/16 - 15:05CALIBRATION STANDARDS0 and 5E-3 SI UnitsCALIBRATION RESULTSZero = 79.94, 5E-3 = 1164.64 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Former Plattsburgh AFB	
WELL	MW-02-30 - Run 2-Down	
LOGGER	Todd Wiedemeier	Run 1-Down had erronous data so Run 1 not used.
DATE	June 6, 2016	



PROJECT	ESTCP 201584		
LOCATION	Former Plattsburgh AFB		
WELL	MW-02-30 - Up - Run 2		
LOGGER	Todd Wiedemeier		
DATE	June 6, 2016		

TOOLHMA-453-SCALIBRATION DATE/TIME6/6/16 - 15:05CALIBRATION STANDARDS0 and 5E-3 SI UnitsCALIBRATION RESULTSZero = 79.94 cps, 5E-3 = 1164.64 cpsREMARKS



E	•	/Down Average de Data	I	•	o/Down Average Ide Data	I	•	p/Down Average 1de Data	E	•	/Down Average de Data	I	•	)/Down Average Ide Data	EPA-21	D-Up/Dowr Sonde Dat	0
Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc
	(10e-3 SI			(10e-3 SI			(10e-3 SI			(10e-3 SI			(10e-3 SI			10e-3 SI	
(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units	(m3/kg)
3.54	0.68	4.02E-07	3.78	0.18	1.03E-07	3.78	0.55	3.25E-07	3.67	0.94	5.51E-07	3.61	0.46	2.68E-07	3.54	0.58	3.42E-07
3.64	0.68	3.98E-07	3.88	0.15	8.56E-08	3.90	0.57	3.34E-07	3.77	0.92	5.42E-07	3.71	0.44	2.59E-07	3.64	0.47	2.79E-07
3.76	0.67	3.96E-07	3.98	0.21	1.25E-07	4.00	0.58	3.41E-07	3.87	1.04	6.09E-07	3.81	0.51	2.98E-07	3.76	0.48	2.83E-07
3.86	0.67	3.96E-07	4.08	0.30	1.75E-07	4.10	0.57	3.38E-07	3.97	1.19	6.98E-07	3.91	0.47	2.74E-07	3.86	0.44	2.60E-07
3.96	0.67	3.94E-07	4.17	0.36	2.11E-07	4.20	0.58	3.39E-07	4.07	1.36	7.99E-07	4.01	0.44	2.59E-07	3.96	0.46	2.69E-07
4.06	0.67	3.91E-07	4.27	0.40	2.38E-07	4.30	0.57	3.33E-07	4.17	1.58	9.30E-07	4.11	0.42	2.44E-07	4.06	0.43	2.52E-07
4.16	0.67	3.94E-07	4.37	0.39	2.31E-07	4.40	0.61	3.59E-07	4.27	1.68	9.89E-07	4.21	0.42	2.45E-07	4.16	0.47	2.78E-07
4.26	0.63	3.70E-07	4.45	0.48	2.80E-07	4.50	0.58	3.43E-07	4.37	1.73	1.02E-06	4.31	0.41	2.41E-07	4.26	0.46	2.69E-07
4.36	0.66	3.86E-07	4.55	0.49	2.89E-07	4.60	0.56	3.28E-07	4.47	1.76	1.04E-06	4.41	0.45	2.66E-07	4.36	0.47	2.78E-07
4.46	0.68	4.01E-07	4.65	0.55	3.23E-07	4.70	0.56	3.31E-07	4.57	1.57	9.22E-07	4.51	0.41	2.39E-07	4.46	0.45	2.63E-07
4.56	0.66	3.90E-07	4.75	0.56	3.28E-07	4.80	0.58	3.40E-07	4.67	1.36	8.03E-07	4.61	0.48	2.80E-07	4.56	0.44	2.61E-07
4.655	0.71	4.15E-07	4.85	0.59	3.46E-07	4.90	0.64	3.74E-07	4.77	1.26	7.39E-07	4.71	0.46	2.68E-07	4.66	0.46	2.73E-07
4.755	0.73	4.29E-07	4.95	0.54	3.15E-07	5.00	0.60	3.50E-07	4.87	1.17	6.87E-07	4.81	0.46	2.69E-07	4.76	0.47	2.75E-07
4.855	0.68	3.98E-07	5.05	0.56	3.29E-07	5.10	0.55	3.25E-07	4.97	1.02	5.99E-07	4.91	0.43	2.53E-07	4.86	0.46	2.72E-07
4.955	0.73	4.27E-07	5.15	0.63	3.68E-07	5.20	0.53	3.11E-07	5.07	0.90	5.29E-07	5.00	0.43	2.55E-07	4.96	0.44	2.60E-07
5.05	0.68	4.03E-07	5.25	0.62	3.67E-07	5.30	0.53	3.12E-07	5.17	0.69	4.07E-07	5.10	0.40	2.38E-07	5.05	0.42	2.46E-07
5.15	0.72	4.24E-07	5.35	0.67	3.96E-07	5.40	0.53	3.14E-07	5.27	0.67	3.92E-07	5.20	0.49	2.87E-07	5.15	0.44	2.57E-07
5.25	0.77	4.52E-07	5.45	0.60	3.55E-07	5.50	0.55	3.23E-07	5.37	0.55	3.26E-07	5.30	0.46	2.72E-07	5.25	0.42	2.49E-07
5.35	0.69	4.07E-07	5.57	0.50	2.94E-07	5.60	0.53	3.11E-07	5.47	0.50	2.96E-07	5.40	0.44	2.60E-07	5.35	0.43	2.55E-07
5.45	0.77	4.51E-07	5.65	0.49	2.88E-07	5.70	0.51	3.00E-07	5.57	0.44	2.60E-07	5.50	0.42	2.49E-07	5.45	0.40	2.33E-07
5.55	0.79	4.63E-07	5.75	0.45	2.66E-07	5.80	0.57	3.35E-07	5.67	0.34	2.00E-07	5.60	0.45	2.66E-07	5.55	0.45	2.64E-07
5.65	0.80	4.69E-07	5.85	0.47	2.77E-07	5.90	0.56	3.30E-07	5.77	0.36	2.09E-07	5.70	0.45	2.67E-07	5.65	0.43	2.53E-07
5.75	0.80	4.72E-07	5.95	0.46	2.71E-07	6.00	0.57	3.35E-07	5.87	0.41	2.39E-07	5.80	0.47	2.75E-07	5.75	0.39	2.30E-07
5.85	0.86	5.08E-07	6.05	0.41	2.42E-07	6.10	0.58	3.39E-07	5.97	0.38	2.21E-07	5.90	0.45	2.63E-07	5.85	0.42	2.45E-07
5.95	0.83	4.86E-07	6.15	0.37	2.20E-07	6.20	0.57	3.35E-07	6.07	0.42	2.49E-07	6.00	0.46	2.71E-07	5.95	0.42	2.45E-07
6.05	0.86	5.03E-07	6.25	0.34	2.01E-07	6.30	0.54	3.18E-07	6.16	0.43	2.52E-07	6.10	0.48	2.84E-07	6.05	0.41	2.41E-07
6.15	0.84	4.97E-07	6.35	0.35	2.08E-07	6.40	0.53	3.13E-07	6.26	0.39	2.28E-07	6.20	0.46	2.68E-07	6.15	0.38	2.26E-07
6.25	0.82	4.84E-07	6.45	0.35	2.05E-07	6.50	0.57	3.36E-07	6.36	0.36	2.11E-07	6.30	0.48	2.81E-07	6.25	0.39	2.28E-07
6.35	0.84	4.91E-07	6.55	0.36	2.14E-07	6.60	0.57	3.36E-07	6.46	0.34	2.00E-07	6.40	0.48	2.80E-07	6.35	0.40	2.37E-07
6.45	0.80	4.72E-07	6.65	0.38	2.21E-07	6.69	0.58	3.44E-07	6.56	0.27	1.60E-07	6.50	0.44	2.62E-07	6.45	0.43	2.53E-07
6.55	0.81	4.76E-07	6.745	0.32	1.90E-07	6.79	0.61	3.59E-07	6.66	0.28	1.67E-07	6.60	0.43	2.51E-07	6.55	0.41	2.41E-07
6.65	0.82	4.84E-07	6.845	0.34	2.00E-07	6.89	0.58	3.43E-07	6.76	0.27	1.57E-07	6.70	0.45	2.62E-07	6.65	0.42	2.49E-07
6.75	0.82	4.84E-07	6.945	0.32	1.90E-07	6.99	0.61	3.61E-07	6.86	0.29	1.70E-07	6.80	0.45	2.67E-07	6.75	0.40	2.36E-07
6.85 6.95	0.80 0.76	4.71E-07 4.48E-07	7.045 7.145	0.31 0.28	1.85E-07 1.64E-07	7.09 7.19	0.62 0.60	3.62E-07 3.51E-07	6.96	0.25 0.21	1.49E-07 1.23E-07	6.90 7.00	0.43 0.45	2.53E-07 2.67E-07	6.85	0.40	2.37E-07 2.24E-07
									7.06					2.53E-07	6.95	0.38	
7.05 7.15	0.76 0.71	4.48E-07 4.17E-07	7.245 7.345	0.29 0.30	1.68E-07 1.74E-07	7.29 7.39	0.58 0.51	3.39E-07 2.99E-07	7.16 7.26	0.19 0.23	1.15E-07 1.35E-07	7.10 7.20	0.43 0.47	2.53E-07 2.77E-07	7.05 7.15	0.41 0.42	2.39E-07 2.47E-07
7.15														2.52E-07	7.15		
7.25	0.77	4.56E-07	7.44 7.54	0.27 0.26	1.56E-07	7.49 7.59	0.50	2.97E-07	7.36 7.46	0.24 0.25	1.44E-07	7.30 7.40	0.43 0.46		7.25	0.40 0.41	2.33E-07
7.35	0.78 0.75	4.59E-07 4.42E-07	7.54	0.26	1.55E-07 1.93E-07	7.59	0.47 0.43	2.76E-07 2.54E-07	7.46	0.25	1.45E-07 1.48E-07	7.40	0.46	2.70E-07 2.59E-07	7.35	0.41	2.38E-07 2.36E-07
						7.69										0.40	
7.55 7.65	0.77 0.78	4.51E-07 4.56E-07	7.74 7.84	0.26 0.25	1.55E-07 1.45E-07	7.79	0.40 0.38	2.36E-07 2.23E-07	7.66 7.76	0.25 0.26	1.50E-07 1.51E-07	7.60 7.70	0.48 0.55	2.81E-07 3.21E-07	7.55 7.65	0.48	2.82E-07 2.43E-07
7.65	0.78	4.56E-07 4.69E-07	7.84	0.25	1.45E-07 1.56E-07	7.89	0.38	2.23E-07 2.09E-07	7.76	0.26	1.51E-07 1.70E-07	7.70	0.55	3.21E-07 3.16E-07	7.65	0.41	2.43E-07 2.42E-07
7.75	0.80	4.69E-07 4.89E-07	7.94 8.04	0.26	1.56E-07 1.66E-07	7.99 8.09	0.35	2.09E-07 2.24E-07	7.86	0.29	1.70E-07 2.11E-07	7.80 7.90	0.54	3.16E-07 2.93E-07	7.75	0.41	2.42E-07 2.44E-07
7.85 7.95	0.83	4.89E-07 4.82E-07	8.04 8.14	0.28	1.80E-07 1.80E-07	8.09 8.19	0.38	2.24E-07 2.00E-07	7.96 8.06	0.36	2.11E-07 2.15E-07	7.90 8.00	0.50	2.93E-07 2.84E-07	7.85	0.41	2.44E-07 2.66E-07
7.95 8.045	0.82	4.82E-07 4.87E-07	8.14	0.31	1.66E-07	8.19	0.34	2.37E-07	8.06	0.37	2.15E-07 2.11E-07	8.00 8.10	0.48	2.84E-07 2.71E-07	7.95 8.05	0.45	2.66E-07 2.42E-07
8.045 8.145	0.83	4.87E-07 5.15E-07	8.24 8.34	0.28	1.90E-07	8.29	0.40	2.53E-07	8.16	0.36	2.23E-07	8.10	0.46	2.64E-07	8.05	0.41	2.42E-07 2.55E-07
0.145	0.00	J.1JL-07	0.54	0.52	1.501-07	0.33	0.45	2.331-07	0.20	0.50	2.231-07	0.20	0.45	2.041-07	0.15	0.45	2.356-07



E	•	/Down Average de Data			o/Down Average nde Data		•	o/Down Average Ide Data	E	•	o/Down Average Ide Data	I		o/Down Average Ide Data	EPA-21	D-Up/Down Sonde Data	-
Depth	Mag Susc		Depth		Mag Susc	Depth	Mag Susc		Depth		Mag Susc	Depth		Mag Susc	Depth	Mag Susc	
	(10e-3 SI			(10e-3 SI	-		(10e-3 SI			(10e-3 SI			(10e-3 SI	-		10e-3 SI	
(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units	(m3/kg)
8.245	0.91	5.36E-07	8.44	0.32	1.86E-07	8.49	0.46	2.71E-07	8.36	0.43	2.54E-07	8.29	0.46	2.74E-07	8.25	0.44	2.61E-07
8.34	0.94	5.52E-07	8.54	0.27	1.60E-07	8.59	0.42	2.49E-07	8.46	0.45	2.66E-07	8.39	0.40	2.32E-07	8.34	0.43	2.55E-07
8.44	0.96	5.64E-07	8.64	0.29	1.68E-07	8.69	0.47	2.78E-07	8.56	0.47	2.77E-07	8.49	0.43	2.54E-07	8.44	0.40	2.35E-07
8.54	0.91	5.33E-07	8.74	0.27	1.58E-07	8.79	0.50	2.94E-07	8.66	0.52	3.04E-07	8.59	0.40	2.34E-07	8.54	0.42	2.48E-07
8.64	0.90	5.31E-07	8.84	0.35	2.04E-07	8.89	0.49	2.87E-07	8.76	0.47	2.78E-07	8.69	0.40	2.36E-07	8.64	0.37	2.19E-07
8.74	0.89	5.26E-07	8.94	0.30	1.79E-07	8.99	0.46	2.70E-07	8.86	0.51	3.00E-07	8.79	0.45	2.63E-07	8.74	0.42	2.45E-07
8.84	0.90	5.28E-07	9.04	0.31	1.81E-07	9.09	0.51	2.99E-07	8.96	0.48	2.81E-07	8.89	0.42	2.50E-07	8.84	0.42	2.45E-07
8.94	0.94	5.55E-07	9.14	0.30	1.77E-07	9.19	0.46	2.73E-07	9.06	0.50	2.96E-07	8.99	0.43	2.53E-07	8.94	0.42	2.45E-07
9.04	0.93	5.45E-07	9.24	0.31	1.85E-07	9.29	0.50	2.92E-07	9.16	0.53	3.13E-07	9.09	0.40	2.34E-07	9.04	0.41	2.41E-07
9.14	0.96	5.62E-07	9.34	0.32	1.85E-07	9.39	0.47	2.78E-07	9.26	0.47	2.77E-07	9.19	0.42	2.45E-07	9.14	0.41	2.39E-07
9.24	0.97	5.70E-07	9.44	0.28	1.65E-07	9.49	0.45	2.66E-07	9.36	0.48	2.84E-07	9.29	0.42	2.47E-07	9.24	0.41	2.39E-07
9.34	0.98	5.75E-07	9.54	0.29	1.68E-07	9.59	0.45	2.62E-07	9.46	0.48	2.84E-07	9.39	0.40	2.32E-07	9.34	0.40	2.34E-07
9.44	0.99	5.84E-07	9.64	0.28	1.66E-07	9.69	0.47	2.76E-07	9.55	0.48	2.80E-07	9.49	0.45	2.67E-07	9.44	0.45	2.63E-07
9.54	1.03	6.05E-07	9.74	0.31	1.82E-07	9.79	0.49	2.90E-07	9.65	0.49	2.91E-07	9.59	0.43	2.54E-07	9.54	0.39	2.28E-07
9.64	0.97	5.73E-07	9.84	0.33	1.92E-07	9.89	0.49	2.87E-07	9.75	0.43	2.53E-07	9.69	0.42	2.49E-07	9.64	0.43	2.54E-07
9.74	0.96	5.64E-07	9.92	0.36	2.12E-07	9.98	0.46	2.73E-07	9.85	0.50	2.96E-07	9.79	0.45	2.66E-07	9.74	0.43	2.55E-07
9.84	0.95	5.60E-07	10.04	0.30	1.77E-07	10.08	0.47	2.75E-07	9.95	0.48	2.85E-07	9.89	0.46	2.71E-07	9.84	0.44	2.60E-07
9.94	0.98	5.75E-07	10.135	0.37	2.16E-07	10.18	0.47	2.79E-07	10.05	0.50	2.97E-07	9.99	0.48	2.80E-07	9.94	0.40	2.38E-07
10.04	0.98	5.79E-07	10.235	0.33	1.95E-07	10.28	0.49	2.86E-07	10.15	0.50	2.93E-07	10.09	0.50	2.93E-07	10.04	0.42	2.47E-07
10.14	0.99	5.83E-07	10.31	0.37	2.19E-07	10.38	0.45	2.67E-07	10.25	0.46	2.74E-07	10.19	0.51	3.03E-07	10.14	0.38	2.25E-07
10.24	0.96	5.63E-07	10.435	0.36	2.10E-07	10.48	0.46	2.69E-07	10.35	0.48	2.83E-07	10.29	0.56	3.28E-07	10.24	0.46	2.68E-07
10.34	0.97	5.70E-07	10.535	0.31	1.85E-07	10.58	0.47	2.75E-07	10.45	0.53	3.14E-07	10.39	0.53	3.10E-07	10.34	0.38	2.24E-07
10.44	0.99	5.83E-07	10.635	0.35	2.06E-07	10.68	0.45	2.63E-07	10.55	0.50	2.96E-07	10.49	0.53	3.12E-07	10.44	0.40	2.38E-07
10.54	0.96	5.64E-07	10.735	0.33	1.92E-07	10.78	0.44	2.61E-07	10.65	0.48	2.82E-07	10.59	0.54	3.16E-07	10.54	0.41	2.43E-07
10.64	0.98	5.78E-07	10.83	0.34	1.98E-07	10.88	0.49	2.89E-07	10.75	0.50	2.93E-07	10.69	0.51	3.02E-07	10.64	0.40	2.33E-07
10.74	1.00	5.87E-07	10.93	0.38	2.22E-07	10.98	0.49	2.87E-07	10.85	0.55	3.23E-07	10.79	0.51	3.02E-07	10.74	0.37	2.20E-07
10.84	0.96	5.66E-07	11.03	0.38	2.21E-07	11.08	0.46	2.73E-07	10.95	0.50	2.96E-07	10.89	0.49	2.89E-07	10.84	0.40	2.36E-07
10.94	0.95	5.60E-07	11.13	0.33	1.95E-07	11.18	0.45	2.63E-07	11.05	0.58	3.43E-07	10.99	0.48	2.79E-07	10.94	0.38	2.21E-07
11.04	0.93	5.46E-07	11.23	0.32	1.90E-07	11.28	0.44	2.56E-07	11.15	0.56	3.27E-07	11.09	0.48	2.85E-07	11.04	0.39	2.29E-07
11.14	0.97	5.70E-07	11.33	0.35	2.03E-07	11.38	0.40	2.38E-07	11.25	0.52	3.05E-07	11.19	0.51	3.00E-07	11.14	0.41	2.43E-07
11.24	1.00	5.91E-07	11.43	0.41	2.43E-07	11.48	0.44	2.60E-07	11.35	0.52	3.05E-07	11.29	0.52	3.04E-07	11.24	0.38	2.24E-07
11.335	1.04	6.09E-07	11.53	0.38	2.24E-07	11.58	0.46	2.72E-07	11.45	0.50	2.92E-07	11.39	0.48	2.83E-07	11.34	0.40	2.34E-07
11.435	1.01	5.95E-07	11.63	0.42	2.49E-07	11.68	0.46	2.70E-07	11.55	0.53	3.11E-07	11.49	0.50	2.96E-07	11.44	0.40	2.36E-07
11.535	0.94	5.53E-07	11.73	0.47	2.75E-07	11.78	0.43	2.53E-07	11.65	0.51	3.02E-07	11.59	0.49	2.90E-07	11.54	0.40	2.37E-07
11.63	0.95	5.62E-07	11.83	0.54	3.21E-07	11.88	0.42	2.45E-07	11.75	0.53	3.13E-07	11.68	0.47	2.79E-07	11.63	0.44	2.57E-07
11.73	1.04	6.11E-07	11.93	0.53	3.11E-07	11.98	0.42	2.45E-07	11.85	0.55	3.22E-07	11.78	0.46	2.71E-07	11.73	0.42	2.44E-07
11.83	1.02	6.02E-07	12.03	0.58	3.43E-07	12.08	0.44	2.61E-07	11.95	0.53	3.11E-07	11.88	0.49	2.88E-07	11.83	0.44	2.60E-07
11.93	1.00	5.90E-07	12.13	0.59	3.44E-07	12.18	0.45	2.63E-07	12.05	0.51	2.99E-07	11.98	0.45	2.65E-07	11.93	0.45	2.64E-07
12.03	1.03	6.04E-07	12.23	0.54	3.18E-07	12.28	0.46	2.73E-07	12.15	0.49	2.90E-07	12.08	0.48	2.81E-07	12.03	0.42	2.45E-07
12.13	1.00	5.88E-07	12.33	0.53	3.13E-07	12.38	0.44	2.60E-07	12.25	0.48	2.84E-07	12.18	0.41	2.43E-07	12.13	0.47	2.76E-07
12.23	0.98	5.74E-07	12.43	0.40	2.35E-07	12.48	0.45	2.67E-07	12.35	0.47	2.79E-07	12.28	0.44	2.61E-07	12.23	0.49	2.87E-07
12.33	0.97	5.72E-07	12.53	0.36	2.15E-07	12.58	0.45	2.65E-07	12.45	0.53	3.13E-07	12.38	0.39	2.32E-07	12.33	0.55	3.26E-07
12.43	0.96	5.66E-07	12.63	0.34	1.99E-07	12.68	0.50	2.93E-07	12.55	0.51	3.02E-07	12.48	0.37	2.18E-07	12.43	0.53	3.14E-07
12.53	0.87	5.14E-07	12.73	0.34	2.02E-07	12.78	0.43	2.52E-07	12.65	0.51	2.97E-07	12.58	0.36	2.14E-07	12.53	0.57	3.34E-07
12.63	0.81	4.79E-07	12.83	0.32	1.88E-07	12.88	0.44	2.59E-07	12.75	0.50	2.94E-07	12.68	0.33	1.91E-07	12.63	0.60	3.55E-07
12.73	0.77	4.53E-07	12.93	0.32	1.87E-07	12.98	0.46	2.69E-07	12.84	0.54	3.16E-07	12.78	0.30	1.75E-07	12.73	0.70	4.09E-07
12.83	0.82	4.82E-07	13.03	0.31	1.85E-07	13.08	0.48	2.81E-07	12.94	0.53	3.11E-07	12.88	0.28	1.62E-07	12.83	0.63	3.72E-07
12.93	0.76	4.48E-07	13.13	0.35	2.04E-07	13.18	0.46	2.70E-07	13.04	0.51	2.98E-07	12.98	0.28	1.62E-07	12.93	0.65	3.81E-07



E	•	/Down Average de Data		•	o/Down Average nde Data		•	o/Down Average Ide Data	E	•	o/Down Average Ide Data		•	)/Down Average de Data	EPA-21	D-Up/Down Sonde Data	-
Depth	Mag Susc		Depth		Mag Susc	Depth	Mag Susc		Depth		Mag Susc	Depth	Mag Susc		Depth		Mag Susc
	(10e-3 SI			(10e-3 SI	-		(10e-3 SI			(10e-3 SI			(10e-3 SI	-		10e-3 SI	
(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units	(m3/kg)
13.03	0.75	4.41E-07	13.23	0.28	1.68E-07	13.27	0.46	2.73E-07	13.14	0.52	3.06E-07	13.08	0.30	1.77E-07	13.03	0.67	3.96E-07
13.13	0.74	4.34E-07	13.33	0.37	2.18E-07	13.37	0.46	2.69E-07	13.24	0.50	2.94E-07	13.18	0.29	1.70E-07	13.13	0.65	3.82E-07
13.23	0.67	3.95E-07	13.425	0.38	2.25E-07	13.47	0.48	2.85E-07	13.34	0.51	3.00E-07	13.28	0.30	1.76E-07	13.23	0.65	3.85E-07
13.33	0.68	4.01E-07	13.525	0.39	2.32E-07	13.57	0.51	3.00E-07	13.44	0.48	2.83E-07	13.38	0.29	1.70E-07	13.33	0.69	4.07E-07
13.43	0.70	4.09E-07	13.625	0.45	2.64E-07	13.67	0.47	2.76E-07	13.54	0.52	3.06E-07	13.48	0.25	1.45E-07	13.43	0.67	3.95E-07
13.53	0.69	4.04E-07	13.725	0.44	2.58E-07	13.77	0.50	2.95E-07	13.64	0.49	2.86E-07	13.58	0.28	1.67E-07	13.53	0.63	3.70E-07
13.63	0.64	3.76E-07	13.825	0.40	2.35E-07	13.87	0.52	3.05E-07	13.74	0.49	2.87E-07	13.68	0.31	1.84E-07	13.63	0.68	4.00E-07
13.73	0.66	3.90E-07	13.925	0.42	2.50E-07	13.97	0.51	2.99E-07	13.84	0.50	2.95E-07	13.78	0.30	1.79E-07	13.73	0.66	3.90E-07
13.83	0.65	3.81E-07	14.025	0.36	2.11E-07	14.07	0.51	2.98E-07	13.94	0.54	3.16E-07	13.88	0.28	1.64E-07	13.83	0.66	3.87E-07
13.93	0.71	4.15E-07	14.12	0.32	1.89E-07	14.17	0.52	3.05E-07	14.04	0.53	3.11E-07	13.98	0.34	1.98E-07	13.93	0.65	3.84E-07
14.03	0.69	4.08E-07	14.22	0.29	1.73E-07	14.27	0.57	3.33E-07	14.14	0.49	2.89E-07	14.08	0.34	2.00E-07	14.03	0.68	4.01E-07
14.13	0.68	4.02E-07	14.32	0.37	2.15E-07	14.37	0.54	3.17E-07	14.24	0.49	2.91E-07	14.18	0.29	1.72E-07	14.13	0.64	3.76E-07
14.23	0.62	3.66E-07	14.42	0.32	1.90E-07	14.47	0.58	3.41E-07	14.34	0.45	2.66E-07	14.28	0.29	1.71E-07	14.23	0.66	3.89E-07
14.33	0.63	3.71E-07	14.52	0.31	1.82E-07	14.57	0.57	3.34E-07	14.44	0.49	2.90E-07	14.38	0.29	1.71E-07	14.33	0.67	3.95E-07
14.43	0.67	3.96E-07	14.62	0.26	1.50E-07	14.67	0.48	2.83E-07	14.54	0.48	2.84E-07	14.48	0.32	1.86E-07	14.43	0.66	3.87E-07
14.53	0.66	3.89E-07	14.72	0.26	1.53E-07	14.77	0.54	3.20E-07	14.64	0.48	2.80E-07	14.58	0.28	1.64E-07	14.53	0.72	4.22E-07
14.625	0.67	3.93E-07	14.82	0.24	1.42E-07	14.87	0.53	3.13E-07	14.74	0.48	2.80E-07	14.68	0.30	1.78E-07	14.63	0.73	4.28E-07
14.725	0.66	3.90E-07	14.92	0.28	1.64E-07	14.97	0.52	3.06E-07	14.84	0.48	2.84E-07	14.78	0.28	1.63E-07	14.73	0.65	3.82E-07
14.825	0.66	3.85E-07	15.02	0.26	1.51E-07	15.07	0.48	2.80E-07	14.94	0.53	3.11E-07	14.88	0.32	1.87E-07	14.83	0.69	4.07E-07
14.925	0.67	3.94E-07	15.12	0.27	1.59E-07	15.17	0.48	2.85E-07	15.04	0.53	3.11E-07	14.97	0.28	1.67E-07	14.93	0.69	4.05E-07
15.02	0.66	3.88E-07	15.22	0.28	1.66E-07	15.27	0.45	2.62E-07	15.14	0.54	3.15E-07	15.07	0.29	1.71E-07	15.02	0.71	4.15E-07
15.12	0.71	4.19E-07	15.32	0.29	1.68E-07	15.37	0.46	2.73E-07	15.24	0.52	3.08E-07	15.17	0.34	2.00E-07	15.12	0.70	4.13E-07
15.22	0.73	4.29E-07	15.42	0.30	1.79E-07	15.47	0.44	2.57E-07	15.34	0.50	2.91E-07	15.27	0.29	1.73E-07	15.22	0.69	4.05E-07
15.32	0.73	4.29E-07	15.52	0.31	1.80E-07	15.57	0.42	2.50E-07	15.44	0.49	2.87E-07	15.37	0.28	1.63E-07	15.32	0.69	4.08E-07
15.42	0.72	4.22E-07	15.62	0.30	1.79E-07	15.67	0.44	2.58E-07	15.54	0.53	3.09E-07	15.47	0.31	1.81E-07	15.42	0.65	3.85E-07
15.52	0.78	4.56E-07	15.72	0.29	1.70E-07	15.77	0.45	2.66E-07	15.64	0.48	2.83E-07	15.57	0.32	1.87E-07	15.52	0.69	4.04E-07
15.62	0.81	4.74E-07	15.82	0.27	1.61E-07	15.87	0.40	2.37E-07	15.74	0.52	3.05E-07	15.67	0.32	1.90E-07	15.62	0.65	3.80E-07
15.72	0.82	4.82E-07	15.92	0.35	2.05E-07	15.97	0.41	2.40E-07	15.84	0.52	3.07E-07	15.77	0.29	1.73E-07	15.72	0.68	3.99E-07
15.82	0.85	5.02E-07	16.02	0.29	1.73E-07	16.07	0.40	2.37E-07	15.94	0.50	2.94E-07	15.87	0.32	1.89E-07	15.82	0.66	3.89E-07
15.92	0.87	5.11E-07	16.12	0.27	1.60E-07	16.17	0.38	2.22E-07	16.04	0.52	3.05E-07	15.97	0.32	1.89E-07	15.92	0.67	3.93E-07
16.02	0.93	5.47E-07	16.22	0.30	1.74E-07	16.27	0.42	2.45E-07	16.13	0.50	2.92E-07	16.07	0.28	1.63E-07	16.02	0.69	4.05E-07
16.12	0.94	5.50E-07	16.32	0.34	1.98E-07	16.37	0.44	2.60E-07	16.23	0.51	2.98E-07	16.17	0.32	1.88E-07	16.12	0.73	4.32E-07
16.22	0.94	5.51E-07	16.42	0.32	1.88E-07	16.47	0.39	2.29E-07	16.33	0.50	2.94E-07	16.27	0.30	1.76E-07	16.22	0.65	3.85E-07
16.32	0.91	5.33E-07	16.52	0.36	2.13E-07	16.56	0.39	2.28E-07	16.43	0.48	2.81E-07	16.37	0.32	1.90E-07	16.32	0.66	3.86E-07
16.42	0.85	4.97E-07	16.62	0.30	1.78E-07	16.66	0.37	2.15E-07	16.53	0.51	2.97E-07	16.47	0.29	1.70E-07	16.42	0.66	3.86E-07
16.52	0.84	4.95E-07	16.715	0.34	1.97E-07	16.76	0.36	2.13E-07	16.63	0.50	2.94E-07	16.57	0.28	1.63E-07	16.52	0.65	3.83E-07
16.62	0.89	5.21E-07	16.815	0.35	2.06E-07	16.86	0.38	2.25E-07	16.73	0.46	2.71E-07	16.67	0.28	1.67E-07	16.62	0.64	3.77E-07
16.72	0.91	5.33E-07	16.915	0.37	2.17E-07	16.96	0.43	2.50E-07	16.83	0.47	2.74E-07	16.77	0.26	1.56E-07	16.72	0.68	3.97E-07
16.82	0.92	5.41E-07	17.015	0.39	2.27E-07	17.06	0.40	2.36E-07	16.93	0.46	2.72E-07	16.87	0.27	1.58E-07	16.82	0.63	3.72E-07
16.92	0.88	5.19E-07	17.115	0.39	2.31E-07	17.16	0.44	2.60E-07	17.03	0.44	2.59E-07	16.97	0.31	1.85E-07	16.92	0.67	3.93E-07
17.02	0.87	5.14E-07	17.215	0.44	2.58E-07	17.26	0.41	2.44E-07	17.13	0.49	2.88E-07	17.07	0.34	1.99E-07	17.02	0.68	3.98E-07
17.12	0.86	5.08E-07	17.315	0.37	2.19E-07	17.36	0.45	2.63E-07	17.23	0.48	2.81E-07	17.17	0.36	2.09E-07	17.12	0.69	4.08E-07
17.22	0.84	4.93E-07	17.41	0.41	2.40E-07	17.46	0.43	2.50E-07	17.33	0.46	2.70E-07	17.27	0.32	1.88E-07	17.22	0.73	4.32E-07
17.32	0.87	5.10E-07	17.51	0.34	1.98E-07	17.56	0.41	2.39E-07	17.43	0.53	3.10E-07	17.37	0.35	2.03E-07	17.32	0.72	4.23E-07
17.42	0.89	5.21E-07	17.61	0.36	2.13E-07	17.66	0.43	2.53E-07	17.53	0.52	3.04E-07	17.47	0.34	2.00E-07	17.42	0.76	4.47E-07
17.52	0.86	5.07E-07	17.71	0.41	2.41E-07	17.76	0.39	2.29E-07	17.63	0.44	2.61E-07	17.57	0.36	2.10E-07	17.52	0.69	4.07E-07
17.62	0.78	4.60E-07	17.81	0.41	2.40E-07	17.86	0.43	2.51E-07	17.73	0.44	2.60E-07	17.67	0.32	1.87E-07	17.62	0.68	4.00E-07
17.72	0.83	4.88E-07	17.91	0.45	2.63E-07	17.96	0.42	2.46E-07	17.83	0.48	2.84E-07	17.77	0.30	1.75E-07	17.72	0.68	3.99E-07
						2						,					



E	•	/Down Average de Data	I	•	)/Down Averago de Data	e	•	o/Down Average Ide Data	E	•	o/Down Averago Ide Data	e	•	/Down Average de Data	EPA-21	D-Up/Down Sonde Data	-
Depth	Mag Susc		Depth	Mag Susc		Depth	Mag Susc		Depth		Mag Susc	Depth	Mag Susc		Depth		Mag Susc
•	(10e-3 SI	0		(10e-3 SI	0	·	(10e-3 SI	0	•	(10e-3 SI	0	•	(10e-3 SI	0	•	10e-3 SI	0
(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units	(m3/kg)
17.82	0.81	4.74E-07	18.01	0.42	2.48E-07	18.06	0.43	2.55E-07	17.93	0.47	2.75E-07	17.87	0.31	1.83E-07	17.82	0.61	3.59E-07
17.92	0.86	5.05E-07	18.11	0.42	2.49E-07	18.16	0.41	2.38E-07	18.03	0.47	2.74E-07	17.97	0.25	1.48E-07	17.92	0.57	3.34E-07
18.015	0.83	4.86E-07	18.21	0.47	2.76E-07	18.26	0.46	2.69E-07	18.13	0.50	2.92E-07	18.07	0.31	1.84E-07	18.02	0.58	3.44E-07
18.115	0.79	4.66E-07	18.31	0.40	2.35E-07	18.36	0.46	2.68E-07	18.23	0.50	2.94E-07	18.17	0.29	1.72E-07	18.12	0.55	3.25E-07
18.215	0.74	4.36E-07	18.41	0.42	2.48E-07	18.46	0.40	2.37E-07	18.33	0.51	3.00E-07	18.26	0.29	1.72E-07	18.22	0.59	3.45E-07
18.31	0.85	5.00E-07	18.51	0.46	2.72E-07	18.56	0.39	2.27E-07	18.43	0.51	2.98E-07	18.36	0.31	1.85E-07	18.31	0.56	3.29E-07
18.41	0.87	5.11E-07	18.61	0.42	2.48E-07	18.66	0.44	2.60E-07	18.53	0.47	2.78E-07	18.46	0.33	1.96E-07	18.41	0.56	3.31E-07
18.51	0.95	5.56E-07	18.71	0.45	2.62E-07	18.76	0.42	2.47E-07	18.63	0.50	2.97E-07	18.56	0.30	1.76E-07	18.51	0.49	2.89E-07
18.81	0.90	5.29E-07	18.81	0.45	2.63E-07	18.86	0.43	2.55E-07	18.73	0.46	2.71E-07	18.66	0.26	1.56E-07	18.61	0.51	2.99E-07
18.91	0.98	5.78E-07	18.91	0.42	2.49E-07	18.96	0.40	2.38E-07	18.83	0.47	2.77E-07	18.76	0.33	1.93E-07	18.71	0.49	2.90E-07
19.01	1.01	5.93E-07	19.01	0.42	2.49E-07	19.06	0.40	2.34E-07	18.93	0.49	2.89E-07	18.86	0.30	1.77E-07	18.81	0.50	2.96E-07
19.11	1.01	5.92E-07	19.11	0.43	2.55E-07	19.16	0.43	2.53E-07	19.03	0.51	3.02E-07	18.96	0.30	1.75E-07	18.91	0.49	2.91E-07
19.21	1.08	6.36E-07	19.21	0.43	2.52E-07	19.26	0.44	2.60E-07	19.13	0.49	2.88E-07	19.06	0.27	1.60E-07	19.01	0.53	3.10E-07
19.31	1.01	5.91E-07	19.31	0.43	2.55E-07	19.36	0.41	2.41E-07	19.23	0.50	2.91E-07	19.16	0.29	1.73E-07	19.11	0.50	2.93E-07
19.41	1.02	6.03E-07	19.41	0.40	2.37E-07	19.46	0.41	2.41E-07	19.33	0.52	3.05E-07	19.26	0.27	1.62E-07	19.21	0.48	2.81E-07
19.51	1.05	6.15E-07	19.51	0.44	2.57E-07	19.56	0.38	2.22E-07	19.43	0.51	3.01E-07	19.36	0.31	1.84E-07	19.31	0.54	3.20E-07
19.61	1.07	6.32E-07	19.61	0.44	2.61E-07	19.66	0.37	2.18E-07	19.52	0.50	2.92E-07	19.46	0.31	1.80E-07	19.41	0.49	2.86E-07
19.71	1.06	6.21E-07	19.71	0.45	2.63E-07	19.76	0.42	2.46E-07	19.62	0.47	2.76E-07	19.56	0.30	1.75E-07	19.51	0.50	2.96E-07
19.81	1.05	6.19E-07	19.81	0.45	2.63E-07	19.86	0.41	2.39E-07	19.72	0.51	3.00E-07	19.66	0.33	1.97E-07	19.61	0.45	2.65E-07
19.91	0.99	5.83E-07	19.91	0.49	2.88E-07	19.95	0.41	2.39E-07	19.82	0.49	2.88E-07	19.76	0.31	1.81E-07	19.71	0.48	2.83E-07
20.01	1.08	6.34E-07	20.005	0.45	2.67E-07	20.05	0.39	2.31E-07	19.92	0.53	3.14E-07	19.86	0.31	1.82E-07	19.81	0.51	3.01E-07
20.11	1.09	6.43E-07	20.105	0.44	2.57E-07	20.15	0.40	2.35E-07	20.02	0.48	2.85E-07	19.96	0.29	1.69E-07	19.91	0.49	2.90E-07
20.21	1.10	6.44E-07	20.205	0.47	2.75E-07	20.25	0.43	2.50E-07	20.12	0.53	3.12E-07	20.06	0.34	1.98E-07	20.01	0.45	2.66E-07
20.31	1.09	6.39E-07	20.305	0.46	2.71E-07	20.35	0.45	2.66E-07	20.22	0.53	3.12E-07	20.16	0.30	1.74E-07	20.11	0.48	2.80E-07
20.41	1.06	6.25E-07	20.405	0.44	2.56E-07	20.45	0.42	2.44E-07	20.32	0.52	3.05E-07	20.26	0.28	1.66E-07	20.21	0.46	2.71E-07
20.51	1.03	6.07E-07	20.505	0.46	2.70E-07	20.55	0.41	2.42E-07	20.42	0.49	2.88E-07	20.36	0.29	1.70E-07	20.31	0.48	2.85E-07
20.61	1.10	6.48E-07	20.605	0.42	2.46E-07	20.65	0.44	2.57E-07	20.52	0.54	3.18E-07	20.46	0.28	1.63E-07	20.41	0.47	2.77E-07
20.71	1.10	6.48E-07	20.705	0.42	2.46E-07	20.75	0.39	2.30E-07	20.72	0.48	2.85E-07	20.56	0.29	1.71E-07	20.51	0.45	2.63E-07
20.81	1.02	5.98E-07	20.8	0.40	2.34E-07	20.85	0.36	2.14E-07	20.82	0.51	2.98E-07	20.66	0.28	1.63E-07	20.61	0.48	2.83E-07
20.91	1.07	6.31E-07	20.9	0.42	2.47E-07	20.95	0.41	2.43E-07	20.92	0.52	3.05E-07	20.76	0.28	1.65E-07	20.71	0.48	2.85E-07
21.01	1.06	6.23E-07	21	0.37	2.17E-07	21.05	0.42	2.46E-07	21.02	0.50	2.92E-07	20.86	0.29	1.69E-07	20.81	0.50	2.95E-07
21.11	1.05	6.16E-07	21.1	0.44	2.60E-07	21.15	0.40	2.33E-07	21.12	0.53	3.11E-07	20.96	0.33	1.92E-07	20.91	0.44	2.57E-07
21.21	1.06	6.26E-07	21.2	0.43	2.51E-07	21.25	0.43	2.51E-07	21.22	0.50	2.94E-07	21.06	0.30	1.79E-07	21.01	0.39	2.32E-07
21.305	1.07	6.27E-07	21.3	0.40	2.34E-07	21.35	0.39	2.28E-07	21.32	0.52	3.03E-07	21.16	0.28	1.65E-07	21.11	0.44	2.61E-07
21.405	1.08	6.38E-07	21.4	0.40	2.38E-07	21.45	0.42	2.44E-07	21.42	0.54	3.20E-07	21.26	0.30	1.77E-07	21.21	0.44	2.58E-07
21.505	1.00	5.91E-07	21.5	0.38	2.26E-07	21.55	0.42	2.45E-07	21.52	0.57	3.36E-07	21.36	0.27	1.59E-07	21.31	0.49	2.86E-07
21.605	0.97	5.69E-07	21.6	0.44	2.57E-07	21.65	0.41	2.41E-07	21.62	0.53	3.14E-07	21.46	0.27	1.58E-07	21.41	0.45	2.65E-07
21.7	1.00	5.86E-07	21.7	0.44	2.57E-07	21.75	0.39	2.32E-07	21.72	0.48	2.83E-07	21.56	0.29	1.72E-07	21.51	0.46	2.71E-07
21.8	1.00	5.88E-07	21.8	0.40	2.34E-07	21.85	0.44	2.56E-07	21.82	0.47	2.75E-07	21.65	0.28	1.62E-07	21.61	0.45	2.65E-07
21.9	1.01	5.92E-07	21.9	0.40	2.38E-07	21.95	0.44	2.60E-07	21.92	0.51	2.99E-07	21.75	0.31	1.82E-07	21.70	0.49	2.88E-07
22	0.97	5.72E-07	22	0.44	2.62E-07	22.05	0.41	2.43E-07	22.02	0.53	3.11E-07	21.85	0.27	1.59E-07	21.80	0.48	2.82E-07
22.1	0.86	5.07E-07	22.1	0.42	2.50E-07	22.15	0.43	2.54E-07	22.12	0.57	3.38E-07	21.95	0.26	1.56E-07	21.90	0.47	2.79E-07
22.2	0.85	5.00E-07	22.2	0.43	2.53E-07	22.25	0.46	2.71E-07	22.22	0.62	3.65E-07	22.05	0.31	1.83E-07	22.00	0.42	2.47E-07
22.3	0.90	5.30E-07	22.3	0.37	2.19E-07	22.35	0.42	2.46E-07	22.32	0.57	3.36E-07	22.15	0.27	1.60E-07	22.10	0.45	2.63E-07
22.4	0.94	5.50E-07	22.4	0.37	2.19E-07	22.45	0.48	2.83E-07	22.42	0.58	3.40E-07	22.25	0.26	1.54E-07	22.20	0.40	2.35E-07
22.5	0.89	5.24E-07	22.5	0.37	2.17E-07	22.55	0.46	2.72E-07	22.52	0.56	3.28E-07	22.35	0.30	1.77E-07	22.30	0.45	2.63E-07
22.6	0.86	5.06E-07	22.6	0.39	2.32E-07	22.65	0.48	2.80E-07	22.62	0.50	2.92E-07	22.45	0.30	1.78E-07	22.40	0.46	2.68E-07
22.7	0.85	5.00E-07	22.7	0.40	2.36E-07	22.75	0.48	2.83E-07	22.72	0.50	2.91E-07	22.55	0.29	1.69E-07	22.50	0.44	2.57E-07
			,									55			0		



E	• •	/Down Averag de Data	ge	•	)/Down Averag Ide Data	ge		o/Down Avera Ide Data	age	E	•	)/Down Average de Data		• •	'Down Average le Data	EPA-21	D-Up/Down Sonde Data	-
Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc		Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc
	(10e-3 SI			(10e-3 SI			(10e-3 SI				(10e-3 SI			(10e-3 SI			10e-3 SI	
(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)		(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units	(m3/kg)
22.8	0.85	5.01E-07	22.8	0.40	2.38E-07	22.85	0.50	2.92E-07		22.81	0.49	2.86E-07	22.65	0.30	1.76E-07	22.60	0.44	2.61E-07
22.9	0.85	5.02E-07	22.9	0.38	2.24E-07	22.95	0.46	2.71E-07		22.91	0.53	3.09E-07	22.75	0.29	1.72E-07	22.70	0.42	2.45E-07
23	0.88	5.17E-07	23	0.38	2.26E-07	23.05	0.43	2.55E-07		23.01	0.52	3.04E-07	22.85	0.28	1.67E-07	22.80	0.43	2.51E-07
23.1	0.85	4.97E-07	23.1	0.40	2.33E-07	23.15	0.45	2.66E-07		23.11	0.48	2.84E-07	22.95	0.31	1.84E-07	22.90	0.44	2.61E-07
23.2	0.76	4.47E-07	23.2	0.35	2.04E-07	23.24	0.42	2.46E-07		23.21	0.50	2.97E-07	23.05	0.32	1.88E-07	23.00	0.46	2.72E-07
23.3	0.82	4.84E-07	23.3	0.36	2.11E-07	23.34	0.42	2.48E-07		23.31	0.54	3.18E-07	23.15	0.28	1.64E-07	23.10	0.39	2.30E-07
23.4	0.82	4.80E-07	23.395	0.39	2.29E-07	23.44	0.36	2.15E-07		23.41	0.50	2.96E-07	23.25	0.28	1.65E-07	23.20	0.40	2.36E-07
23.5	0.82	4.83E-07	23.495	0.41	2.40E-07	23.54	0.41	2.39E-07		23.51	0.52	3.08E-07	23.35	0.27	1.59E-07	23.30	0.42	2.50E-07
23.6	0.83	4.85E-07	23.595	0.41	2.40E-07	23.64	0.34	1.99E-07		23.61	0.52	3.06E-07	23.45	0.30	1.76E-07	23.40	0.41	2.39E-07
23.7	0.76	4.49E-07	23.695	0.37	2.15E-07	23.74	0.38	2.21E-07		23.71	0.56	3.28E-07	23.55	0.31	1.81E-07	23.50	0.39	2.27E-07
23.8	0.74	4.32E-07	23.795	0.38	2.25E-07	23.84	0.40	2.37E-07		23.81	0.51	2.99E-07	23.65	0.33	1.96E-07	23.60	0.42	2.48E-07
23.9	0.75	4.42E-07	23.895	0.38	2.25E-07	23.94	0.33	1.97E-07		23.91	0.55	3.23E-07	23.75	0.34	2.02E-07	23.70	0.41	2.43E-07
24	0.76	4.44E-07	23.995	0.43	2.53E-07	24.04	0.42	2.48E-07		24.01	0.54	3.17E-07	23.85	0.34	1.98E-07	23.80	0.45	2.67E-07
24.1	0.79	4.65E-07	24.09	0.39	2.32E-07	24.14	0.42	2.46E-07		24.11	0.53	3.14E-07	23.95	0.34	1.98E-07	23.90	0.42	2.48E-07
24.2	0.81	4.79E-07	24.19	0.35	2.04E-07	24.24	0.41	2.40E-07		24.21	0.53	3.14E-07				24.00	0.43	2.54E-07
24.3	0.88	5.18E-07	24.29	0.36	2.09E-07	24.34	0.46	2.71E-07		24.31	0.54	3.17E-07				24.10	0.41	2.42E-07
24.4	0.91	5.37E-07	24.39	0.37	2.15E-07	24.44	0.41	2.43E-07		24.41	0.52	3.06E-07		Mean	1.76E-07	24.20	0.38	2.21E-07
24.5	0.88	5.20E-07	24.49	0.37	2.18E-07	24.54	0.44	2.61E-07		24.51	0.57	3.33E-07		Count	71	24.30	0.42	2.49E-07
24.6	0.85	5.01E-07	24.59	0.39	2.31E-07	24.64	0.40	2.32E-07		24.61	0.53	3.09E-07	Confi	dence Level(	3.30E-09	24.40	0.41	2.43E-07
24.695	0.85	5.02E-07	24.69	0.41	2.40E-07	24.74	0.38	2.21E-07		24.71	0.54	3.19E-07				24.50	0.42	2.47E-07
24.795	0.83	4.90E-07	24.79	0.40	2.37E-07	24.84	0.38	2.22E-07		24.81	0.52	3.07E-07				24.60	0.43	2.51E-07
24.895	0.87	5.15E-07	24.89	0.36	2.10E-07	24.94	0.33	1.96E-07		24.91	0.55	3.24E-07				24.70	0.43	2.54E-07
24.99	0.81	4.74E-07	24.99	0.38	2.22E-07	25.04	0.33	1.96E-07		25.01	0.57	3.34E-07				24.80	0.44	2.58E-07
25.09	0.81	4.79E-07	25.09	0.45	2.63E-07	25.14	0.28	1.67E-07		25.11	0.55	3.26E-07				24.90	0.41	2.43E-07
25.19	0.77	4.52E-07	25.19	0.38	2.26E-07	25.24	0.28	1.63E-07		25.21	0.46	2.69E-07				24.99	0.44	2.56E-07
25.29	0.77	4.55E-07	25.29	0.36	2.10E-07	25.34	0.27	1.58E-07		25.31	0.54	3.15E-07				25.09	0.44	2.60E-07
25.39	0.75	4.41E-07	25.39	0.34	2.03E-07	25.44	0.26	1.53E-07		25.41	0.54	3.18E-07				25.19	0.45	2.65E-07
25.49	0.69	4.07E-07	25.49	0.36	2.10E-07	25.54	0.23	1.36E-07		25.51	0.54	3.18E-07				25.29	0.41	2.42E-07
25.59	0.69	4.04E-07	25.59	0.41	2.40E-07	25.64	0.22	1.29E-07		25.61	0.53	3.13E-07				25.39	0.44	2.58E-07
25.69	0.66	3.86E-07	25.69	0.37	2.18E-07	25.74	0.28	1.64E-07		25.71	0.56	3.28E-07				25.49	0.43	2.54E-07
25.79	0.62	3.67E-07	25.79	0.41	2.40E-07	25.84	0.26	1.55E-07		25.81	0.53	3.11E-07				25.59	0.48	2.81E-07
25.89	0.60	3.54E-07	25.89	0.37	2.17E-07	25.94	0.29	1.73E-07		25.91	0.51	2.98E-07				25.69	0.40	2.37E-07
25.99	0.55	3.21E-07	25.99	0.33	1.93E-07	26.04	0.27	1.57E-07		26.01	0.47	2.78E-07				25.79	0.44	2.58E-07
26.09	0.52	3.06E-07	26.09	0.34	2.01E-07	26.14	0.31	1.81E-07		26.11	0.57	3.33E-07				25.89	0.53	3.13E-07
26.19	0.53	3.12E-07	26.19	0.33	1.93E-07	26.24	0.30	1.79E-07		26.20	0.52	3.09E-07				25.99	0.55	3.23E-07
26.29	0.47	2.74E-07	26.29	0.36	2.11E-07	26.34	0.28	1.67E-07		26.30	0.53	3.14E-07				26.09	0.66	3.87E-07
26.39	0.50	2.96E-07	26.39	0.36	2.12E-07	26.44	0.33	1.96E-07	#REF!	26.40	0.51	2.99E-07				26.19	0.63	3.70E-07
26.49	0.54	3.18E-07	26.49	0.35	2.07E-07	26.54	0.37	2.15E-07		26.50	0.53	3.13E-07				26.29	0.62	3.64E-07
26.59	0.52	3.08E-07	26.59	0.38	2.21E-07	26.63	0.34	1.99E-07		26.60	0.48	2.85E-07				26.39	0.54	3.16E-07
26.69	0.54	3.20E-07	26.685	0.35	2.05E-07	26.73	0.34	1.99E-07		26.70	0.51	3.00E-07				26.49	0.50	2.95E-07
26.79	0.59	3.45E-07	26.785	0.36	2.11E-07	26.83	0.34	1.99E-07		26.80	0.56	3.27E-07				26.59	0.46	2.73E-07
26.89	0.54	3.19E-07	26.885	0.37	2.17E-07	26.93	0.32	1.90E-07		26.90	0.55	3.26E-07				26.69	0.43	2.54E-07
26.99	0.52	3.06E-07	26.985	0.34	2.01E-07	27.03	0.32	1.86E-07		27.00	0.54	3.18E-07				26.79	0.39	2.32E-07
27.09	0.61	3.56E-07	27.085	0.40	2.35E-07	27.13	0.32	1.89E-07		27.10	0.56	3.28E-07				26.89	0.43	2.51E-07
27.19	0.61	3.59E-07	27.185	0.37	2.16E-07	27.23	0.31	1.85E-07		27.20	0.56	3.32E-07				26.99	0.41	2.43E-07
27.29	0.65	3.81E-07	27.285	0.38	2.25E-07	27.33	0.29	1.71E-07		27.30	0.57	3.34E-07				27.09	0.40	2.35E-07
27.39	0.66	3.86E-07	27.38	0.35	2.05E-07	27.43	0.24	1.43E-07		27.40	0.54	3.17E-07				27.19	0.48	2.81E-07
27.49	0.66	3.89E-07	27.48	0.36	2.14E-07	27.53	0.27	1.60E-07		27.50	0.53	3.10E-07				27.29	0.48	2.83E-07
			0													0		



E		/Down Averag de Data	ge	•	)/Down Average de Data		•	)/Down Aver de Data	age	E	•	/Down Average de Data		•	/Down Average de Data	EPA-21	D-Up/Dowr Sonde Dat	-
Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc		Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc
	(10e-3 SI			(10e-3 SI			(10e-3 SI				(10e-3 SI			(10e-3 SI			10e-3 SI	
(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)		(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units	(m3/kg)
27.59	0.62	3.66E-07	27.58	0.41	2.39E-07	27.63	0.25	1.48E-07		27.60	0.55	3.25E-07				27.39	0.48	2.80E-07
27.69	0.66	3.86E-07	27.68	0.42	2.48E-07	27.73	0.24	1.39E-07		27.70	0.56	3.27E-07				27.49	0.48	2.85E-07
27.79	0.64	3.78E-07	27.78	0.45	2.65E-07	27.83	0.26	1.53E-07		27.80	0.58	3.41E-07				27.59	0.47	2.75E-07
27.89	0.62	3.62E-07	27.88	0.42	2.45E-07	27.93	0.22	1.32E-07		27.90	0.54	3.20E-07				27.69	0.46	2.73E-07
27.985	0.59	3.49E-07	27.98	0.42	2.47E-07	28.03	0.27	1.57E-07		28.00	0.55	3.25E-07				27.79	0.45	2.67E-07
28.085	0.60	3.54E-07	28.08	0.49	2.90E-07	28.13	0.25	1.49E-07		28.10	0.54	3.19E-07				27.89	0.47	2.77E-07
28.185	0.60	3.53E-07	28.18	0.47	2.75E-07	28.23	0.26	1.52E-07	#REF!	28.20	0.57	3.38E-07				27.99	0.51	2.99E-07
28.28	0.64	3.75E-07	28.28	0.46	2.72E-07	28.33	0.27	1.57E-07		28.30	0.53	3.10E-07				28.09	0.45	2.64E-07
28.38	0.62	3.62E-07	28.4	0.42	2.46E-07	28.43	0.26	1.51E-07		28.40	0.56	3.29E-07				28.19	0.47	2.78E-07
28.48	0.57	3.35E-07	28.48	0.40	2.36E-07	28.53	0.28	1.65E-07		28.50	0.56	3.30E-07				28.28	0.43	2.53E-07
28.58	0.56	3.31E-07	28.58	0.40	2.36E-07	28.63	0.27	1.56E-07		28.60	0.52	3.08E-07				28.38	0.42	2.48E-07
28.68	0.55	3.25E-07	28.68	0.38	2.25E-07	28.73	0.31	1.80E-07		28.70	0.54	3.18E-07				28.48	0.48	2.83E-07
28.78	0.54	3.18E-07	28.78	0.41	2.39E-07	28.83	0.33	1.93E-07		28.80	0.53	3.11E-07				28.58	0.45	2.64E-07
28.88	0.53	3.13E-07	28.88	0.41	2.43E-07	28.93	0.32	1.87E-07		28.90	0.50	2.94E-07				28.68	0.46	2.73E-07
28.98	0.51	3.02E-07	28.98	0.48	2.82E-07	29.03	0.31	1.83E-07	#REF!	29.00	0.56	3.32E-07				28.78	0.43	2.52E-07
29.08	0.47	2.77E-07	29.06	0.53	3.12E-07	29.13	0.34	2.01E-07		29.10	0.54	3.17E-07				28.88	0.43	2.54E-07
29.18	0.46	2.68E-07	29.18	0.51	2.98E-07	29.23	0.30	1.77E-07		29.20	0.54	3.15E-07				28.98	0.46	2.68E-07
29.28	0.44	2.60E-07	29.28	0.60	3.52E-07	29.33	0.30	1.77E-07		29.30	0.56	3.32E-07				29.08	0.45	2.66E-07
29.38	0.44	2.61E-07	29.38	0.58	3.44E-07	29.43	0.30	1.75E-07		29.40	0.57	3.33E-07				29.18	0.47	2.76E-07
29.48	0.43	2.53E-07	29.48	0.57	3.33E-07	29.53	0.27	1.59E-07		29.49	0.58	3.43E-07				29.28	0.45	2.63E-07
29.58	0.44	2.57E-07	29.58	0.51	2.99E-07	29.63	0.21	1.24E-07		29.59	0.58	3.41E-07				29.38	0.51	3.00E-07
29.68	0.42	2.46E-07	29.68	0.44	2.59E-07	29.73	0.25	1.45E-07		29.69	0.50	2.94E-07				29.48	0.44	2.61E-07
29.78	0.45	2.64E-07	29.78	0.40	2.35E-07	29.83	0.24	1.43E-07		29.79	0.55	3.24E-07				29.58	0.45	2.62E-07
29.88	0.42	2.45E-07	29.9	0.36	2.13E-07	29.92	0.24	1.42E-07		29.89	0.52	3.07E-07				29.68	0.46	2.69E-07
29.98	0.46	2.68E-07	29.975	0.30	1.75E-07	30.02	0.26	1.53E-07		29.99	0.55	3.24E-07				29.78	0.43	2.52E-07
30.08	0.43	2.52E-07	30.075	0.24	1.41E-07	30.12	0.29	1.72E-07		30.09	0.55	3.25E-07				29.88	0.46	2.70E-07
30.18	0.41	2.42E-07	30.175	0.24	1.38E-07	30.22	0.31	1.84E-07		30.19	0.55	3.21E-07				29.98	0.41	2.38E-07
30.28	0.44	2.59E-07	30.275	0.25	1.45E-07	30.32	0.28	1.66E-07		30.29	0.57	3.36E-07				30.08	0.45	2.65E-07
30.38	0.51	3.00E-07	30.375	0.25	1.50E-07	30.42	0.30	1.74E-07		30.39	0.54	3.16E-07				30.18	0.44	2.61E-07
30.48	0.67	3.95E-07	30.475	0.23	1.34E-07	30.52	0.31	1.81E-07	#REF!	30.49	0.51	3.00E-07				30.28	0.45	2.67E-07
30.58	0.75	4.39E-07	30.575	0.22	1.32E-07	30.62	0.35	2.09E-07		30.59	0.51	2.99E-07				30.38	0.42	2.49E-07
30.68	0.79	4.62E-07	30.675	0.25	1.47E-07	30.72	0.39	2.29E-07		30.69	0.53	3.09E-07				30.48	0.45	2.66E-07
30.78	0.83	4.91E-07	30.77	0.25	1.47E-07	30.82	0.42	2.45E-07		30.79	0.55	3.21E-07				30.58	0.45	2.62E-07
30.88	0.89	5.22E-07	30.87	0.25	1.46E-07	30.92	0.47	2.79E-07		30.89	0.55	3.25E-07				30.68	0.48	2.80E-07
30.98	0.91	5.32E-07	30.97	0.23	1.35E-07	31.02	0.40	2.33E-07		30.99	0.55	3.25E-07				30.78	0.42	2.46E-07
31.08	0.91	5.34E-07	31.07	0.24	1.43E-07	31.12	0.43	2.54E-07		31.09	0.58	3.44E-07				30.88	0.47	2.74E-07
31.18	0.84	4.92E-07	31.17	0.31	1.84E-07	31.22	0.36	2.09E-07		31.19	0.55	3.26E-07				30.98	0.46	2.68E-07
31.275	0.71	4.19E-07	31.27	0.29	1.74E-07	31.32	0.36	2.11E-07		31.29	0.52	3.07E-07				31.08	0.45	2.65E-07
31.375	0.69	4.09E-07	31.37	0.24	1.42E-07	31.42	0.37	2.19E-07		31.39	0.54	3.16E-07				31.18	0.43	2.51E-07
31.475	0.61	3.57E-07	31.47	0.22	1.30E-07	31.52	0.39	2.27E-07	#REF!	31.49	0.50	2.94E-07				31.28	0.44	2.62E-07
31.57	0.57	3.34E-07	31.57	0.25	1.44E-07	31.62	0.40	2.35E-07		31.59	0.54	3.17E-07				31.38	0.44	2.60E-07
31.67	0.52	3.04E-07	31.67	0.22	1.30E-07	31.72	0.34	2.00E-07		31.69	0.53	3.12E-07				31.48	0.49	2.85E-07
31.77	0.50	2.95E-07	31.77	0.19	1.10E-07	31.82	0.39	2.28E-07		31.79	0.57	3.33E-07				31.57	0.41	2.40E-07
31.87	0.52	3.05E-07	31.87	0.15	8.91E-08	31.92	0.33	1.94E-07		31.89	0.49	2.90E-07				31.67	0.45	2.64E-07
31.97	0.56	3.32E-07	31.97	0.12	6.81E-08	32.02	0.36	2.14E-07		31.99	0.49	2.90E-07				31.77	0.46	2.70E-07
32.07	0.60	3.54E-07	32.07	0.12	7.34E-08	32.12	0.38	2.22E-07		32.09	0.53	3.09E-07				31.87	0.47	2.75E-07
32.17	0.54	3.20E-07	32.17	0.14	8.06E-08	32.22	0.37	2.20E-07		32.19	0.53	3.13E-07				31.97	0.44	2.59E-07
32.27	0.51	2.97E-07	32.27	0.15	8.68E-08	32.32	0.38	2.21E-07		32.29	0.56	3.27E-07				32.07	0.45	2.62E-07



E	• •	/Down Avera le Data	ge	•	/Down Average de Data		•	/Down Avera de Data	age	E	• •	/Down Averag de Data	ge I	•	/Down Average de Data	EPA-21	D-Up/Down Sonde Data	Average
Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc		Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc
	(10e-3 SI			(10e-3 SI			(10e-3 SI				(10e-3 SI			(10e-3 SI			10e-3 SI	
(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)		(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units	(m3/kg)
32.37	0.51	2.99E-07	32.37	0.12	7.19E-08	32.42	0.39	2.31E-07		32.39	0.52	3.07E-07				32.17	0.48	2.82E-07
32.47	0.50	2.92E-07	32.47	0.16	9.61E-08	32.52	0.42	2.46E-07	#REF!	32.49	0.53	3.13E-07				32.27	0.46	2.72E-07
32.57	0.45	2.65E-07	32.57	0.18	1.05E-07	32.62	0.43	2.53E-07		32.59	0.53	3.15E-07				32.37	0.49	2.87E-07
32.67	0.48	2.79E-07	32.67	0.21	1.22E-07	32.72	0.41	2.43E-07		32.69	0.51	2.99E-07				32.47	0.45	2.63E-07
32.77	0.43	2.53E-07	32.77	0.21	1.24E-07	32.82	0.41	2.40E-07		32.78	0.51	3.02E-07				32.57	0.44	2.61E-07
32.87	0.43	2.50E-07	32.87	0.18	1.06E-07	32.92	0.37	2.20E-07		32.88	0.53	3.10E-07				32.67	0.51	2.98E-07
32.97	0.38	2.22E-07	32.97	0.17	9.90E-08	33.02	0.41	2.43E-07		32.98	0.54	3.18E-07				32.77	0.50	2.96E-07
33.07	0.37	2.15E-07	33.07	0.16	9.67E-08	33.12	0.41	2.41E-07		33.08	0.50	2.93E-07				32.87	0.41	2.42E-07
33.17	0.39	2.30E-07	33.17	0.15	9.07E-08	33.21	0.42	2.47E-07		33.18	0.54	3.16E-07				32.97	0.40	2.38E-07
33.27	0.34	1.99E-07	33.27	0.19	1.12E-07	33.31	0.43	2.52E-07		33.28	0.55	3.23E-07				33.07	0.46	2.70E-07
33.37	0.33	1.94E-07	33.365	0.15	8.75E-08	33.41	0.39	2.31E-07	#REF!	33.38	0.48	2.82E-07				33.17	0.46	2.72E-07
33.47	0.31	1.81E-07	33.465	0.17	9.89E-08	33.51	0.38	2.23E-07		33.48	0.56	3.29E-07				33.27	0.46	2.71E-07
33.57	0.34	1.97E-07	33.565	0.18	1.05E-07	33.61	0.42	2.47E-07		33.58	0.55	3.22E-07				33.37	0.55	3.23E-07
33.67	0.33	1.94E-07	33.665	0.17	9.75E-08	33.71	0.39	2.29E-07		33.68	0.52	3.06E-07				33.47	0.49	2.87E-07
33.77	0.29 0.34	1.73E-07	33.765	0.16	9.14E-08 8.05E-08	33.81	0.43 0.43	2.53E-07		33.78	0.50 0.55	2.92E-07				33.57	0.51 0.46	3.01E-07
33.87 33.97	0.34	1.98E-07 2.01E-07	33.865 33.965	0.14 0.18	1.03E-07	33.91 34.01	0.43	2.54E-07 2.36E-07		33.88 33.98	0.55	3.23E-07 2.93E-07				33.67 33.77	0.46	2.70E-07 2.65E-07
34.07	0.34	2.01E-07 2.17E-07	34.06	0.18	8.30E-08	34.01 34.11	0.40	2.36E-07 2.34E-07		34.08	0.50	2.93E-07 3.34E-07				33.87	0.45	2.69E-07
34.07 34.17	0.37	2.17E-07 2.37E-07	34.06	0.14	8.98E-08	34.11	0.40	2.34E-07 2.26E-07		34.08 34.18	0.57	3.40E-07				33.97	0.48	2.89E-07 2.81E-07
34.17	0.40	2.29E-07	34.10	0.13	8.25E-08	34.21	0.38	2.20L-07 2.40E-07		34.18	0.58	3.34E-07				33.97	0.48	2.81L-07 2.82E-07
34.27	0.39	2.23L-07 2.47E-07	34.36	0.14	1.06E-07	34.31	0.41	2.40L-07 2.29E-07		34.28	0.58	3.34L-07 3.39E-07				34.07	0.48	2.54E-07
34.47	0.42	2.50E-07	34.46	0.18	1.07E-07	34.51	0.39	2.32E-07		34.48	0.58	3.45E-07				34.27	0.44	2.61E-07
34.565	0.43	2.77E-07	34.56	0.10	1.16E-07	34.61	0.35	2.32E-07 2.24E-07		34.58	0.60	3.55E-07				34.37	0.44	2.55E-07
34.665	0.51	3.00E-07	34.66	0.25	1.46E-07	34.71	0.35	2.04E-07		34.68	0.60	3.52E-07				34.47	0.41	2.44E-07
34.765	0.49	2.88E-07	34.76	0.20	1.19E-07	34.81	0.33	1.94E-07		34.78	0.59	3.46E-07				34.57	0.44	2.58E-07
34.865	0.54	3.20E-07	34.86	0.22	1.29E-07	34.91	0.33	1.93E-07		34.88	0.63	3.73E-07				34.67	0.43	2.54E-07
34.96	0.60	3.54E-07	34.96	0.20	1.16E-07	35.01	0.35	2.08E-07		34.98	0.56	3.29E-07				34.77	0.43	2.54E-07
35.06	0.58	3.43E-07	35.04	0.19	1.09E-07	35.11	0.28	1.63E-07		35.08	0.61	3.61E-07				34.87	0.47	2.75E-07
35.16	0.62	3.62E-07	35.16	0.18	1.06E-07	35.21	0.28	1.63E-07		35.18	0.62	3.62E-07				34.96	0.47	2.74E-07
35.26	0.62	3.65E-07	35.26	0.14	8.08E-08	35.31	0.30	1.78E-07		35.28	0.64	3.76E-07				35.06	0.40	2.36E-07
35.36	0.68	3.97E-07	35.36	0.10	6.09E-08	35.41	0.25	1.48E-07		35.38	0.66	3.86E-07				35.16	0.46	2.72E-07
35.46	0.58	3.38E-07	35.46	0.19	1.11E-07	35.51	0.28	1.67E-07	#REF!	35.48	0.66	3.91E-07				35.26	0.48	2.82E-07
35.56	0.64	3.74E-07	35.56	0.24	1.41E-07	35.61	0.30	1.74E-07		35.58	0.66	3.89E-07				35.36	0.44	2.61E-07
35.66	0.60	3.52E-07	35.66	0.29	1.72E-07	35.71	0.29	1.70E-07		35.68	0.63	3.72E-07				35.46	0.47	2.74E-07
35.76	0.64	3.79E-07	35.76	0.40	2.38E-07	35.81	0.31	1.85E-07		35.78	0.71	4.15E-07				35.56	0.43	2.54E-07
35.86	0.63	3.70E-07	35.86	0.39	2.27E-07	35.91	0.34	2.01E-07		35.88	0.71	4.18E-07				35.66	0.44	2.57E-07
35.96	0.65	3.85E-07	35.96	0.39	2.32E-07	36.01	0.33	1.93E-07		35.98	0.66	3.87E-07				35.76	0.46	2.68E-07
36.06	0.65	3.80E-07	36.06	0.35	2.05E-07	36.11	0.38	2.21E-07		36.08	0.65	3.81E-07				35.86	0.58	3.43E-07
36.16	0.62	3.66E-07	36.16	0.30	1.76E-07	36.21	0.34	2.01E-07		36.17	0.62	3.68E-07						
36.26	0.63	3.69E-07	36.26	0.24	1.39E-07	36.31	0.41	2.43E-07		36.27	0.55	3.26E-07						
36.36	0.63	3.69E-07	36.36	0.16	9.20E-08	36.41	0.36	2.12E-07		36.37	0.54	3.20E-07					Mean	2.87E-07
36.46	0.65	3.83E-07	36.46	0.14	8.09E-08	36.51	0.42	2.46E-07		36.47	0.54	3.15E-07					Count	204.00
36.56	0.65	3.81E-07	36.56	0.15	8.98E-08	36.60	0.38	2.24E-07		36.57	0.46	2.68E-07				Confidence L	evel(95.0%)	6.75E-09
36.66	0.61	3.58E-07	36.655	0.17	9.77E-08	36.70	0.43	2.55E-07		36.67	0.48	2.84E-07						
36.76	0.64	3.78E-07	36.755	0.18	1.06E-07	36.80	0.45	2.64E-07		36.77	0.48	2.84E-07						
36.86	0.59	3.47E-07	36.855	0.20	1.17E-07	36.90	0.43	2.55E-07		36.87	0.44	2.57E-07						
36.96	0.63	3.71E-07	36.955	0.20	1.19E-07	37.00	0.49	2.89E-07		36.97	0.45	2.62E-07						
37.06	0.60	3.53E-07	37.055	0.19	1.11E-07	37.10	0.49	2.87E-07		37.07	0.39	2.31E-07						



E	• •	/Down Avera de Data	ge	•	/Down Average de Data		•	/Down Average de Data	E	•	/Down Average de Data	E	•	/Down Average de Data		)-Up/Down Sonde Data	-
Depth	Mag Susc		Depth	Mag Susc		Depth	Mag Susc		Depth	Mag Susc		Depth	Mag Susc			Mag Susc	
	(10e-3 SI			(10e-3 SI			(10e-3 SI			(10e-3 SI			(10e-3 SI			10e-3 SI	
(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units	(m3/kg)
37.16	0.64	3.75E-07	37.155	0.21	1.22E-07	37.20	0.49	2.88E-07	37.17	0.38	2.26E-07						
37.26	0.68	3.98E-07	37.255	0.25	1.48E-07	37.30	0.48	2.81E-07	37.27	0.35	2.08E-07						
37.36	0.63	3.68E-07	37.355	0.23	1.37E-07	37.40	0.48	2.83E-07	37.37	0.35	2.04E-07						
37.46	0.62	3.66E-07	37.45	0.30	1.76E-07	37.50	0.49	2.86E-07	37.47	0.32	1.88E-07						
37.56	0.62	3.64E-07	37.55	0.26	1.54E-07	37.60	0.49	2.90E-07	37.57	0.33	1.97E-07						
37.66	0.57	3.37E-07	37.65	0.23	1.35E-07	37.70	0.44	2.59E-07	37.67	0.31	1.84E-07						
37.76	0.58	3.44E-07	37.75	0.26	1.52E-07	37.80	0.47	2.74E-07	37.77	0.37	2.15E-07						
37.86	0.57	3.35E-07	37.85	0.23	1.35E-07	37.90	0.48	2.80E-07	37.87	0.36	2.12E-07						
37.955 38.055	0.58 0.64	3.40E-07	37.95	0.24	1.40E-07	38.00	0.43	2.56E-07	37.97	0.34	1.97E-07						
		3.74E-07	38.05	0.21	1.24E-07	38.10	0.48	2.85E-07	38.07	0.41	2.39E-07						
38.155	0.63	3.73E-07	38.15	0.21 0.25	1.24E-07	38.20	0.48	2.80E-07	38.17	0.37	2.19E-07						
38.25	0.64	3.74E-07	38.25		1.47E-07	38.30	0.43	2.53E-07	38.27	0.31	1.84E-07						
38.35	0.60	3.51E-07	38.35	0.20	1.18E-07	38.40	0.42	2.47E-07	38.37	0.34	2.00E-07						
38.45	0.64	3.79E-07	38.45	0.23	1.36E-07	38.50	0.42	2.50E-07	38.47	0.37	2.16E-07						
38.55	0.64	3.78E-07	38.55	0.17	1.02E-07	38.60	0.46	2.69E-07	38.57	0.34	1.97E-07						
38.65	0.67 0.66	3.96E-07 3.88E-07	38.65	0.24 0.20	1.41E-07 1.19E-07	38.70 38.80	0.45 0.44	2.66E-07	38.67	0.36 0.34	2.10E-07 2.02E-07						
38.75	0.66	3.88E-07 3.67E-07	38.75	0.20	1.19E-07 1.19E-07		0.44	2.61E-07	38.77	0.34	2.02E-07 2.24E-07						
38.85 38.95	0.62	3.67E-07 3.75E-07	38.85 38.95	0.20	1.09E-07	38.90 39.00	0.41	2.40E-07 2.38E-07	38.87 38.97	0.38	2.31E-07						
	0.59	3.49E-07		0.19		39.00	0.40	2.38E-07 2.43E-07		0.39	2.39E-07						
39.05 39.15	0.59	3.49E-07 3.32E-07	39.05	0.20	1.16E-07 9.76E-08	39.10	0.41	2.43E-07 2.62E-07	39.07 39.17	0.41	2.39E-07 2.43E-07						
39.15	0.58	3.42E-07	39.15 39.25	0.17	1.36E-07	39.20	0.43	2.37E-07	39.17	0.41	2.35E-07						
39.25	0.58	3.71E-07	39.25	0.23	1.32E-07	39.30	0.40	2.37E-07 2.11E-07	39.37	0.40	2.36E-07						
39.35	0.63	3.71E-07 3.71E-07	39.35	0.22	8.86E-08	39.40	0.30	2.17E-07 2.17E-07	39.46	0.40	2.17E-07						
39.45	0.57	3.34E-07	39.55	0.13	1.05E-07	39.50	0.37	1.71E-07	39.56	0.37	2.41E-07						
39.55	0.56	3.34E-07 3.32E-07	39.65	0.18	9.44E-08	39.00	0.29	1.81E-07	39.66	0.41	2.54E-07						
39.05	0.55	3.32L-07 3.25E-07	39.05	0.10	9.33E-08	39.70	0.31	2.38E-07	39.76	0.45	2.63E-07						
39.85	0.59	3.50E-07	39.85	0.15	8.92E-08	39.87	0.40	1.81E-07	39.86	0.43	2.39E-07						
39.95	0.60	3.51E-07	39.945	0.18	1.06E-07	39.97	0.30	1.77E-07	39.96	0.37	2.16E-07						
40.05	0.58	3.42E-07	40.045	0.18	1.08E-07	40.07	0.28	1.67E-07	40.06	0.40	2.33E-07						
40.15	0.57	3.38E-07	40.145	0.16	9.56E-08	40.17	0.26	1.53E-07	40.00	0.40	2.06E-07						
40.25	0.56	3.29E-07	40.245	0.16	9.68E-08	40.27	0.26	1.51E-07	40.26	0.42	2.46E-07						
40.35	0.61	3.56E-07	40.345	0.18	1.06E-07	40.37	0.26	1.51E-07	40.36	0.39	2.30E-07						
40.45	0.62	3.68E-07	40.445	0.20	1.17E-07				40.46	0.33	1.91E-07						
40.55	0.62	3.63E-07	40.545	0.17	9.78E-08	·			40.56	0.31	1.79E-07						
40.65	0.60	3.55E-07	40.645	0.15	9.10E-08		Mean	1.98E-07	40.66	0.31	1.80E-07						
40.75	0.59	3.47E-07	40.74	0.14	8.20E-08		Count	92	40.76	0.28	1.65E-07						
40.85	0.57	3.32E-07	40.84	0.13	7.43E-08	Confidence I			40.86	0.30	1.76E-07						
40.95	0.59	3.45E-07	40.94	0.17	9.92E-08				40.96	0.29	1.72E-07						
41.05	0.64	3.74E-07	41.04	0.15	9.07E-08				41.06	0.29	1.72E-07						
41.15	0.67	3.94E-07	41.14	0.13	7.36E-08				41.16	0.34	2.00E-07						
41.245	0.69	4.08E-07	41.24	0.16	9.29E-08				41.26	0.31	1.82E-07						
41.345	0.65	3.82E-07	41.34	0.16	9.43E-08				41.36	0.33	1.94E-07						
41.445	0.59	3.46E-07	41.44	0.16	9.64E-08				41.46	0.36	2.14E-07						
41.54	0.64	3.74E-07	41.54	0.15	8.93E-08				41.56	0.34	2.02E-07						
41.64	0.65	3.82E-07	41.64	0.15	8.90E-08				41.66	0.34	1.97E-07						
41.74	0.67	3.91E-07	41.74	0.15	8.81E-08				41.76	0.37	2.19E-07						
41.84	0.64	3.79E-07	41.84	0.13	7.91E-08				41.86	0.36	2.09E-07						



E	•	/Down Average de Data	E		/Down Average de Data		•	)/Down Average de Data	E		/Down Average de Data	E	•	)/Down Average de Data		D-Up/Down Sonde Data	-
Depth	Mag Susc (10e-3 SI	Mag Susc	Depth	Mag Susc (10e-3 SI	Mag Susc	Depth	Mag Susc (10e-3 SI	Mag Susc	Depth	Mag Susc (10e-3 SI	Mag Susc	Depth	Mag Susc (10e-3 SI	Mag Susc	Depth	Mag Susc 10e-3 SI	Mag Susc
(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units	(m3/kg)
41.94	0.65	3.85E-07	41.94	0.14	8.29E-08	(10 080)	unicoj	(110) 16)	41.96	0.39	2.27E-07	(10 080)	unicoj	(	(10 080)	unito	(110) (18)
42.04	0.65	3.82E-07	42.04	0.15	8.67E-08				42.06	0.36	2.14E-07						
42.14	0.67	3.95E-07	42.14	0.15	8.91E-08				42.16	0.38	2.25E-07						
42.24	0.63	3.70E-07	42.24	0.16	9.22E-08				42.26	0.39	2.29E-07						
42.34	0.65	3.85E-07	42.34	0.13	7.61E-08				42.36	0.41	2.43E-07						
42.44	0.61	3.58E-07	42.44	0.14	8.32E-08				42.46	0.42	2.45E-07						
42.54	0.63	3.68E-07	42.54	0.16	9.56E-08				42.56	0.43	2.51E-07						
42.64	0.64	3.74E-07	42.64	0.15	8.77E-08				42.66	0.42	2.50E-07						
42.74	0.65	3.81E-07	42.74	0.16	9.15E-08				42.75	0.46	2.73E-07						
42.84	0.62	3.64E-07	42.84	0.18	1.05E-07				42.85	0.48	2.85E-07						
42.94	0.61	3.61E-07	42.94	0.09	5.17E-08				42.95	0.42	2.46E-07						
43.04	0.66	3.88E-07							43.05	0.44	2.60E-07						
43.14	0.67	3.92E-07		Mean	1.67E-07				43.25	0.44	2.59E-07						
43.24	0.60	3.56E-07		Count	224				43.35	0.44	2.61E-07						
43.34	0.64	3.74E-07	Confidence L	evel(95.0%)	8.99E-09				43.45	0.44	2.57E-07						
43.44	0.64	3.77E-07							43.55	0.46	2.69E-07						
43.54	0.73	4.27E-07							43.65	0.43	2.51E-07						
43.64	0.70	4.11E-07							43.75	0.43	2.55E-07						
43.74	0.68	3.99E-07							43.85	0.42	2.45E-07						
43.84	0.73	4.28E-07							43.95	0.46	2.71E-07						
43.94	0.71	4.18E-07							44.05	0.46	2.68E-07						
44.04	0.76	4.46E-07							44.15	0.40	2.37E-07						
44.14	0.78	4.59E-07							44.25	0.49	2.87E-07						
44.24	0.81	4.74E-07							44.35	0.47	2.75E-07						
44.34	0.79	4.66E-07							44.45	0.46	2.73E-07						
44.44	0.77	4.55E-07							44.55	0.48	2.80E-07						
44.535	0.72	4.23E-07							44.65	0.47	2.78E-07						
44.635	0.73	4.31E-07							44.75	0.49	2.87E-07						
44.735	0.73	4.29E-07							44.85	0.43	2.55E-07						
44.835	0.68	4.03E-07							44.95	0.44	2.60E-07						
44.93	0.75	4.39E-07							45.05	0.44	2.57E-07						
45.13	0.68	4.02E-07							45.15	0.42	2.46E-07						
45.23	0.67	3.92E-07							45.25	0.42	2.46E-07						
45.33	0.72	4.24E-07							45.35	0.36	2.13E-07						
45.43	0.73	4.28E-07							45.45	0.38	2.22E-07						
45.53	0.71	4.17E-07							45.55	0.38	2.24E-07						
45.63	0.76	4.46E-07							45.65	0.39	2.28E-07						
45.73	0.68	3.97E-07							45.75	0.37	2.16E-07						
45.83	0.69	4.05E-07							45.85	0.35	2.09E-07						
45.93	0.74	4.34E-07							45.95	0.40	2.37E-07						
46.03	0.72	4.23E-07							46.05	0.43	2.51E-07						
46.13	0.69	4.07E-07							46.14	0.41 0.35	2.43E-07						
46.23	0.65	3.81E-07							46.24		2.07E-07						
46.33 46.43	0.64 0.61	3.76E-07 3.56E-07							46.34 46.44	0.39 0.42	2.32E-07 2.46E-07						
46.43	0.51	3.20E-07							46.44	0.42	2.26E-07						
46.53	0.54	3.04E-07							46.64	0.38	2.26E-07 2.45E-07						
46.73	0.32	2.74E-07							46.74	0.42	2.49E-07						
	0.47	0,							40.74	0.72							



E		/Down Average le Data	E		'Down Average le Data	E		/Down Average de Data	E		/Down Average de Data	E		'Down Average le Data		-Up/Down Sonde Data	
Depth	Mag Susc		Depth	Mag Susc		Depth	Mag Susc		Depth	Mag Susc		Depth	Mag Susc			Mag Susc	
(ft has)	(10e-3 SI	(100)	(ft h co)	(10e-3 SI	(	(ft h co)	(10e-3 SI	(	(ft has)	(10e-3 SI	(	(ft has)	(10e-3 SI	(	(ft has)	10e-3 SI	(
(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units	(m3/kg)
46.83	0.44	2.60E-07							46.84	0.42	2.50E-07						
46.93	0.45	2.63E-07							46.94	0.39	2.28E-07						
47.03	0.43	2.54E-07							47.04	0.41	2.42E-07						
47.13	0.40	2.34E-07							47.14	0.42	2.49E-07						
47.23	0.44	2.57E-07							47.24	0.41	2.41E-07						
47.33	0.40	2.36E-07							47.34	0.40	2.34E-07						
47.43	0.43	2.54E-07							47.44	0.42	2.45E-07						
47.53	0.48	2.83E-07							47.54	0.42	2.46E-07						
47.63	0.56	3.28E-07							47.64	0.44	2.58E-07						
47.73	0.60	3.51E-07							47.74	0.39	2.28E-07						
47.83	0.58	3.39E-07							47.84	0.45	2.62E-07						
47.925	0.59	3.50E-07							47.94	0.48	2.80E-07						
48.025	0.62	3.63E-07															
48.125	0.66	3.86E-07															
48.22	0.69	4.06E-07								Mean	2.84E-07						
48.32	0.68	4.01E-07								Count	273						
48.42	0.65	3.80E-07							Confidence Le	evel(95.0%)	6.1E-09						
48.52	0.66	3.88E-07															
48.62	0.68	4.01E-07															
48.72	0.70	4.15E-07															
48.82	0.75	4.41E-07															
48.92	0.76	4.46E-07															
49.02	0.72	4.22E-07															
49.12	0.75	4.40E-07															
49.22	0.75	4.43E-07															
49.32	0.70	4.10E-07															
49.42	0.74	4.33E-07															
49.52	0.69	4.05E-07															
49.62	0.64	3.75E-07															
49.72	0.68	3.98E-07															
49.82	0.62	3.64E-07															
49.92	0.61	3.57E-07															
50.02	0.59	3.46E-07															
50.12	0.54	3.16E-07															
50.22	0.52	3.06E-07															
50.32	0.48	2.84E-07															
50.42	0.41	2.40E-07															
50.52	0.39	2.30E-07															
50.62	0.36	2.11E-07															
50.72	0.35	2.05E-07															
50.82	0.36	2.11E-07	_														
50.92	0.31	1.85E-07															
51.02	0.36	2.10E-07															
51.12	0.36	2.15E-07															
51.215	0.39	2.30E-07															
51.315	0.39	2.28E-07															
51.415	0.42	2.46E-07															
51.51	0.41	2.42E-07															



E		'Down Average le Data	I	•	/Down Average de Data	I	•	o/Down Average Ide Data	E		/Down Average de Data	E	• •	/Down Average de Data		)-Up/Down Sonde Data	0
Depth	Mag Susc	Mag Susc	Depth	Mag Susc	0	Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc	Depth	Mag Susc	Mag Susc
	(10e-3 SI			(10e-3 SI			(10e-3 SI			(10e-3 SI			(10e-3 SI			10e-3 SI	
(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units)	(m3/kg)	(ft bgs)	units	(m3/kg)
51.61	0.46	2.68E-07															
51.71	0.50	2.92E-07															
51.81	0.49	2.90E-07															
	Mean	3.47E-07															
	Count																
Confi	dence																
Level(	95.0%)	8.47E-09															

-AV	F	TOOL HMA-453-S
		CALIBRATION DATE/TIME 6/8/16 11:36
WIEDEN		CALIBRATION STANDARDS 0 and 5E-3 SI Units
& ASSO(	CIATES	CALIBRATION RESULTS Zero = 70.532, 5E-3 = 1105.86
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	
WELL	EPA-16D - Down	
LOGGER	Todd Wiedemeier	
DATE	June 8, 2016	

Depth		Mag Susc
1ft:100	)ft	0 10e-3 SI units 1
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-AA	L	TOOL HMA-453-S
		CALIBRATION DATE/TIME 6/8/16
WIEDEMEIER		CALIBRATION STANDARDS 0 and 5E-3 SI Units
& ASSO(	CIATES	CALIBRATION RESULTS Zero = 70.53, 5E-3 = 1105.86 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	
WELL	EPA-16D Up	
LOGGER	Todd Wiedemeier	
DATE	June 8, 2016	

Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 1
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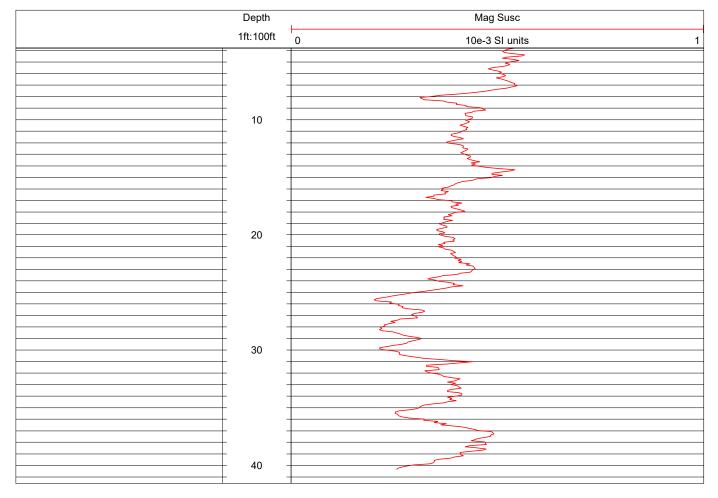
		TOOL HMA-453-S CALIBRATION DATE/TIME 6/8/16 11:36 CALIBRATION STANDARDS 0 and 5E-3 SI Units CALIBRATION RESULTS Zero = 70.53, 5E-3 = 1105.86
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	NEWIARKS
WELL	EPA-16S Down	
LOGGER	Todd Wiedemeier	
DATE	June 8, 2016	

De	pth		Mag Susc	
1ft: 1	100ft	0	10e-3 SI units	1
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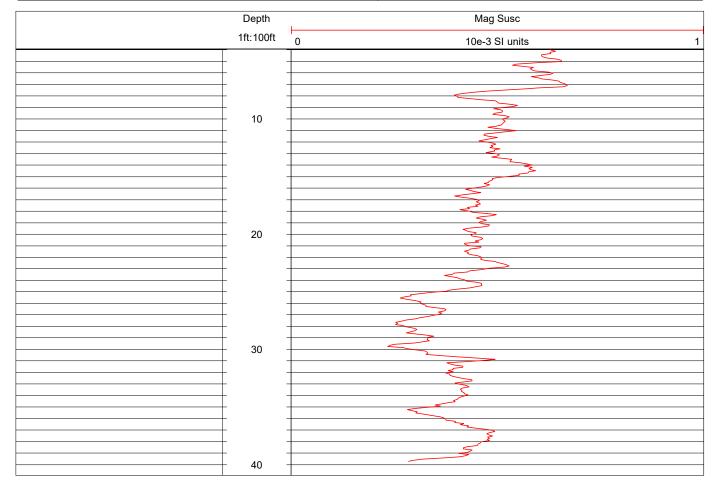
		TOOL HMA-453-S CALIBRATION DATE/TIME 6/8/16 11:36 CALIBRATION STANDARDS 0 and 5E-3 SI Units CALIBRATION RESULTS Zero = 70.53, 5E-3 = 1105.86 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	REMARKS
WELL	EPA-16S Up	
LOGGER	Todd Wiedemeier	
DATE	June 8, 2016	

Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 1
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		TOOL HMA-453-S CALIBRATION DATE/TIME 6/8/16 15:52 CALIBRATION STANDARDS 0 and 5E-3 SI Units
PROJECT	ESTCP 201584	CALIBRATION RESULTS Zero = 75.065, 5E-3 = 1137.69 cps REMARKS
LOCATION	Hopewell Junction, NY	
WELL	EPA-15D Down	
LOGGER	Todd Wiedemeier	
DATE	June 8, 2016	



		TOOL HMA-453-S CALIBRATION DATE/TIME 6/8/16 15:52 CALIBRATION STANDARDS 0 and 5E-3 SI Units CALIBRATION RESULTS Zero = 75.065, 1137.69 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	
WELL	EPA-15D Up	
LOGGER	Todd Wiedemeier	
DATE	June 8, 2016	



		TOOL HMA-453-S CALIBRATION DATE/TIME 6/8/16 17:40 CALIBRATION STANDARDS 0 and 5E-3 SI Units
PROJECT LOCATION WELL	ESTCP 201584 Hopewell Junction, NY EPA-21S Down	CALIBRATION RESULTS Zero = 69.75, 5E-3 = 1140.53 cps REMARKS
LOGGER DATE	Todd Wiedemeier June 8, 2016	

Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 1
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		TOOL HMA-453-S CALIBRATION DATE/TIME 6/8/16 17:40 CALIBRATION STANDARDS 0 and 5E-3 SI Units CALIBRATION RESULTS Zero = 69.75, 5E-3 = 1140.53 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	
WELL	EPA-21S Up	
LOGGER	Todd Wiedemeier	
DATE	June 8, 2016	

Ift:100ft     0     10e-3 Sl units	Depth	Mag Susc
	1ft:100ft	0 10e-3 SI units 1
	10	
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		TOOLHMA-453-SCALIBRATION DATE/TIME6/8/16 17:40CALIBRATION STANDARDS0 and 5E-3 SI Units	
PROJECT LOCATION WELL LOGGER DATE	ESTCP 201584 Hopewell Junction, NY EPA-21D Down Todd Wiedemeier June 8, 2016	CALIBRATION RESULTS Zero = 69.75, 5E-3 = 1140.52 cps REMARKS	

Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 1
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		TOOL HMA-453S CALIBRATION DATE/TIME 6/8/16 17:40 CALIBRATION STANDARDS 0 and 5E-3 SI Units CALIBRATION RESULTS Zero = 69.75, 5E-3 = 1140.53 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	
WELL	EPA-21D Up	
LOGGER	Todd Wiedemeier	
DATE	June 8,2016	

Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 1
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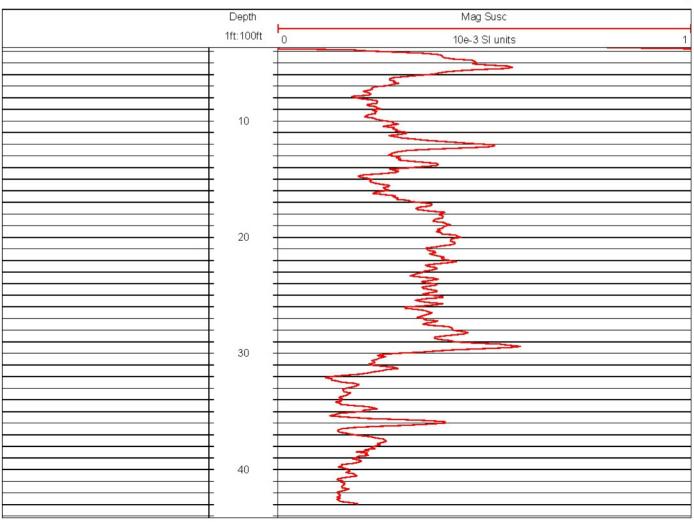
		TOOL HMA-453-S CALIBRATION DATE/TIME 6/9/16 11:27 CALIBRATION STANDARDS 0 and 5E-3 SI Units CALIBRATION RESULTS Zero = 97.5, 5E-3 = 1148.78 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	
WELL	EPA-12S Down	
LOGGER	Todd Wiedemeier	
DATE	June 9, 2016	

Depth		Mag Susc
1ft:100ft	0	10e-3 SI units 1
10		

		TOOL HMA-453-S CALIBRATION DATE/TIME 6/9/16 11:27 CALIBRATION STANDARDS 0 and 5E-3 CALIBRATION RESULTS Zero = 97.5, 5E-3 = 1148.78
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	
WELL	EPA-12S Up	
LOGGER	Todd Wiedemeier	
DATE	June 9, 2016	

Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 1
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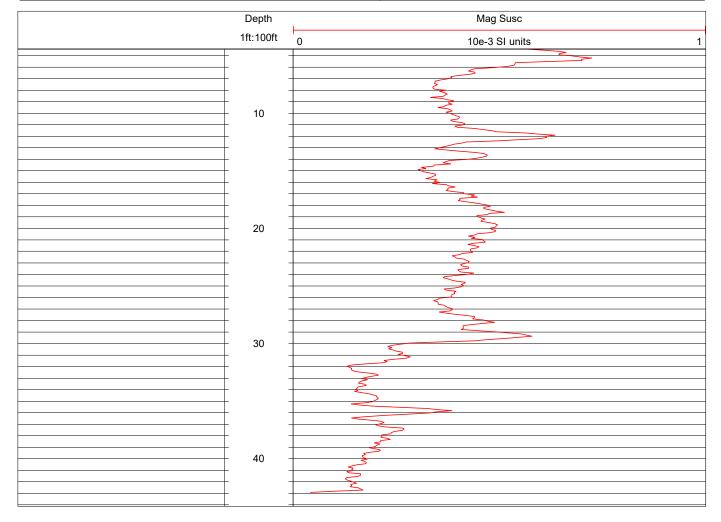
		TOOL HMA-453-S CALIBRATION DATE/TIME 6/9//16 11:27 CALIBRATION STANDARDS 0 and 5E-3 SI Units CALIBRATION RESULTS Zero = 97.5, 5E-3 = 1148.78 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction	
WELL	EPA-12D Down	
LOGGER	Todd Wiedemeier	
DATE	6/9/2016	



- AV	F	TOOL HMA-453-S
		CALIBRATION DATE/TIME 6/9//16 11:27
WIEDEN		CALIBRATION STANDARDS 0 and 5E-3 SI Units
& ASSOC	CIATES	CALIBRATION RESULTS Zero = 97.5, 5E-3 = 1148.78 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction	
WELL	EPA-12D Down	
LOGGER	Todd Wiedemeier	
DATE	6/9/2016	

Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 1
10	
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		TOOL HMA-453-S CALIBRATION DATE/TIME 6/9/16 11:27 CALIBRATION STANDARDS 0 and 5E-3 SI Units
PROJECT	ESTCP 201584	CALIBRATION RESULTS Zero = 97.5, 5E-3 = 1148.78 cps
LOCATION	Hopewell Junction, NY	REMARKS
WELL	EPA-12D - Up	
LOGGER	Todd Wiedemeier	
DATE	June 9, 2015	



		TOOL HMA-453-S CALIBRATION DATE/TIME 6/9/16 15:16 CALIBRATION STANDARDS 0 and 5E-3 SI Units
PROJECT	ESTCP 201584 Hopewell Junction, NY	CALIBRATION RESULTS Zero = 60.86, 5E-3 = 1151.1 cps REMARKS
WELL	EPA-10S - Down	
LOGGER DATE	Todd Wiedemeier June 9, 2016	

Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 1
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		TOOLHMA-453-SCALIBRATION DATE/TIME6/9/16 15:16CALIBRATION STANDARDS0 and 5E-3 SI UnitsCALIBRATION RESULTSZero = 60.86, 1151.1 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	
WELL	EPA-10S Up	
LOGGER	Todd Wiedemeier	
DATE	June 9, 2016	

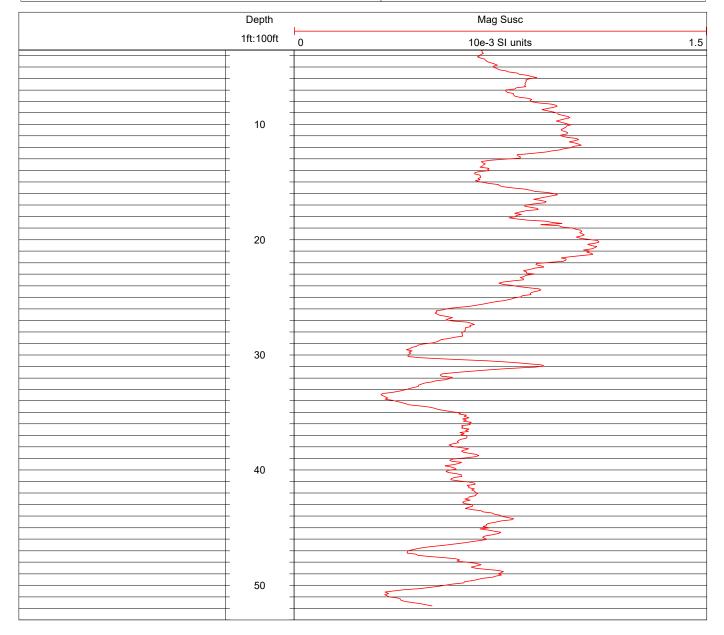
Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 1
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47	L	TOOL HMW-453-S
		CALIBRATION DATE/TIME 6/9/16 15:16
WIEDEMEIER		CALIBRATION STANDARDS 0 and 5E-3 SI Units
& ASSO(	CIATES	CALIBRATION RESULTS Zero = 60.86, 5E-3 = 1151.1 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	
WELL	EPA-10D - Down	
LOGGER	Todd Wiedemeier	
DATE	June 9, 2016	

Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 1.5
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Page 1

		TOOL Hma-453-S CALIBRATION DATE/TIME 6/9/16 15:16 CALIBRATION STANDARDS 0 and 5E-3 SI Units
PROJECT	ESTCP 201584	CALIBRATION RESULTS Zero = 60.86, 5E-3 = 1151.1 cps
LOCATION	Hopewell Junction, NY	REMARKS
WELL	EPA-10D -Up	
LOGGER	Todd Wiedemeier	
DATE	June 9, 2016	



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		TOOL HMW-453-S CALIBRATION DATE/TIME CALIBRATION STANDARDS CALIBRATION RESULTS
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	
WELL	EPA-19D Down	
LOGGER	Todd Wiedemeier	
DATE	June 10, 2016	

Depth	Mag Susc	
1ft:100ft	0 10e-3 SI units	1
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		TOOL HMA-453-S
		CALIBRATION DATE/TIME 6/10/16 09:53
WIEDEMEIER		CALIBRATION STANDARDS 0 and 5E-3 SI Units
& ASSO(	CIATES	CALIBRATION RESULTS Zero = 65.7, 5E-3 = 1128.81 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	
WELL	EPA-19D Up	
LOGGER	Todd Wiedemeier	
DATE	June 10, 2016	

Depth	
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WIEDEMEIER & ASSOCIATES		TOOL HMA-453-S CALIBRATION DATE/TIME 6/10/16 09:53 CALIBRATION STANDARDS 0 and 5E-3 CALIBRATION RESULTS Zero = 65.7, 5E-3 = 1128.81 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	
WELL	EPA-19S Down	
LOGGER	Todd Wiedemeier	
DATE	June 10, 2016	

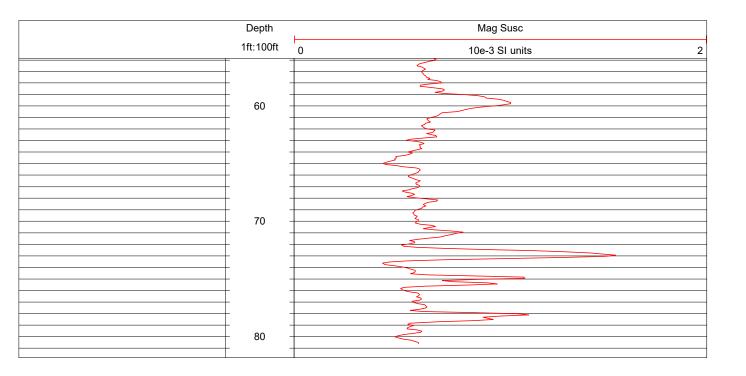
Depth		Mag Susc	
1ft:100	ft 0	10e-3 SI units	1
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WIEDEMEIER & ASSOCIATES		TOOLHMA-453-SCALIBRATION DATE/TIME6/10/16 09:53CALIBRATION STANDARDS0 and 5E-3 SI UnitsCALIBRATION RESULTSZero = 65.7, 5E-3 = 1128.81 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	
WELL	EPA-19S Up	
LOGGER	Todd Wiedemeier	
DATE	June 10, 2016	

Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 1
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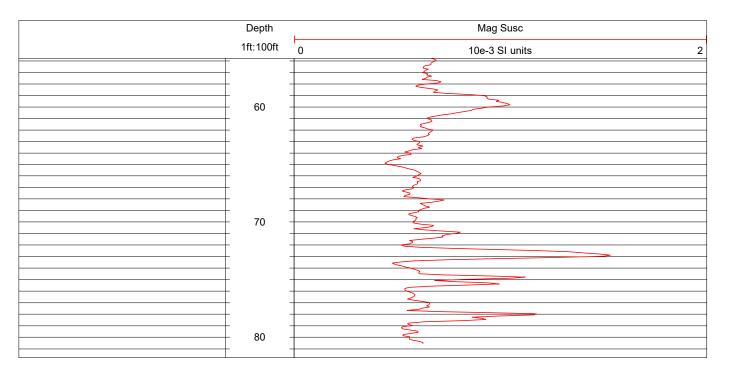
		TOOL HMA-453-S
		CALIBRATION DATE/TIME 6/10/16 09:53
WIEDEMEIER		CALIBRATION STANDARDS 0 and 5E-3 SI Units
& ASSOC	IATES	CALIBRATION RESULTS Zero = 65.7, 5E-3 = 1128.81 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	
WELL	EPA-8D - Down	
LOGGER	Todd Wiedemeier	Calibration from last well (EPA-19D) used at this location.
DATE	June 10, 2016	

	Depth	Mag Susc
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		TOOL HMA-453-S CALIBRATION DATE/TIME 6/10/16 - 09:53 CALIBRATION STANDARDS 0 and 5E-3 SI Units CALIBRATION RESULTS Zero = 65.7, 5E-3 = 1128.81
PROJECT	ESTCP 201584	REMARKS
LOCATION	Hopewell Junction, NY	REMARKS
WELL	EPA-8D Up	
LOGGER	Todd Wiedemeier	Calibration from last well (EPA-19D) used at this location.
DATE	June 10, 2016	

Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 2
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Depth	Mag Susc 10e-3 SI	Mag Susc	
ft bgs	units	m3/kg	
3.44	1.69055	9.94E-07	
3.54	1.16235	6.84E-07	Average of Sonde Data = 2.46E-07
3.64	0.895231	5.27E-07	Count = 261
3.74	0.531828	3.13E-07	Confidence Level(95.0%) = 6.52E-09
3.84	0.371208	2.18E-07	
3.94	0.34978	2.06E-07	
4.04	0.283215	1.67E-07	
4.135	0.278451	1.64E-07	
4.235	0.215895	1.27E-07	
4.335	0.255615	1.5E-07	
4.435	0.251539	1.48E-07	
4.535	0.199511	1.17E-07	
4.635	0.238739	1.4E-07	
4.735	0.192836	1.13E-07	
4.835	0.246782	1.45E-07	
4.935	0.194686	1.15E-07	
5.035	0.132187	7.78E-08	
5.135	0.188122	1.11E-07	
5.235	0.19569	1.15E-07	
5.335	0.109956	6.47E-08	
5.435	0.206306	1.21E-07	
5.535	0.17163	1.01E-07	
5.635	0.166942	9.82E-08	
5.735	0.17498	1.03E-07	
5.835	0.170584	1E-07	
5.935	0.181353	1.07E-07	
6.035	0.164262	9.66E-08	
6.135	0.187772	1.1E-07	
6.235	0.243613	1.43E-07	
6.335	0.157469	9.26E-08	
6.435	0.190972	1.12E-07	
6.535	0.183463	1.08E-07	
6.635	0.130419	7.67E-08	
6.735	0.220579	1.3E-07	
6.83	0.183959	1.08E-07	
6.93	0.182316	1.07E-07	
7.03	0.130899	7.7E-08	
7.13	0.111387	6.55E-08	
7.23	0.128301	7.55E-08	
7.33	0.118673	6.98E-08	
7.43	0.133415	7.85E-08	



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
7.525	0.184472	1.09E-07
7.625	0.137897	8.11E-08
7.725	0.135017	7.94E-08
7.825	0.170448	1E-07
7.925	0.137141	8.07E-08
8.025	0.162297	9.55E-08
8.025	0.150722	8.87E-08
8.225	0.208968	1.23E-07
8.325	0.191417	1.13E-07
8.425	0.153666	9.04E-08
8.525	0.160186	9.42E-08
8.625	0.161213	9.48E-08
8.725	0.105271	6.19E-08
8.825	0.129586	7.62E-08
8.925	0.16234	9.55E-08
9.025	0.182686	1.07E-07
9.125	0.223996	1.32E-07
9.225	0.101517	5.97E-08
9.325	0.229676	1.35E-07
9.425	0.119332	7.02E-08
9.525	0.210713	1.24E-07
9.625	0.890024	5.24E-07
9.725	0.133057	7.83E-08
9.825	0.088556	5.21E-08
9.925	0.17221	1.01E-07
10.025	0.187223	1.1E-07
10.125	0.127135	7.48E-08
10.22	0.142682	8.39E-08
10.32	0.154721	9.1E-08
10.32	0.135821	7.99E-08
10.52	0.1444	8.49E-08
10.62	0.111748	6.57E-08
10.72	0.124625	7.33E-08
10.815	0.11761	6.92E-08
10.915	0.099482	5.85E-08
11.015	0.159061	9.36E-08
11.115	0.131129	7.71E-08
11.215	0.151866	8.93E-08
11.315	0.126367	7.43E-08
11.415	0.116297	6.84E-08
11.515	0.166098	9.77E-08
11.515	5.100050	5.772 00



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
11.615	0.134975	7.94E-08
11.715	0.154975	9.13E-08
11.815	0.133294	9.13E-08 1.09E-07
11.915	0.161222 0.134097	9.48E-08
12.015		7.89E-08
12.115	0.176131 0.182179	1.04E-07
12.215 12.315	0.182179	1.07E-07 8.35E-08
	0.141896	
12.415		1.02E-07
12.515	0.142215	8.37E-08
12.615	0.138053	8.12E-08
12.715	0.170079	1E-07
12.815	0.111963	6.59E-08
12.915	0.172664	1.02E-07 1.12E-07
13.015	0.190196	
13.115	0.105279	6.19E-08
13.215	0.119774	7.05E-08
13.315	0.166831	9.81E-08
13.415	0.177746	1.05E-07
13.51	0.189258	1.11E-07
13.61	0.148565	8.74E-08
13.71	0.14231	8.37E-08
13.81	0.114136	6.71E-08
13.91	0.174597	1.03E-07
14.01	0.148307	8.72E-08
14.105	0.190885	1.12E-07
14.205	0.15769	9.28E-08
14.305	0.157931	9.29E-08
14.405	0.127977	7.53E-08
14.505	0.102739	6.04E-08
14.605	0.15465	9.1E-08
14.705	0.194658	1.15E-07
14.805	0.162563	9.56E-08
14.905	0.156581	9.21E-08
15.005	0.140754	8.28E-08
15.105	0.093629	5.51E-08
15.205	0.139335	8.2E-08
15.305	0.149177	8.78E-08
15.405	0.170509	1E-07
15.505	0.128606	7.57E-08
15.605	0.134787	7.93E-08



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
15.705	0.165646	9.74E-08
15.805	0.155248	9.13E-08
15.905	0.15047	8.85E-08
16.005	0.141743	8.34E-08
16.105	0.190799	1.12E-07
16.205	0.1051	6.18E-08
16.305	0.155201	9.13E-08
16.405	0.115882	6.82E-08
16.505	0.159931	9.41E-08
16.605	0.116253	6.84E-08
16.705	0.143407	8.44E-08
16.8	0.131416	7.73E-08
16.9	0.119013	7E-08
17	0.106058	6.24E-08
17.1	0.22728	1.34E-07
17.2	0.160029	9.41E-08
17.3	0.13231	7.78E-08
17.4	0.187613	1.1E-07
17.495	0.196514	1.16E-07
17.595	0.118814	6.99E-08
17.695	0.172558	1.02E-07
17.795	0.129523	7.62E-08
17.895	0.138826	8.17E-08
17.995	0.165395	9.73E-08
18.095	0.185824	1.09E-07
18.195	0.158265	9.31E-08
18.295	0.186449	1.1E-07
18.395	0.161006	9.47E-08
18.495	0.134713	7.92E-08
18.595	0.206029	1.21E-07
18.695	0.176227	1.04E-07
18.795	0.176474	1.04E-07
18.895	0.218374	1.28E-07
18.995	0.192614	1.13E-07
19.095	0.121349	7.14E-08
19.195	0.143974	8.47E-08
19.295	0.164899	9.7E-08
19.395	0.167512	9.85E-08
19.495	0.167066	9.83E-08
19.595	0.159554	9.39E-08
19.695	0.158398	9.32E-08



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
19.795	0.139999	8.24E-08
19.895	0.133839	7.87E-08
19.895	0.137845	8.11E-08
20.09	0.1378608	1.05E-07
20.09	0.178608	9.01E-07
20.19	0.155115	9.01E-08 9.06E-08
20.29	0.1341	9.00E-08 1.07E-07
20.39	0.156735	9.22E-08
20.49	0.150755	9.22E-08 9.12E-08
20.69	0.191653	1.13E-07
20.785	0.20887	1.23E-07
20.885	0.211641	1.24E-07
20.985	0.140292	8.25E-08
21.085	0.210792	1.24E-07
21.185	0.177117	1.04E-07
21.285	0.19011	1.12E-07
21.385	0.136887	8.05E-08
21.485	0.165735	9.75E-08
21.585	0.191378	1.13E-07
21.685	0.146538	8.62E-08
21.785	0.16802	9.88E-08
21.885	0.176045	1.04E-07
21.985	0.129906	7.64E-08
22.085	0.147908	8.7E-08
22.185	0.128643	7.57E-08
22.285	0.19475	1.15E-07
22.385	0.146842	8.64E-08
22.485	0.14908	8.77E-08
22.585	0.152097	8.95E-08
22.685	0.169409	9.97E-08
22.785	0.17264	1.02E-07
22.885	0.123756	7.28E-08
22.985	0.162499	9.56E-08
23.085	0.200075	1.18E-07
23.185	0.167254	9.84E-08
23.285	0.154943	9.11E-08
23.385	0.184181	1.08E-07
23.48	0.198268	1.17E-07
23.58	0.188245	1.11E-07
23.68	0.140919	8.29E-08
23.78	0.142058	8.36E-08



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
23.88	0.204919	1.21E-07
23.98	0.177276	1.04E-07
24.075	0.190483	1.12E-07
24.175	0.19024	1.12E-07
24.275	0.183927	1.08E-07
24.375	0.262052	1.54E-07
24.475	0.234156	1.38E-07
24.575	0.26548	1.56E-07
24.675	0.263013	1.55E-07
24.775	0.273585	1.61E-07
24.875	0.314269	1.85E-07
24.975	0.308106	1.81E-07
25.075	0.303449	1.78E-07
25.175	0.293637	1.73E-07
25.275	0.311662	1.83E-07
25.375	0.294133	1.73E-07
25.475	0.264119	1.55E-07
25.575	0.274063	1.61E-07
25.675	0.187541	1.1E-07
25.775	0.165488	9.73E-08
25.875	0.230344	1.35E-07
25.975	0.130784	7.69E-08
26.075	0.184801	1.09E-07
26.175	0.159298	9.37E-08
26.275	0.155483	9.15E-08
26.375	0.208677	1.23E-07
26.475	0.204966	1.21E-07
26.575	0.178517	1.05E-07
26.675	0.264702	1.56E-07 1.22E-07
26.77	0.207529	
26.87 26.97	0.15215	8.95E-08 1.16E-07
20.97	0.198033 0.21196	1.16E-07 1.25E-07
27.07	0.239349	1.23E-07 1.41E-07
27.17	0.239349	1.41L-07 1.1E-07
27.27	0.210194	1.24E-07
27.465	0.207977	1.24L-07 1.22E-07
27.565	0.176081	1.04E-07
27.665	0.211163	1.24E-07
27.765	0.163357	9.61E-08
27.865	0.188206	1.11E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
27.965	0.19021	1.12E-07
28.065	0.191763	1.13E-07
28.165	0.185928	1.09E-07
28.265	0.188269	1.11E-07
28.365	0.161797	9.52E-08
28.465	0.18384	1.08E-07
28.565	0.148928	8.76E-08
28.665	0.141839	8.34E-08
28.765	0.16783	9.87E-08
28.865	0.116424	6.85E-08
28.965	0.163746	9.63E-08
29.065	0.172129	1.01E-07
29.165	0.164264	9.66E-08
29.265	0.149646	8.8E-08
29.365	0.202507	1.19E-07
29.465	0.217	1.28E-07
29.565	0.167956	9.88E-08
29.665	0.251256	1.48E-07
29.765	0.188935	1.11E-07
29.865	0.200639	1.18E-07
29.965	0.20837	1.23E-07
30.065	0.187905	1.11E-07
30.16	0.219584	1.29E-07
30.26	0.226081	1.33E-07
30.36	0.237822	1.4E-07
30.46	0.176907	1.04E-07
30.56	0.198309	1.17E-07
30.66	0.231063	1.36E-07
30.755	0.174266	1.03E-07
30.855	0.197488	1.16E-07
30.955	0.235003	1.38E-07
31.055	0.199255	1.17E-07
31.155	0.231583	1.36E-07
31.255	0.229644	1.35E-07
31.355	0.190976	1.12E-07
31.455	0.205442	1.21E-07
31.555	0.233086	1.37E-07
31.655	0.208906	1.23E-07
31.755	0.193595	1.14E-07
31.855	0.161523	9.5E-08
31.955	0.240854	1.42E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
32.055	0.136932	8.05E-08
32.055	0.18696	1.1E-07
32.255	0.190284	1.12E-07
32.355	0.231281	1.36E-07
32.355	0.186595	1.30L-07 1.1E-07
32.455	0.232083	1.37E-07
32.655	0.213346	1.25E-07
32.755	0.229872	1.35E-07
32.855	0.260838	1.53E-07
32.955	0.305811	1.8E-07
33.055	0.308947	1.82E-07
33.155	0.386698	2.27E-07
33.255	0.377791	2.22E-07
33.355	0.361354	2.13E-07
33.45	0.333117	1.96E-07
33.55	0.296979	1.75E-07
33.65	0.370701	2.18E-07
33.75	0.385629	2.27E-07
33.85	0.321451	1.89E-07
33.95	0.340719	2E-07
34.045	0.318301	1.87E-07
34.145	0.275612	1.62E-07
34.245	0.317718	1.87E-07
34.345	0.297132	1.75E-07
34.445	0.35727	2.1E-07
34.545	0.324578	1.91E-07
34.645	0.359298	2.11E-07
34.745	0.338536	1.99E-07
34.845	0.349008	2.05E-07
34.945	0.331007	1.95E-07
35.045	0.294981	1.74E-07
35.145	0.300083	1.77E-07
35.245	0.272628	1.6E-07
35.345	0.25286	1.49E-07
35.445	0.276348	1.63E-07
35.545	0.264852	1.56E-07
35.645	0.266528	1.57E-07
35.745	0.272631	1.6E-07
35.845	0.255697	1.5E-07
35.945	0.25155	1.48E-07
36.045	0.298896	1.76E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
36.145	0.29878	1.76E-07
36.245	0.262734	1.55E-07
36.345	0.250088	1.47E-07
36.445	0.296028	1.74E-07
36.545	0.281923	1.66E-07
36.645	0.293679	1.73E-07
36.74	0.274239	1.61E-07
36.84	0.24737	1.46E-07
36.94	0.288593	1.7E-07
37.04	0.24204	1.42E-07
37.14	0.235722	1.39E-07
37.24	0.227873	1.34E-07
37.34	0.311416	1.83E-07
37.435	0.2802	1.65E-07
37.535	0.279355	1.64E-07
37.635	0.273363	1.61E-07
37.735	0.280567	1.65E-07
37.835	0.273214	1.61E-07
37.935	0.279426	1.64E-07
38.035	0.325584	1.92E-07
38.135	0.282269	1.66E-07
38.235	0.260836	1.53E-07
38.335	0.321073	1.89E-07
38.435	0.244714	1.44E-07
38.535	0.259504	1.53E-07
38.635	0.311889	1.83E-07
38.735	0.265777	1.56E-07
38.835	0.213637	1.26E-07
38.935	0.169306	9.96E-08
39.035	0.182731	1.07E-07
39.135	0.190821	1.12E-07
39.235	0.177668	1.05E-07
39.335	0.175959	1.04E-07
39.435	0.148038	8.71E-08
39.535	0.174137	1.02E-07
39.635	0.181706	1.07E-07
39.735	0.229401	1.35E-07
39.835	0.18163	1.07E-07
39.935	0.198098	1.17E-07
40.03	0.210198	1.24E-07
40.13	0.211522	1.24E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
40.23	0.181153	1.07E-07
40.33	0.247498	1.46E-07
40.43	0.180063	1.06E-07
40.53	0.258182	1.52E-07
40.63	0.226563	1.33E-07
40.725	0.204097	1.2E-07
40.825	0.248561	1.46E-07
40.925	0.22087	1.3E-07
41.025	0.218235	1.28E-07
41.125	0.192843	1.13E-07
41.225	0.193795	1.14E-07
41.325	0.203776	1.2E-07
41.425	0.191026	1.12E-07
41.525	0.194844	1.15E-07
41.625	0.157564	9.27E-08
41.725	0.176001	1.04E-07
41.825	0.160095	9.42E-08
41.925	0.181204	1.07E-07
42.025	0.229058	1.35E-07
42.125	0.169196	9.95E-08
42.225	0.20913	1.23E-07
42.325	0.235077	1.38E-07
42.425	0.225658	1.33E-07
42.525	0.198064	1.17E-07
42.625	0.270756	1.59E-07
42.725	0.268367	1.58E-07
42.825	0.293318	1.73E-07
42.925	0.313423	1.84E-07
43.025	0.330232	1.94E-07
43.125	0.32806	1.93E-07
43.225	0.460502	2.71E-07
43.325	0.335455	1.97E-07
43.42	0.294187	1.73E-07
43.52	0.281201	1.65E-07
43.62	0.337865	1.99E-07
43.72 43.82	0.322038	1.89E-07
43.82 43.92	0.272793	1.6E-07 1.44E-07
43.92 44.015		1.44E-07 1.87E-07
44.015	0.317103 0.213985	
44.115	0.213985	1.26E-07 1.97E-07
44.213	0.555153	1.3/E-0/



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
44.315	0.341939	2.01E-07
44.415	0.379068	2.23E-07
44.515	0.310564	1.83E-07
44.615	0.405848	2.39E-07
44.715	0.446981	2.63E-07
44.815	0.433898	2.55E-07
44.915	0.407511	2.4E-07
45.015	0.415645	2.44E-07
45.115	0.464887	2.73E-07
45.215	0.464176	2.73E-07
45.315	0.489992	2.88E-07
45.415	0.396607	2.33E-07
45.515	0.433553	2.55E-07
45.615	0.430177	2.53E-07
45.715	0.38691	2.28E-07
45.815	0.377046	2.22E-07
45.915	0.349783	2.06E-07
46.015	0.292939	1.72E-07
46.115	0.384274	2.26E-07
46.215	0.31243	1.84E-07
46.315	0.285408	1.68E-07
46.415	0.27503	1.62E-07
46.515	0.293411	1.73E-07
46.615	0.216289	1.27E-07
46.71	0.315831	1.86E-07
46.81	0.259951	1.53E-07
46.91	0.270291	1.59E-07
47.01	0.266724	1.57E-07
47.11	0.263748	1.55E-07
47.21	0.325641	1.92E-07
47.31	0.271799	1.6E-07
47.405	0.310891	1.83E-07
47.505	0.28251	1.66E-07
47.605	0.338565	1.99E-07
47.705	0.289705	1.7E-07
47.805	0.287032	1.69E-07
47.905	0.309485	1.82E-07
48.005	0.274668	1.62E-07
48.105	0.288158	1.7E-07
48.205	0.284728	1.67E-07
48.305	0.24801	1.46E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
48.405	0.230483	1.36E-07
48.505	0.292099	1.72E-07
48.605	0.335671	1.97E-07
48.705	0.410309	2.41E-07
48.805	0.414168	2.44E-07
48.905	0.447929	2.63E-07
49.005	0.506946	2.98E-07
49.105	0.507579	2.99E-07
49.205	0.548586	3.23E-07
49.305	0.488968	2.88E-07
49.405	0.523458	3.08E-07
49.505	0.501876	2.95E-07
49.605	0.449906	2.65E-07
49.705	0.439492	2.59E-07
49.805	0.380148	2.24E-07
49.905	0.405645	2.39E-07
50.005	0.370831	2.18E-07
50.1	0.385053	2.27E-07
50.2	0.389286	2.29E-07
50.3	0.413855	2.43E-07
50.4	0.384105	2.26E-07
50.5	0.425872	2.51E-07
50.6	0.404955	2.38E-07
50.695	0.38839	2.28E-07
50.795	0.39916	2.35E-07
50.895	0.395056	2.32E-07
50.995	0.407516	2.4E-07
51.095	0.34356	2.02E-07
51.195	0.355765	2.09E-07
51.295	0.357398	2.1E-07
51.395	0.376339	2.21E-07
51.495 51.595	0.313477 0.350217	1.84E-07
51.595	0.350217	2.06E-07 1.62E-07
51.795	0.275413	1.62E-07 2.14E-07
51.895	0.261889	2.14E-07 1.54E-07
51.895	0.201889	1.34E-07 1.87E-07
52.095	0.31875	2.24E-07
52.195	0.298874	1.76E-07
52.295	0.360606	2.12E-07
52.395	0.358296	2.11E-07
52.555	5.555250	2.112 0/



Depth	Depth Mag Susc Mag 10e-3 SI	
ft bgs	units	m3/kg
52.495	0.320531	1.89E-07
52.595	0.423316	2.49E-07
52.695	0.298077	1.75E-07
52.795	0.343402	2.02E-07
52.895	0.3045	1.79E-07
52.995	0.34021	2E-07
53.095	0.341346	2.01E-07
53.195	0.37467	2.2E-07
53.295	0.360006	2.12E-07
53.39	0.362622	2.13E-07
53.49	0.321306	1.89E-07
53.59	0.340587	2E-07
53.69	0.34982	2.06E-07
53.79	0.312528	1.84E-07
53.89	0.280134	1.65E-07
53.99	0.363988	2.14E-07
54.085	0.344054	2.02E-07
54.185	0.32732	1.93E-07
54.285	0.352854	2.08E-07
54.385	0.406385	2.39E-07
54.485	0.261919	1.54E-07
54.585	0.358091	2.11E-07
54.685	0.380848	2.24E-07
54.785	0.352976	2.08E-07
54.885	0.311699	1.83E-07
54.985	0.371698	2.19E-07
55.085	0.359793	2.12E-07
55.185	0.361149	2.12E-07
55.285	0.356491	2.1E-07
55.385	0.430504	2.53E-07
55.485	0.445871	2.62E-07
55.585	0.451251	2.65E-07
55.685	0.477142	2.81E-07
55.785	0.509408	3E-07
55.885	0.502846	2.96E-07
55.985	0.434792	2.56E-07
56.085	0.470384	2.77E-07
56.185	0.487326	2.87E-07
56.285	0.455398	2.68E-07
56.385	0.439726	
56.485	0.458021	2.69E-07



Depth Mag Susc 10e-3 SI		Mag Susc
ft bgs	units	m3/kg
56.585	0.451129	2.65E-07
56.68	0.383152	2.25E-07
56.78	0.333775	1.96E-07
56.88	0.378335	2.23E-07
56.98	0.322348	1.9E-07
57.08	0.420463	2.47E-07
57.18	0.322137	1.89E-07
57.28	0.361742	2.13E-07
57.375	0.324968	1.91E-07
57.475	0.278814	1.64E-07
57.575	0.315342	1.85E-07
57.675	0.322766	1.9E-07
57.775	0.369596	2.17E-07
57.875	0.353895	2.08E-07
57.975	0.357912	2.11E-07
58.075	0.366868	2.16E-07
58.175	0.370795	2.18E-07
58.275	0.321029	1.89E-07
58.375	0.351829	2.07E-07
58.475	0.348939	2.05E-07
58.575	0.384775	2.26E-07
58.675	0.395831	2.33E-07
58.775	0.398589	2.34E-07
58.875	0.437301	2.57E-07
58.975	0.415324	2.44E-07
59.075	0.454978	2.68E-07
59.175	0.412349	2.43E-07
59.275	0.43958	2.59E-07
59.375	0.383352	2.26E-07
59.475	0.443898	2.61E-07
59.575	0.472325	2.78E-07
59.675	0.452333	2.66E-07
59.775	0.473192	2.78E-07
59.875	0.511072	3.01E-07
59.97	0.512558	3.02E-07
60.07	0.460286	2.71E-07
60.17	0.453628	2.67E-07
60.27	0.480501	2.83E-07
60.37	0.483029	2.84E-07
60.47	0.413162	2.43E-07
60.57	0.490979	2.89E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
60.665	0.452257	2.66E-07
60.765	0.46171	2.72E-07
60.865	0.440119	2.59E-07
60.965	0.463071	2.72E-07
61.065	0.369532	2.17E-07
61.165	0.356235	2.1E-07
61.265	0.377196	2.22E-07
61.365	0.400768	2.36E-07
61.465	0.377656	2.22E-07
61.565	0.364577	2.14E-07
61.665	0.439683	2.59E-07
61.765	0.364588	2.14E-07
61.865	0.351816	2.07E-07
61.965	0.424172	2.5E-07
62.065	0.391966	2.31E-07
62.165	0.31597	1.86E-07
62.265	0.34421	2.02E-07
62.365	0.369003	2.17E-07
62.465	0.41074	2.42E-07
62.565	0.369417	2.17E-07
62.665	0.371978	2.19E-07
62.765	0.406147	2.39E-07
62.865	0.395566	2.33E-07
62.965	0.368151	2.17E-07
63.065	0.372801	2.19E-07
63.165	0.435814	2.56E-07
63.265	0.409868	2.41E-07
63.36	0.383783	2.26E-07
63.46	0.397872	2.34E-07
63.56	0.404306	2.38E-07
63.66	0.403817	2.38E-07
63.76	0.394369	2.32E-07
63.86	0.35449	2.09E-07
63.96	0.359019	2.11E-07
64.055	0.398393	2.34E-07
64.155	0.402836	2.37E-07
64.255	0.418417	2.46E-07
64.355	0.398882	2.35E-07
64.455	0.477395	2.81E-07
64.555		2.47E-07
64.655	0.401098	2.36E-07

63.5 1.48E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
64.76	0.440485	2.59E-07
64.855	0.452978	2.66E-07
64.955	0.421117	2.48E-07
65.055	0.412648	2.43E-07
65.155	0.464431	2.73E-07
65.255	0.429502	2.53E-07
65.355	0.447182	2.63E-07
65.455	0.446488	2.63E-07
65.555	0.48248	2.84E-07
65.655	0.455947	2.68E-07
65.755	0.43782	2.58E-07
65.855	0.485215	2.85E-07
65.955	0.440328	2.59E-07
66.055	0.431187	2.54E-07
66.155	0.440995	2.59E-07
66.255	0.448309	2.64E-07
66.355	0.453203	2.67E-07
66.455	0.451867	2.66E-07
66.555	0.467126	2.75E-07
66.65	0.481437	2.83E-07
66.75	0.428828	2.52E-07
66.85	0.382799	2.25E-07
66.95	0.408642	2.4E-07
67.05	0.363043	2.14E-07
67.15	0.407626	2.4E-07
67.25	0.401995	2.36E-07
67.345	0.37866	2.23E-07
67.445	0.353613	2.08E-07
67.545		1.96E-07
67.645	0.377981	2.22E-07
67.745	0.368031	2.16E-07
67.845	0.361423	2.13E-07
67.945	0.35496	2.09E-07
68.045	0.365711	2.15E-07
68.145	0.353	2.08E-07
68.245	0.326622	1.92E-07
68.345	0.355203	2.09E-07
68.445	0.400638	2.36E-07
68.545	0.37758	2.22E-07
68.645	0.405415	2.38E-07
68.745	0.373552	2.2E-07

67.5 1.04E-07



Depth	Mag Susc 10e-3 SI	Mag Susc		
ft bgs	units	m3/kg		
68.845	0.390506	2.3E-07		
68.95	0.402888	2.37E-07		
69.045	0.345534	2.03E-07		
69.145	0.40465	2.38E-07		
69.245	0.420465	2.47E-07		
69.345	0.378911	2.23E-07		
69.445	0.353995	2.08E-07		
69.545	0.358322	2.11E-07	69.5	2.41E-07
69.645	0.347283	2.04E-07		
69.745	0.386627	2.27E-07		
69.845	0.410628	2.42E-07		
69.94	0.349121	2.05E-07		
70.04	0.390858	2.3E-07		
70.14	0.375948	2.21E-07		
70.24	0.418147	2.46E-07		
70.34	0.390163	2.3E-07		
70.44	0.373892	2.2E-07		
70.54	0.421445	2.48E-07		
70.635	0.414119	2.44E-07		
70.735	0.436978	2.57E-07		
70.835	0.363067	2.14E-07		
70.935	0.406585	2.39E-07		
71.035	0.382411	2.25E-07		
71.135	0.416065	2.45E-07		
71.235	0.405206	2.38E-07		
71.335	0.415771	2.45E-07		
71.435	0.367034	2.16E-07		
71.535	0.414098	2.44E-07		
71.635	0.428533	2.52E-07		
71.735	0.389814	2.29E-07		
71.835	0.370541	2.18E-07		
71.935	0.393584	2.32E-07		
72.035	0.333899	1.96E-07		
72.135	0.372863	2.19E-07		
72.235	0.378106	2.22E-07		
72.335	0.389837	2.29E-07		
72.435	0.345501	2.03E-07		
72.535	0.347697	2.05E-07		
72.635	0.341784	2.01E-07		
72.735	0.339024	1.99E-07		
72.835	0.342489	2.01E-07		

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73.630.376682.22E-0773.730.3956552.33E-0773.830.4468112.63E-0773.930.325121.91E-0774.030.3866592.27E-0774.1250.4209622.48E-0774.250.369642.17E-0774.3250.3761992.21E-0774.4250.4296192.53E-0774.5250.3795442.23E-0774.6250.4493372.64E-0774.8250.3134851.84E-0774.9250.377442.22E-0775.0250.3922152.31E-0775.1250.3445632.03E-0775.2250.3925142.31E-0775.3250.3007441.77E-0775.4250.3619912.13E-07	Depth	Mag Susc 10e-3 SI	Mag Susc		
73.035       0.399241       2.35E-07         73.135       0.389468       2.29E-07         73.235       0.420887       2.48E-07         73.33       0.351532       2.07E-07         73.33       0.400913       2.39E-07         73.53       0.420973       2.48E-07         73.63       0.37668       2.22E-07         73.73       0.395655       2.33E-07         73.83       0.446811       2.63E-07         74.03       0.386659       2.27E-07         74.125       0.420962       2.48E-07         74.25       0.36964       2.17E-07         74.25       0.36964       2.17E-07         74.25       0.37619       2.21E-07         74.25       0.379544       2.23E-07         74.25       0.379544       2.22E-07         74.625       0.49337       2.64E-07         74.725       0.36566       2.16E-07         74.825       0.313485       1.84E-07         75.025       0.39215       2.31E-07         75.125       0.30744       1.77E-07         75.25       0.30744       1.77E-07         75.25       0.30754       2.31E-07	ft bgs	units	m3/kg		
73.135       0.389468       2.29E-07         73.235       0.420887       2.48E-07         73.33       0.351532       2.07E-07         73.43       0.406913       2.39E-07         73.53       0.420973       2.48E-07       73.5       3.31E-07         73.63       0.37668       2.22E-07       73.5       3.31E-07         73.63       0.446811       2.63E-07       74.03       0.386659       2.27E-07         74.03       0.336659       2.27E-07       74.125       0.420962       2.48E-07         74.25       0.376199       2.21E-07       74.325       0.379544       2.23E-07         74.425       0.429619       2.53E-07       74.625       0.44937       2.64E-07         74.725       0.366566       2.16E-07       74.825       0.313485       1.84E-07         74.925       0.37744       2.22E-07       75.025       0.392215       2.31E-07         75.025       0.39215       2.31E-07       75.52       2.25E-07         75.525       0.30744       1.77E-07       75.52       2.25E-07         75.525       0.30731       1.81E-07       75.52       2.25E-07         75.525       0.30342       1.77E-	72.935	0.321699	1.89E-07		
73.235       0.420887       2.48E-07         73.33       0.351532       2.07E-07         73.43       0.406913       2.39E-07         73.53       0.420973       2.48E-07         73.63       0.37668       2.22E-07         73.73       0.395655       2.33E-07         73.83       0.446811       2.63E-07         74.03       0.386659       2.27E-07         74.125       0.420962       2.48E-07         74.225       0.36964       2.17E-07         74.325       0.376199       2.21E-07         74.425       0.429619       2.53E-07         74.525       0.379544       2.22E-07         74.625       0.449337       2.64E-07         74.725       0.366566       2.16E-07         74.825       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.125       0.300744       1.77E-07         75.255       0.310864       1.83E-07         75.525       0.300744       1.77E-07         75.525       0.30735       1.81E-07         75.255       0.30342       1.77E-07         75.625       0.303632       2.28E-07	73.035	0.399241	2.35E-07		
73.33       0.351532       2.07E-07         73.43       0.406913       2.39E-07         73.53       0.420973       2.48E-07         73.63       0.37668       2.22E-07         73.73       0.395655       2.33E-07         73.83       0.446811       2.63E-07         74.03       0.386659       2.27E-07         74.125       0.420962       2.48E-07         74.225       0.36964       2.17E-07         74.325       0.376199       2.21E-07         74.425       0.429619       2.53E-07         74.525       0.379544       2.22E-07         74.625       0.49337       2.64E-07         74.725       0.366566       2.16E-07         74.825       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.025       0.300744       1.77E-07         75.525       0.300744       1.77E-07         75.525       0.300744       1.77E-07         75.525       0.301864       1.83E-07         75.525       0.303032       1.77E-07         75.625       0.303032       1.72E-07         75.625       0.3030342       1.77E-07 <td>73.135</td> <td>0.389468</td> <td>2.29E-07</td> <td></td> <td></td>	73.135	0.389468	2.29E-07		
73.43       0.406913       2.39E-07         73.53       0.420973       2.48E-07         73.63       0.37668       2.22E-07         73.73       0.395655       2.33E-07         73.83       0.446811       2.63E-07         73.93       0.32512       1.91E-07         74.03       0.386659       2.27E-07         74.125       0.420962       2.48E-07         74.255       0.36964       2.17E-07         74.325       0.376199       2.21E-07         74.425       0.429619       2.53E-07         74.525       0.379544       2.22E-07         74.625       0.449337       2.64E-07         74.625       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.025       0.39215       2.31E-07         75.125       0.300744       1.77E-07         75.525       0.300744       1.77E-07         75.525       0.300744       1.78E-07         75.525       0.300342       1.77E-07         75.525       0.303951       1.99E-07         75.525       0.30342       1.77E-07         75.525       0.30342       1.77E-07	73.235	0.420887	2.48E-07		
73.53       0.420973       2.48E-07         73.63       0.37668       2.22E-07         73.73       0.395655       2.33E-07         73.83       0.446811       2.63E-07         74.03       0.386659       2.27E-07         74.125       0.420962       2.48E-07         74.225       0.36964       2.17E-07         74.25       0.376199       2.21E-07         74.425       0.429619       2.53E-07         74.425       0.379544       2.23E-07         74.625       0.379544       2.22E-07         74.625       0.379544       2.22E-07         74.825       0.313485       1.84E-07         74.825       0.37744       2.22E-07         75.025       0.392215       2.31E-07         75.125       0.344563       2.03E-07         75.255       0.300744       1.77E-07         75.525       0.310864       1.83E-07         75.525       0.36547       2.15E-07         75.525       0.3073       1.81E-07         75.525       0.330751       1.99E-07         75.525       0.339051       1.99E-07         75.525       0.339051       2.90E-07	73.33	0.351532	2.07E-07		
73.63       0.37668       2.22E-07         73.73       0.395655       2.33E-07         73.83       0.446811       2.63E-07         74.03       0.386659       2.27E-07         74.125       0.420962       2.48E-07         74.25       0.36964       2.17E-07         74.25       0.376199       2.21E-07         74.425       0.429619       2.53E-07         74.525       0.379544       2.23E-07         74.625       0.449337       2.64E-07         74.725       0.366566       2.16E-07         74.825       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.025       0.392215       2.31E-07         75.125       0.30744       1.77E-07         75.255       0.300744       1.77E-07         75.525       0.310864       1.83E-07         75.525       0.3073       1.81E-07         75.525       0.3073       1.81E-07         75.525       0.30742       1.77E-07         75.625       0.3073       1.88E-07         75.525       0.30342       1.77E-07         76.25       0.30342       1.77E-07 <tr< td=""><td>73.43</td><td>0.406913</td><td>2.39E-07</td><td></td><td></td></tr<>	73.43	0.406913	2.39E-07		
73.73       0.395655       2.33E-07         73.83       0.446811       2.63E-07         73.93       0.32512       1.91E-07         74.03       0.386659       2.27E-07         74.125       0.420962       2.48E-07         74.225       0.36964       2.17E-07         74.325       0.376199       2.21E-07         74.425       0.429619       2.53E-07         74.525       0.379544       2.23E-07         74.625       0.449337       2.64E-07         74.725       0.366566       2.16E-07         74.825       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.025       0.392215       2.31E-07         75.125       0.30744       1.77E-07         75.25       0.30744       1.77E-07         75.525       0.300744       1.77E-07         75.525       0.361991       2.13E-07         75.525       0.3073       1.81E-07         75.525       0.3073       1.81E-07         75.525       0.30951       1.99E-07         75.525       0.30342       1.77E-07         76.25       0.30342       1.77E-07      <	73.53	0.420973	2.48E-07	73.5	3.31E-07
73.83       0.446811       2.63E-07         73.93       0.32512       1.91E-07         74.03       0.386659       2.27E-07         74.125       0.420962       2.48E-07         74.225       0.36964       2.17E-07         74.325       0.376199       2.21E-07         74.425       0.429619       2.53E-07         74.525       0.379544       2.23E-07         74.625       0.449337       2.64E-07         74.725       0.366566       2.16E-07         74.825       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.025       0.392215       2.31E-07         75.125       0.344563       2.03E-07         75.25       0.300744       1.77E-07         75.25       0.300744       1.77E-07         75.525       0.36547       2.15E-07         75.525       0.36547       2.15E-07         75.525       0.30734       1.87E-07         75.825       0.339051       1.99E-07         75.925       0.387152       2.28E-07         75.925       0.339051       1.99E-07         75.925       0.339051       1.99E-07 <td>73.63</td> <td>0.37668</td> <td>2.22E-07</td> <td></td> <td></td>	73.63	0.37668	2.22E-07		
73.93       0.32512       1.91E-07         74.03       0.386659       2.27E-07         74.125       0.420962       2.48E-07         74.225       0.36964       2.17E-07         74.325       0.376199       2.21E-07         74.425       0.429619       2.53E-07         74.525       0.379544       2.23E-07         74.625       0.449337       2.64E-07         74.625       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.025       0.392215       2.31E-07         75.125       0.344563       2.03E-07         75.255       0.30744       1.77E-07         75.255       0.300744       1.77E-07         75.525       0.310864       1.83E-07         75.525       0.361991       2.13E-07         75.625       0.361991       2.13E-07         75.625       0.36547       2.15E-07         75.825       0.339051       1.99E-07         75.825       0.339051       1.99E-07         75.925       0.387152       2.28E-07         75.925       0.339051       1.99E-07         76.25       0.30342       1.77E-07 </td <td>73.73</td> <td>0.395655</td> <td>2.33E-07</td> <td></td> <td></td>	73.73	0.395655	2.33E-07		
74.03       0.386659       2.27E-07         74.125       0.420962       2.48E-07         74.225       0.36964       2.17E-07         74.325       0.376199       2.21E-07         74.425       0.429619       2.53E-07         74.525       0.379544       2.23E-07         74.625       0.449337       2.64E-07         74.725       0.366566       2.16E-07         74.825       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.025       0.392215       2.31E-07         75.125       0.344563       2.03E-07         75.255       0.30744       1.77E-07         75.325       0.300744       1.77E-07         75.425       0.361991       2.13E-07         75.525       0.300744       1.77E-07         75.625       0.36547       2.15E-07         75.525       0.361991       1.88E-07         75.825       0.339051       1.99E-07         75.925       0.387152       2.28E-07         76.025       0.31965       1.88E-07         76.225       0.30342       1.77E-07         76.25       0.30342       1.77E-07 </td <td>73.83</td> <td>0.446811</td> <td>2.63E-07</td> <td></td> <td></td>	73.83	0.446811	2.63E-07		
74.125       0.420962       2.48E-07         74.225       0.36964       2.17E-07         74.325       0.376199       2.21E-07         74.425       0.429619       2.53E-07         74.525       0.379544       2.23E-07         74.625       0.449337       2.64E-07         74.625       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.025       0.39215       2.31E-07         75.125       0.344563       2.03E-07         75.255       0.300744       1.77E-07         75.255       0.300744       1.77E-07         75.625       0.36547       2.15E-07         75.725       0.3073       1.83E-07         75.925       0.387152       2.28E-07         76.025       0.390342       1.77E-07         76.125       0.30342       1.77E-07         76.325       0.278654       1.64E-07	73.93	0.32512	1.91E-07		
74.225       0.36964       2.17E-07         74.325       0.376199       2.21E-07         74.425       0.429619       2.53E-07         74.525       0.379544       2.23E-07         74.625       0.449337       2.64E-07         74.725       0.366566       2.16E-07         74.825       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.025       0.39215       2.31E-07         75.125       0.344563       2.03E-07         75.255       0.300744       1.77E-07         75.255       0.310864       1.83E-07         75.625       0.36547       2.15E-07         75.925       0.387152       2.28E-07         76.125       0.300342       1.77E-07	74.03	0.386659	2.27E-07		
74.325       0.376199       2.21E-07         74.425       0.429619       2.53E-07         74.525       0.379544       2.23E-07         74.625       0.449337       2.64E-07         74.725       0.366566       2.16E-07         74.825       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.025       0.39215       2.31E-07         75.125       0.344563       2.03E-07         75.255       0.300744       1.77E-07         75.425       0.36547       2.13E-07         75.525       0.300744       1.77E-07         75.625       0.36547       2.13E-07         75.752       0.301864       1.83E-07         75.752       0.3073       1.81E-07         75.825       0.339051       1.99E-07         75.825       0.339051       1.99E-07         76.125       0.30342       1.77E-07         76.25       0.31965       1.88E-07         76.25       0.355817       2.09E-07         76.25       0.30342       1.77E-07         76.325       0.278654       1.64E-07         76.425       0.362817       2.13E-07	74.125	0.420962	2.48E-07		
74.425       0.429619       2.53E-07         74.525       0.379544       2.23E-07         74.625       0.449337       2.64E-07         74.725       0.366566       2.16E-07         74.825       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.025       0.392215       2.31E-07         75.125       0.344563       2.03E-07         75.255       0.30744       1.77E-07         75.325       0.300744       1.77E-07         75.425       0.36547       2.13E-07         75.525       0.310864       1.83E-07         75.755       0.30733       1.81E-07         75.825       0.339051       1.99E-07         75.925       0.339051       1.99E-07         75.925       0.337152       2.28E-07         76.025       0.31965       1.88E-07         76.125       0.30342       1.77E-07         76.25       0.30342       1.77E-07         76.25       0.355817       2.09E-07         76.325       0.278654       1.64E-07         76.425       0.362817       2.13E-07         76.525       0.402683       2.37E-07 </td <td>74.225</td> <td>0.36964</td> <td>2.17E-07</td> <td></td> <td></td>	74.225	0.36964	2.17E-07		
74.525       0.379544       2.23E-07         74.625       0.449337       2.64E-07         74.725       0.366566       2.16E-07         74.825       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.025       0.392215       2.31E-07         75.125       0.344563       2.03E-07         75.255       0.392514       2.31E-07         75.325       0.300744       1.77E-07         75.525       0.310864       1.83E-07         75.625       0.36547       2.15E-07         75.625       0.339051       1.99E-07         75.825       0.339051       1.99E-07         75.925       0.339051       1.99E-07         76.025       0.31965       1.88E-07         76.125       0.300342       1.77E-07         76.25       0.339051       1.99E-07         76.625       0.31965       1.88E-07         76.125       0.300342       1.77E-07         76.325       0.278654       1.64E-07         76.325       0.278654       1.64E-07         76.425       0.362817       2.13E-07         76.525       0.402683       2.37E-07	74.325	0.376199	2.21E-07		
74.625       0.449337       2.64E-07         74.725       0.366566       2.16E-07         74.825       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.025       0.392215       2.31E-07         75.125       0.344563       2.03E-07         75.225       0.392514       2.31E-07         75.325       0.300744       1.77E-07         75.425       0.361991       2.13E-07         75.625       0.361991       2.13E-07         75.625       0.361991       2.13E-07         75.625       0.361991       2.13E-07         75.625       0.36547       2.15E-07         75.625       0.33073       1.81E-07         75.925       0.337152       2.28E-07         76.025       0.31965       1.88E-07         76.125       0.30342       1.77E-07         76.225       0.355817       2.09E-07         76.325       0.278654       1.64E-07         76.425       0.362817       2.13E-07         76.525       0.402683       2.37E-07         76.525       0.402683       2.37E-07         76.525       0.402683       2.37E-07	74.425	0.429619	2.53E-07		
74.725       0.366566       2.16E-07         74.825       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.025       0.392215       2.31E-07         75.125       0.344563       2.03E-07         75.225       0.392514       2.31E-07         75.225       0.300744       1.77E-07         75.325       0.300744       1.77E-07         75.425       0.361991       2.13E-07         75.525       0.310864       1.83E-07         75.625       0.36547       2.15E-07         75.625       0.339051       1.99E-07         75.925       0.339051       1.99E-07         76.025       0.31965       1.88E-07         76.125       0.300342       1.77E-07         76.225       0.355817       2.09E-07         76.25       0.355817       2.09E-07         76.325       0.278654       1.64E-07         76.425       0.362817       2.13E-07         76.525       0.402683       2.37E-07         76.525       0.402683       2.37E-07         76.525       0.402683       2.37E-07         76.62       0.31843       1.887E-07	74.525	0.379544	2.23E-07		
74.825       0.313485       1.84E-07         74.925       0.37744       2.22E-07         75.025       0.392215       2.31E-07         75.125       0.344563       2.03E-07         75.225       0.392514       2.31E-07         75.225       0.30744       1.77E-07         75.325       0.300744       1.77E-07         75.525       0.310864       1.83E-07         75.625       0.36547       2.15E-07         75.625       0.36547       2.15E-07         75.725       0.3073       1.81E-07         75.925       0.387152       2.28E-07         76.025       0.31965       1.88E-07         76.125       0.30342       1.77E-07         76.25       0.355817       2.09E-07         76.325       0.278654       1.64E-07         76.325       0.362817       2.09E-07         76.425       0.362817       2.13E-07         76.525       0.402683       2.37E-07         76.525       0.402683       2.37E-07         76.525       0.402683       2.37E-07         76.62       0.31843       1.87E-07         76.62       0.314715       2.01E-07	74.625	0.449337	2.64E-07		
74.925       0.37744       2.22E-07         75.025       0.392215       2.31E-07         75.125       0.344563       2.03E-07         75.225       0.392514       2.31E-07         75.325       0.300744       1.77E-07         75.425       0.361991       2.13E-07         75.525       0.310864       1.83E-07         75.625       0.36547       2.15E-07         75.625       0.36547       2.15E-07         75.725       0.3073       1.81E-07         75.925       0.339051       1.99E-07         75.925       0.337152       2.28E-07         76.025       0.31965       1.88E-07         76.125       0.300342       1.77E-07         76.225       0.355817       2.09E-07         76.325       0.278654       1.64E-07         76.425       0.362817       2.13E-07         76.525       0.402683       2.37E-07         76.525       0.402683       2.37E-07         76.62       0.31843       1.87E-07         76.62       0.314715       2.01E-07         76.72       0.341715       2.01E-07         76.82       0.336069       1.98E-07 <td>74.725</td> <td>0.366566</td> <td>2.16E-07</td> <td></td> <td></td>	74.725	0.366566	2.16E-07		
75.025       0.392215       2.31E-07         75.125       0.344563       2.03E-07         75.225       0.392514       2.31E-07         75.325       0.300744       1.77E-07         75.425       0.361991       2.13E-07         75.525       0.310864       1.83E-07         75.625       0.36547       2.15E-07         75.725       0.3073       1.81E-07         75.825       0.339051       1.99E-07         75.925       0.387152       2.28E-07         76.025       0.31965       1.88E-07         76.125       0.300342       1.77E-07         76.225       0.339051       1.99E-07         76.125       0.300342       1.77E-07         76.225       0.355817       2.09E-07         76.325       0.278654       1.64E-07         76.425       0.362817       2.13E-07         76.525       0.402683       2.37E-07         76.525       0.402683       2.37E-07         76.62       0.31843       1.87E-07         76.72       0.341715       2.01E-07         76.82       0.336069       1.98E-07	74.825	0.313485	1.84E-07		
75.125       0.344563       2.03E-07         75.225       0.392514       2.31E-07         75.325       0.300744       1.77E-07         75.425       0.361991       2.13E-07         75.525       0.310864       1.83E-07         75.625       0.36547       2.15E-07         75.625       0.36547       2.15E-07         75.725       0.3073       1.81E-07         75.825       0.339051       1.99E-07         75.925       0.387152       2.28E-07         76.025       0.31965       1.88E-07         76.125       0.30342       1.77E-07         76.325       0.278654       1.64E-07         76.325       0.362817       2.09E-07         76.525       0.402683       2.37E-07         76.525       0.402683       2.37E-07         76.525       0.402683       2.37E-07         76.525       0.402683       2.37E-07         76.62       0.31843       1.87E-07         76.72       0.341715       2.01E-07         76.82       0.336069       1.98E-07	74.925	0.37744	2.22E-07		
75.225       0.392514       2.31E-07         75.325       0.300744       1.77E-07         75.425       0.361991       2.13E-07         75.525       0.310864       1.83E-07         75.625       0.36547       2.15E-07         75.725       0.3073       1.81E-07         75.725       0.3073       1.81E-07         75.925       0.339051       1.99E-07         75.925       0.31965       1.88E-07         76.025       0.31965       1.88E-07         76.225       0.355817       2.09E-07         76.325       0.278654       1.64E-07         76.425       0.362817       2.13E-07         76.525       0.402683       2.37E-07         76.525       0.402683       1.88F-07         76.525       0.402683       2.37E-07         76.62       0.31843       1.87E-07         76.62       0.314715       2.01E-07         76.72       0.341715       2.01E-07         76.82       0.336069       1.98E-07	75.025	0.392215	2.31E-07		
75.325       0.300744       1.77E-07         75.425       0.361991       2.13E-07         75.525       0.310864       1.83E-07         75.625       0.36547       2.15E-07         75.725       0.3073       1.81E-07         75.825       0.339051       1.99E-07         75.925       0.387152       2.28E-07         76.025       0.31965       1.88E-07         76.125       0.300342       1.77E-07         76.25       0.355817       2.09E-07         76.325       0.278654       1.64E-07         76.425       0.362817       2.13E-07         76.525       0.402683       2.37E-07         76.62       0.31843       1.87E-07         76.62       0.31843       1.87E-07         76.62       0.31843       1.87E-07         76.62       0.31843       1.87E-07         76.72       0.341715       2.01E-07         76.82       0.336069       1.98E-07	75.125	0.344563	2.03E-07		
75.425       0.361991       2.13E-07         75.525       0.310864       1.83E-07         75.625       0.36547       2.15E-07         75.625       0.3073       1.81E-07         75.725       0.3073       1.81E-07         75.925       0.339051       1.99E-07         75.925       0.387152       2.28E-07         76.025       0.31965       1.88E-07         76.125       0.30342       1.77E-07         76.325       0.278654       1.64E-07         76.425       0.362817       2.13E-07         76.525       0.402683       2.37E-07         76.525       0.402683       1.87E-07         76.62       0.31843       1.87E-07         76.62       0.314715       2.01E-07         76.72       0.341715       2.01E-07         76.82       0.336069       1.98E-07	75.225	0.392514	2.31E-07		
75.525       0.310864       1.83E-07       75.5       2.25E-07         75.625       0.36547       2.15E-07         75.725       0.3073       1.81E-07         75.825       0.339051       1.99E-07         75.925       0.387152       2.28E-07         76.025       0.31065       1.88E-07         76.125       0.300342       1.77E-07         76.325       0.278654       1.64E-07         76.425       0.362817       2.13E-07         76.525       0.402683       2.37E-07         76.62       0.31843       1.87E-07         76.72       0.341715       2.01E-07         76.72       0.336069       1.98E-07	75.325	0.300744	1.77E-07		
75.6250.365472.15E-0775.7250.30731.81E-0775.8250.3390511.99E-0775.9250.3871522.28E-0776.0250.319651.88E-0776.1250.3003421.77E-0776.3250.2786541.64E-0776.4250.3628172.13E-0776.5250.4026832.37E-0776.620.318431.87E-0776.720.3417152.01E-0776.820.3360691.98E-07	75.425	0.361991	2.13E-07		
75.7250.30731.81E-0775.8250.3390511.99E-0775.9250.3871522.28E-0776.0250.319651.88E-0776.1250.3003421.77E-0776.2250.3558172.09E-0776.3250.2786541.64E-0776.4250.3628172.13E-0776.5250.4026832.37E-0776.620.318431.87E-0776.720.3417152.01E-0776.820.3360691.98E-07	75.525	0.310864	1.83E-07	75.5	2.25E-07
75.8250.3390511.99E-0775.9250.3871522.28E-0776.0250.319651.88E-0776.1250.3003421.77E-0776.2250.3558172.09E-0776.3250.2786541.64E-0776.4250.3628172.13E-0776.5250.4026832.37E-0776.620.318431.87E-0776.720.3417152.01E-0776.820.3360691.98E-07	75.625	0.36547	2.15E-07		
75.9250.3871522.28E-0776.0250.319651.88E-0776.1250.3003421.77E-0776.2250.3558172.09E-0776.3250.2786541.64E-0776.4250.3628172.13E-0776.5250.4026832.37E-0776.620.318431.87E-0776.720.3417152.01E-0776.820.3360691.98E-07	75.725	0.3073	1.81E-07		
76.0250.319651.88E-0776.1250.3003421.77E-0776.2250.3558172.09E-0776.3250.2786541.64E-0776.4250.3628172.13E-0776.5250.4026832.37E-0776.620.318431.87E-0776.720.3417152.01E-0776.820.3360691.98E-07	75.825	0.339051	1.99E-07		
76.1250.3003421.77E-0776.2250.3558172.09E-0776.3250.2786541.64E-0776.4250.3628172.13E-0776.5250.4026832.37E-0776.620.318431.87E-0776.720.3417152.01E-0776.820.3360691.98E-07	75.925	0.387152	2.28E-07		
76.2250.3558172.09E-0776.3250.2786541.64E-0776.4250.3628172.13E-0776.5250.4026832.37E-0776.620.318431.87E-0776.720.3417152.01E-0776.820.3360691.98E-07	76.025	0.31965	1.88E-07		
76.3250.2786541.64E-0776.4250.3628172.13E-0776.5250.4026832.37E-0776.620.318431.87E-0776.720.3417152.01E-0776.820.3360691.98E-07	76.125	0.300342	1.77E-07		
76.4250.3628172.13E-0776.5250.4026832.37E-0776.620.318431.87E-0776.720.3417152.01E-0776.820.3360691.98E-07	76.225	0.355817	2.09E-07		
76.5250.4026832.37E-0776.620.318431.87E-0776.720.3417152.01E-0776.820.3360691.98E-07	76.325	0.278654	1.64E-07		
76.620.318431.87E-0776.720.3417152.01E-0776.820.3360691.98E-07	76.425	0.362817	2.13E-07		
76.720.3417152.01E-0776.820.3360691.98E-07	76.525	0.402683	2.37E-07		
76.82 0.336069 1.98E-07	76.62	0.31843	1.87E-07		
	76.72	0.341715	2.01E-07		
76.92 0.376118 2.21E-07	76.82	0.336069	1.98E-07		
	76.92	0.376118	2.21E-07		

ft bgsunitsm3/kg77.020.3228011.9E-0777.120.3390181.99E-0777.3150.3407192E-0777.4150.3310511.95E-0777.4150.3652532.15E-0777.5150.3625332.02E-0777.5150.3241351.91E-0777.7150.3429532.02E-0777.7150.3266271.92E-0777.8150.3266271.92E-0778.0150.3266271.92E-0778.150.3670862.16E-0778.150.3670862.16E-0778.150.3670862.16E-0778.150.3670822.28E-0778.150.365621.98E-0778.150.365621.98E-0778.150.3899612.29E-0778.6150.4056092.39E-0778.6150.3895671.99E-0778.7150.3899612.29E-0778.7150.3899612.29E-0778.7150.3895671.99E-0778.7150.3892612.17E-0778.7150.3892612.17E-0779.6150.3024131.92E-0779.150.3016041.77E-0779.150.3016041.77E-0779.5150.3016041.77E-0779.6150.3024131.78E-0779.7150.3274372.05E-0779.7150.3274372.05E-0779.7150.3274372.05E-0779.7150.3274131.91E-0780.710.279307<	Depth	Mag Susc 10e-3 SI	Mag Susc
77.020.3228011.9E-0777.120.3593292.11E-0777.220.3390181.99E-0777.3150.3407192E-0777.4150.3310511.95E-0777.5150.3652532.15E-0777.6150.3241351.91E-0777.7150.3429532.02E-0777.8150.3606682.12E-0778.0150.3266271.92E-0778.1150.3670862.16E-0778.1150.3670862.16E-0778.1150.3670862.16E-0778.1150.3670862.28E-0778.5150.3365621.98E-0778.5150.3365621.98E-0778.6150.4167282.45E-0778.6150.3682742.17E-0778.6150.3682742.17E-0778.6150.3636922.14E-0779.0150.3636922.14E-0779.1150.4180942.46E-0779.1150.3402062E-0779.5150.3016041.77E-0779.6150.3024131.78E-0779.6150.3024131.78E-0779.6150.3024131.78E-0779.6150.2946691.73E-0779.6150.3478772.05E-0779.6150.3209611.89E-0780.110.3446812.03E-0780.210.29941.76E-0780.510.3735362.2E-0780.6050.3512332.07E-0780.6050.3512332.07E-0780.6050	fthee		m2/ka
77.120.3593292.11E-0777.220.3390181.99E-0777.3150.3407192E-0777.4150.3310511.95E-0777.5150.3652532.15E-0777.6150.3241351.91E-0777.7150.3429532.02E-0777.8150.3606682.12E-0778.0150.3266271.92E-0778.1150.3670862.16E-0778.1150.3670862.16E-0778.1150.3670862.18E-0778.1150.3670862.18E-0778.1150.3670862.39E-0778.5150.3365621.98E-0778.6150.4167282.45E-0778.6150.3682742.17E-0778.6150.3682742.17E-0778.6150.3636922.14E-0779.0150.3636922.14E-0779.0150.3636922.14E-0779.1150.4180942.46E-0779.1150.3402062E-0779.5150.3016041.77E-0779.5150.3024131.78E-0779.5150.3024131.78E-0779.6150.2946691.73E-0779.6150.2946691.73E-0780.110.3420811.91E-0780.110.3209611.89E-0780.210.299541.76E-0780.510.3735362.2E-0780.6050.3512332.07E-0780.6050.3512332.07E-0780.6050.3512332.07E-0780.605 <td< td=""><td>-</td><td></td><td>-</td></td<>	-		-
77.220.3390181.99E-0777.3150.3407192E-0777.4150.3310511.95E-0777.5150.3652532.15E-0777.6150.3241351.91E-0777.7150.3429532.02E-0777.8150.3606682.12E-0778.0150.3266271.92E-0778.1150.3670862.16E-0778.1150.3670862.16E-0778.1150.3869822.28E-0778.5150.3365621.98E-0778.5150.3365621.98E-0778.5150.3365621.98E-0778.5150.3365621.98E-0778.5150.3365621.98E-0778.5150.33682742.17E-0778.5150.3682742.17E-0778.5150.3682742.17E-0779.5150.3308281.95E-0779.5150.3308281.95E-0779.5150.3016041.77E-0779.5150.3016041.77E-0779.5150.3024131.78E-0779.5150.3024131.78E-0779.5150.3024131.78E-0779.5150.3024131.78E-0779.6150.32251411.91E-0780.110.3229611.89E-0780.210.2994691.76E-0780.310.3209611.89E-0780.410.2995641.76E-0780.6050.3512332.07E-0780.6050.3512332.07E-0780.6050.3512332.07E-0780.605			
77.3150.3407192E-0777.4150.3310511.95E-0777.5150.3652532.15E-0777.6150.3241351.91E-0777.7150.3429532.02E-0777.8150.3606682.12E-0778.0150.3262271.92E-0778.1150.3670862.16E-0778.1150.3670862.16E-0778.1150.3670862.16E-0778.1150.3670862.18E-0778.1150.3365621.98E-0778.5150.3365621.98E-0778.5150.3365621.98E-0778.6150.4056092.39E-0778.6150.3682742.17E-0778.6150.3682742.17E-0778.9150.3636922.14E-0779.0150.3636922.14E-0779.150.3108281.95E-0779.150.3016041.77E-0779.150.3016041.77E-0779.5150.3016041.77E-0779.6150.3024131.78E-0779.7150.3478772.05E-0779.7150.3478772.05E-0779.910.2793071.64E-0780.110.3209611.89E-0780.210.29941.76E-0780.310.3209611.89E-0780.410.2995641.76E-0780.6050.3512332.07E-0780.6050.3512332.07E-0780.6050.3512332.07E-0780.6050.3512332.07E-0780.605 <t< td=""><td></td><td></td><td></td></t<>			
77.4150.3310511.95E-0777.5150.3652532.15E-0777.6150.3241351.91E-0777.7150.3429532.02E-0777.8150.3548052.09E-0778.0150.3266271.92E-0778.1150.3670862.16E-0778.1150.3869822.28E-0778.3150.3365621.98E-0778.5150.3365621.98E-0778.5150.3365621.98E-0778.6150.4056092.39E-0778.6150.4056092.39E-0778.6150.3682742.17E-0778.7150.3385671.99E-0779.0150.3636922.14E-0779.150.3308281.95E-0779.150.3308281.95E-0779.150.3308281.95E-0779.5150.3016041.77E-0779.5150.3024131.78E-0779.6150.3024131.78E-0779.6150.3024131.78E-0779.6150.3024131.78E-0779.6150.3251411.91E-0780.010.3251411.91E-0780.110.3209611.89E-0780.210.2995641.76E-0780.410.2995641.76E-0780.6050.3512332.07E-0780.6050.3512332.07E-0780.6050.3512332.07E-0780.6050.335671.97E-0780.8050.335671.97E-0780.8050.335671.97E-07			
77.5150.3652532.15E-0777.6150.3241351.91E-0777.7150.3429532.02E-0777.8150.3548052.09E-0778.0150.3266271.92E-0778.1150.3670862.16E-0778.1150.3670862.18E-0778.1150.3869822.28E-0778.5150.3365621.98E-0778.5150.3365621.98E-0778.5150.33899612.29E-0778.6150.4056092.39E-0778.6150.3682742.17E-0778.5150.3385671.99E-0779.0150.3636922.14E-0779.1150.4180942.46E-0779.1150.3402062E-0779.5150.3016041.77E-0779.5150.3024131.78E-0779.5150.3024131.78E-0779.5150.3024131.78E-0779.6150.3251411.91E-0780.010.3251411.91E-0780.110.3446812.03E-0780.210.299461.76E-0780.310.3209611.89E-0780.410.2995641.76E-0780.6050.3512332.07E-0780.6050.3512332.07E-0780.6050.3512332.07E-0780.6050.335671.97E-0780.8050.335671.97E-0780.8050.335671.97E-0780.8050.335671.97E-0780.8050.335671.97E-0780.805 <t< td=""><td></td><td></td><td></td></t<>			
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79.3150.3933122.31E-0779.4150.3402062E-0779.5150.3016041.77E-0779.6150.3024131.78E-0779.7150.3478772.05E-0779.8150.2946691.73E-0779.910.2793071.64E-0780.010.3251411.91E-0780.210.29941.76E-0780.310.3209611.89E-0780.410.2995641.76E-0780.6050.3512332.07E-0780.6050.3979572.34E-0780.8050.335671.97E-0780.9050.3818642.25E-07	79.115	0.418094	2.46E-07
79.4150.3402062E-0779.5150.3016041.77E-0779.6150.3024131.78E-0779.7150.3478772.05E-0779.8150.2946691.73E-0779.910.2793071.64E-0780.010.3251411.91E-0780.110.3446812.03E-0780.210.29941.76E-0780.310.3209611.89E-0780.410.2995641.76E-0780.550.3512332.07E-0780.6050.3979572.34E-0780.8050.335671.97E-0780.9050.3818642.25E-07	79.215	0.330828	1.95E-07
79.5150.3016041.77E-0779.6150.3024131.78E-0779.7150.3478772.05E-0779.8150.2946691.73E-0779.910.2793071.64E-0780.010.3251411.91E-0780.110.3446812.03E-0780.210.29941.76E-0780.310.3209611.89E-0780.410.2995641.76E-0780.510.3735362.2E-0780.6050.3512332.07E-0780.7050.3979572.34E-0780.8050.335671.97E-0780.9050.3818642.25E-07	79.315	0.393312	2.31E-07
79.6150.3024131.78E-0779.7150.3478772.05E-0779.8150.2946691.73E-0779.910.2793071.64E-0780.010.3251411.91E-0780.110.3446812.03E-0780.210.29941.76E-0780.310.3209611.89E-0780.410.2995641.76E-0780.510.3735362.2E-0780.6050.3512332.07E-0780.7050.3979572.34E-0780.8050.335671.97E-0780.9050.3818642.25E-07	79.415	0.340206	2E-07
79.7150.3478772.05E-0779.8150.2946691.73E-0779.910.2793071.64E-0780.010.3251411.91E-0780.110.3446812.03E-0780.210.29941.76E-0780.310.3209611.89E-0780.410.2995641.76E-0780.550.3735362.2E-0780.6050.3512332.07E-0780.7050.3979572.34E-0780.8050.335671.97E-0780.9050.3818642.25E-07	79.515	0.301604	1.77E-07
79.8150.2946691.73E-0779.910.2793071.64E-0780.010.3251411.91E-0780.110.3446812.03E-0780.210.29941.76E-0780.310.3209611.89E-0780.410.2995641.76E-0780.510.3735362.2E-0780.6050.3512332.07E-0780.7050.3979572.34E-0780.8050.335671.97E-0780.9050.3818642.25E-07	79.615	0.302413	1.78E-07
79.910.2793071.64E-0780.010.3251411.91E-0780.110.3446812.03E-0780.210.29941.76E-0780.310.3209611.89E-0780.410.2995641.76E-0780.510.3735362.2E-0780.6050.3512332.07E-0780.7050.3979572.34E-0780.8050.335671.97E-0780.9050.3818642.25E-07	79.715	0.347877	2.05E-07
80.010.3251411.91E-0780.110.3446812.03E-0780.210.29941.76E-0780.310.3209611.89E-0780.410.2995641.76E-0780.500.3735362.2E-0780.6050.3512332.07E-0780.7050.3979572.34E-0780.8050.335671.97E-0780.9050.3818642.25E-07	79.815	0.294669	1.73E-07
80.110.3446812.03E-0780.210.29941.76E-0780.310.3209611.89E-0780.410.2995641.76E-0780.510.3735362.2E-0780.6050.3512332.07E-0780.7050.3979572.34E-0780.8050.335671.97E-0780.9050.3818642.25E-07	79.91	0.279307	1.64E-07
80.210.29941.76E-0780.310.3209611.89E-0780.410.2995641.76E-0780.510.3735362.2E-0780.6050.3512332.07E-0780.7050.3979572.34E-0780.8050.335671.97E-0780.9050.3818642.25E-07	80.01	0.325141	1.91E-07
80.310.3209611.89E-0780.410.2995641.76E-0780.510.3735362.2E-0780.6050.3512332.07E-0780.7050.3979572.34E-0780.8050.335671.97E-0780.9050.3818642.25E-07	80.11	0.344681	2.03E-07
80.410.2995641.76E-0780.510.3735362.2E-0780.6050.3512332.07E-0780.7050.3979572.34E-0780.8050.335671.97E-0780.9050.3818642.25E-07	80.21	0.2994	1.76E-07
80.510.3735362.2E-0780.6050.3512332.07E-0780.7050.3979572.34E-0780.8050.335671.97E-0780.9050.3818642.25E-07	80.31	0.320961	1.89E-07
80.6050.3512332.07E-0780.7050.3979572.34E-0780.8050.335671.97E-0780.9050.3818642.25E-07	80.41	0.299564	1.76E-07
80.7050.3979572.34E-0780.8050.335671.97E-0780.9050.3818642.25E-07	80.51	0.373536	2.2E-07
80.805 0.33567 1.97E-07 80.905 0.381864 2.25E-07	80.605	0.351233	2.07E-07
80.905 0.381864 2.25E-07	80.705	0.397957	2.34E-07
	80.805	0.33567	1.97E-07
81.005 0.362138 2.13E-07	80.905	0.381864	2.25E-07
	81.005	0.362138	2.13E-07

78.5 4.72E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
81.105	0.361151	2.12E-07
81.205	0.340882	2.01E-07
81.305	0.378727	2.23E-07
81.405	0.408585	2.4E-07
81.505	0.36326	2.14E-07
81.605	0.366843	2.16E-07
81.705	0.3296	1.94E-07
81.805	0.329917	1.94E-07
81.905	0.410404	2.41E-07
82.005	0.376525	2.21E-07
82.105	0.382996	2.25E-07
82.205	0.419366	2.47E-07
82.305	0.408078	2.4E-07
82.405	0.428898	2.52E-07
82.505	0.506463	2.98E-07
82.605	0.471022	2.77E-07
82.705	0.453109	2.67E-07
82.805	0.467603	2.75E-07
82.905	0.550191	3.24E-07
83.005	0.441638	2.6E-07
83.105	0.452225	2.66E-07
83.205	0.43247	2.54E-07
83.3	0.434022	2.55E-07
83.4	0.432269	2.54E-07
83.5	0.48128	2.83E-07
83.6	0.528755	3.11E-07
83.7	0.497656	2.93E-07
83.8	0.48022	2.82E-07
83.895	0.538754	3.17E-07
83.995	0.579697	3.41E-07
84.095	0.541499	3.19E-07
84.195	0.631475	3.71E-07
84.295	0.684187	4.02E-07
84.395	0.636337	3.74E-07
84.495	0.583453	3.43E-07
84.595	0.671214	3.95E-07
84.695	0.628209	3.7E-07
84.795	0.635119	3.74E-07
84.895	0.628343	3.7E-07
84.995	0.581156	3.42E-07
85.095	0.53886	3.17E-07



Depth	Mag Susc 10e-3 SI	Mag Susc			
ft bgs	units	m3/kg			
85.195	0.575722	3.39E-07			
85.295	0.556689	3.27E-07			
85.395	0.671196	3.95E-07			
85.495	0.587744	3.46E-07	85	.5	9.37E-07
85.595	0.627879	3.69E-07	89	.5	1.47E-07
85.695	0.5816	3.42E-07			
85.795	0.690807	4.06E-07			
85.895	0.715992	4.21E-07			
85.995	0.730151	4.3E-07			
86.095	0.763459	4.49E-07			
86.195	0.760655	4.47E-07			
86.295	0.672583	3.96E-07			
86.395	0.669032	3.94E-07			
86.495	0.69161	4.07E-07			
86.59	0.546369	3.21E-07			
86.69	0.487527	2.87E-07			
86.79	0.486377	2.86E-07			
86.89	0.442036	2.6E-07			
86.99	0.428098	2.52E-07			
87.09	0.460821	2.71E-07			
87.19	0.40068	2.36E-07			
87.285	0.458172	2.7E-07			
87.385	0.43236	2.54E-07			
87.485	0.462122	2.72E-07			
87.585	0.40397	2.38E-07			
87.685	0.473935				
87.785	0.482139	2.84E-07			
87.885	0.446684	2.63E-07			
87.985		2.61E-07			
88.085	0.451592	2.66E-07			
88.185	0.421443	2.48E-07			
88.285	0.436054	2.57E-07			
88.385	0.42118	2.48E-07			
88.485	0.46874	2.76E-07			
88.585	0.463045	2.72E-07			
88.685	0.445602	2.62E-07			
88.785	0.431397	2.54E-07			
88.885	0.421247	2.48E-07			
88.985	0.52103	3.06E-07			
89.085	0.408542	2.4E-07			
89.185	0.398879	2.35E-07			



Depth	Mag Susc 10e-3 SI	Mag Susc		
ft bgs	units	m3/kg		
89.285	0.446917	2.63E-07		
89.385	0.409891	2.41E-07		
89.485	0.37705	2.22E-07	89.5	1.47E-07
89.585	0.400587	2.36E-07		
89.685	0.409328	2.41E-07		
89.785	0.390412	2.3E-07		
89.885	0.372868	2.19E-07		
89.98	0.322846	1.9E-07		
90.08	0.364927	2.15E-07		
90.18	0.315034	1.85E-07		
90.28	0.351656	2.07E-07		
90.38	0.337452	1.99E-07		
90.48	0.37318	2.2E-07		
90.575	0.361626	2.13E-07		
90.675	0.411126	2.42E-07		
90.775	0.394517	2.32E-07		
90.875	0.348643	2.05E-07		
90.975	0.382733	2.25E-07		
91.075	0.405308	2.38E-07		
91.175	0.425441	2.5E-07		
91.275	0.446246	2.62E-07		
91.375	0.436132	2.57E-07		
91.475	0.421236	2.48E-07		
91.575	0.393538	2.31E-07		
91.675				
91.775	0.376694	2.22E-07		
91.875		2.13E-07		
	0.398765			
	0.361054			
92.175	0.401029	2.36E-07		
92.275	0.37227	2.19E-07		
92.375	0.355707	2.09E-07		
92.475	0.382001	2.25E-07		
92.575	0.375171	2.21E-07		
92.675	0.376439	2.21E-07		
92.775	0.377916	2.22E-07		
92.875	0.373206	2.2E-07		
92.975	0.327521	1.93E-07		
93.075	0.427902	2.52E-07		
93.175	0.395651	2.33E-07		
93.27	0.395564	2.33E-07		



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
93.37	0.419232	2.47E-07
93.47	0.439699	2.59E-07
93.57	0.413612	2.43E-07
93.67	0.443265	2.61E-07
93.77	0.466475	2.74E-07
93.865	0.43879	2.58E-07
93.965	0.500116	2.94E-07
94.065	0.401844	2.36E-07
94.165	0.532446	3.13E-07
94.265	0.459886	2.71E-07
94.365	0.431298	2.54E-07
94.465	0.477186	2.81E-07
94.565	0.576939	3.39E-07
94.665	0.53026	3.12E-07
94.765	0.480921	2.83E-07
94.865	0.528892	3.11E-07
94.965	0.551821	3.25E-07
95.065	0.538989	3.17E-07
95.165	0.516325	3.04E-07
95.265	0.57691	3.39E-07
95.365	0.512112	3.01E-07
95.465	0.537247	3.16E-07
95.565	0.546681	3.22E-07
95.665	0.563588	3.32E-07
95.765	0.544448	3.2E-07
95.865	0.497408	2.93E-07
95.965	0.453594	2.67E-07
96.065	0.477012	2.81E-07
96.165	0.418455	2.46E-07
96.265	0.445185	2.62E-07
96.365	0.372669	2.19E-07
96.465	0.348088	2.05E-07
96.56	0.388704	2.29E-07
96.66	0.387686	2.28E-07
96.76	0.374193	2.2E-07
96.86	0.337382	1.98E-07
96.96	0.341595	2.01E-07
97.06	0.38175	2.25E-07
97.16	0.308598	1.82E-07
97.255	0.331314	1.95E-07
97.355	0.334107	1.97E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
97.455	0.353449	2.08E-07
97.555	0.371242	2.08L-07 2.18E-07
97.655	0.330616	1.94E-07
97.755	0.358908	2.11E-07
97.855	0.318031	1.87E-07
97.955	0.364319	2.14E-07
98.055	0.322535	1.9E-07
98.155	0.357387	2.1E-07
98.255	0.317031	1.86E-07
98.355	0.363233	2.14E-07
98.455	0.315553	1.86E-07
98.555	0.323202	1.9E-07
98.655	0.316166	1.86E-07
98.755	0.351829	2.07E-07
98.855	0.297343	1.75E-07
98.955	0.319211	1.88E-07
99.055	0.314239	1.85E-07
99.155	0.331793	1.95E-07
99.255	0.346115	2.04E-07
99.355	0.360698	2.12E-07
99.455	0.352562	2.07E-07
99.555	0.356805	2.1E-07
99.655	0.288138	1.69E-07
99.755	0.301613	1.77E-07
99.855	0.311022	1.83E-07
99.95	0.289649	1.7E-07
100.05	0.333369	1.96E-07
100.15	0.340053	2E-07
100.25	0.364714	2.15E-07
100.35	0.385504	2.27E-07
100.45	0.355135	2.09E-07
100.545	0.36016	2.12E-07
100.645	0.330182	1.94E-07
100.745	0.338767	1.99E-07
100.845	0.362904	2.13E-07
100.945	0.333523	1.96E-07
101.045	0.346569	2.04E-07
101.145	0.344499	2.03E-07
101.245	0.3478	2.05E-07
101.345	0.345899	2.03E-07
101.445	0.297384	1.75E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
101.545	0.363253	2.14E-07
101.645	0.328006	1.93E-07
101.745	0.33699	1.98E-07
101.845	0.291209	1.71E-07
101.945	0.37544	2.21E-07
102.045	0.324126	1.91E-07
102.145	0.354278	2.08E-07
102.245	0.350843	2.06E-07
102.345	0.354006	2.08E-07
102.445	0.291329	1.71E-07
102.545	0.319908	1.88E-07
102.645	0.342731	2.02E-07
102.745	0.348639	2.05E-07
102.845	0.338655	1.99E-07
102.945	0.291948	1.72E-07
103.045	0.310279	1.83E-07
103.145	0.310931	1.83E-07
103.24	0.346294	2.04E-07
103.34	0.297098	1.75E-07
103.44	0.322831	1.9E-07
103.54	0.271142	1.59E-07
103.64	0.291359	1.71E-07
103.74	0.301061	1.77E-07
103.835	0.276009	1.62E-07
103.935	0.304645	1.79E-07
104.035	0.315928	1.86E-07
104.135	0.284906	1.68E-07
104.235	0.31094	1.83E-07
104.335	0.245145	1.44E-07
104.435	0.311396	1.83E-07
104.535	0.283976	1.67E-07
104.635	0.269176	1.58E-07
104.735	0.31068	1.83E-07
104.835	0.309702	1.82E-07
104.935	0.237091	1.39E-07
105.035	0.35967	2.12E-07
105.135	0.302475	1.78E-07
105.235	0.304077	1.79E-07
105.335	0.341521	2.01E-07
105.435	0.359386	2.11E-07
105.535	0.254863	1.5E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
105.635	0.28775	1.69E-07
105.735	0.286493	1.69E-07
105.835	0.276764	1.63E-07
105.935	0.252081	1.48E-07
106.035	0.305065	1.79E-07
106.135	0.289849	1.7E-07
106.235	0.300046	1.76E-07
106.335	0.249066	1.47E-07
106.435	0.281439	1.47E 07
106.53	0.325649	1.92E-07
106.63	0.297878	1.75E-07
106.73	0.294717	1.73E-07
106.83	0.296326	1.74E-07
106.93	0.352889	2.08E-07
100.93	0.301332	1.77E-07
107.03	0.282839	1.66E-07
107.225	0.328568	1.00E-07 1.93E-07
107.325	0.328508	1.93E-07 1.99E-07
107.325	0.288865	1.99E-07 1.7E-07
107.525		1.84E-07
	0.313249	
107.625	0.269484	1.59E-07
107.725	0.326019	1.92E-07
107.825	0.31987	1.88E-07
107.925	0.301906	1.78E-07
108.025 108.125	0.302064	1.78E-07
		1.85E-07
108.225	0.245934	1.45E-07
108.325	0.316004	1.86E-07
108.425	0.296674	1.75E-07
108.525	0.370838	2.18E-07
108.625	0.274153	1.61E-07
108.725	0.304768	1.79E-07
108.825	0.264173	1.55E-07
108.925	0.333153	1.96E-07
109.025	0.30662	1.8E-07
109.125	0.294532	1.73E-07
109.225	0.300116	1.77E-07
109.325	0.367778	2.16E-07
109.425	0.3184	1.87E-07
109.525	0.329602	1.94E-07
109.625	0.278399	1.64E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
109.725	0.305155	1.8E-07
109.82	0.320084	1.88E-07
109.92	0.31155	1.83E-07
110.02	0.317185	1.87E-07
110.12	0.293078	1.72E-07
110.22	0.353803	2.08E-07
110.32	0.339908	2E-07
110.42	0.303533	1.79E-07
110.515	0.363863	2.14E-07
110.615	0.253043	1.49E-07
110.715	0.360272	2.12E-07
110.815	0.316136	1.86E-07
110.915	0.333553	1.96E-07
111.015	0.380103	2.24E-07
111.115	0.330965	1.95E-07
111.215	0.350055	2.06E-07
111.315	0.324116	1.91E-07
111.415	0.370236	2.18E-07
111.515	0.313515	1.84E-07
111.615	0.334472	1.97E-07
111.715	0.343802	2.02E-07
111.815	0.340327	2E-07
111.915	0.288235	1.7E-07
112.015	0.348662	2.05E-07
112.115	0.315615	1.86E-07
112.215	0.307946	1.81E-07
112.315	0.310528	1.83E-07
112.415	0.277398	1.63E-07
112.515	0.273634	1.61E-07
112.615	0.234211	1.38E-07
112.715	0.22542	1.33E-07
112.815	0.24262	1.43E-07
112.915	0.265339	1.56E-07
113.015	0.262394	1.54E-07
113.115	0.303201	1.78E-07
113.21	0.322111	1.89E-07
113.31	0.352111	2.07E-07
113.41	0.33093	1.95E-07
113.51	0.375522	2.21E-07
113.61	0.364042	2.14E-07
113.71	0.337864	1.99E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
113.805	0.285832	1.68E-07
113.905	0.310388	1.83E-07
114.005	0.308512	1.81E-07
114.105	0.33504	1.97E-07
114.205	0.273902	1.61E-07
114.205	0.340727	2E-07
114.305	0.340727	1.98E-07
114.505	0.349145	2.05E-07
114.505	0.289101	2.03L-07 1.7E-07
114.005	0.293802	1.73E-07
114.705	0.293802	1.73E-07 1.96E-07
	0.332564	
114.905	0.288519	1.7E-07
115.005		1.75E-07
115.105	0.278611	1.64E-07
115.205	-499.377	-0.00029
115.305	0.307625	1.81E-07
115.405	0.275727	1.62E-07
115.505	0.279304	1.64E-07
115.605	0.210019	1.24E-07
115.705	0.246157	1.45E-07
115.805	0.316753	1.86E-07
115.905	0.338947	1.99E-07
116.005	0.339875	2E-07
116.105	0.339263	2E-07
116.205	0.348804	2.05E-07
116.305	0.293225	1.72E-07
116.405	0.324615	1.91E-07
116.5	0.298925	1.76E-07
116.6	0.333	1.96E-07
116.7	0.321971	1.89E-07
116.8	0.345873	2.03E-07
116.9	0.301632	1.77E-07
117	0.307366	1.81E-07
117.1	0.363556	2.14E-07
117.195	0.331594	1.95E-07
117.295	0.308223	1.81E-07
117.395	0.282558	1.66E-07
117.495	0.309405	1.82E-07
117.595	0.307975	1.81E-07
117.695	0.328454	1.93E-07
117.795	0.331745	1.95E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
117.895	0.291751	1.72E-07
117.995	0.305501	1.8E-07
118.095	0.324362	1.91E-07
118.195	0.351742	2.07E-07
118.195	0.301811	1.78E-07
118.295	0.349432	2.06E-07
118.495	0.302582	1.78E-07
118.595	0.354227	2.08E-07
118.695	0.394539	2.32E-07
118.795	0.341568	2.01E-07
118.895	0.341308	1.84E-07
118.995	0.329462	1.94L-07 1.94E-07
119.095	0.329402	1.94L-07 1.88E-07
119.095	0.319278	1.88L-07
119.195	0.311030	1.83L-07 1.88E-07
119.295	0.31928	2.07E-07
	0.344974	
119.495	0.344974	2.03E-07
119.595		1.8E-07
119.695	0.407106	2.39E-07
119.79	0.387387	2.28E-07
119.89	0.314047	1.85E-07
119.99	0.281449	1.66E-07
120.09	0.324541	1.91E-07
120.19	0.329055	1.94E-07
120.29	0.269045	1.58E-07
120.39	0.252851	1.49E-07
120.485	0.258035	1.52E-07
120.585	0.361141	2.12E-07
120.685	0.273249	1.61E-07
120.785	0.272622	1.6E-07
120.885	0.286272	1.68E-07
120.985	0.321095	1.89E-07
121.085	0.315024	1.85E-07
121.185	0.304502	1.79E-07
121.285	0.305612	1.8E-07
121.385	0.334845	1.97E-07
121.485	0.334691	1.97E-07
121.585	0.346591	2.04E-07
121.685	0.328583	1.93E-07
121.785	0.326508	1.92E-07
121.885	0.301409	1.77E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
121.985	0.337221	1.98E-07
122.085	0.272462	1.6E-07
122.185	0.328341	1.93E-07
122.285	0.349424	2.06E-07
122.385	0.340578	2E-07
122.485	0.389791	2.29E-07
122.585	0.35067	2.06E-07
122.685	0.297617	1.75E-07
122.785	0.336525	1.98E-07
122.885	0.344514	2.03E-07
122.985	0.293891	1.73E-07
123.085	0.345745	2.03E-07
123.18	0.326885	1.92E-07
123.28	0.328602	1.93E-07
123.38	0.343966	2.02E-07
123.48	0.393469	2.31E-07
123.58	0.340202	2E-07
123.68	0.347292	2.04E-07
123.775	0.354556	2.09E-07
123.875	0.380064	2.24E-07
123.975	0.380754	2.24E-07
124.075	0.470518	2.77E-07
124.175	0.386466	2.27E-07
124.275	0.437467	2.57E-07
124.375	0.433951	2.55E-07
124.475	0.453099	2.67E-07
124.575	0.430176	2.53E-07
124.675	0.360398	2.12E-07
124.775	0.36439	2.14E-07
124.875	0.398777	2.35E-07
124.975	0.377624	2.22E-07
125.075	0.332181	1.95E-07
125.175	0.403999	2.38E-07
125.275	0.367013	2.16E-07
125.375	0.381829	2.25E-07
125.475	0.366903	2.16E-07
125.575	0.39419	2.32E-07
125.675	0.359966	2.12E-07
125.775	0.367494	2.16E-07
125.875	0.353646	2.08E-07
125.975	0.350013	2.06E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
126.075	0.406193	2.39E-07
126.175	0.413652	2.43E-07
126.275	0.471322	2.77E-07
126.375	0.411116	2.42E-07
126.47	0.391354	2.3E-07
126.57	0.483967	2.85E-07
126.67	0.444288	2.61E-07
126.77	0.429173	2.52E-07
126.87	0.461874	2.72E-07
126.97	0.408713	2.4E-07
127.07	0.423453	2.49E-07
127.165	0.438433	2.58E-07
127.265	0.414233	2.44E-07
127.365	0.393096	2.31E-07
127.465	0.327476	1.93E-07
127.565	0.412627	2.43E-07
127.665	0.363737	2.14E-07
127.765	0.358951	2.11E-07
127.865	-499.3	-0.00029
127.965	0.416739	2.45E-07
128.065	0.370744	2.18E-07
128.165	0.373923	2.2E-07
128.265	0.437777	2.58E-07
128.365	0.362388	2.13E-07
128.465	0.369871	2.18E-07
128.565	0.388894	2.29E-07
128.665	0.385351	2.27E-07
128.765	0.389706	2.29E-07
128.865	0.351481	2.07E-07
128.965	0.362858	2.13E-07
129.065	0.345268	2.03E-07
129.165	0.415987	2.45E-07
129.265	0.378994	2.23E-07
129.365	0.387535	2.28E-07
129.465	0.434017	2.55E-07
129.565	0.422646	2.49E-07
129.665	0.408365	2.4E-07
129.76	0.407386	2.4E-07
129.86	0.411818	2.42E-07
129.96	0.391257	2.3E-07
130.06	0.372737	2.19E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
130.16	0.381495	2.24E-07
130.26	0.32429	1.91E-07
130.36	0.371584	2.19E-07
130.455	0.374748	2.2E-07
130.555	0.354969	2.09E-07
130.655	0.350544	2.06E-07
130.755	0.341564	2.01E-07
130.855	0.348428	2.05E-07
130.955	0.375096	2.21E-07
131.055	0.337162	1.98E-07
131.155	0.392228	2.31E-07
131.255	0.350435	2.06E-07
131.355	0.358496	2.11E-07
131.455	0.399305	2.35E-07
131.555	0.408295	2.4E-07
131.655	0.347643	2.04E-07
131.755	0.339785	2E-07
131.855	0.394764	2.32E-07
131.955	0.36722	2.16E-07
132.055	0.397178	2.34E-07
132.155	0.359392	2.11E-07
132.255	0.388646	2.29E-07
132.355	0.369505	2.17E-07
132.455	0.409344	2.41E-07
132.555	0.413114	2.43E-07
132.655	0.3868	2.28E-07
132.755	0.352656	2.07E-07
132.855	0.337367	1.98E-07
132.955	0.37962	2.23E-07
133.055	0.373604	2.2E-07
133.15	0.290965	
133.25	0.337894	
133.35	0.362131	2.13E-07
133.45	0.316057	1.86E-07
133.55	0.30641	1.8E-07
133.65	0.323178	1.9E-07
133.745	-499.334	
133.845	0.299512	1.76E-07
133.945	0.267448	1.57E-07
134.045	0.309325	
134.145	0.393627	2.32E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
134.245	0.336544	1.98E-07
134.345	0.400723	2.36E-07
134.445	0.416286	2.36E 07
134.545	0.408376	2.4E-07
134.645	0.405543	2.39E-07
134.745	0.366202	2.15E-07
134.845	0.410824	2.13E 07 2.42E-07
134.945	0.381677	2.42E 07 2.25E-07
135.045	0.4116	2.23E 07 2.42E-07
135.145	0.348924	2.42L-07 2.05E-07
135.245	0.348924	1.89E-07
135.345	0.321813	1.78F-07
135.345	0.328303	1.93E-07
135.445	0.328303	2.08E-07
135.645	0.360537	2.08E-07 2.12E-07
		-
135.745	0.370393	2.18E-07
135.845	0.283626	1.67E-07
135.945	0.344627	2.03E-07
136.045	0.366277	2.15E-07
136.145	0.37656	2.22E-07
136.245	0.421838	2.48E-07
136.345	0.385732	2.27E-07
136.44	0.378714	2.23E-07
136.54	0.398099	2.34E-07
136.64	0.381395	2.24E-07
136.74	0.377	2.22E-07
136.84	0.384099	2.26E-07
136.94	0.389276	2.29E-07
137.04	0.421351	2.48E-07
137.135	0.407003	2.39E-07
137.235	0.390936	2.3E-07
137.335	0.3829	2.25E-07
137.435	0.405308	2.38E-07
137.535	0.385453	2.27E-07
137.635	0.386152	2.27E-07
137.735	0.409121	2.41E-07
137.835	0.407234	2.4E-07
137.935	0.404184	2.38E-07
138.035	0.448291	2.64E-07
138.135	0.384614	2.26E-07
138.235	0.348049	2.05E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
138.335	0.343082	2.02E-07
138.435	0.362741	2.02E 07 2.13E-07
138.535	0.34686	2.13E 07 2.04E-07
138.635	0.369035	2.04L 07 2.17E-07
138.735	0.366656	2.17L-07 2.16E-07
138.835	0.412118	2.10L-07 2.42E-07
138.935	0.323523	2.42L-07 1.9E-07
139.035	0.402233	2.37E-07
139.035	0.402233	2.37L-07 2.39E-07
139.135	0.364979	2.39E-07 2.15E-07
139.235	0.304979	2.15E-07 2.31E-07
	0.392138	
139.435		2.22E-07
139.535	0.382999	2.25E-07
139.635	0.417356	2.46E-07
139.735	0.415804	2.45E-07
139.83	0.423179	2.49E-07
139.93	0.400829	2.36E-07
140.03	0.379439	2.23E-07
140.13	0.434481	2.56E-07
140.23	0.407184	2.4E-07
140.33	0.48763	2.87E-07
140.425	0.410255	2.41E-07
140.525	0.430185	2.53E-07
140.625	0.424691	2.5E-07
140.725	0.460063	2.71E-07
140.825	0.431786	2.54E-07
140.925	0.425723	2.5E-07
141.025	0.408512	2.4E-07
141.125	0.3944	2.32E-07
141.225	0.402405	2.37E-07
141.325	0.401285	2.36E-07
141.425	0.397714	2.34E-07
141.525	0.415374	2.44E-07
141.625	0.392473	2.31E-07
141.725	0.430576	2.53E-07
141.825	0.432447	2.54E-07
141.925	0.424541	2.5E-07
142.025	0.415522	2.44E-07
142.125	0.432785	2.55E-07
142.225	0.423331	2.49E-07
142.325	0.450761	2.65E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
142.425	0.445793	2.62E-07
142.525	0.415752	2.45E-07
142.625	0.384252	2.26E-07
142.725	0.452163	2.66E-07
142.825	0.449667	2.65E-07
142.925	0.463165	2.72E-07
143.025	0.472348	2.72E 07 2.78E-07
143.12	0.44892	2.64E-07
143.22	0.416258	2.45E-07
143.32	0.50097	2.95E-07
143.42	0.410656	2.33E 07 2.42E-07
143.52	0.430391	2.53E-07
143.62	0.404329	2.38E-07
143.715	0.368427	2.17E-07
143.815	0.355138	2.09E-07
143.915	0.344335	2.03E-07
144.015	0.320244	1.88E-07
144.115	0.301484	1.77E-07
144.215	0.257188	1.51E-07
144.315	0.294032	1.73E-07
144.415	0.212717	1.25E-07
144.515	0.256875	1.51E-07
144.615	0.290322	1.71E-07
144.715	0.276815	1.63E-07
144.815	0.343131	2.02E-07
144.915	0.296046	1.74E-07
145.015	0.351385	2.07E-07
145.115	0.382893	2.25E-07
145.215	0.388206	2.28E-07
145.315	0.467565	2.75E-07
145.415	0.450562	2.65E-07
145.515	0.401603	2.36E-07
145.615	0.417844	
145.715	0.442571	2.6E-07
145.815	0.371499	2.19E-07
145.915	0.400954	2.36E-07
146.015		
146.115	0.342509	
146.215		1.92E-07
146.315		
146.41		



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
146.51	0.271575	1.6E-07
146.61	0.295308	1.74E-07
146.71	0.349477	2.06E-07
146.81	0.284736	1.67E-07
146.91	0.24579	1.45E-07
147.01	0.268312	1.58E-07
147.105	0.303424	1.78E-07
147.205	0.317658	1.87E-07
147.305	0.250608	1.47E-07
147.405	0.317739	1.87E-07
147.505	0.273077	1.61E-07
147.605	0.23995	1.41E-07
147.705	0.252767	1.49E-07
147.805	0.313632	1.84E-07
147.905	0.337536	1.99E-07
148.005	0.307328	1.81E-07
148.105	0.299174	1.76E-07
148.205	0.318248	1.87E-07
148.305	0.322361	1.9E-07
148.405	0.352809	2.08E-07
148.505	0.326699	1.92E-07
148.605	0.437093	2.57E-07
148.705	0.5216	3.07E-07
148.805	-499.174	-0.00029
148.905	0.560386	3.3E-07
149.005	0.584708	3.44E-07
149.105	0.642153	3.78E-07
149.205	0.634393	3.73E-07
149.305	0.682707	4.02E-07
149.405	0.696599	4.1E-07
149.505	0.635418	3.74E-07
149.605	0.589906	3.47E-07
149.705	0.620046	3.65E-07
149.8	0.515826	3.03E-07
149.9	0.552915	3.25E-07
150	0.513105	3.02E-07
150.1	0.500958	2.95E-07
150.2	0.524597	3.09E-07
150.3	0.479885	2.82E-07
150.395	0.422907	2.49E-07
150.495	0.447615	2.63E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
150.595	0.393054	2.31E-07
150.695	0.408915	2.31L-07 2.41E-07
150.795	0.420471	2.41E 07 2.47E-07
150.895	0.409538	2.47E-07 2.41E-07
150.895	0.450093	2.41L-07 2.65E-07
151.095	0.419443	2.03L-07 2.47E-07
151.195	0.414699	2.47E-07 2.44E-07
151.295	0.369285	2.17E-07
151.395	0.415145	2.17E 07 2.44E-07
151.495	-499.305	-0.00029
151.495	-499.305	-0.00029
151.695	0.384188	2.26E-07
151.795	0.384188	2.20L-07 2.42E-07
151.795	0.411870	2.42L-07 2.46E-07
151.895	0.354082	2.40L-07 2.08E-07
151.995	0.336522	1.98E-07
152.095	0.293563	1.98E-07 1.73E-07
152.295	0.410364	2.41E-07
152.395 152.495	0.328453 0.311552	1.93E-07
		1.83E-07
152.595	0.312556	1.84E-07
152.695	0.321598	1.89E-07
152.795	0.320392	1.88E-07
152.895	0.318359	1.87E-07
152.995	0.306642	1.8E-07
153.09	0.319973	1.88E-07
153.19	0.277209	1.63E-07
153.29	0.289574	1.7E-07
153.39	0.270385	1.59E-07
153.49	0.326554	1.92E-07
153.59	0.302172	1.78E-07
153.685	0.357008	2.1E-07
153.785	0.391018	2.3E-07
153.885	0.430463	2.53E-07
153.985	0.398925	2.35E-07
154.085	0.352526	2.07E-07
154.185	0.353987	2.08E-07
154.285	0.370316	2.18E-07
154.385	0.324117	1.91E-07
154.485	0.324493	1.91E-07
154.585	0.319929	1.88E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
154.685	0.354378	2.08E-07
154.785	0.316184	1.86E-07
154.885	0.33583	1.98E-07
154.985	0.301831	1.78E-07
155.085	0.340815	2E-07
155.185	0.404168	2L-07 2.38E-07
155.285	0.410924	2.38L-07 2.42E-07
155.385	0.454476	2.42L 07 2.67E-07
155.485	0.47175	2.78E-07
155.585	0.457997	2.69E-07
155.685	0.528588	2.09L-07 3.11E-07
155.785	0.550022	3.24E-07
155.885	0.567023	3.24L-07 3.34E-07
155.985	0.506218	2.98E-07
156.085	0.523177	2.98L-07 3.08E-07
156.185	0.525177	3.08E-07 3.05E-07
	0.31908	2.74E-07
156.285		
156.38	0.444142	2.61E-07
156.48	0.402206	2.37E-07
156.58	0.416249	2.45E-07
156.68	-499.386	-0.00029
156.78	0.307585	1.81E-07
156.88	0.239442	1.41E-07
156.98	0.296761	1.75E-07
157.075	0.278938	1.64E-07
157.175	0.254853	1.5E-07
157.275	0.226118	1.33E-07
157.375	0.291951	1.72E-07
157.475	-499.369	-0.00029
157.575	0.289621	1.7E-07
157.675	0.31094	1.83E-07
157.775	0.227888	1.34E-07
157.875	0.307046	1.81E-07
157.975	0.285732	1.68E-07
158.075	0.321239	1.89E-07
158.175	0.279214	1.64E-07
158.275	0.332734	1.96E-07
158.375	0.287036	1.69E-07
158.475	0.307287	1.81E-07
158.575	0.298631	1.76E-07
158.675	0.270235	1.59E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
158.775	0.284152	1.67E-07
158.875	0.310206	1.82E-07
158.975	0.267053	1.57E-07
159.075	0.249386	1.47E-07
159.175	0.239946	1.41E-07
159.275	0.258896	1.52E-07
159.375	0.243177	1.32E 07 1.43E-07
159.475	0.321203	1.49E-07
159.575	0.289692	1.7E-07
159.675	0.328349	1.93E-07
159.075	0.326349	1.93L-07 1.8E-07
159.77	0.285146	1.68E-07
	0.397013	2.34E-07
159.97 160.07		
160.07	0.328166 0.345778	1.93E-07 2.03E-07
160.27	0.322807	1.9E-07
160.365	0.327378	1.93E-07
160.465	0.297371	1.75E-07
160.565	0.267075	1.57E-07
160.665	0.297871	1.75E-07
160.765	0.290377	1.71E-07
160.865	0.313297	1.84E-07
160.965	0.264508	1.56E-07
161.065	0.251506	1.48E-07
161.165	0.290237	1.71E-07
161.265	0.289829	1.7E-07
161.365	0.331899	1.95E-07
161.465	0.318905	1.88E-07
161.565	0.289327	1.7E-07
161.665	0.297447	1.75E-07
161.765	0.327439	1.93E-07
161.865	0.363393	2.14E-07
161.965	0.326184	1.92E-07
162.065	0.321324	1.89E-07
162.165	0.34404	2.02E-07
162.265	0.378694	2.23E-07
162.365	0.360555	2.12E-07
162.465	0.331106	1.95E-07
162.565	0.319738	1.88E-07
162.665	0.282718	1.66E-07
162.765	0.283752	1.67E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
162.865	0.313191	1.84E-07
162.965	0.285993	1.68E-07
163.06	0.254772	1.5E-07
163.16	0.292126	1.72E-07
163.26	0.240691	1.42E-07
163.36	0.232379	1.37E-07
163.46	0.299246	1.76E-07
163.56	0.22578	1.33E-07
163.655	0.28437	1.67E-07
163.755	0.228372	1.34E-07
163.855	0.249512	1.47E-07
163.955	0.259389	1.53E-07
164.055	0.277922	1.63E-07
164.155	0.272779	1.6E-07
164.255	0.384993	2.26E-07
164.355	0.364208	2.14E-07
164.455	0.353037	2.08E-07
164.555	0.319216	1.88E-07
164.655	0.391346	2.3E-07
164.755	0.430978	2.54E-07
164.855	0.461884	2.72E-07
164.955	0.548894	3.23E-07
165.055	0.534855	3.15E-07
165.155	0.534284	3.14E-07
165.255	0.540587	3.18E-07
165.355	0.589182	3.47E-07
165.455	0.737611	4.34E-07
165.555	0.838933	4.93E-07
165.655	0.773635	4.55E-07
165.755	0.705218	4.15E-07
165.855	0.688216	4.05E-07
165.955	0.709301	4.17E-07
166.055	0.798363	4.7E-07
166.155	0.821935	4.83E-07
166.255	0.665809	3.92E-07
166.35	0.601414	3.54E-07
166.45	0.672024	3.95E-07
166.55	0.653572	3.84E-07
166.65	0.80357	4.73E-07
166.75	0.686177	
166.85	0.644766	3.79E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
166.95	0.594318	3.5E-07
167.045	0.546836	3.22E-07
167.145	0.543532	3.2E-07
167.245	0.533628	3.14E-07
167.345	0.51367	3.02E-07
167.445	0.463085	2.72E-07
167.545	0.475401	2.8E-07
167.645	0.467458	2.75E-07
167.745	0.474465	2.79E-07
167.845	0.398686	2.35E-07
167.945	0.47918	2.82E-07
168.045	0.479456	2.82E-07
168.145	0.522257	3.07E-07
168.245	0.490385	2.88E-07
168.345	0.566856	3.33E-07
168.445	0.550832	3.24E-07
168.545	0.568493	3.34E-07
168.645	0.531134	3.12E-07
168.745	0.575909	3.39E-07
168.845	0.592006	3.48E-07
168.945	0.55871	3.29E-07
169.045	0.526768	3.1E-07
169.145	0.523237	3.08E-07
169.245	0.553358	3.26E-07
169.345	0.523582	3.08E-07
169.445	0.465129	2.74E-07
169.545	0.447407	2.63E-07
169.64	0.410223	2.41E-07
169.74	0.507272	2.98E-07
169.84	0.470121	2.77E-07
169.94	0.42959	2.53E-07
170.04	0.427188	2.51E-07
170.14	0.429961	2.53E-07
170.24	0.427728	2.52E-07
170.335	0.449581	2.64E-07
170.435	0.472162	2.78E-07
170.535	0.680597	4E-07
170.635	0.715101	4.21E-07
170.735	0.814996	4.79E-07
170.835	0.827937	4.87E-07
170.935	0.855229	5.03E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
171.035	0.95775	5.63E-07
171.135	1.05698	6.22E-07
171.235	0.974072	5.73E-07
171.335	0.857685	5.05E-07
171.435	0.774335	4.55E-07
171.535	0.788684	4.64E-07
171.635	0.731533	4.3E-07
171.735	0.762005	4.48E-07
171.835	0.641957	3.78E-07
171.935	0.581375	3.42E-07
172.035	0.598937	3.52E-07
172.135	0.68575	4.03E-07
172.235	0.68342	4.02E-07
172.335	0.742977	4.37E-07
172.335	0.629023	4.57E-07
172.535	0.609966	3.59E-07
172.535	0.576584	3.39E-07 3.39E-07
172.035	0.581283	3.42E-07
172.835	0.498621	2.93E-07
172.835	-499.33	-0.00029
172.955	0.409573	-0.00029 2.41E-07
173.03	0.409973	2.41E-07 2.41E-07
173.13	0.409907	2.41E-07 2.53E-07
173.23	0.430070	2.33E-07 2.81E-07
173.43	0.478303	2.81E-07 2.6E-07
173.43	0.442577	2.6E-07 2.66E-07
173.63	0.452555	
173.725	0.592488	3.49E-07
173.725	0.606647	3.57E-07 4.14E-07
173.925	0.726773	4.14E-07 4.28F-07
174.025 174.125	0.680825	4E-07
-	0.762029	4.48E-07
174.225	0.797775	4.69E-07
174.325 174.425	0.734023	4.32E-07
	0.770725	4.53E-07
174.525	0.747142	4.39E-07
174.625	0.711265	4.18E-07
174.725	0.665588	3.92E-07
174.825	0.678453	3.99E-07
174.925	0.681018	4.01E-07
175.025	0.781957	4.6E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
175.125	0.756792	4.45E-07
175.225	0.680906	4.01E-07
175.325	0.753573	4.43E-07
175.425	0.816214	4.8E-07
175.525	0.744172	4.38E-07
175.625	0.719293	4.38L-07 4.23E-07
175.725	0.723397	4.23E-07 4.26E-07
175.825	0.722781	4.25E-07
175.925	0.698319	4.11E-07
176.025	0.681401	4.01E-07
176.125	0.714589	4.2E-07
176.225	0.675572	3.97E-07
176.32	0.677521	3.99E-07
176.42	0.773407	4.55E-07
176.52	0.674816	3.97E-07
176.62	0.738852	4.35E-07
176.72	0.734789	4.32E-07
176.82	0.752729	4.43E-07
176.92	0.856173	5.04E-07
177.015	0.888081	5.22E-07
177.115	0.86398	5.08E-07
177.215	0.889855	5.23E-07
177.315	0.875356	5.15E-07
177.415	0.80137	4.71E-07
177.515	0.779688	4.59E-07
177.615	0.80994	4.76E-07
177.715	0.664979	3.91E-07
177.815	0.712253	4.19E-07
177.915	0.727146	4.28E-07
178.015	0.648545	3.81E-07
178.115	0.602065	3.54E-07
178.215	0.560284	3.3E-07
178.315	0.579837	3.41E-07
178.415	0.584158	3.44E-07
178.515	0.604649	3.56E-07
178.615	0.573065	3.37E-07
178.715	0.625933	3.68E-07
178.815	0.582031	3.42E-07
178.915	0.606495	3.57E-07
179.015	0.692498	4.07E-07
179.115	0.657295	3.87E-07
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Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
179.215	0.640593	3.77E-07
179.315	0.683987	4.02E-07
179.415	0.613885	3.61E-07
179.515	0.634522	3.73E-07
179.61	0.640595	3.77E-07
179.71	0.598446	3.52E-07
179.81	0.558519	3.29E-07
179.91	0.561111	3.3E-07
180.01	0.589418	3.47E-07
180.11	0.635891	3.74E-07
180.21	0.683734	4.02E-07
180.305	0.677305	3.98E-07
180.405	0.706926	4.16E-07
180.505	0.656131	3.86E-07
180.605	0.702227	4.13E-07
180.705	0.691032	4.06E-07
180.805	0.695052	4.09E-07
180.905	0.717829	4.22E-07
181.005	0.761316	4.48E-07
181.105	0.791133	4.65E-07
181.205	0.704512	4.14E-07
181.305	0.67222	3.95E-07
181.405	0.621721	3.66E-07
181.505	0.625192	3.68E-07
181.605	0.713794	4.2E-07
181.705	0.724367	4.26E-07
181.805	0.830539	4.89E-07
181.905	0.825079	4.85E-07
182.005	0.767333	4.51E-07
182.105	0.695222	4.09E-07
182.205	0.758945	4.46E-07
182.305	0.975257	5.74E-07
182.405	1.110565	6.53E-07
182.505	0.954735	5.62E-07
182.605	0.739485	4.35E-07
182.705	0.676087	3.98E-07
182.805	0.803123	4.72E-07
182.905	0.895525	5.27E-07
183	0.879399	5.17E-07
183.1	0.781068	4.59E-07
183.2	0.799227	4.7E-07

Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
183.3	0.874175	5.14E-07
183.4	0.831548	4.89E-07
183.5	0.896169	5.27E-07
183.6	0.961736	5.66E-07
183.695	0.906541	5.33E-07
183.795	0.899839	5.29E-07
183.895	0.839126	4.94E-07
183.995	0.807505	4.75E-07
184.095	0.763589	4.49E-07
184.195	-499.225	-0.00029
184.295	0.745284	4.38E-07
184.395	0.644056	3.79E-07
184.495	0.586578	3.45E-07
184.595	0.552464	3.25E-07
184.695	0.501722	2.95E-07
184.795	0.493384	2.9E-07
184.895	0.499852	2.94E-07
184.995	0.529564	3.12E-07
185.095	0.586035	3.45E-07
185.195	0.573993	3.38E-07
185.295	0.520718	3.06E-07
185.395	0.535747	3.15E-07
185.495	0.500985	2.95E-07
185.595	0.525644	3.09E-07
185.695	0.572536	3.37E-07
185.795	0.540208	3.18E-07
185.895	0.526131	3.09E-07
185.995	0.518963	3.05E-07
186.095	0.501033	2.95E-07
186.195	0.559723	3.29E-07
186.29	0.56412	3.32E-07
186.39	0.53404	
186.49	0.503572	2.96E-07
186.59	0.519747	3.06E-07
186.69	0.553958	3.26E-07
186.79	0.803551	4.73E-07
186.89	0.928286	
186.985	0.857858	5.05E-07
187.085	0.842875	4.96E-07
187.185	0.839566	
187.285	1.046329	6.15E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
187.385	1.158695	6.82E-07
187.485	0.962139	5.66E-07
187.585	0.814797	4.79E-07
187.685	0.670671	3.95E-07
187.785	0.796213	4.68E-07
187.885	0.801058	4.08L-07 4.71E-07
187.985	0.58364	4.71L-07 3.43E-07
188.085	0.538419	3.43E 07 3.17E-07
188.185	0.431286	2.54E-07
188.285	0.464239	2.73E-07
188.385	0.430983	2.54E-07
188.485	0.4895	2.34L-07 2.88E-07
188.585	0.4893	2.88L-07 3.47E-07
188.685	0.650306	3.47L-07 3.83E-07
188.785	0.716843	4.22E-07
188.885	0.72317	4.22L-07 4.25E-07
188.985	0.688261	4.23E-07 4.05E-07
	0.703521	
189.085		4.14E-07
189.185 189.285	0.761599 0.891829	4.48E-07 5.25E-07
189.385	1.017921	5.99E-07
189.485	1.039638	6.12E-07
189.58	0.974505	5.73E-07
189.68	1.0021	5.89E-07
189.78	1.008096	5.93E-07
189.88	1.070216	6.3E-07
189.98	0.986251	5.8E-07
190.08	0.835192	4.91E-07
190.18	0.811606	4.77E-07
190.275	0.847584	4.99E-07
190.375	0.856073	5.04E-07
190.475	0.814646	4.79E-07
190.575	0.668259	3.93E-07
190.675	0.692452	4.07E-07
190.775	0.721394	4.24E-07
190.875	0.71504	4.21E-07
190.975	0.730016	4.29E-07
191.075	0.751895	4.42E-07
191.175	0.760308	4.47E-07
191.275	0.758786	4.46E-07
191.375	0.705149	4.15E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
191.475	0.684223	4.02E-07
191.575	0.671493	3.95E-07
191.675	0.606972	3.55E-07
191.775	0.5372	3.16E-07
191.875	0.580868	3.42E-07
191.975	0.602067	3.54E-07
192.075	0.677583	3.99E-07
192.175	0.685648	4.03E-07
192.275	0.755775	4.45E-07
192.375	0.746396	4.39E-07
192.475	0.783472	4.61E-07
192.575	0.887668	5.22E-07
192.675	0.872549	5.13E-07
192.775	0.803857	4.73E-07
192.875	0.788356	4.64E-07
192.97	0.803869	4.73E-07
193.07	0.730364	4.3E-07
193.17	0.644636	3.79E-07
193.27	0.618094	3.64E-07
193.37	0.560389	3.3E-07
193.47	0.561485	3.3E-07
193.47	0.715061	4.21E-07
193.665	0.707954	4.16E-07
193.765	0.666983	3.92E-07
193.865	0.73095	4.3E-07
193.965	0.705085	4.15E-07
194.065	0.665286	3.91E-07
194.165	0.745527	4.39E-07
194.265	0.682211	4.01E-07
194.365	0.660839	3.89E-07
194.465	0.628463	3.7E-07
194.565	0.596054	3.51E-07
194.665	0.546047	3.21E-07
194.765	0.454725	2.67E-07
194.865	0.501141	2.07L-07 2.95E-07
194.965	0.427693	2.52E-07
194.905	0.491836	2.89E-07
195.065	0.491830	2.89E-07 3.02E-07
195.165	0.579695	3.02E-07 3.41E-07
195.265	0.545308	3.41E-07 3.21E-07
195.365		
195.405	0.520323	3.06E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
195.565	0.592295	3.48E-07
195.665	0.616741	3.63E-07
195.765	0.622106	3.66E-07
195.865	0.667865	3.93E-07
195.965	0.597519	3.53E-07
196.065	0.523698	3.08E-07
196.165	0.540061	3.18E-07
196.26	0.532842	3.13E-07
196.36	0.550044	3.24E-07
196.46	0.524365	3.08E-07
196.56	0.566826	3.33E-07
196.66	0.654785	3.85E-07
196.76	0.63708	3.75E-07
196.86	0.580475	3.41E-07
196.955	0.602651	3.55E-07
197.055	0.690901	4.06E-07
197.155	0.761238	4.48E-07
197.255	0.773148	4.55E-07
197.355	0.692967	4.08E-07
197.455	0.620953	3.65E-07
197.555	0.603573	3.55E-07
197.655	0.566306	3.33E-07
197.755	0.489977	2.88E-07
197.855	0.492752	2.9E-07
197.955	0.459574	2.7E-07
198.055	0.388547	2.29E-07
198.155	0.287272	1.69E-07
198.255	0.358676	2.11E-07
198.355	0.33586	1.98E-07
198.455	0.350137	2.06E-07
198.555	0.462332	2.72E-07
198.655	0.514336	3.03E-07
198.755	0.516809	3.04E-07
198.855	0.50531	2.97E-07
198.955	0.498643	2.93E-07
199.055	0.43219	2.54E-07
199.155	0.618645	3.64E-07
199.255	0.731103	4.3E-07
199.355	0.753419	
199.455	0.759007	
199.55	0.654921	3.85E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
199.65	0.660961	3.89E-07
199.75	0.724408	4.26E-07
199.85	0.834201	4.91E-07
199.95	0.870937	5.12E-07
200.05	0.832355	4.9E-07
200.05	0.739491	4.35E-07
200.245	0.661784	3.89E-07
200.345	0.656561	3.86E-07
200.445	0.681786	4.01E-07
200.545	0.641195	3.77E-07
200.645	0.627736	3.69E-07
200.745	0.718276	4.23E-07
200.845	0.717097	4.22E-07
200.945	0.769756	4.53E-07
201.045	0.837796	4.93E-07
201.145	0.785704	4.62E-07
201.245	0.835949	4.92E-07
201.345	0.847627	4.99E-07
201.445	0.711571	4.19E-07
201.545	0.650178	3.82E-07
201.645	0.841109	4.95E-07
201.745	0.849189	5E-07
201.845	0.710185	4.18E-07
201.945	0.515027	3.03E-07
202.045	0.373515	2.2E-07
202.145	0.404392	2.38E-07
202.245	0.53065	3.12E-07
202.345	0.517974	3.05E-07
202.445	0.535171	3.15E-07
202.545	0.519303	3.05E-07
202.645	0.511605	3.01E-07
202.745	0.597729	3.52E-07
202.845	0.584541	3.44E-07
202.94	0.630366	3.71E-07
203.04	0.677933	3.99E-07
203.14	0.630015	3.71E-07
203.24	0.670818	3.95E-07
203.34	0.639776	3.76E-07
203.44	0.65789	3.87E-07
203.54	0.704181	4.14E-07
203.635	0.662283	3.9E-07



Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
203.735	0.602384	3.54E-07
203.835	0.632605	3.72E-07
203.935	0.55525	3.27E-07
204.035	0.57918	3.41E-07
204.135	0.566467	3.33E-07
204.235	0.545259	3.21E-07
204.335	0.542099	3.19E-07
204.435	0.493603	2.9E-07
204.535	0.503506	2.96E-07
204.635	0.437199	2.57E-07
204.735	0.470571	2.77E-07
204.835	0.574535	3.38E-07
204.935	0.602738	3.55E-07
205.035	0.538374	3.17E-07
205.135	0.484859	2.85E-07
205.235	0.508482	2.99E-07
205.335	0.691795	4.07E-07
205.435	0.925797	5.45E-07
205.535	0.821804	4.83E-07
205.635	0.660702	4.83E 07 3.89E-07
205.735	0.646072	3.8E-07
205.835	0.666778	3.92E-07
205.935	0.774633	4.56E-07
206.035	0.82916	4.88E-07
206.135	0.688431	4.05E-07
206.23	0.63468	3.73E-07
206.33	0.650728	3.83E-07
206.43	0.647698	3.81E-07
206.53	0.609481	3.59E-07
206.63	0.545088	3.21E-07
206.73	0.488253	2.87E-07
206.83	0.486697	2.87E 07
206.925	0.514895	3.03E-07
207.025	0.539394	3.17E-07
207.125	0.585237	3.44E-07
207.225	0.569072	3.35E-07
207.325	0.520675	3.06E-07
207.425	0.431846	2.54E-07
207.525	0.434065	2.55E-07
207.625	0.461511	2.71E-07
207.725	0.505719	2.97E-07
207.725	5.565715	2.372 07

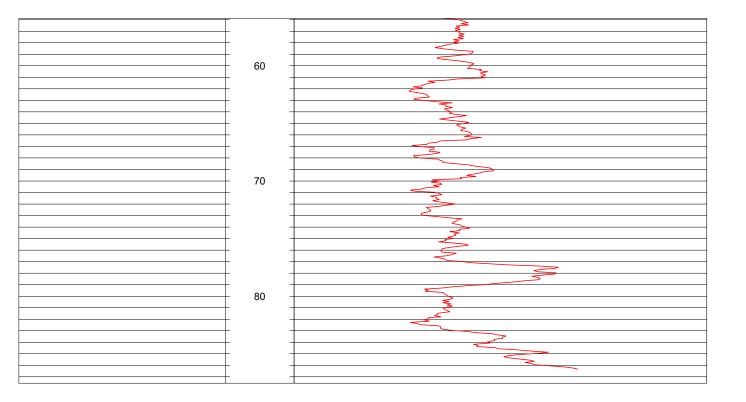


Depth	Mag Susc 10e-3 SI	Mag Susc
ft bgs	units	m3/kg
207.825	0.523851	3.08E-07
207.925	0.59776	3.52E-07
208.025	0.608457	3.58E-07
208.125	0.510087	3E-07
208.225	0.525836	3.09E-07
208.325	0.537279	3.16E-07
208.425	0.618975	3.64E-07
208.525	0.650798	3.83E-07
208.625	0.640392	3.77E-07
208.725	0.597685	3.52E-07
208.825	0.610317	3.59E-07
208.93	0.695498	4.09E-07
209.03	0.700919	4.12E-07
209.13	0.675432	3.97E-07
209.23	0.655904	3.86E-07
209.33	0.74349	4.37E-07
209.43	0.670265	3.94E-07
209.52	0.706701	4.16E-07
209.62	0.678592	3.99E-07
209.72	0.726418	4.27E-07
209.82	0.7568	4.45E-07
209.92	0.635666	3.74E-07
210.02	0.651881	3.83E-07
210.12	0.693402	4.08E-07
210.22	0.668349	3.93E-07
210.32	0.654885	3.85E-07
210.42	0.682838	4.02E-07
210.52	0.752626	4.43E-07
210.62	0.675642	3.97E-07
210.72	0.640173	3.77E-07
210.82	0.686351	4.04E-07



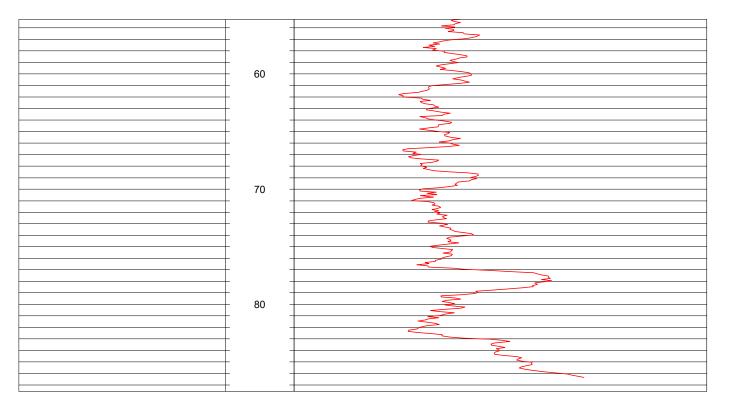
		TOOLHMA-453-SCALIBRATION DATE/TIME7/25/16CALIBRATION STANDARDS0 and 5E-3 SI UnitsCALIBRATION RESULTS0 = 230 and 5E-3 = 1326.4 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Tooele Army Ammunition Depot	
WELL	D-20 Down	
LOGGER	T.H. Wiedemeier	4" Well
DATE	7/25/16	

Depth	٦ ۱	Mag Susc
1ft:100	)ft	0 10e-3 SI units 1
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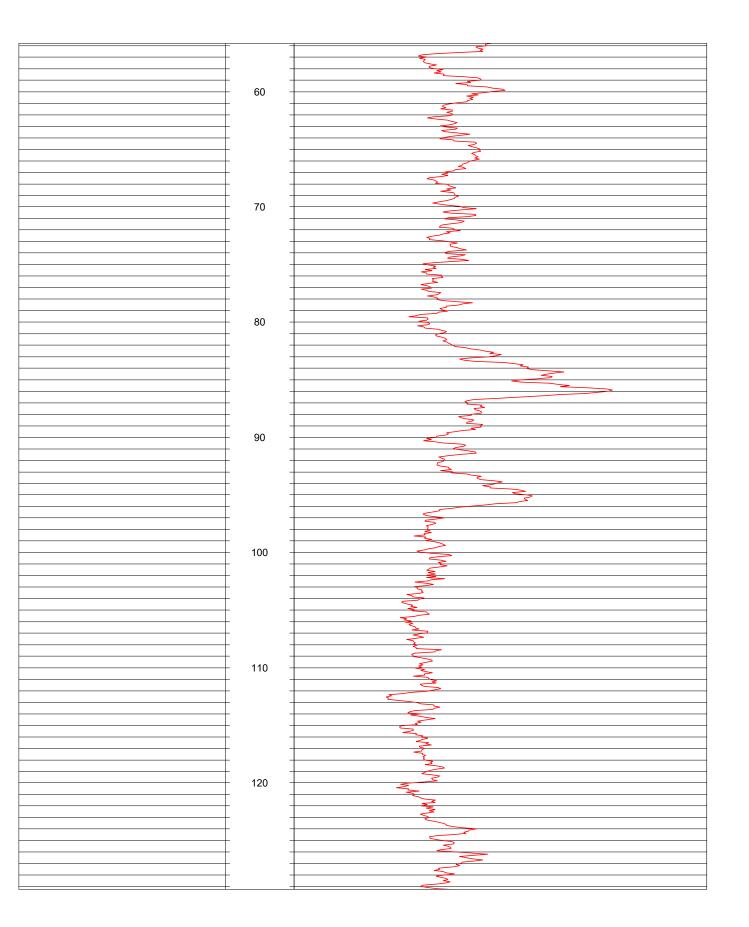
		TOOLHMA-453-SCALIBRATION DATE/TIME7/25/16CALIBRATION STANDARDS0 and 5E-3 SI UnitsCALIBRATION RESULTS0 = 230 and 5E-3 = 1326.4 cps
PROJECT	ESTCP 201584	REMARKS
LOCATION	Tooele Army Ammunition Depot	
WELL	D-20 Up	
LOGGER	T.H. Wiedemeier	4" Well
DATE	7/25/16	

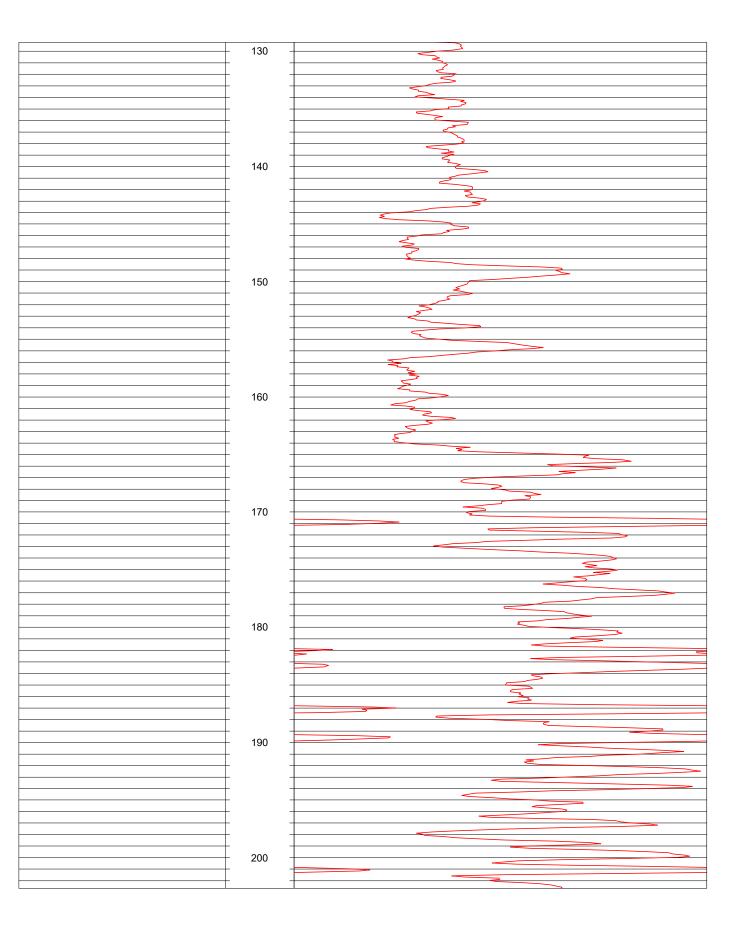
Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 1
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		TOOL HMA-453-S CALIBRATION DATE/TIME 7/25/16 - 13:20 CALIBRATION STANDARDS 0 and 5E-3 SI Units CALIBRATION RESULTS 0 = 230 and 5E-3 = 1326.4 cps
PROJECT LOCATION WELL	ESTCP 201584 Tooele Army Ammunition Depot D-23 Down	DEPTH TO WATER, TD 67.38 ft BTOC, 212 ft BGS CASING INNER DIAMETER 4" REMARKS
LOGGER DATE	T.H. Wiedemeier 7/25/16	REMARNS

Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 1
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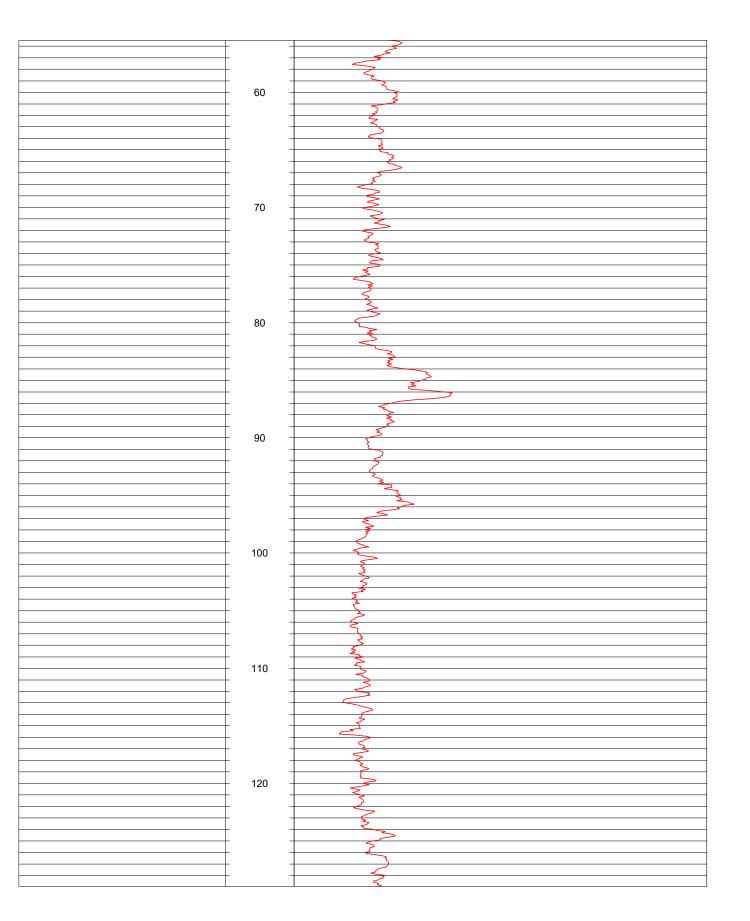




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WIEDEMEIER & ASSOCIATES		TOOL HMA-453-S CALIBRATION DATE/TIME 7/25/16 CALIBRATION STANDARDS 0 and 5E-3 SI Units CALIBRATION RESULTS 0 = 230 and 5E-3 = 1326.4 cps
PROJECT	ESTCP 201584	DEPTH TO WATER, TD 67.38 ft BTOC, 212 ft BGS
LOCATION	Tooele Army Ammunition Depot	
WELL	D-23 Up	CASING INNER DIAMETER 4"
LOGGER	T.H. Wiedemeier	REMARKS
DATE	7/25/16	

Depth	Mag Susc
 1ft:100ft	0 10e-3 SI units 2
10	
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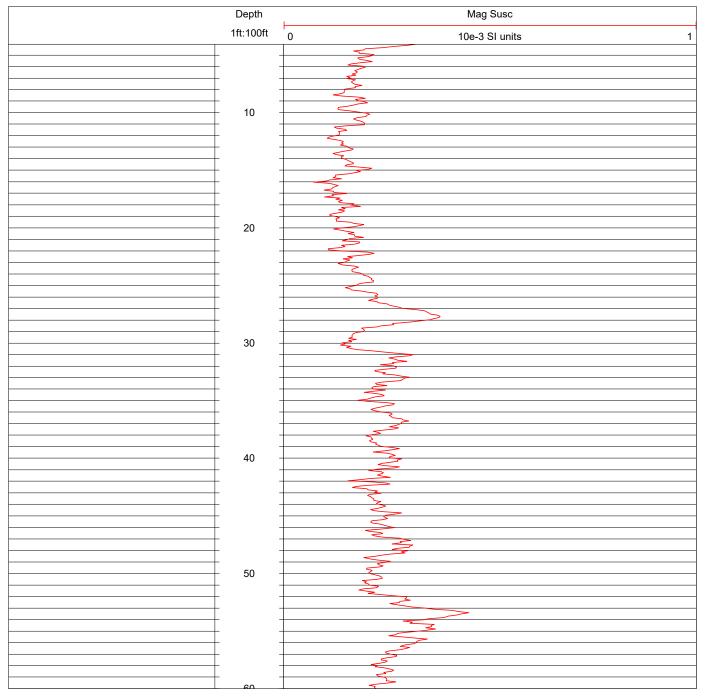


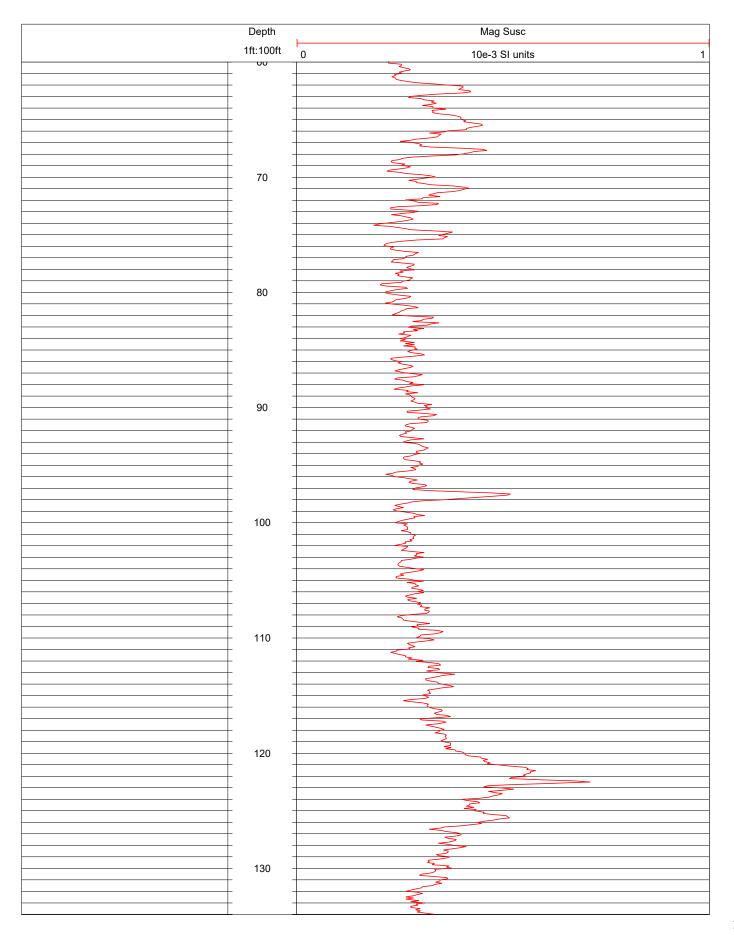
Page 2

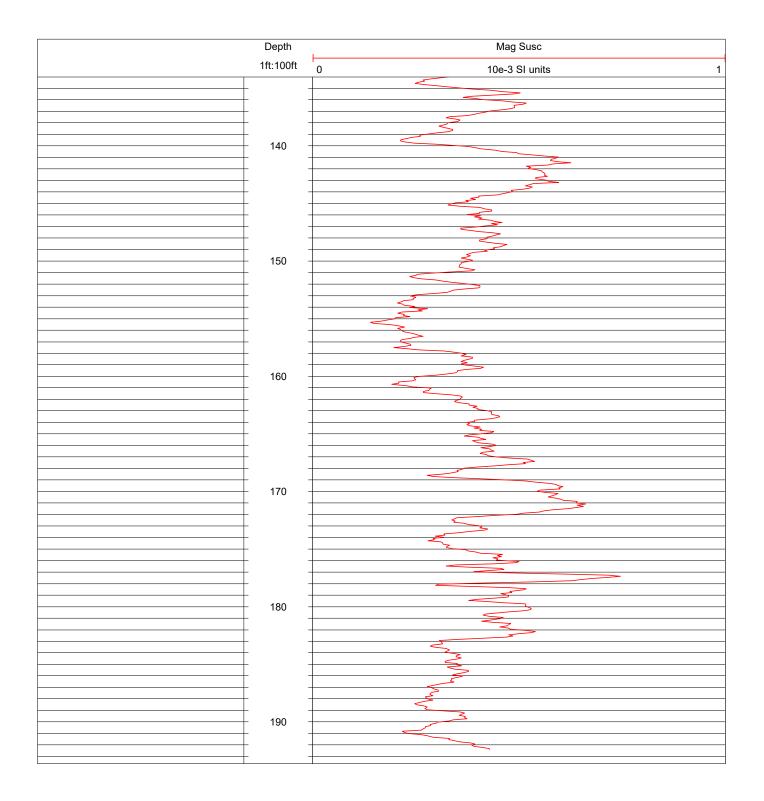


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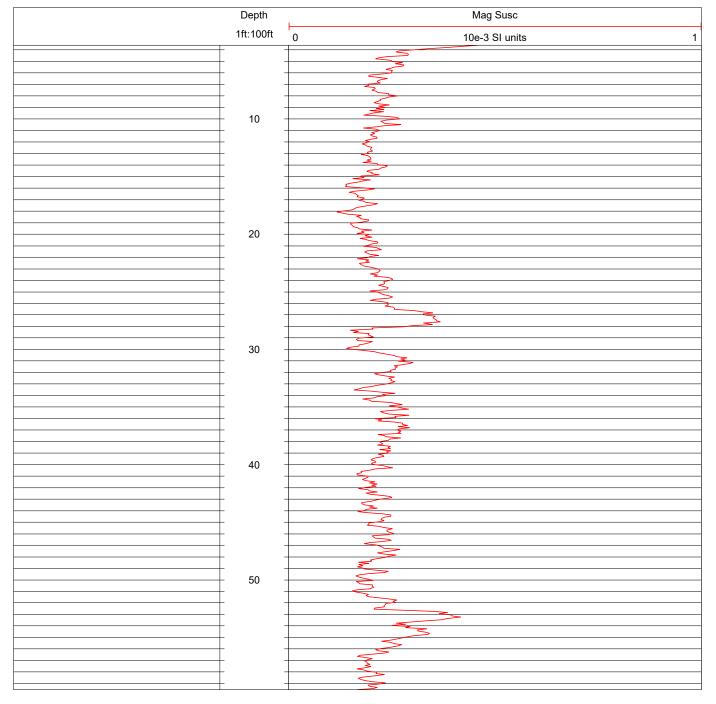
774		TOOL HMA-453-S
		CALIBRATION DATE/TIME 7/26/16 10:23
WIEDEMEIER		CALIBRATION STANDARDS 0 and 5E-3
& ASSOC	IATES	CALIBRATION RESULTS 0 = 236.4 and 5E-3 = 1433 cps
PROJECT	ESTCP 201584	DEPTH TO WATER, TD 87.42 ft BTOC, 195 ft BGS
LOCATION	Tooele Army Ammunition Depot	
WELL	D-25 Down	CASING INNER DIAMETER 4"
LOGGER	T.H. Wiedemeier	REMARKS
DATE	7/26/16	

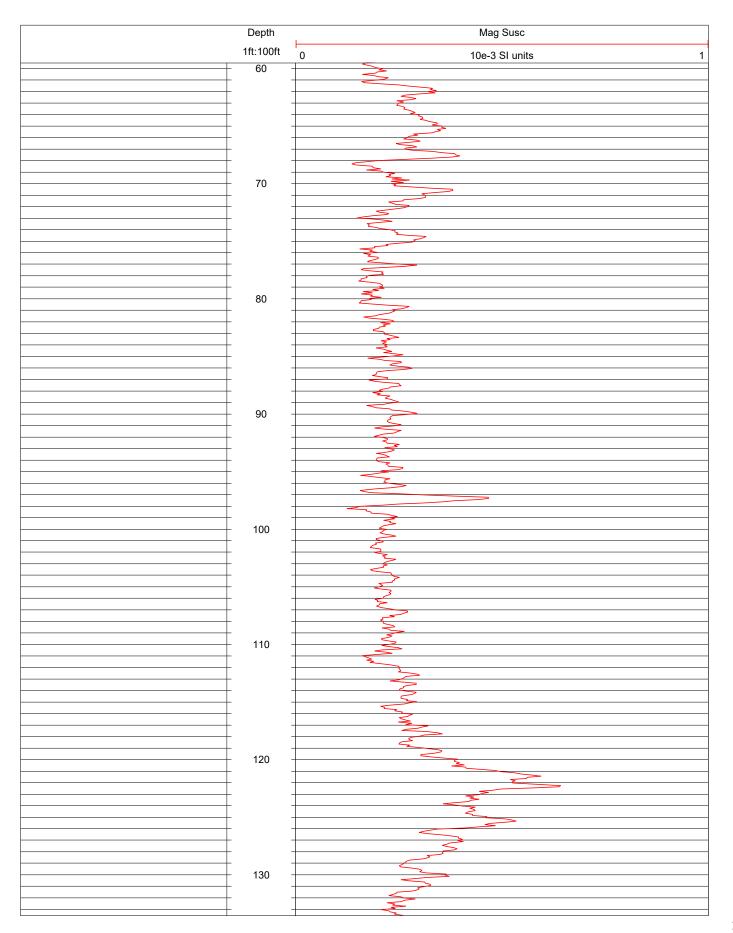


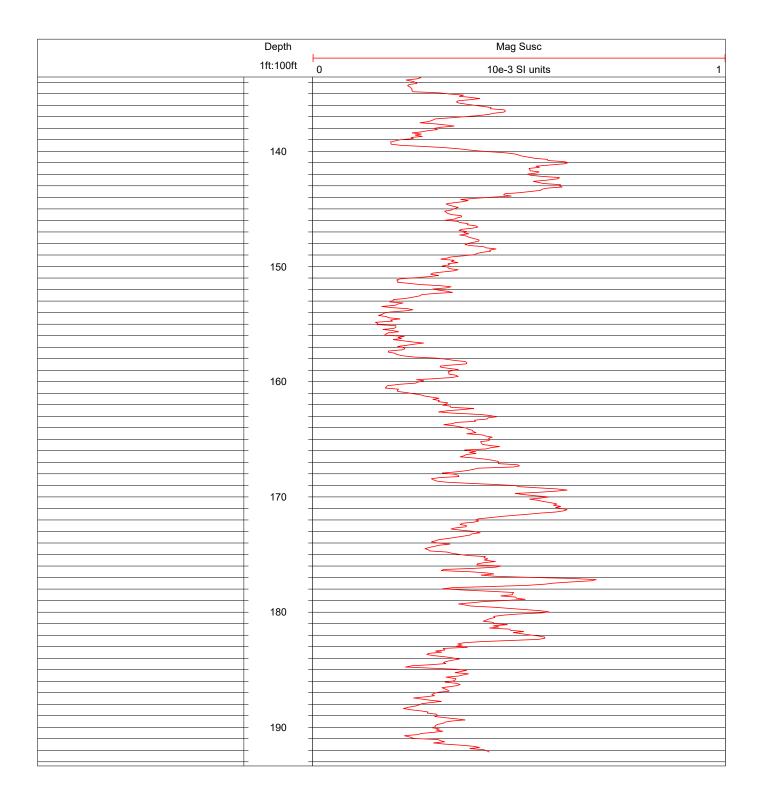




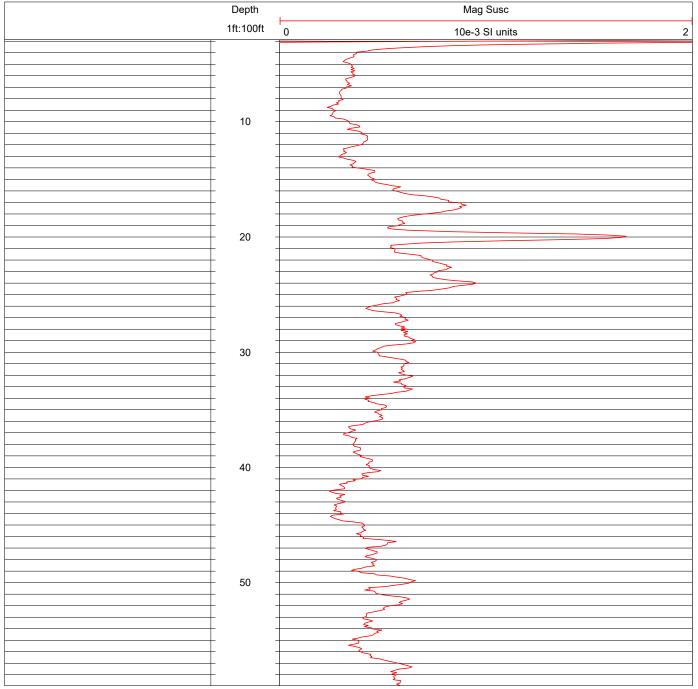
774		TOOL HMA-453-S
		CALIBRATION DATE/TIME 7/26/16 10:23
WIEDEMEIER		CALIBRATION STANDARDS 0 and 5E-3 SI Units
& ASSOC	IATES	CALIBRATION RESULTS 0 = 236.4 and 5E-3 = 1433 cps
PROJECT	ESTCP 201584	DEPTH TO WATER, TD 87.42 ft BTOC, 195 ft BGS
LOCATION	Tooele Army Ammunition Depot	
WELL	D-25 Up	CASING INNER DIAMETER 4"
LOGGER	T.H. Wiedemeier	REMARKS
DATE	7/26/16	



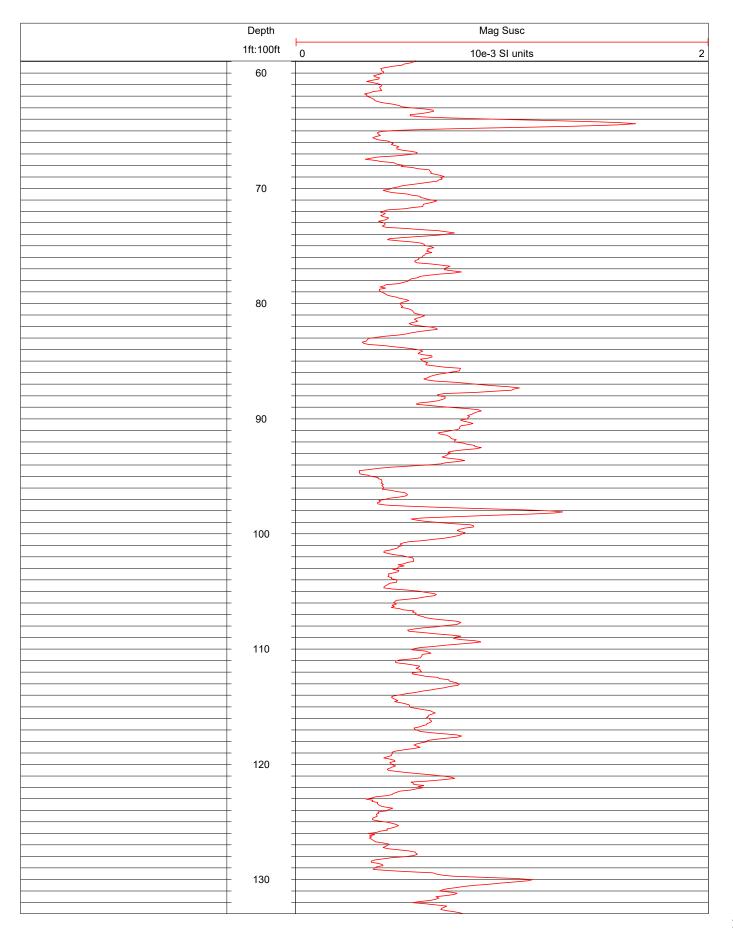


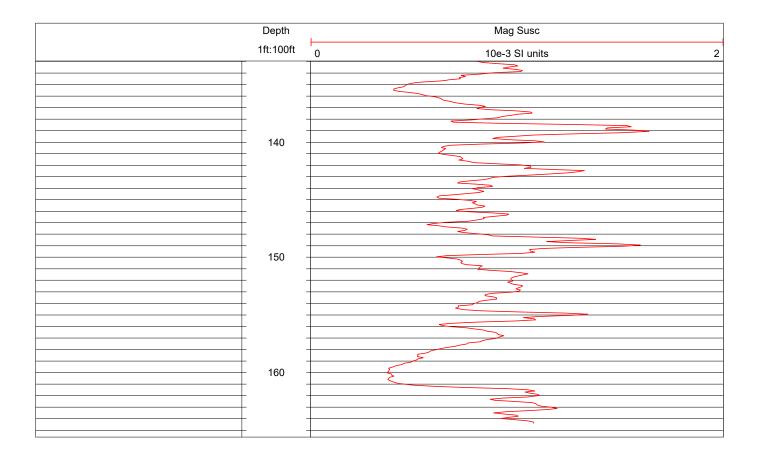


		TOOL HMA-453-S CALIBRATION DATE/TIME 7/26/16 - 14:44 CALIBRATION STANDARDS 0 and 5E-3 SI Units CALIBRATION RESULTS Did not record
PROJECT	ESTCP 201584	REMARKS
LOCATION	Tooele Army Ammunition Depot	REWARKS
WELL	D-19 Down	
LOGGER	TH Wiedemeier	4" Well
DATE	7/26/16	
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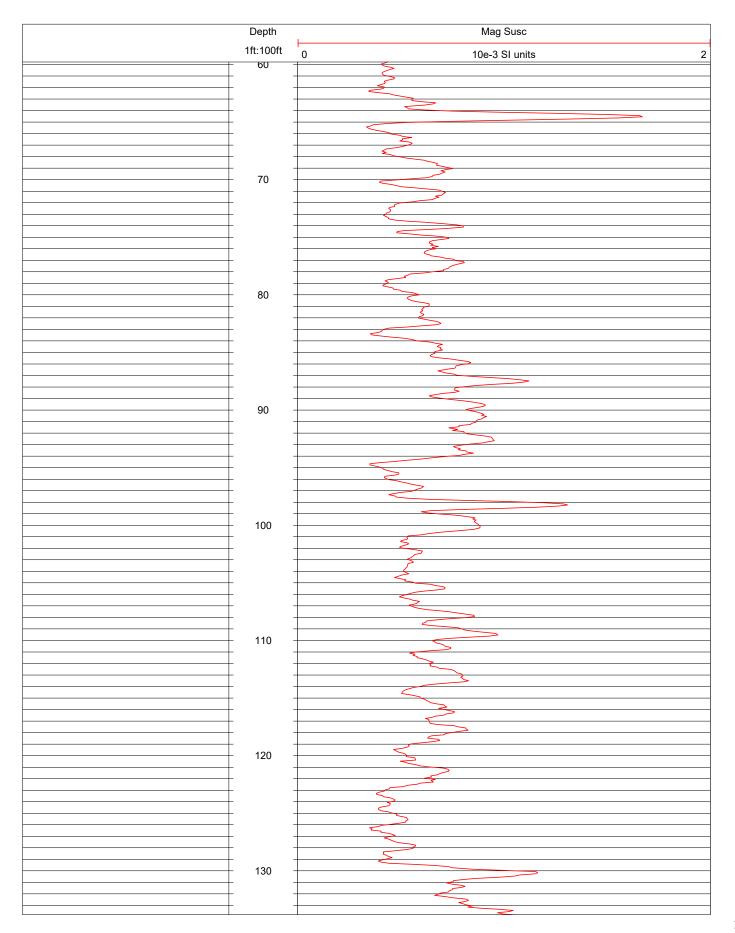
Page 1

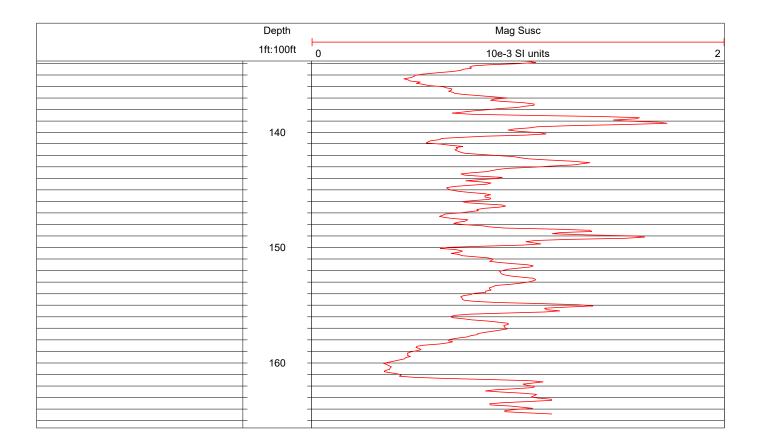




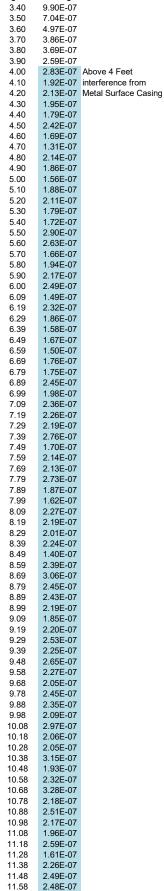
WIEDEMEIER & ASSOCIATES		TOOL HMA-453-S CALIBRATION DATE/TIME 7/26/16 - 14:44 CALIBRATION STANDARDS 0 and 5E-3 CALIBRATION RESULTS Not Recorded
PROJECT	ESTCP 201584	REMARKS
LOCATION	Tooele Army Ammunition Depot	
WELL	D-19 Up	
LOGGER	TH Wiedemeier	4" Well
DATE	7/26/16	

Depth	Mag Susc	
1ft:100ft	0 10e-3 SI units	2
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U10	)-025	U1	0-043	ı	J10-51 SON	NDE D		ID STATS
Depth	Mag Susc	Depth	Mag Susc		D	epth	Mag Susc	
ft bgs	m <sup>3</sup> /kg	ft bgs	m <sup>3</sup> /kg		ft	bgs	m <sup>3</sup> /kg	
3.60	2.19E-07	3.72	1.03E-06			3.40	9.90E-07	
3.69	2.80E-07	3.82	9.56E-07 8.58E-07			3.50	7.04E-07	
3.79 3.89	2.56E-07 2.79E-07	3.92 4.02	8.65E-07			3.60 3.70	4.97E-07 3.86E-07	
3.99	2.77E-07	4.12	7.80E-07			3.80	3.69E-07	
4.09	2.42E-07	4.22	8.17E-07			3.90	2.59E-07	
4.19 4.29	2.46E-07 2.69E-07	4.32 4.42	8.77E-07 7.65E-07			4.00 4.10		Above 4 Feet interference fro
4.29	2.09E-07 2.44E-07	4.42	6.55E-07			4.10		Metal Surface (
4.49	2.47E-07	4.62	5.24E-07			4.30	1.95E-07	
4.59	2.91E-07	4.71	4.48E-07			4.40	1.79E-07	
4.69 4.79	2.70E-07 2.49E-07	4.81 4.91	4.55E-07 3.56E-07			4.50 4.60	2.42E-07 1.69E-07	
4.89	2.84E-07	5.01	3.03E-07			4.70	1.31E-07	
4.99	2.74E-07	5.11	2.47E-07			4.80	2.14E-07	
5.09 5.19	2.36E-07 2.63E-07	5.21 5.31		Above 5.21 feet interference from		4.90 5.00	1.86E-07 1.56E-07	
5.29	2.03E-07 2.85E-07	5.41		Metal Surface Casing		5.10	1.88E-07	
5.39	2.34E-07	5.51	2.96E-07	Ŭ		5.20	2.11E-07	
5.49	2.40E-07	5.61	3.05E-07			5.30	1.79E-07	
5.59 5.69	2.35E-07 2.32E-07	5.71 5.81	3.02E-07 3.30E-07			5.40 5.50	1.72E-07 2.90E-07	
5.79	2.62E-07	5.91	3.09E-07			5.60	2.63E-07	
5.89	2.38E-07	6.01	3.46E-07			5.70	1.66E-07	
5.99	2.54E-07	6.11	2.78E-07			5.80	1.94E-07	
6.09 6.19	2.50E-07 2.51E-07	6.21 6.31	3.12E-07 2.97E-07			5.90 6.00	2.17E-07 2.49E-07	
6.29	2.48E-07	6.41	3.11E-07			6.09	1.49E-07	
6.39	2.36E-07	6.51	3.09E-07			6.19	2.32E-07	
6.49	2.36E-07	6.61	2.88E-07			6.29	1.86E-07	
6.59 6.69	3.17E-07 2.73E-07	6.71 6.81	2.72E-07 2.71E-07			6.39 6.49	1.58E-07 1.67E-07	
6.79	2.74E-07	6.91	3.13E-07			6.59	1.50E-07	
6.89	3.44E-07	7.01	2.82E-07			6.69	1.76E-07	
6.99 7.08	3.78E-07 3.39E-07	7.11 7.21	2.59E-07 2.58E-07			6.79 6.89	1.75E-07 2.45E-07	
7.18	3.46E-07	7.31	2.67E-07			6.99	1.98E-07	
7.28	2.72E-07	7.41	2.26E-07			7.09	2.36E-07	
7.38	3.10E-07	7.51	2.44E-07			7.19	2.26E-07	
7.48 7.58	3.60E-07 3.44E-07	7.61 7.71	2.24E-07 1.91E-07			7.29 7.39	2.19E-07 2.76E-07	
7.68	3.13E-07	7.81	1.92E-07			7.49	1.70E-07	
7.78	3.00E-07	7.91	2.03E-07			7.59	2.14E-07	
7.88 7.98	2.75E-07 2.56E-07	8.00 8.10	1.94E-07 1.59E-07			7.69 7.79	2.13E-07 2.73E-07	
8.08	2.81E-07	8.20	2.03E-07			7.89	1.87E-07	
8.18	2.94E-07	8.30	2.04E-07			7.99	1.62E-07	
8.28	2.44E-07 2.65E-07	8.40	2.33E-07			8.09 8.19	2.27E-07	
8.38 8.48	2.83E-07 2.82E-07	8.50 8.60	2.03E-07 2.43E-07			8.29	2.19E-07 2.01E-07	
8.58	2.93E-07	8.70	2.44E-07			8.39	2.24E-07	
8.68	2.83E-07	8.80	2.41E-07			8.49	1.40E-07	
8.78 8.88	2.79E-07 2.68E-07	8.90 9.00	2.66E-07 2.42E-07			8.59 8.69	2.39E-07 3.06E-07	
8.98	2.91E-07	9.10	2.60E-07			8.79	2.45E-07	
9.08	2.43E-07	9.20	3.25E-07			8.89	2.43E-07	
9.18 9.28	2.89E-07 2.86E-07	9.30 9.40	3.05E-07 3.01E-07			8.99 9.09	2.19E-07 1.85E-07	
9.38	3.06E-07	9.50	2.93E-07			9.19	2.20E-07	
9.48	3.20E-07	9.60	2.46E-07			9.29	2.53E-07	
9.58	2.88E-07	9.70	2.59E-07			9.39	2.25E-07	
9.68 9.78	2.54E-07 2.27E-07	9.80 9.90	2.69E-07 2.51E-07			9.48 9.58	2.65E-07 2.27E-07	
9.88	3.07E-07	10.00	2.31E-07			9.68	2.05E-07	
9.98	2.99E-07	10.10	2.11E-07			9.78	2.45E-07	
10.08 10.18	3.02E-07 2.69E-07	10.20 10.30	2.16E-07 2.03E-07			9.88 9.98	2.35E-07 2.09E-07	
10.18	2.09L-07 2.78E-07	10.30	2.03L-07 2.21E-07			10.08	2.03L-07 2.97E-07	
10.37	2.77E-07	10.50	2.15E-07			10.18	2.06E-07	
10.47	2.79E-07	10.60	2.11E-07			10.28	2.05E-07	
10.57 10.67	3.04E-07 3.09E-07	10.70 10.80	2.31E-07 2.00E-07			10.38 10.48	3.15E-07 1.93E-07	
10.77	2.81E-07	10.90	2.43E-07			10.58	2.32E-07	
10.87	2.83E-07	11.00	2.35E-07			10.68	3.28E-07	
10.97 11.07	3.13E-07 3.31E-07	11.10 11.20	2.00E-07 2.35E-07			10.78 10.88	2.18E-07 2.51E-07	
11.07	3.31E-07 3.12E-07	11.20	2.35E-07 2.28E-07			10.88	2.51E-07 2.17E-07	
11.27	3.21E-07	11.39	2.37E-07			11.08	1.96E-07	
11.37	3.29E-07	11.49	2.56E-07			11.18	2.59E-07	
11.47 11.57	3.64E-07 2.85E-07	11.59 11.69	2.43E-07 2.04E-07			11.28 11.38	1.61E-07 2.26E-07	
11.67	2.66E-07	11.79	2.45E-07			11.48	2.49E-07	
11.77	2.98E-07	11.89	2.20E-07			11.58	2.48E-07	
11.87	3.20E-07	11.99	2.11E-07	l		11.68	1.94E-07	





#### MASS MA I THE SONDE FOR HILL AFB-OU10, HILL AFB, UTAH

AGNETIC SUSCEPTIBILITY DATA FROM TH				
U10-025		U10	-043	
Depth	Mag Susc	Depth	Mag Susc	
ft bgs	m³/kg	ft bgs	m³/kg	
11.97	3.38E-07	12.09	2.35E-07	
12.07	3.79E-07	12.19	2.50E-07	
12.17	3.31E-07	12.29	2.69E-07	
12.27	3.68E-07	12.39	2.81E-07	
12.37	3.70E-07	12.49	2.85E-07	
12.47	3.51E-07	12.59	2.79E-07	
12.57	4.04E-07	12.69	2.87E-07	
12.67	4.14E-07	12.79	2.34E-07	
12.77	4.18E-07	12.89	2.64E-07	
12.87	4.04E-07	12.99	2.81E-07	
12.97	4.64E-07	13.09	2.90E-07	
13.07 13.17	4.28E-07 4.50E-07	13.19 13.29	2.73E-07 2.84E-07	
13.17	4.67E-07	13.39	2.55E-07	
13.37	4.49E-07	13.49	2.40E-07	
13.47	5.38E-07	13.59	2.40L-07 2.52E-07	
13.57	5.77E-07	13.69	2.58E-07	
13.66	5.78E-07	13.79	2.36E-07	
13.76	4.74E-07	13.89	2.51E-07	
13.86	4.82E-07	13.99	2.59E-07	
13.96	4.90E-07	14.09	2.38E-07	
14.06	5.03E-07	14.19	2.30E-07	
14.16	5.01E-07	14.29	2.47E-07	
14.26	3.98E-07	14.39	2.41E-07	
14.36	3.65E-07	14.49	2.62E-07	
14.46	3.38E-07	14.59	2.35E-07	
14.56	3.23E-07	14.68	2.73E-07	
14.66	3.24E-07	14.78	2.57E-07	
14.76	3.83E-07	14.88	2.44E-07	
14.86	3.77E-07	14.98	2.52E-07	
14.96	3.28E-07	15.08	2.09E-07	
15.06	3.32E-07	15.18	2.56E-07	
15.16	3.82E-07	15.28	2.81E-07	
15.26	3.54E-07	15.38	2.53E-07	
15.36 15.46	3.41E-07 3.67E-07	15.48 15.58	2.63E-07 2.80E-07	
15.56	3.47E-07	15.68	2.71E-07	
15.66	3.82E-07	15.78	2.61E-07	
15.76	3.56E-07	15.88	2.51E-07	
15.86	3.54E-07	15.98	2.66E-07	
15.96	3.69E-07	16.08	2.91E-07	
16.06	3.53E-07	16.18	2.64E-07	
16.16	3.92E-07	16.28	2.54E-07	
16.26	3.43E-07	16.38	2.72E-07	
16.36	3.49E-07	16.48	2.70E-07	
16.46	3.59E-07	16.58	2.76E-07	
16.56	3.94E-07	16.68	2.66E-07	
16.66	3.39E-07	16.78	3.00E-07	
16.76	3.54E-07	16.88	2.80E-07	
16.86 16.96	3.45E-07	16.98	3.01E-07	
17.05	3.52E-07 3.42E-07	17.08 17.18	3.04E-07 2.93E-07	
17.05	3.42E-07 3.57E-07	17.18	2.93E-07 2.91E-07	
17.25	3.32E-07	17.38	2.93E-07	
17.35	3.39E-07	17.48	2.57E-07	
17.45	3.70E-07	17.58	2.57E-07	
17.55	3.96E-07	17.68	2.67E-07	
17.65	3.52E-07	17.78	3.22E-07	
17.75	3.63E-07	17.88	3.07E-07	
17.85	3.27E-07	17.97	2.86E-07	
17.95	2.78E-07	18.07	2.71E-07	
18.05	3.19E-07	18.17	2.76E-07	
18.15	3.53E-07	18.27	2.52E-07	
18.25	3.65E-07	18.37	2.67E-07	
18.35	2.76E-07	18.47	2.88E-07	
18.45 18.55	2.79E-07	18.57 18.67	2.78E-07	
18.55 18.65	2.58E-07	18.67 18.77	2.56E-07	
18.65 18.75	2.65E-07 2.60E-07	18.77 18.87	2.50E-07 2.78E-07	
18.85	2.82E-07	18.97	2.78E-07 2.68E-07	
18.95	2.82E-07 2.95E-07	19.07	2.66E-07	
19.05	3.04E-07	19.17	2.63E-07	
19.15	2.79E-07	19.27	2.84E-07	
19.25	3.05E-07	19.37	2.24E-07	
19.35	2.85E-07	19.47	2.73E-07	
19.45	2.93E-07	19.57	2.41E-07	
19 55	3 28E-07	19.67	2 19E-07	

Depth	Mag Susc
ft bgs	m <sup>3</sup> /kg
11.78 11.88	1.71E-07 2.24E-07
11.98	2.24E-07 2.40E-07
12.08	2.49E-07
12.18 12.28	2.53E-07 2.68E-07
12.28	2.08E-07 2.15E-07
12.48	2.01E-07
12.58 12.68	2.26E-07
12.68	2.13E-07 2.74E-07
12.87	2.23E-07
12.97	2.30E-07
13.07 13.17	2.52E-07 2.13E-07
13.27	1.98E-07
13.37	1.44E-07
13.47 13.57	2.30E-07 1.98E-07
13.67	2.54E-07
13.77	2.40E-07
13.87 13.97	2.04E-07 1.86E-07
14.07	2.95E-07
14.17	2.19E-07
14.27	2.92E-07
14.37 14.47	3.08E-07 2.59E-07
14.57	3.57E-07
14.67	2.91E-07
14.77	3.35E-07
14.87 14.97	3.45E-07 4.01E-07
15.07	3.34E-07
15.17	3.46E-07
15.27 15.37	3.78E-07 4.18E-07
15.47	4.10L-07 4.21E-07
15.57	3.84E-07
15.67	3.82E-07
15.77 15.87	3.66E-07 3.88E-07
15.97	3.70E-07
16.07	3.37E-07
16.17 16.27	3.32E-07 2.98E-07
16.36	4.00E-07
16.46	3.98E-07
16.56 16.66	4.50E-07 5.04E-07
16.66	4.91E-07
16.86	4.45E-07
16.96	4.40E-07
17.06 17.16	4.37E-07 4.23E-07
17.26	3.11E-07
17.36	3.32E-07
17.46 17.56	3.20E-07 2.96E-07
17.66	2.93E-07
17.76	3.18E-07
17.86 17.96	2.74E-07 2.85E-07
18.06	2.51E-07
18.16	2.62E-07
18.26	2.31E-07
18.36 18.46	2.95E-07 1.88E-07
18.56	2.67E-07
18.66	2.44E-07
18.76 18.86	2.28E-07 2.92E-07
18.96	3.10E-07
19.06	2.93E-07
19.16	3.44E-07
19.26 19.36	2.60E-07 2.97E-07
19.46	3.50E-07
19.56	2.67E-07
19.66 19.75	2.44E-07 2.85E-07
19.75	2.82E-07
19.95	2.86E-07
20.05	2.89E-07

**U10-51 SONDE DATA AND STATS** 



19.55

19.65

19.75 19.85 19.95

20.05

20.15

20.25

3.28E-07

3.07E-07

3.33E-07 3.50E-07

3.48E-07

3.24E-07

3.36E-07

3.38E-07

19.67

19.77

2.19E-07

1.87E-07

#N/A

Mean 2.59E-07

Median 2.59E-07

Standard Error 2.77E-09

Mode

U	0-025	U10-	-043	U10-51 SONDE	DATA AND ST
Depth	Mag Susc	Depth	Mag Susc	Depth	Mag Susc
ft bgs	m³/kg	ft bgs	m³/kg	ft bgs	m³/kg
20.34		Standard Deviation		20.15	
20.44		Sample Variance Kurtosis	1.13E-15	20.25	
20.54 20.64		Skewness	-0.10717 -0.19807	20.35 20.45	
20.74		Range		20.55	
20.84		Minimum	1.59E-07	20.65	
20.94		Maximum		20.75	
21.04 21.14		Sum Count	3.8E-05 147	20.85 20.95	
21.24		Confidence Level(95.0%)	5.48E-09	21.05	
21.34				21.15	
21.44				21.25	
21.54 21.64				21.35 21.45	
21.74				21.55	
21.84				21.65	
21.94 22.04				21.75 21.85	
22.04				21.85	
22.24				22.05	
22.34				22.15	
22.44 22.54				22.25 22.35	
22.64				22.45	
22.74				22.55	
22.84				22.65	
22.94 23.04				22.75 22.85	
23.04				22.85	
23.24				23.05	
23.34				23.15	
23.44 23.54				23.24 23.34	
23.63				23.44	
23.73	3.09E-07			23.54	2.82E-07
23.83				23.64	
23.93 24.03				23.74 23.84	
24.03				23.94	
24.23	2.84E-07			24.04	3.18E-07
24.33				24.14	
24.43 24.53				24.24 24.34	
24.63				24.44	
24.73	2.79E-07			24.54	2.91E-07
24.83				24.64	
24.93 25.03				24.74 24.84	
25.13				24.94	
25.23				25.04	
25.33				25.14	
25.43 25.53				25.24 25.34	
25.63				25.44	
25.73				25.54	
25.83				25.64 25.74	
25.93 26.03				25.74	
26.13				25.94	
26.23				26.04	
26.33				26.14 26.24	
26.43 26.53				26.34	
26.63				26.44	
26.73				26.54	
26.83				26.63	
26.92 27.02				26.73 26.83	
27.12				26.93	
27.22				27.03	
27.32 27.42				27.13 27.23	
27.42				27.33	
27.62				27.43	2.47E-07
27.72				27.53	
27.82				27.63	
27.92 28.02				27.73 27.83	
28.12				27.93	
28.22				28.03	
28.32 28.42				28.13 28.23	
28.52				28.33	
28.62				28.43	



U10	)-025	U10-043	U10-51 SONDE D	ATA AND STATS
Depth	Mag Susc	Depth Mag Susc	Depth	Mag Susc
ft bgs	m <sup>3</sup> /kg	ft bgs m <sup>3</sup> /kg	ft bgs	m <sup>3</sup> /kg
28.72	2.65E-07	it bys in rkg	28.53	2.69E-07
28.82	2.72E-07		28.63	2.11E-07
28.92	2.75E-07		28.73	1.83E-07
29.02	2.82E-07		28.83	2.20E-07
29.12	2.84E-07		28.93	1.93E-07
29.22	2.82E-07		29.03	2.22E-07
29.32 29.42	2.86E-07 2.98E-07		29.13 29.23	2.74E-07 2.40E-07
29.52	2.86E-07		29.33	2.60E-07
29.62	2.66E-07		29.43	2.47E-07
29.72	2.54E-07		29.53	3.54E-07
29.82	2.69E-07		29.63	2.69E-07
29.92	2.53E-07		29.73	2.71E-07
30.02	2.65E-07		29.83	2.65E-07
30.12 30.22	2.76E-07 2.57E-07		29.93 30.02	2.44E-07 2.58E-07
30.31	2.57E-07		30.12	2.57E-07
30.41	3.06E-07		30.22	2.55E-07
30.51	2.70E-07		30.32	2.20E-07
30.61	2.72E-07		30.42	2.12E-07
30.71	2.69E-07		30.52	2.52E-07
30.81	2.81E-07		30.62	2.06E-07
30.91	2.81E-07		30.72	2.97E-07
31.01	2.76E-07		30.82	2.61E-07
31.11 31.21	2.60E-07 2.70E-07		30.92 31.02	2.43E-07 2.28E-07
31.31	2.48E-07		31.12	2.63E-07
31.41	2.47E-07		31.22	2.79E-07
31.51	2.85E-07		31.32	2.52E-07
31.61	2.46E-07		31.42	2.13E-07
31.71	2.54E-07		31.52	2.58E-07
31.81	2.87E-07		31.62	2.52E-07
31.91	2.57E-07		31.72	2.71E-07
32.01	2.63E-07		31.82	2.28E-07
32.11 32.21	2.78E-07 2.94E-07		31.92 32.02	2.47E-07 2.46E-07
32.31	2.94E-07		32.12	2.22E-07
32.41	3.07E-07		32.22	2.42E-07
32.51	2.87E-07		32.32	2.78E-07
32.61	2.58E-07		32.42	2.45E-07
32.71	2.98E-07		32.52	2.64E-07
32.81	2.82E-07		32.62	3.00E-07
32.91	2.97E-07		32.72	2.33E-07
33.01	2.89E-07		32.82 32.92	2.13E-07
33.11 33.21	2.77E-07 2.76E-07		33.02	1.96E-07 2.62E-07
33.31	2.62E-07		33.12	3.02E-07
33.41	3.05E-07		33.22	2.15E-07
33.51	2.76E-07		33.32	2.45E-07
33.60	2.52E-07		33.42	2.73E-07
33.70	2.84E-07		33.51	2.75E-07
33.80	2.84E-07		33.61	2.55E-07
33.90 34.00	2.91E-07 2.73E-07		33.71 33.81	2.51E-07 2.05E-07
34.00 34.10	2.73E-07 2.32E-07		33.81 33.91	2.05E-07 2.81E-07
34.10	2.32E-07 2.66E-07		33.91	2.29E-07
34.30	2.63E-07		34.11	1.99E-07
34.40	3.03E-07		34.21	2.45E-07
34.50	2.65E-07		34.31	2.78E-07
34.60	2.59E-07		34.41	3.07E-07
34.70	2.53E-07		34.51	2.16E-07
34.80	2.54E-07		34.61	2.45E-07
34.90 35.00	2.64E-07 2.68E-07		34.71 34.81	3.02E-07
35.00 35.10	2.68E-07 2.67E-07		34.81	2.57E-07 2.59E-07
35.20	2.84E-07		35.01	2.55E-07
35.30	2.63E-07		35.11	2.61E-07
35.40	2.55E-07		35.21	2.62E-07
35.50	2.74E-07		35.31	2.89E-07
35.60	2.84E-07		35.41	2.58E-07
35.70	2.84E-07		35.51	3.00E-07
35.80	2.70E-07		35.61	2.68E-07
35.90 36.00	3.00E-07 2.77E-07		35.71 35.81	2.56E-07 3.02E-07
36.00	2.77E-07 2.84E-07		35.81	3.02E-07 3.02E-07
36.20	2.84E-07 2.82E-07		36.01	2.51E-07
36.30	2.77E-07		36.11	2.88E-07
36.40	2.96E-07		36.21	3.08E-07
36.50	2.92E-07		36.31	2.72E-07
36.60	2.89E-07		36.41	2.87E-07
36.70	3.05E-07		36.51	2.99E-07
36.80	2.82E-07		36.61 36.71	2.84E-07
36.90 36.99	2.97E-07 3.02E-07		36.71 36.81	2.57E-07 2.69E-07
20.00			00.01	



U10-025		U10-043		-043	U10-51 SONDE DATA AND STAT		
Depth M	lag Susc		Depth	Mag Susc	F	Depth	Mag Susc
ft bgs	m <sup>3</sup> /kg		ft bgs	m <sup>3</sup> /kg		tbgs	m <sup>3</sup> /kg
-	3.10E-07					36.90	3.08E-07
	2.86E-07					37.00	2.30E-07
	3.41E-07					37.10	2.49E-07
	2.80E-07					37.20	3.40E-07
	3.10E-07					37.30	3.06E-07
	3.33E-07					37.40	2.67E-07
	3.11E-07					37.50	2.96E-07
	3.30E-07					37.60	2.84E-07
	2.91E-07					37.70	2.52E-07
	2.93E-07					37.80	2.83E-07
	2.89E-07					37.90	2.65E-07
	3.54E-07					38.00	2.88E-07
	3.62E-07					38.10	2.79E-07
	3.11E-07					38.20	3.50E-07
38.49 3	3.17E-07					38.30	2.85E-07
38.59 3	3.18E-07					38.40	2.50E-07
38.69 3	3.49E-07					38.50	3.02E-07
38.79 3	3.55E-07					38.60	2.52E-07
38.89 3	3.64E-07					38.70	2.63E-07
39.02 3	3.84E-07					38.80	2.48E-07
39.12 3	3.67E-07					38.90	2.49E-07
39.22 3	3.82E-07					39.00	2.57E-07
39.32 4	1.05E-07					39.10	2.44E-07
	1.33E-07					39.20	2.97E-07
	1.31E-07					39.30	2.85E-07
39.62 4	1.32E-07					39.40	3.25E-07
						39.50	3.02E-07
						39.60	2.19E-07
- · ·		3.16E-07				39.70	3.08E-07
Stand		3.39E-09				39.80	2.55E-07
	Median	3.01E-07				39.90	2.68E-07
Standard [	Mode	#N/A				40.00 40.10	2.58E-07 3.02E-07
	Variance	3.4E-15				40.10	2.56E-07
Sample	Kurtosis	3.15558				40.20	2.45E-07
S		1.411555				40.30	2.77E-07
0		3.59E-07				40.49	3.09E-07
		2.19E-07				40.59	3.03E-07
		5.78E-07				40.69	2.82E-07
I.	Sum	9.36E-05				40.79	3.38E-07
	Count	296				40.89	2.75E-07
Confidence Leve						40.99	2.65E-07
	(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,					41.09	2.56E-07
						41.19	2.86E-07
						41.29	2.42E-07
						41.39	2.73E-07
						41.49	2.68E-07
						41.59	3.07E-07
						41.69	2.97E-07
						11 70	3 20 - 07



3.20E-07 2.89E-07 2.45E-07

3.02E-07

2.91E-07

3.13E-07

2.42E-07

2.42E-07 2.81E-07 2.70E-07 2.65E-07 2.86E-07

2.90E-07

3.79E-07

3.14E-07

3.14E-07 3.23E-07 3.16E-07 2.71E-07 2.69E-07

3.05E-07

2.40E-07

2.52E-07 3.24E-07 3.50E-07 2.90E-07 2.44E-07

2.65E-07

3.42E-07

3.25E-07

3.57E-07

3.13E-07 2.82E-07 2.56E-07

2.72E-07

2.92E-07

2.78E-07

41.79 41.89 41.99

42.09 42.19

42.29

42.39

42.39 42.49 42.59 42.69 42.79

42.89

42.99

43.09

43.19 43.29 43.39 43.49

43.59

43.69

43.78

43.88 43.98 44.08 44.18 44.28

44.38

44.48

44.58

44.68 44.78 44.88

44.98

45.08

45.18

#### U10-025

Depth Mag Susc ft bgs m<sup>3</sup>/kg

U10-043		
Depth	Mag Susc	

ftbgs m³/kg

Depth	Mag Susc
ft bgs	m <sup>3</sup> /kg
45.28 45.38	2.85E-07 2.54E-07
45.48	2.71E-07
45.58 45.68	2.67E-07 2.62E-07
45.78	2.55E-07
45.88 45.98	3.03E-07 2.74E-07
46.08	3.02E-07
46.18 46.28	3.21E-07 2.72E-07
46.38	2.95E-07
46.48 46.58	3.04E-07 3.33E-07
46.68	2.98E-07
46.78 46.88	3.49E-07 3.10E-07
46.98	3.02E-07
47.08 47.17	2.54E-07 3.45E-07
47.27	3.01E-07
47.37 47.47	3.17E-07 2.84E-07
47.57	2.99E-07
47.67 47.77	2.47E-07 3.06E-07
47.87	2.75E-07
47.97 48.07	2.87E-07 3.27E-07
48.17	3.02E-07 3.66E-07
48.27 48.37	3.72E-07
48.47 48.57	3.58E-07 3.56E-07
48.67	3.20E-07
48.77 48.87	3.62E-07 3.88E-07
48.97	4.03E-07
49.07 49.17	4.15E-07 4.22E-07
49.27	3.87E-07
49.37 49.47	3.50E-07 3.51E-07
49.57	3.83E-07
49.67 49.77	3.22E-07 2.32E-07
49.87	3.94E-07
49.97 50.07	2.70E-07 2.93E-07
50.17	3.03E-07
50.27 50.37	2.85E-07 2.91E-07
50.47	2.08E-07
50.57 50.66	3.39E-07 3.07E-07
50.76	3.75E-07
50.86 50.96	2.78E-07 2.43E-07
51.06	2.40E-07
51.16 51.26	2.63E-07 3.27E-07
51.36	2.78E-07
51.46 51.56	2.76E-07 2.92E-07
51.66	2.71E-07
51.76 51.86	2.36E-07 3.29E-07
51.96 52.06	2.99E-07 2.57E-07
52.16	3.09E-07
52.26 52.36	3.15E-07 2.30E-07
52.46	3.12E-07
52.56 52.66	3.50E-07 2.83E-07
52.76	2.53E-07
52.86 52.96	2.92E-07 3.27E-07
53.06	2.78E-07
53.16 53.26	3.26E-07 3.04E-07
53.36	2.61E-07
53.46 53.56	2.46E-07 2.10E-07



#### U10-025

Depth Mag Susc

ftbgs m³/kg

U10-043
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Depth Mag Susc

ftbgs m³/kg

ONDE	DATA AN
Depth	Mag Susc
ft bgs	m <sup>3</sup> /kg
53.66	2.85E-07
53.76 53.86	2.63E-07 3.16E-07
53.96	2.54E-07
54.05	3.07E-07
54.15	2.49E-07
54.25 54.35	2.56E-07 2.69E-07
54.45	2.26E-07
54.55	2.54E-07
54.65	2.78E-07
54.75 54.85	2.91E-07 2.86E-07
54.95	3.14E-07
55.05	3.55E-07
55.15 55.25	2.98E-07 2.88E-07
55.35	3.23E-07
55.45	2.60E-07
55.55	3.54E-07
55.65 55.75	3.39E-07 2.47E-07
55.85	3.19E-07
55.95	2.72E-07
56.05	2.95E-07
56.15 56.25	2.80E-07 2.34E-07
56.35	2.94E-07
56.45	3.07E-07
56.55	3.53E-07
56.65 56.75	2.34E-07 2.94E-07
56.85	2.79E-07
56.95	2.48E-07
57.05	2.44E-07
57.15 57.25	2.18E-07 2.80E-07
57.35	2.56E-07
57.45	2.43E-07
57.54	2.41E-07
57.64 57.74	2.51E-07 2.35E-07
57.84	2.36E-07
57.94	2.69E-07
58.04 58.14	2.86E-07 2.64E-07
58.24	1.97E-07
58.34	2.76E-07
58.44	2.52E-07
58.54 58.64	2.68E-07 2.79E-07
58.74	2.39E-07
58.84	3.05E-07
58.94	2.66E-07
59.04 59.14	3.12E-07 2.86E-07
59.24	2.95E-07
59.34	2.83E-07
59.44 59.54	2.34E-07 2.89E-07
59.64	3.19E-07
59.74	3.19E-07 2.87E-07
59.84	2.97E-07
59.94 60.04	3.69E-07 3.13E-07
60.14	2.86E-07
60.24	2.67E-07
60.34	2.99E-07
60.44 60.54	2.48E-07 2.77E-07
60.64	3.11E-07
60.74	2.27E-07
60.84	2.87E-07 2.86E-07
60.93 61.03	2.50E-07 2.50E-07
61.13	2.59E-07
61.23	2.23E-07
61.33 61.43	3.08E-07 2.91E-07
61.53	2.59E-07
61.63	2.70E-07
61.73 61.83	2.53E-07 2.56E-07
61.83	2.56E-07 2.97E-07



#### U10-025

ftbgs m³/kg

Depth Mag Susc

U10-043	
Depth	Mag Susc

ftbgs m³/kg

ONDE D	
Depth	Mag Susc
ft bgs	m <sup>3</sup> /kg
62.03 62.13	2.75E-07 2.28E-07
62.23	2.20L-07 2.17E-07
62.33	2.44E-07
62.43	2.59E-07
62.53	2.75E-07
62.63	3.08E-07
62.73	2.32E-07
62.83	2.72E-07
62.93	2.33E-07
63.03	2.88E-07
63.13	2.88E-07
63.23 63.33	2.40E-07 2.67E-07
63.43	2.52E-07
63.53	3.18E-07
63.63	2.40E-07
63.73	2.43E-07
63.83	2.72E-07
63.93	2.58E-07
64.03	2.43E-07
64.13	2.57E-07
64.23	2.34E-07
64.32	1.73E-07
64.42 64.52	2.72E-07 2.59E-07
64.52 64.62	2.59E-07 2.61E-07
64.72	2.86E-07
64.82	2.23E-07
64.92	2.99E-07
65.02	2.54E-07
65.12	2.64E-07
65.22	2.76E-07
65.32	3.08E-07
65.42	2.59E-07
65.52	2.81E-07
65.62	2.65E-07 2.60E-07
65.72 65.82	2.00E-07 2.74E-07
65.92	2.74E-07 2.56E-07
66.02	2.75E-07
66.12	2.48E-07
66.22	2.81E-07
66.32	2.87E-07
66.42	2.27E-07
66.52	2.70E-07
66.62	2.48E-07
66.72	2.76E-07
66.82 66.92	2.60E-07
67.02	2.19E-07 2.35E-07
67.12	2.62E-07
67.22	2.98E-07
67.32	2.50E-07
67.42	3.08E-07
67.52	2.33E-07
67.62	2.18E-07
67.72	2.45E-07
67.81 67.91	2.17E-07 2.19E-07
68.01	2.19E-07 2.67E-07
68.11	2.22E-07
68.21	2.92E-07
68.31	2.13E-07
68.41	2.46E-07
68.51	2.63E-07
68.61	2.37E-07
68.71	2.46E-07
68.81	2.69E-07
68.91 69.01	1.77E-07
69.01 69.11	2.47E-07 2.54E-07
69.11	2.54E-07 2.68E-07
69.31	2.61E-07
69.41	2.31E-07
69.51	2.45E-07
69.61	2.95E-07
69.71	2.66E-07
69.81	2.84E-07
69.91	2.33E-07
70.01	2.71E-07 2.82E-07
70.11 70.21	2.82E-07 3.27E-07
70.21	2.33E-07



m<sup>3</sup>/kg

### U10-025 Depth Mag Susc

ft bgs

m<sup>3</sup>/kg

#### U10-043

ft bgs

Depth Mag Susc

#### m<sup>3</sup>/kg ft bgs 70.41 2.33E-07 70.51 2.66E-07 70.61 3.08E-07 70.71 2.70E-07 70.81 2.66E-07 70.91 2.14E-07 71.01 2.73E-07 71.11 3.02E-07 71.20 3.43E-07 71.30 2.91E-07 71.40 2.50E-07 71.50 2.93E-07 71.60 71.70 2.75E-07 2.83E-07 71.80 3.26E-07 71.90 2.38E-07 72.00 2.83E-07 72.10 2.81E-07 72.20 3.16E-07 72.30 2.65E-07 72.40 72.50 2.39E-07 2.84E-07 72.60 2.93E-07 72.70 2.56E-07 72.80 2.64E-07 72.90 2.64E-07 73.00 2.94E-07 73.10 3.00E-07 73.20 3.12E-07 73.30 2.22E-07 73.40 3.03E-07 73.50 1.97E-07 73.60 2.87E-07 73.70 2.38E-07 2.68E-07 2.61E-07 73.80 73.90 74.00 2.76E-07 74.10 2.86E-07 74.20 3.08E-07 74.30 2.37E-07 74.40 3.00E-07 74.50 74.60 2.65E-07 2.66E-07 2.74E-07 74.69 74.79 2.47E-07 74.89 2.71E-07 74.99 2.80E-07 75.09 2.80E-07 75.19 2.08E-07 75.29 2.67E-07 75.39 1.99E-07 75.49 1.95E-07 75.59 2.61E-07 75.69 2.43E-07 75.79 2.37E-07 75.89 2.69E-07 75.99 2.69E-07 76.09 2.46E-07 2.59E-07 76.19 2.46E-07 76.29 76.39 2.36E-07 76.49 2.78E-07 76.59 2.53E-07 76.69 2.84E-07 2.45E-07 76.79 2.91E-07 76.89 76.99 2.82E-07 1.96E-07 77.09 77.19 2.74E-07 77.29 2.45E-07 77.39 2.27E-07 2.47E-07 2.42E-07 77.49 77.59 2.84E-07 77.69 77.79 2.96E-07 77.89 2.64E-07 77.99 3.04E-07 78.08 2.68E-07 78.18 2.59E-07 78.28 2.77E-07 78.38 2.82E-07 78.48 2.46E-07 78.58 2.02E-07

78.68

2.99E-07



#### **U10-51 SONDE DATA AND STATS**

Mag Susc

Depth

#### U10-025

ftbgs m³/kg

Depth Mag Susc

#### U10-043

ftbgs m³/kg

Depth Mag Susc

Depth	Mag Susc
ft bgs	m <sup>3</sup> /kg
78.78 78.88	3.04E-07 2.89E-07
78.98	2.81E-07
79.08 79.18	2.91E-07 3.17E-07
79.28	2.29E-07
79.38 79.48	2.49E-07 2.47E-07
79.58	2.44E-07
79.68 79.78	2.93E-07 2.17E-07
79.88	2.36E-07
79.98 80.08	2.68E-07 2.26E-07
80.18	2.83E-07
80.28 80.38	2.85E-07 2.79E-07
80.48	3.18E-07
80.58 80.68	2.44E-07 2.33E-07
80.78 80.88	2.72E-07 3.34E-07
80.88	2.31E-07
81.08 81.18	2.83E-07 3.08E-07
81.28	2.62E-07
81.38 81.47	3.35E-07 2.49E-07
81.57	2.69E-07
81.67 81.77	2.35E-07 2.60E-07
81.87	2.85E-07
81.97 82.07	2.81E-07 2.58E-07
82.17	2.97E-07
82.27 82.37	3.05E-07 2.87E-07
82.47	2.64E-07
82.57 82.67	2.49E-07 2.64E-07
82.77 82.87	2.74E-07 3.02E-07
82.97	3.19E-07
83.07 83.17	2.81E-07 2.89E-07
83.27	2.74E-07
83.37 83.47	2.46E-07 2.32E-07
83.57 83.67	3.42E-07 3.00E-07
83.77	2.74E-07
83.87 83.97	2.74E-07 3.00E-07
84.07	2.87E-07
84.17 84.27	2.42E-07 2.59E-07
84.37	2.46E-07
84.47 84.57	2.35E-07 2.18E-07
84.67	2.70E-07
84.77 84.87	3.13E-07 2.87E-07
84.96 85.06	2.37E-07
85.16	2.45E-07 2.37E-07
85.26 85.36	2.30E-07 2.63E-07
85.46	2.92E-07
85.56 85.66	2.70E-07 3.09E-07
85.76	2.87E-07
85.86 85.96	2.20E-07 2.11E-07
86.06	2.66E-07
86.16 86.26	2.12E-07 3.13E-07
86.36	2.72E-07 2.57E-07
86.46 86.56	2.80E-07
86.66 86.76	2.59E-07 2.86E-07
86.86	2.19E-07
86.96 87.06	2.54E-07 2.69E-07



#### U10-025

ftbgs m³/kg

Depth Mag Susc

U10-043	
Depth	Mag Susc

ftbgs m³/kg

ONDE	DATA AN
Depth	Mag Susc
ft bgs	m³/kg
87.16	2.55E-07
87.26	2.17E-07
87.36 87.46	2.63E-07 1.63E-07
87.56	3.10E-07
87.66	2.18E-07
87.76	1.76E-07
87.86	2.72E-07
87.96	1.95E-07
88.06 88.16	1.94E-07 2.90E-07
88.26	1.81E-07
88.35	2.25E-07
88.45	2.25E-07
88.55	2.64E-07
88.65 88.75	2.18E-07 2.60E-07
88.85	2.37E-07
88.95	2.42E-07
89.05	2.21E-07
89.15	1.81E-07
89.25	2.42E-07
89.35 89.45	1.90E-07 2.17E-07
89.55	2.17E-07 2.18E-07
89.65	1.97E-07
89.75	2.20E-07
89.85	2.43E-07
89.95	2.46E-07
90.05 90.15	2.76E-07 2.26E-07
90.25	2.09E-07
90.35	2.41E-07
90.45	2.61E-07
90.55	2.37E-07
90.65	1.92E-07
90.75 90.85	1.89E-07 1.84E-07
90.95	2.37E-07
91.05	2.18E-07
91.15	2.02E-07
91.25	1.89E-07
91.35	2.29E-07
91.45 91.55	1.87E-07 1.90E-07
91.65	1.83E-07
91.75	1.86E-07
91.84	2.43E-07
91.94	2.18E-07
92.04 92.14	2.35E-07 1.82E-07
92.24	2.31E-07
92.34	2.72E-07 1.75E-07
92.44	
92.54	1.81E-07
92.64 92.74	1.61E-07 1.81E-07
92.84	2.32E-07
92.94	2.69E-07
93.04	1.84E-07
93.14	2.08E-07
93.24 93.34	1.74E-07 2.08E-07
93.34 93.44	1.91E-07
93.54	2.49E-07
93.64	1.60E-07
93.74	1.98E-07
93.84	2.15E-07
93.94 94.04	1.73E-07 2.45E-07
94.14	1.62E-07
94.24	1.94E-07
94.34	1.98E-07
94.44	2.23E-07
94.54	1.98E-07
94.64 94.74	2.08E-07 2.00E-07
94.74 94.84	1.90E-07
94.94	1.76E-07
95.04	2.62E-07
95.14	1.70E-07
95.23 95.33	1.76E-07 1.83E-07
95.33 95.43	1.83E-07 1.90E-07
00.10	



# U10-025 Depth Mag Susc

#### U10-043

ftbgs m³/kg

Depth Mag Susc

Depth	Mag Susc
ft bgs	m³/kg
95.53	1.94E-07
95.63 95.73	1.76E-07 2.25E-07
95.83	2.23E-07 2.11E-07
95.93	2.38E-07
96.03	2.26E-07
96.13	1.62E-07 2.61E-07
96.23 96.33	1.90E-07
96.43	2.12E-07
96.53	2.38E-07
96.63 96.73	1.80E-07 1.78E-07
96.73 96.83	1.78E-07 1.93E-07
96.93	2.61E-07
97.03	1.99E-07
97.13	1.96E-07 2.00E-07
97.23 97.33	2.00E-07 1.90E-07
97.43	2.21E-07
97.53	2.56E-07
97.63	2.53E-07
97.73 97.83	3.47E-07 3.35E-07
97.93	2.84E-07
98.03	3.42E-07
98.13	3.13E-07
98.23 98.33	3.07E-07 3.08E-07
98.43	2.06E-07
98.53	2.33E-07
98.62	2.44E-07
98.72 98.82	2.67E-07 2.49E-07
98.92	2.49L-07 2.22E-07
99.02	2.29E-07
99.12	1.99E-07
99.22 99.32	2.53E-07 2.69E-07
99.32 99.42	2.09E-07 2.02E-07
99.52	2.33E-07
99.62	2.32E-07
99.72	2.65E-07
99.82 99.92	2.72E-07 2.30E-07
100.02	2.36E-07
100.12	2.36E-07
100.22 100.32	2.27E-07 2.52E-07
100.32	1.75E-07
100.52	2.30E-07
100.62	2.58E-07
100.72 100.82	2.44E-07
100.82	3.05E-07 1.92E-07
101.02	2.32E-07
101.12	2.39E-07
101.22 101.32	2.61E-07
101.32	2.42E-07 2.72E-07
101.52	2.82E-07
101.62	2.26E-07
101.72 101.82	3.03E-07 2.82E-07
101.82	
102.02	2.68E-07 2.87E-07
102.21	2.61E-07
102.31 102.41	2.22E-07
102.41	3.05E-07 2.45E-07
102.61	2.45E-07 3.50E-07
102.71	3.17E-07
102.81	2.93E-07 2.90E-07
102.91 103.01	2.90E-07 2.57E-07
103.11	3.37E-07
103.21	3.02E-07
103.31	2.29E-07
103.41 103.51	2.74E-07 2.77E-07
103.61	3.66E-07
103.71	3.13E-07
103.81	2.92E-07 2.92E-07
103.91	2.92E-07



#### U10-025

#### U10-043

Depth Mag Susc ft bgs m<sup>3</sup>/kg

Depth	Mag Susc
ft bgs	m³/kg

SONDE D	
Depth	Mag Susc
ft bgs	m³/kg
104.01	3.24E-07
104.11 104.21	2.79E-07 3.57E-07
104.21	3.11E-07
104.41	3.79E-07
104.51	3.31E-07
104.61 104.71	3.28E-07 3.39E-07
104.81	3.04E-07
104.91	3.10E-07
105.01	3.43E-07
105.11 105.21	3.19E-07 3.09E-07
105.31	3.04E-07
105.41	2.88E-07
105.50 105.60	2.26E-07 3.56E-07
105.70	2.42E-07
105.80	2.34E-07
105.90 106.00	3.06E-07
106.00	3.08E-07 2.69E-07
106.20	2.32E-07
106.30	2.63E-07
106.40 106.50	2.54E-07 2.48E-07
106.60	1.92E-07
106.70	2.35E-07
106.80	2.81E-07
106.90 107.00	3.11E-07 3.14E-07
107.10	2.76E-07
107.20	2.92E-07
107.30 107.40	2.31E-07 2.12E-07
107.40	2.12E-07 2.97E-07
107.60	2.52E-07
107.70	2.56E-07
107.80 107.90	2.68E-07 1.74E-07
108.00	2.16E-07
108.10	2.60E-07
108.20 108.30	2.65E-07 1.92E-07
108.30	2.83E-07
108.50	2.71E-07
108.60	2.51E-07
108.70 108.80	2.17E-07 2.47E-07
108.90	2.85E-07
108.99	2.29E-07
109.09 109.19	2.87E-07 2.43E-07
109.29	2.85E-07
109.39	2.31E-07
109.49 109.59	3.17E-07 2.67E-07
109.69	2.72E-07
109.79	2.84E-07
109.89 109.99	2.14E-07 2.62E-07
110.09	2.02E-07 2.30E-07
110.19	2.86E-07
110.29	2.41E-07
110.39 110.49	2.18E-07 2.39E-07
110.59	2.56E-07
110.69	3.15E-07
110.79 110.89	2.35E-07 2.34E-07
110.09	2.34E-07 2.36E-07
111.09	2.24E-07
111.19 111.29	2.25E-07 2.59E-07
111.29	2.59E-07 2.07E-07
111.49	1.77E-07
111.59	1.88E-07
111.69 111.79	2.00E-07 2.31E-07
111.89	2.74E-07
111.99	2.72E-07
112.09 112.19	2.23E-07 2.12E-07
112.19	1.83E-07



#### U10-025

#### U10-043

Depth	Mag Susc
ft bgs	m <sup>3</sup> /kg

Depth	Mag Susc
ft bgs	m³/kg

Depth	Mag Susc
ft bgs	m³/kg
112.38	1.74E-07
112.48 112.58	1.81E-07 2.09E-07
112.68	2.09E-07 2.34E-07
112.78	2.05E-07
112.88	2.28E-07
112.98	2.12E-07
113.08	2.73E-07
113.18 113.28	2.11E-07 2.01E-07
113.28	2.26E-07
113.48	2.13E-07
113.58	3.02E-07
113.68	2.75E-07
113.78	2.37E-07
113.88 113.98	2.10E-07 1.77E-07
114.08	2.18E-07
114.18	2.48E-07
114.28	1.92E-07
114.38	2.06E-07
114.48	2.32E-07
114.58 114.68	2.42E-07 2.00E-07
114.78	2.41E-07
114.88	2.31E-07
114.98	2.09E-07
115.08	1.58E-07
115.18 115.28	1.61E-07 1.60E-07
115.28	1.86E-07
115.48	2.32E-07
115.58	2.04E-07
115.68	1.85E-07
115.77	1.81E-07
115.87 115.97	2.01E-07 2.11E-07
116.07	2.24E-07
116.17	1.98E-07
116.27	2.09E-07
116.37	1.30E-07
116.47	2.29E-07
116.57 116.67	2.40E-07 1.41E-07
116.77	2.21E-07
116.87	1.85E-07
116.97	1.93E-07
117.07	2.07E-07
117.17 117.27	2.37E-07 2.42E-07
117.37	2.42E-07 2.00E-07
117.47	1.88E-07
117.57	2.30E-07
117.67	1.77E-07
117.77	2.22E-07
117.87 117.97	1.96E-07 2.24E-07
118.07	2.38E-07
118.17	2.08E-07
118.27	1.94E-07
118.37	2.62E-07
118.47 118.57	1.78E-07 2.57E-07
118.67	2.13E-07
118.77	1.56E-07
118.87	1.74E-07
118.97	1.86E-07
119.07 119.17	2.05E-07 2.37E-07
119.26	2.23E-07
119.36	1.78E-07
119.46	1.82E-07
119.56	1.75E-07
119.66	2.07E-07
119.76 119.86	2.18E-07 1.18E-07
119.00	1.18E-07 1.98E-07
120.06	1.49E-07
120.16	1.90E-07
120.26	2.58E-07
120.36	1.91E-07
120.46 120.56	1.73E-07 2.51E-07
120.66	2.36E-07



#### U10-025

## U10-043

Depth Mag Susc ft bgs m<sup>3</sup>/kg

Depth	Mag Susc
ft bgs	m <sup>3</sup> /kg
120.76 120.86	2.22E-07
120.80	1.57E-07 1.82E-07 1.95E-07 1.37E-07 2.67E-07 1.98E-07
121.06	1.95E-07
121.16 121.26	1.37E-07
121.20	1.98E-07
121.46	2.320-07
121.56 121.66	2.31E-07 2.01E-07
121.00	2.01E-07 1.67E-07
121.86	1.89E-07
122.06	2.19E-07
122.16 122.26	1.32E-07 1.36E-07
122.36	2.32E-07
122.46	2.13E-07
122.56 122.65	1.58E-07 1.57E-07
122.75	2.35E-07
122.85	2.13E-07
122.95 123.05	1.81E-07 2.12E-07
123.15	2.13E-07
123.25	1.85E-07
123.35	2.07E-07
123.45 123.55	2.19E-07 2.18E-07
123.65	2.24E-07
123.75	1.82E-07
123.85 123.95	1.92E-07 1.89E-07
123.95	1.09E-07 1.24E-07
124.15	2.33E-07
124.25	1.63E-07
124.35 124.45	1.37E-07 1.73E-07
124.55	1.78E-07
124.65	1.59E-07 2.22E-07
124.75 124.85	2.22E-07 2.22E-07
124.85	
125.05	1.96E-07 2.18E-07
125.15 125.25	1.63E-07
125.25	2.05E-07 1.37E-07
125.45	1 51E-07
125.55	1.67E-07
125.65 125.75	1.90E-07
125.85	1.67E-07 1.90E-07 1.45E-07 2.03E-07 2.21E-07
125.95	2.21E-07
126.05 126.14	1.40E-07 2.31E-07
126.24	2.31E-07 1.27E-07
126.34	2.00E-07 1.69E-07
126.44 126.54	1.69E-07 2.36E-07
126.64	2.12E-07
126.74	1.89E-07
126.84 126.94	1.76E-07 1.61E-07
127.04	2.33E-07
127.14	1.65E-07
127.24 127.34	2.05E-07 1.65E-07
127.44	1.92E-07
127.54	1.88E-07
127.64 127.74	2.30E-07 2.06E-07
127.74	2.06E-07 1.93E-07
127.94	1.92E-07
128.04	2.12E-07
128.14 128.24	1.90E-07 2.02E-07
128.34	2.02E-07 2.30E-07
128.44	1.79E-07
128.54	1.62E-07 1.92E-07
128.64 128.74	2.07E-07
128.84	1.63E-07
128.94	1.68E-07
129.04 129.14	1.64E-07 1.64E-07

$\mathbf{W}$
& ASSOCIATES

Depth	Mag Susc
ft bgs	m³/kg

#### U10-025

ft bgs m<sup>3</sup>/kg

Depth Mag Susc

#### U10-043

Depth Mag Susc

ftbgs m³/kg

Depth	Mag Susc
ft bgs	m <sup>3</sup> /kg
129.24	1.73E-07
129.34 129.44	1.96E-07 1.53E-07
129.53	1.58E-07
129.63	1.81E-07
129.73 129.83	1.96E-07 1.63E-07
129.93	2.42E-07
130.03	1.84E-07
130.13 130.23	2.36E-07 2.00E-07
130.33	1.76E-07
130.43	1.75E-07
130.53 130.63	2.32E-07 2.24E-07
130.73	1.96E-07
130.83	2.14E-07
130.93 131.03	2.02E-07 1.56E-07
131.13	1.56E-07 1.96E-07
131.23	1.84E-07
131.33 131.43	1.81E-07 2.19E-07
131.53	2.21E-07
131.63	1.77E-07 1.97E-07
131.73 131.83	1.97E-07 2.03E-07
131.93	2.05E-07 2.40E-07
132.03	2.40E-07
132.13 132.23	2.00E-07 2.03E-07
132.33	2.00E-07
132.43	1.82E-07 1.97E-07
132.53 132.63	1.97E-07 1.83E-07
132.73	1.70E-07 2.00E-07
132.83	
132.92 133.02	1.84E-07 2.02E-07
133.12	1.88E-07
133.22	1.79E-07
133.32 133.42	1.98E-07 2.35E-07
133.52	2.35E-07 1.89E-07
133.62	1.48E-07
133.72 133.82	1.89E-07 1.68E-07
133.92	1.58E-07
134.02	1.49E-07
134.12 134.22	2.04E-07 1.82E-07
134.32	1 74F-07
134.42 134.52	2.17E-07 1.89E-07
134.62	2.41E-07
134.72	1.78E-07
134.82 134.92	1.94E-07 2.02E-07
135.02	1.95E-07
135.12	1.81E-07
135.22 135.32	1.93E-07 1.95E-07
135.42	1.52E-07
135.52	1.79E-07
135.62 135.72	1.96E-07
135.82	2.28E-07 9.68E-08
135.92	1.65E-07
136.02 136.12	2.28E-07 1.86E-07
136.22	2.20E-07
136.32	1.83E-07 1.18E-07
136.41 136.51	1 00F_07
136.61	1.74E-07
136.71	2.05E-07
136.81 136.91	1.80E-07 1.75E-07
137.01	1.74E-07 2.05E-07 1.80E-07 1.75E-07 6.85E-08
137.11	1.51E-07
137.21 137.31	1.51E-07 1.55E-07 1.46E-07
137.41	1.03E-07
137.51	1.60E-07



## U10-025 Depth Mag Susc

#### U10-043

ftbgs m³/kg

Depth Mag Susc

Depth	Mag Susc
<b>ft bgs</b> 137.61	m <sup>3</sup> /kg 1.99E-07
137.71	2.21E-07
137.81	1.56E-07
137.91 138.01	1.19E-07 2.06E-07
138.01	2.00E-07 1.94E-07
138.21	1.97E-07
138.31	2.31E-07
138.41	1.98E-07
138.51 138.61	1.69E-07 6.48E-08
138.71	2.14E-07
138.81	2.14E-07
138.91	2.30E-07
139.01 139.11	2.07E-07 1.66E-07
139.21	1.98E-07
139.31	1.62E-07
139.41	1.87E-07
139.51 139.61	1.73E-07 2.11E-07
139.71	1.55E-07
139.80	2.13E-07
139.90	1.68E-07
140.00 140.10	1.93E-07 2.08E-07
140.10	1.67E-07
140.30	1.90E-07
140.40	2.07E-07
140.50 140.60	1.73E-07 2.08E-07
140.00	2.62E-07
140.80	1.76E-07
140.90	1.74E-07
141.00	2.49E-07
141.10 141.20	1.56E-07 1.74E-07
141.30	1.37E-07
141.40	1.21E-07
141.50	1.67E-07
141.60 141.70	1.95E-07 1.99E-07
141.80	2.12E-07
141.90	2.10E-07
142.00	1.81E-07
142.10 142.20	2.22E-07 1.68E-07
142.30	2.07E-07
142.40	2.09E-07
142.50	1.63E-07
142.60 142.70	1.99E-07 1.68E-07
142.80	1.55E-07
142.90	1.57E-07
143.00 143.10	1.48E-07 1.36E-07
143.10	1.90E-07
143.29	2.07E-07
143.39	2.08E-07
143.49 143.59	1.67E-07
143.69	2.72E-07 2.12E-07
143.79	1.60E-07
143.89	2.01E-07
143.99 144.09	2.00E-07 1.82E-07
144.09	1.32E-07
144.29	1.91E-07
144.39	2.02E-07
144.49 144.59	1.87E-07 1.69E-07
144.69	2.00E-07
144.79	2.30E-07
144.89	2.10E-07
144.99 145.09	1.79E-07 1.74E-07
145.09	1.74E-07 1.51E-07
145.29	2.04E-07
145.39	1.49E-07
145.49 145.59	2.31E-07 2.35E-07
145.69	1.57E-07
145.79	1.37E-07
145.89	2.41E-07

# 

#### **U10-51 SONDE DATA AND STATS**

Mag Susc

Depth

#### U10-025

ftbgs m³/kg

Depth Mag Susc ff bos m³/kɑ

#### U10-043

ft bgs m³/kg

Depth Mag Susc

Depth	Mag Susc
ft bgs	m³/kg
145.99	2.13E-07
146.09	2.12E-07
146.19	1.83E-07
146.29	2.29E-07
146.39	2.00E-07
146.49	1.84E-07
146.59	2.00E-07
146.68	1.54E-07
146.78	1.66E-07
146.88 146.98	2.13E-07 2.46E-07
146.98	
147.08	2.58E-07 1.83E-07
147.28	1.86E-07
147.38	1.54E-07
147.48	1.87E-07
147.58	1.61E-07
147.68	1.74E-07
147.78	1.78E-07
147.88	2.00E-07
147.98	1.31E-07
148.08	2.26E-07
148.18	2.03E-07
148.28	2.34E-07
148.38	2.13E-07
148.48	1.77E-07
148.58	2.39E-07
148.68	2.28E-07
148.78	2.30E-07 1.98E-07
148.88 148.98	1.98E-07 1.61E-07
140.90	2.21E-07
149.08	2.21E-07 2.59E-07
149.10	1.99E-07
149.38	1.84E-07
149.48	1.82E-07
149.58	1.83E-07
149.68	1.98E-07
149.78	1.99E-07
149.88	1.91E-07
149.98	2.33E-07
150.07	1.75E-07
150.17	1.49E-07
150.27	1.48E-07
150.37	1.85E-07
150.47	2.04E-07
150.57	1.76E-07
150.67	1.77E-07
150.77	2.02E-07
150.87	1.97E-07
150.97	1.99E-07
151.07	1.99E-07
151.17	2.34E-07
151.27	1.65E-07
151.37	2.24E-07 2.07E-07
151.47 151.57	1.69E-07
151.67	1.42E-07
151.77	
151.87	2.37E-07 2.54E-07
151.97	1.40E-07
152.07	
152.17	2.86E-07 1.62E-07
152.27	1.73E-07
152.37	3.02E-07 1.94E-07
152.47	1.94E-07
152.57	2.82E-07
152.67	2.00E-07
152.77	2.29E-07
152.87	1.92E-07
152.97	1.93E-07
153.07	1.91E-07
153.17	2.00E-07 1.53E-07
153.27	1.53E-07
153.37	1.81E-07
153.47	1.92E-07 1.19E-07
153.56 153.66	1.19E-07 2.07E-07
153.66	2.07E-07 2.14E-07
153.76	2.14E-07 1.85E-07
153.96	1.94E-07
154.06	2.33E-07
154.16	1.75E-07
154.26	1.91E-07



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Depth Mag Susc ft bgs m<sup>3</sup>/kg

Depth ft bgs	Mag Susc m <sup>3</sup> /kg
154.36	1.90E-07
154.46 154.56	1.49E-07 1.77E-07
154.66	1.82E-07
154.76	1.93E-07
154.86	1.84E-07 2.06E-07
154.96 155.06	1.45E-07
155.16	1.51E-07
155.26	2.15E-07
155.36 155.46	2.25E-07 1.59E-07
155.56	2.00E-07
155.66	2.05E-07
155.76 155.86	1.77E-07 1.45E-07
155.96	2.35E-07
156.06	1.71E-07
156.16 156.26	1.89E-07 2.10E-07
156.36	2.58E-07
156.46	2.06E-07
156.56 156.66	1.74E-07 2.09E-07
156.76	2.09E-07 2.26E-07
156.86	2.12E-07
156.95	1.94E-07
157.05 157.15	1.76E-07 2.17E-07
157.25	1.69E-07
157.35	2.01E-07
157.45 157.55	2.20E-07 1.66E-07
157.65	1.98E-07
157.75	2.14E-07
157.85	1.91E-07
157.95 158.05	2.06E-07 1.63E-07
158.15	1.73E-07
158.25	2.59E-07
158.35 158.45	2.30E-07 2.25E-07
158.55	1.95E-07
158.65	1.73E-07
158.75 158.85	2.46E-07 1.60E-07
158.95	1.85E-07
159.05	1.48E-07
159.15 159.25	1.72E-07 2.08E-07
159.35	2.14E-07
159.45	1.69E-07
159.55 159.65	1.69E-07 1.75E-07
159.75	1.42E-07
159.85	2.03E-07
159.95 160.05	1.69E-07 1.78E-07
160.15	2.34E-07
160.25	1.88E-07
160.35 160.44	2.44E-07 2.00E-07
160.54	2.36E-07
160.64	2.26E-07
160.74 160.84	2.23E-07 2.02E-07
160.94	1.88E-07
161.04	1.84E-07
161.14 161.24	2.32E-07 1.68E-07
161.34	2.26E-07
161.44	1.90E-07
161.54 161.64	1.54E-07 2.21E-07
161.74	1.88E-07
161.84	2.19E-07
161.94 162.04	1.49E-07 2.02E-07
162.04	2.40E-07
162.24	2.15E-07
162.34 162.44	1.79E-07 2.02E-07
162.54	1.99E-07
162.64	2.00E-07

- <b>V</b> V-		
& ASSOCIATES		

Depth	Mag Susc
ft bgs	m³/kg

#### U10-025

U10-043
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Depth	Mag Susc
ft bgs	m <sup>3</sup> /kg

Depth	Mag Susc
ft bgs	m³/kg

Depth	Mag Susc
ft bgs	m <sup>3</sup> /kg
162.74	1.86E-07
162.84	2.05E-07
162.94	2.03E-07
163.04 163.14	2.14E-07 1.86E-07
163.24	2.81E-07
163.34	2.47E-07
163.44	2.17E-07
163.54 163.64	1.87E-07 2.27E-07
163.74	1.94E-07
163.83	1.90E-07
163.93	1.66E-07
164.03 164.13	2.04E-07 1.99E-07
164.13	1.51E-07
164.33	1.69E-07
164.43	2.39E-07
164.53 164.63	2.58E-07 2.15E-07
164.03	2.13E-07 2.27E-07
164.83	1.98E-07
164.93	2.39E-07
165.03	2.18E-07
165.13 165.23	2.54E-07 2.80E-07
165.33	2.78E-07
165.43	2.52E-07
165.53	2.95E-07
165.63 165.73	3.16E-07 2.92E-07
165.83	2.92E-07 2.49E-07
165.93	2.99E-07
166.03	3.30E-07
166.13	2.88E-07
166.23 166.33	2.90E-07 2.90E-07
166.43	3.65E-07
166.53	2.76E-07
166.63	3.04E-07
166.73 166.83	2.87E-07 3.52E-07
166.93	2.98E-07
167.03	3.65E-07
167.13	3.46E-07
167.22 167.32	3.30E-07 2.84E-07
167.32	2.84E-07 3.56E-07
167.52	2.95E-07
167.62	3.46E-07
167.72 167.82	3.34E-07
167.92	2.54E-07 2.76E-07
168.02	3.21E-07
168.12	2.74E-07
168.22	2.93E-07
168.32 168.42	2.70E-07 2.78E-07
168.52	2.72E-07
168.62	2.86E-07
168.72	3.47E-07
168.82 168.92	3.00E-07 2.87E-07
169.02	3.46E-07
169.12	3.35E-07
169.22	2.88E-07
169.32 169.42	3.72E-07 3.24E-07
169.42	3.24E-07 3.09E-07
169.62	2.99E-07
169.72	2.75E-07
169.82	2.83E-07
169.92 170.02	3.24E-07 3.58E-07
170.02	2.64E-07
170.22	2.95E-07
170.32	2.98E-07
170.42 170.52	3.12E-07 3.27E-07
170.52	3.34E-07
170.71	3.29E-07
170.81	2.95E-07
170.91 171.01	2.99E-07
171.01	3.06E-07



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Depth	Mag Susc
ft bgs	m³/kg

Depth	Mag Susc
ft bgs	m³/kg

Depth	Mag Susc
ft bgs	m³/kg
171.11	3.55E-07
171.21	3.04E-07
171.31	2.90E-07 3.04E-07
171.41	3.04E-07
171.51	2.95E-07
171.61 171.71	2.93E-07 3.12E-07
171.81	3.46E-07
171.91	
172.01	2.94E-07 2.83E-07
172.11	3.41E-07
172.21	3.16E-07
172.31	2.65E-07
172.41	2.49E-07
172.51 172.61	3.04E-07 2.79E-07
172.01	2.79E-07
172.81	2.97E-07 2.35E-07
172.91	2.81E-07
173.01	2.95E-07
173.11	2.46E-07
173.21	3.04E-07
173.31	2.95E-07 2.69E-07
173.41	
173.51	3.12E-07
173.61	2.86E-07
173.71 173.81	2.95E-07 2.98E-07
173.81	2.98E-07 3.08E-07
174.01	3.45E-07
174.10	3.52E-07
174.20	3.04E-07
174.30	2.92E-07
174.40	2.41E-07
174.50	2.95E-07
174.60	2.57E-07
174.70	2.59E-07
174.80	2.64E-07
174.90 175.00	2.67E-07 3.07E-07
175.10	2.64E-07
175.20	2.22E-07
175.30	2.57E-07
175.40	2.25E-07
175.50	2.89E-07
175.60	2.68E-07
175.70 175.80	2.04E-07 1.88E-07
175.90	2.62E-07
176.00	2.02E-07
176.10	2.37E-07 2.13E-07
176.20	1.93E-07
176.30	2.10E-07
176.40	2.51E-07
176.50	2.31E-07
176.60	2.44E-07 2.08E-07
176.70	
176.80 176.90	2.09E-07 2.29E-07
177.00	2.23L-07 2.47E-07
177.10	1.89E-07
177.20	1.63E-07
177.30	1.84E-07
177.40	1.84E-07
177.50	2.33E-07
177.59	2.44E-07
177.69	2.10E-07 2.08E-07
177.79 177.89	2.08E-07 2.16E-07
177.99	1.89E-07
178.09	2.62E-07
178.19	2.06E-07
178.29	2.31E-07
178.39	2.04E-07
178.49	2.00E-07
178.59	1.55E-07
178.69 178.79	2.16E-07 1.67E-07
178.79	2.16E-07
178.99	2.49E-07
179.09	2.32E-07
179.19	2.06E-07
179.29	2.21E-07
179.39	1.96E-07



#### U10-025

Depth Mag Susc

ftbgs m³/kg

U10-043	
Depth	Mag Susc

ftbgs m³/kg

Depth	Mag Susc
ft bgs	m³/kg
179.49	1.94E-07
179.59 179.69	1.89E-07 2.00E-07
179.79	2.07E-07
179.89	1.79E-07
179.99	2.65E-07
180.09 180.19	2.09E-07 2.15E-07
180.29	2.13E-07 2.27E-07
180.39	2.45E-07
180.49	2.09E-07
180.59 180.69	1.82E-07 1.65E-07
180.79	2.48E-07
180.89	2.01E-07
180.98	1.98E-07
181.08 181.18	2.27E-07 1.89E-07
181.28	2.13E-07
181.38	2.41E-07
181.48 181.58	2.01E-07
181.58	1.81E-07 2.40E-07
181.78	1.92E-07
181.88	1.91E-07
181.98	1.96E-07
182.08 182.18	1.66E-07 1.71E-07
182.18	2.40E-07
182.38	2.78E-07
182.48	2.34E-07
182.58 182.68	2.55E-07 1.92E-07
182.08	1.88E-07
182.88	1.81E-07
182.98	1.49E-07
183.08	1.79E-07 2.47E-07
183.18 183.28	2.47E-07 2.10E-07
183.38	2.23E-07
183.48	2.10E-07
183.58	1.92E-07
183.68 183.78	2.10E-07 1.80E-07
183.88	2.13E-07
183.98	2.09E-07
184.08	2.11E-07
184.18 184.28	1.54E-07 2.19E-07
184.37	2.02E-07
184.47	2.29E-07
184.57	2.52E-07
184.67 184.77	2.20E-07 2.07E-07
184.87	2.31E-07
184.97	1.83E-07
185.07	1.73E-07
185.17 185.27	1.83E-07 1.78E-07
185.37	2.46E-07
185.47	1.99E-07
185.57	1.96E-07
185.67 185.77	2.22E-07 1.87E-07
185.87	2.29E-07
185.97	2.26E-07
186.07	2.13E-07
186.17 186.27	2.52E-07 2.19E-07
186.37	2.37E-07
186.47	1.99E-07
186.57	2.48E-07
186.67 186.77	2.16E-07 1.97E-07
186.87	2.55E-07
186.97	1.87E-07
187.07	1.59E-07
187.17 187.27	2.56E-07 2.19E-07
187.27	2.19E-07 2.26E-07
187.47	1.90E-07
187.57	2.44E-07
187.67 187.77	2.03E-07 1.67E-07
107.77	1.07 E-07



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Depth Mag Susc ft bgs m<sup>3</sup>/kg

#### Depth Mag Susc ft bgs m<sup>3</sup>/kg

Depth	Mag Susc
ft bgs	m <sup>3</sup> /kg
187.86	1.92E-07
187.96	1.83E-07
188.06	2.09E-07
188.16 188.26	2.01E-07 2.09E-07
188.36	1.53E-07
188.46	2.11E-07
188.56 188.66	1.99E-07 2.30E-07
188.76	1.60E-07
188.86	1.65E-07
188.96 189.06	1.54E-07 2.07E-07
189.16	1.61E-07
189.26	2.11E-07
189.36 189.46	1.99E-07 1.62E-07
189.56	2.53E-07
189.66	1.95E-07
189.76 189.86	2.00E-07 1.97E-07
189.96	1.90E-07
190.06	1.83E-07
190.16	1.67E-07
190.26 190.36	1.67E-07 1.83E-07
190.46	2.05E-07
190.56	1.81E-07
190.66 190.76	1.52E-07 1.62E-07
190.86	2.01E-07
190.96	1.65E-07
191.06 191.16	1.73E-07 1.59E-07
191.25	2.61E-07
191.35	1.24E-07
191.45 191.55	1.88E-07
191.55	1.57E-07 2.05E-07
191.75	1.63E-07
191.85	1.32E-07
191.95 192.05	1.46E-07 2.02E-07
192.15	1.51E-07
192.25	1.63E-07
192.35 192.45	1.64E-07 1.74E-07
192.55	1.24E-07
192.65	1.90E-07
192.75 192.85	1.62E-07 1.32E-07
192.05	1.40E-07
193.05	1.66E-07
193.15	1.66E-07
193.25 193.35	1.80E-07 1.61E-07
193.45	1.38E-07
193.55	1.93E-07
193.65 193.75	1.50E-07 1.59E-07
193.85	1.57E-07
193.95	1.31E-07
194.05 194.15	2.06E-07 1.90E-07
194.25	1.55E-07
194.35	1.12E-07
194.45 194.55	2.12E-07 1.44E-07
194.65	1.81E-07
194.74	1.12E-07
194.84 194.94	1.55E-07 1.76E-07
195.04	1.33E-07
195.14	1.45E-07
195.24 195.34	1.57E-07
195.34 195.44	1.56E-07 1.61E-07
195.54	2.15E-07
195.64	1.51E-07
195.74 195.84	1.13E-07 1.48E-07
195.94	1.73E-07
196.04	1.21E-07
196.14	1.55E-07



#### U10-025

ftbgs m³/kg

### U10-043

ftbgs m³/kg

Depth Mag Susc Depth Mag Susc ft bas m<sup>3</sup>/kg ft bas m<sup>3</sup>/kg

Depth	Mag Susc
ft bgs	m³/kg
196.24	1.52E-07
196.34 196.44	1.54E-07 1.74E-07
196.54	1.78E-07
196.64	1.69E-07
196.74 196.84	2.02E-07 1.83E-07
196.94	1.42E-07
197.04	1.18E-07
197.14 197.24	1.84E-07 1.62E-07
197.34	1.72E-07
197.44	1.63E-07
197.54 197.64	1.65E-07 7.98E-08
197.04	2.23E-07
197.84	1.20E-07
197.94 198.04	1.48E-07
198.04	1.84E-07 1.40E-07
198.23	1.62E-07
198.33	1.91E-07
198.43 198.53	1.82E-07 1.75E-07
198.63	1.85E-07
198.73	2.08E-07
198.83 198.93	1.44E-07 1.20E-07
198.93	2.12E-07
199.13	1.76E-07
199.23	2.06E-07
199.33 199.43	1.89E-07 1.84E-07
199.53	1.77E-07
199.63	1.49E-07
199.73	1.56E-07
199.83 199.93	1.41E-07 1.38E-07
200.03	1.85E-07
200.13	1.48E-07
200.23 200.33	2.23E-07 1.30E-07
200.43	1.06E-07
200.53	1.94E-07
200.63 200.73	1.84E-07 1.56E-07
200.73	1.83E-07
200.93	1.40E-07
201.03	1.26E-07
201.13 201.23	1.97E-07 1.94E-07
201.33	2.05E-07
201.43	1.88E-07
201.52 201.62	1.77E-07 1.61E-07
201.72	1.27E-07
201.82	1.94E-07
201.92 202.02	1.85E-07 1.37E-07
202.02	1.61E-07
202.22	1.39E-07
202.32	2.05E-07
202.42 202.52	1.79E-07 1.48E-07
202.62	1.57E-07
202.72	1.75E-07
202.82 202.92	1.68E-07 2.02E-07
203.02	1.82E-07
203.12	1.45E-07
203.22 203.32	1.58E-07 2.01E-07
203.42	1.45E-07
203.52	1.76E-07
203.62	1.48E-07
203.72 203.82	1.33E-07 1.52E-07
203.92	1.89E-07
204.02	1.60E-07
204.12 204.22	1.57E-07 1.69E-07
204.22	1.33E-07
204.42	2.25E-07
204.52	2.23E-07

U10-043

Depth Mag Susc

ftbgs m³/kg

#### **U10-51 SONDE DATA AND STATS**

Depth	Mag Susc
ft bgs	m <sup>3</sup> /kg
204.62	1.10E-07
204.72	1.55E-07
204.82	1.77E-07
204.92	1.66E-07
205.01	1.55E-07
205.11	2.30E-07
205.21	1.71E-07
205.31	2.32E-07
205.41	1.62E-07
205.51	1.82E-07
205.61	2.11E-07
205.71	1.66E-07
205.81	1.89E-07
205.91	1.88E-07
206.01	1.60E-07
206.11	1.83E-07
206.21	1.81E-07
206.31	2.39E-07
206.41	1.63E-07
206.51	1.19E-07
206.61	1.51E-07
206.71	1.55E-07
206.81	1.23E-07
206.91	1.75E-07
207.01	1.81E-07
207.11	1.58E-07

#### SUMMARY STATS FOR THE SHALLOW INTERVAL - 4-33 feet bgs

	0 1001 890
Mean	2.61E-07
Standard Error	3.59E-09
Median	2.53E-07
Mode	#N/A
Standard Deviation	6.14E-08
Sample Variance	3.77E-15
Kurtosis	1.625866
Skewness	0.903494
Range	3.73E-07
Minimum	1.31E-07
Maximum	5.04E-07
Sum	7.62E-05
Count	292
Confidence Level(95.0%)	7.07E-09

#### SUMMARY STATS FOR THE DEEP INTERVAL 50-185 ft

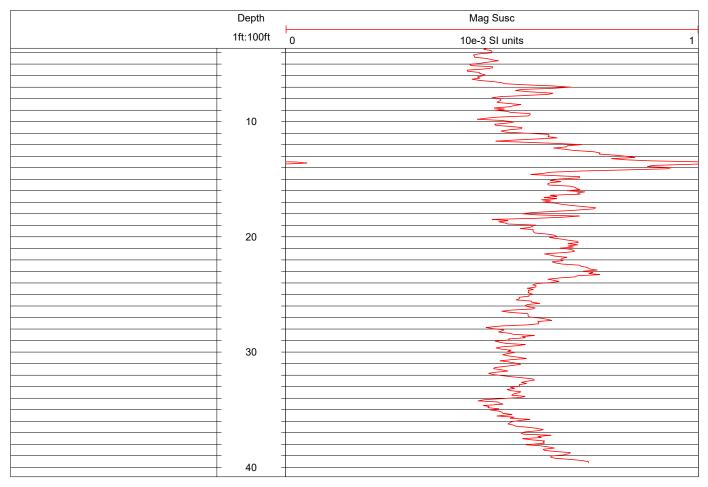
Mean	2.33E-07
Standard Error	1.37E-09
Median	2.31E-07
Mode	2.59E-07
Standard Deviation	5.05E-08
Sample Variance	2.55E-15
Kurtosis	-0.36649
Skewness	0.20777
Range	3.14E-07
Minimum	6.48E-08
Maximum	3.79E-07
Sum	0.000315
Count	1352
Confidence Level(95.0%)	2.7E-09



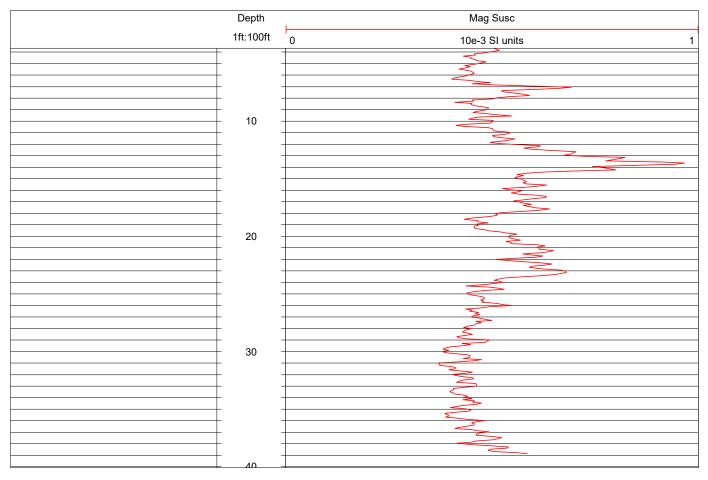
U10-025

Depth Mag Susc

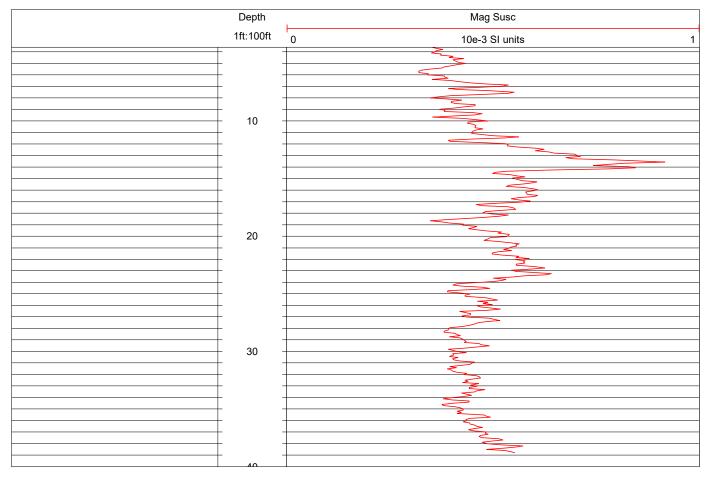
- AV	L	TOOL HMA-453-S
		CALIBRATION DATE/TIME 7/27/16 16:25
WIEDEMEIER		CALIBRATION STANDARDS 0 and 5E-3 SI Units
& ASSOC	IATES	CALIBRATION RESULTS 0 = 224.375 and 5E-3 = 1281.87 cps
PROJECT	ESTCP 201584	DEPTH TO WATER, TD 14.45 ft BTOC; 41.87 ft BGS
LOCATION	Hill AFB Operable Unit 10	
WELL	U10-025 Up - Run 1	CASING INNER DIAMETER 2"
LOGGER	T.H. Wiedemeier	REMARKS
DATE	7/27/16	



776		TOOL HMA-453-S
		CALIBRATION DATE/TIME 7/27/16 16:25
WIEDEMEIER		CALIBRATION STANDARDS 0 and 5E-3 SI Units
& ASSOC	IATES	CALIBRATION RESULTS 0 = 224.38 and 5E-3 = 1281.87
PROJECT	ESTCP 201584	DEPTH TO WATER, TD 14.45 ft BTOC; 41.87 ft BGS
LOCATION	Hill AFB Operable Unit 10	
WELL	U10-025 Down Run 2	CASING INNER DIAMETER 2"
LOGGER	T.H. Wiedemeier	REMARKS
DATE	7/27/16	



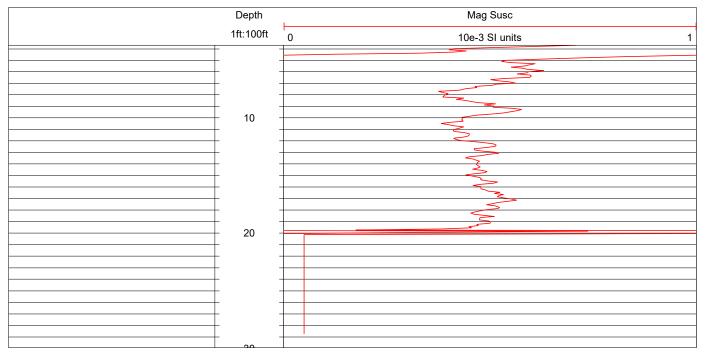
4	F	TOOL HMA-453-S
		CALIBRATION DATE/TIME 7/27/16 1625
WIEDEMEIER		CALIBRATION STANDARDS 0 and 5E-3 SI Units
& ASSOC	IATES	CALIBRATION RESULTS 0 = 224.38 and 5E-3 = 1281.87
PROJECT	ESTCP 201584	DEPTH TO WATER. TD 14.45 ft BTOC; 41.87 ft BGS
LOCATION	Hill AFB Operable Unit 10	
WELL	U10-025 Up - Run 2	CASING INNER DIAMETER 2"
LOGGER	T.H. Wiedemeier	REMARKS
DATE	7/27/16	



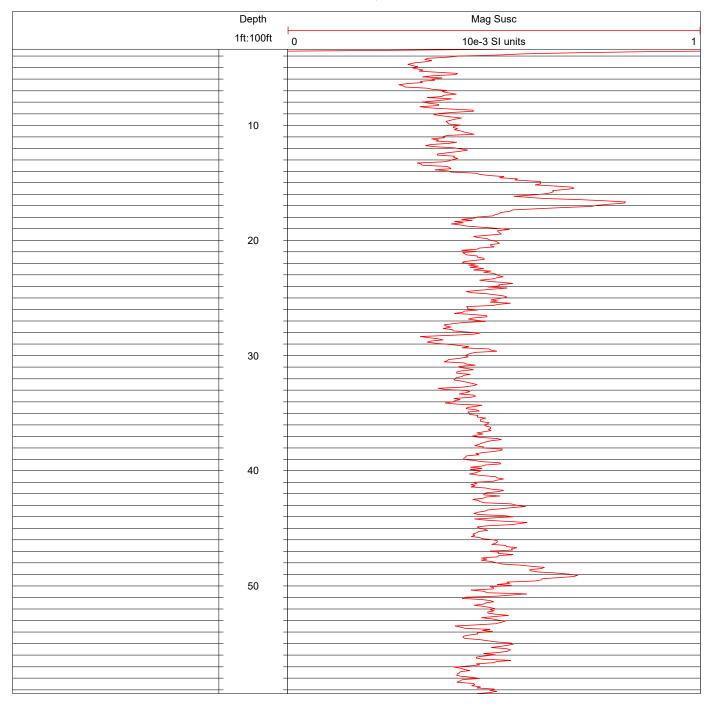
- - A	L	TOOL HMA-453-S
		CALIBRATION DATE/TIME 7/27/16 11:10
WIEDEMEIER		CALIBRATION STANDARDS 0 and 5E-3 SI Units
& ASSOC	IATES	CALIBRATION RESULTS 0=213.33 and 5E-3 = 1335.6 cps
PROJECT	ESTCP 201584	DEPTH TO WATER. TD 10.55 ft BTOC, 30.38 ft BGS
LOCATION	Hill AFB Operable Unit 10	
WELL	U10-043 Down	CASING INNER DIAMETER 2
LOGGER	T.H. Wiedemeier	REMARKS
DATE	7/27/16	Strange Response at 20 ft BGS. Metal in Well?
L		<u> </u> ]

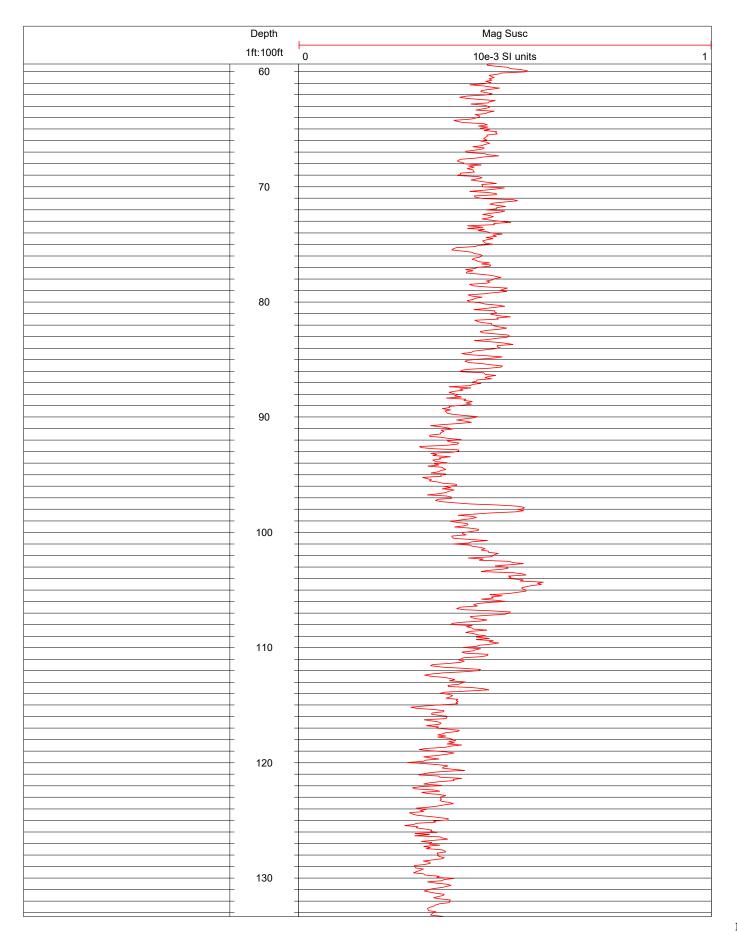
[	Depth	Mag Susc
1f	ft:100ft	0 10e-3 SI units 2
	-	
	-	
	-	
	10 -	
	-	
	-	
	-	
	-	
	20 -	
	-	
	-	
	-	
	-	
	- 20	

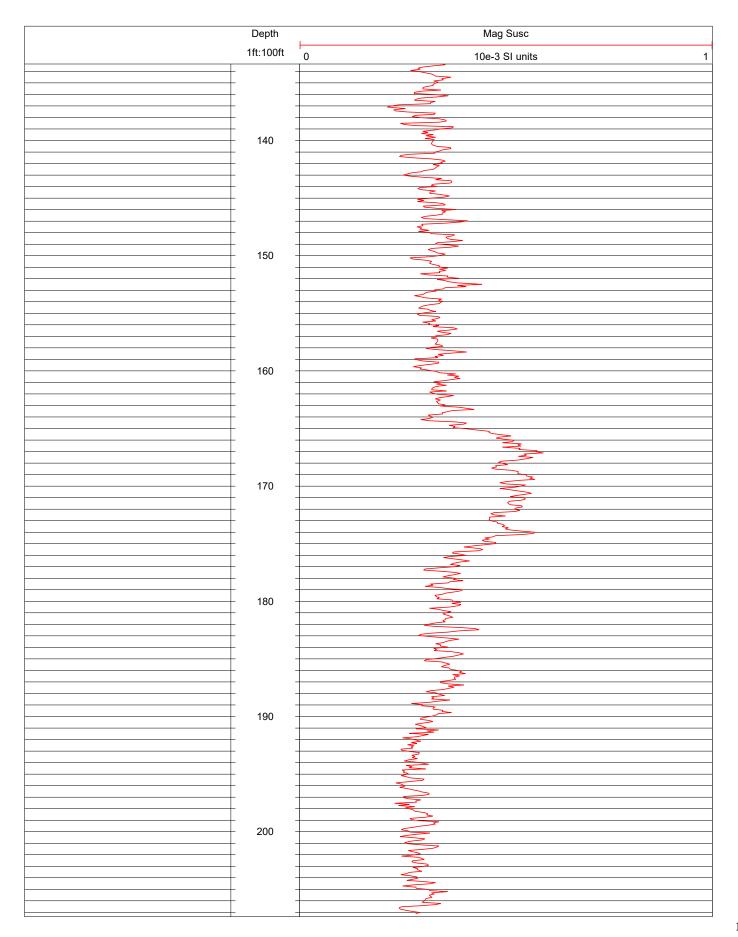
<b>₩</b>		TOOLHMA-453-SCALIBRATION DATE/TIME7/27/16, 11:10
<b>WIEDEMEIER</b> & ASSOCIATES		CALIBRATION STANDARDS 0 and 5E-3 SI Units CALIBRATION RESULTS 0 = 213.33 and 5E-3 = 1335.6 cps
PROJECT	ESTCP 201584	DEPTH TO WATER, TD 10.55 ft BTOC, 30.38 ft BGS
LOCATION	Hill AFB Operable Unit 10	
WELL	U10-043 Up	CASING INNER DIAMETER 2"
LOGGER	T.H. Wiedemeier	REMARKS
DATE	7/27/16	Metal in well at ~20 ft BGS



7	L	TOOL HMA-453-S
		CALIBRATION DATE/TIME 7/27/16, 16:25
WIEDEMEIER		CALIBRATION STANDARDS 0 and 5E-3 SI Units
& ASSO	CIATES	CALIBRATION RESULTS 0 = 224.375 and 5E-3 = 1281.87 cps
PROJECT	ESTCP 201584	DEPTH TO WATER. TD
LOCATION	Hill AFB Operable Unit 10	
WELL	U10-051 Up	CASING INNER DIAMETER 4"
LOGGER	T.H. Wiedemeier	REMARKS
DATE	7/27/16 at 19:03	Used U10-025 Calib because of overhead wires and transformer







Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 1

Depth	Mag Susc	Mag Susc
ft bgs	10e-3 SI units	m <sup>3</sup> /kg
3.53	0.206945	1.21732E-07
3.63	0.281035	1.65315E-07
3.73	0.235039	1.38258E-07
3.84	0.215387	1.26698E-07
3.94	0.1795885	1.0564E-07
4.04	0.1878875	1.10522E-07
4.135	0.1530485	9.00285E-08
4.235	0.1680189	9.88346E-08
4.335	0.2198645	1.29332E-07
4.435	0.18366	1.08035E-07
4.535	0.2198005	1.29294E-07
4.635	0.196391	1.15524E-07
4.735	0.2159235	1.27014E-07
4.835	0.190641	1.12142E-07
4.935	0.217026	1.27662E-07
5.035	0.217414	1.27891E-07
5.135	0.1753915	1.03171E-07
5.235	0.225085	1.32403E-07
5.335	0.1740585	1.02387E-07
5.435	0.1982115	1.16595E-07
5.535	0.218373	1.28455E-07
5.635	0.2184505	1.285E-07
5.735	0.193147	1.13616E-07
5.835	0.2068045	1.2165E-07
5.935	0.2367195	1.39247E-07
6.03	0.1849475	1.08793E-07
6.13	0.215298	1.26646E-07
6.23	0.2270895	1.33582E-07
6.33	0.2061265	1.21251E-07
6.43	0.2049035	1.20531E-07
6.53	0.2253525	1.3256E-07
6.63	0.1863265	1.09604E-07
6.73	0.1899375	1.11728E-07
6.83	0.190751	1.12206E-07
6.93	0.17973	1.05724E-07
7.03	0.261364	1.53744E-07
7.13	0.1732625	1.01919E-07
7.23	0.207729	1.22194E-07
7.33	0.196908	1.15828E-07
7.425	0.217219	1.27776E-07
7.525	0.1984745	1.1675E-07
7.625	0.21287	1.25218E-07
7.725	0.1920775	1.12987E-07
7.825	0.25823	1.519E-07
7.925	0.2001545	1.17738E-07
8.025	0.2395705	1.40924E-07
8.125	0.2436885	1.43346E-07



Depth	Mag Susc	Mag Susc
ft bgs	10e-3 SI units	m <sup>3</sup> /kg
8.225	0.2268185	1.33423E-07
8.325	0.247283	1.45461E-07
8.425	0.2484425	1.46143E-07
8.525	0.2667115	1.56889E-07
8.625	0.250434	1.47314E-07
8.725	0.235691	1.38642E-07
8.825	0.2476585	1.45681E-07
8.925	0.3062105	1.80124E-07
9.025	0.28471	1.67476E-07
9.125	0.2980755	1.75339E-07
9.225	0.3088785	1.81693E-07
9.325	0.2840735	1.67102E-07
9.42	0.2992635	1.76037E-07
9.52	0.25577	1.50453E-07
9.62	0.3359045	1.97591E-07
9.72	0.3434735	2.02043E-07
9.82	0.33217	1.95394E-07
9.92	0.27773	1.63371E-07
10.02	0.361375	2.12574E-07
10.12	0.3503825	2.06107E-07
10.22	0.3296415	1.93907E-07
10.32	0.3482175	2.04834E-07
10.42	0.2894955	1.70291E-07
10.52	0.3163575	1.86093E-07
10.62	0.318099	1.87117E-07
10.72	0.286294	1.68408E-07
10.815	0.2656335	1.56255E-07
10.915	0.3237865	1.90463E-07
11.015	0.2822255	1.66015E-07
11.115	0.28905	1.70029E-07
11.215	0.3266695	1.92159E-07
11.315	0.2829115	1.66419E-07
11.415	0.329946	1.94086E-07
11.515	0.27559	1.62112E-07
11.615	0.305425	1.79662E-07
11.715	0.27033	1.59018E-07
11.815	0.220557	1.29739E-07
11.915	0.283389	1.66699E-07
12.015	0.3372505	1.98383E-07
12.115	0.3042295	1.78959E-07
12.215	0.2692945	1.58409E-07
12.315	0.275889	1.62288E-07
12.415	0.3529025	2.0759E-07
12.515	0.345433	2.03196E-07
12.615	0.281335	1.65491E-07
12.71	0.3244135	1.90831E-07
12.81	0.3209475	1.88793E-07



Depth	Mag Susc	Mag Susc
ft bgs	10e-3 SI units	m³/kg
12.91	0.360913	2.12302E-07
13.01	0.2858065	1.68121E-07
13.11	0.392107	2.30651E-07
13.21	0.3810905	2.24171E-07
13.31	0.387758	2.28093E-07
13.41	0.3712485	2.18381E-07
13.51	0.389948	2.29381E-07
13.61	0.3857895	2.26935E-07
13.71	0.451197	2.6541E-07
13.81	0.4643955	2.73174E-07
13.91	0.443728	2.61016E-07
14.01	0.4958385	2.9167E-07
14.105	0.4494485	2.64381E-07
14.205	0.430615	2.53303E-07
14.305	0.4320525	2.54149E-07
14.405	0.4429225	2.60543E-07
14.505	0.376105	2.21238E-07
14.605	0.4177145	2.45714E-07
14.705	0.3722625	2.18978E-07
14.805	0.4107165	2.41598E-07
14.905	0.428343	2.51966E-07
15.005	0.4414135	2.59655E-07
15.105	0.407592	2.3976E-07
15.205	0.346134	2.03608E-07
15.305	0.392078	2.30634E-07
15.405	0.4580905	2.69465E-07
15.505	0.381892	2.24642E-07
15.605	0.3659755	2.1528E-07
15.705	0.362373	2.13161E-07
15.805	0.393872	2.31689E-07
15.905	0.4050095	2.38241E-07
16.000	0.3931615	2.31271E-07
16.1	0.363765	2.13979E-07
16.2	0.3461415	2.03613E-07
16.3	0.4744665	2.79098E-07
16.4	0.4670225	2.74719E-07
16.5	0.515486	3.03227E-07
16.6	0.426028	2.50605E-07
16.7	0.3713985	2.1847E-07
16.8	0.3841925	2.25996E-07
16.9	0.4553695	2.67864E-07
10.9	0.431301	2.53706E-07
17.1	0.4355795	2.56223E-07
17.1	0.4355795	2.49859E-07
17.2	0.3778755	2.49859E-07 2.2228E-07
17.3	0.3778755	
17.4	0.4197255	2.43904E-07 2.46897E-07
17.490	0.4197200	2.40091E-01



Depth	Mag Susc	Mag Susc
ft bgs	10e-3 SI units	m <sup>3</sup> /kg
17.595	0.427253	2.51325E-07
17.695	0.4362835	2.56637E-07
17.795	0.402828	2.36958E-07
17.895	0.3716895	2.18641E-07
17.995	0.42081	2.47535E-07
18.095	0.448994	2.64114E-07
18.195	0.4925965	2.89763E-07
18.295	0.578711	3.40418E-07
18.395	0.5069765	2.98221E-07
18.495	0.504192	2.96584E-07
18.595	0.5145565	3.0268E-07
18.695	0.5540725	3.25925E-07
18.795	0.45717	2.68924E-07
18.895	0.479401	2.82001E-07
18.995	0.4430365	2.6061E-07
19.095	0.4784665	2.81451E-07
19.195	0.405122	2.38307E-07
19.295	0.407267	2.39569E-07
19.39	0.4062565	2.38974E-07
19.49	0.3405105	2.003E-07
19.59	0.409796	2.41056E-07
19.69	0.4354275	2.56134E-07
19.09	0.432488	2.54405E-07
19.89	0.4496335	2.6449E-07
19.99	0.385124	2.26544E-07
20.09	0.417604	2.45649E-07
20.03	0.4346445	2.55673E-07
20.19	0.42724	2.51318E-07
20.29	0.4858235	2.85779E-07
20.39	0.4465095	2.62653E-07
20.49	0.3803225	2.23719E-07
20.59	0.346421	2.03777E-07
20.09	0.2844175	1.67304E-07
20.785	0.2767415	1.62789E-07
20.885	0.247473	1.45572E-07
20.985	0.2020735	1.18867E-07
21.085	0.1595515	9.38538E-08
21.105	0.1166708	6.86299E-08
21.285	0.158861	9.34476E-08
21.385	0.1462765	8.6045E-08
21.585	0.136482	8.02835E-08
		6.53977E-08
21.685	0.1111761	
21.785	0.1230828	7.24016E-08
21.885	0.2048615	1.20507E-07
21.985	0.23032635	1.35486E-07
22.085	0.3219955 0.279094	1.89409E-07
22.185	0.279094	1.64173E-07



Depth	Mag Susc	Mag Susc
ft bgs	10e-3 SI units	m³/kg
22.285	0.254495	1.49703E-07
22.385	0.2693045	1.58414E-07
22.485	0.3369405	1.982E-07
22.585	0.328369	1.93158E-07
22.68	0.297388	1.74934E-07
22.78	0.219047	1.28851E-07
22.88	0.1344725	7.91015E-08
22.98	0.1552365	9.13156E-08
23.08	0.1664855	9.79326E-08
23.18	0.1565505	9.20885E-08
23.28	0.2275135	1.33831E-07
23.38	0.1518585	8.93285E-08
23.48	0.2158085	1.26946E-07
23.58	0.2083395	1.22553E-07
23.68	0.245417	1.44363E-07
23.78	0.2811895	1.65406E-07
23.88	0.3111005	1.83E-07
23.98	0.312463	1.83802E-07
24.075	0.4066485	2.39205E-07
24.175	0.453674	2.66867E-07
24.275	0.438149	2.57735E-07
24.375	0.4347685	2.55746E-07
24.475	0.4434965	2.6088E-07
24.575	0.3895695	2.29159E-07
24.675	0.3908015	2.29883E-07
24.775	0.3644165	2.14363E-07
24.875	0.3574375	2.10257E-07
24.975	0.273459	1.60858E-07
25.075	0.3059105	1.79947E-07
25.175	0.299719	1.76305E-07
25.275	0.3231925	1.90113E-07
25.375	0.3642185	2.14246E-07
25.475	0.349047	2.05322E-07
25.575	0.292398	1.71999E-07
25.675	0.344726	2.0278E-07
25.775	0.3359575	1.97622E-07
25.875	0.3194735	1.87926E-07
25.97	0.297649	1.75088E-07
26.07	0.303819	1.78717E-07
26.17	0.2750915	1.61819E-07
26.27	0.2997945	1.7635E-07
26.37	0.285384	1.67873E-07
26.47	0.2883815	1.69636E-07
26.57	0.309782	1.82225E-07
26.67	0.29281	1.72241E-07
26.77	0.293942	1.72907E-07
26.87	0.295942	1.67662E-07
20.07	0.200020	1.070022-07



Depth	Mag Susc	Mag Susc
ft bgs	10e-3 SI units	m <sup>3</sup> /kg
26.97	0.314637	1.85081E-07
27.07	0.29139	1.71406E-07
27.17	0.3479575	2.04681E-07
27.27	0.342658	2.01564E-07
27.365	0.2946815	1.73342E-07
27.465	0.403155	2.3715E-07
27.565	0.3693985	2.17293E-07
27.665	0.413222	2.43072E-07
27.765	0.3536495	2.08029E-07
27.865	0.292689	1.7217E-07
27.965	0.3641545	2.14209E-07
28.065	0.3495185	2.05599E-07
28.165	0.411663	2.42155E-07
28.265	0.3259255	1.91721E-07
28.365	0.369658	2.17446E-07
28.465	0.3247645	1.91038E-07
28.565	0.352418	2.07305E-07
28.665	0.3892065	2.28945E-07
28.765	0.3562605	2.09565E-07
28.865	0.357698	2.10411E-07
28.965	0.380116	2.23598E-07
29.065	0.3341305	1.96547E-07
29.165	0.365273	2.14866E-07
29.265	0.38359	2.25641E-07
29.36	0.3649765	2.14692E-07
29.46	0.3355565	1.97386E-07
29.56	0.289534	1.70314E-07
29.66	0.2411365	1.41845E-07
29.76	0.2544805	1.49694E-07
29.86	0.299897	1.7641E-07
29.96	0.1941405	1.142E-07
30.06	0.28707	1.68865E-07
30.16	0.2082705	1.22512E-07
30.26	0.24991	1.47006E-07
30.36	0.2455895	1.44464E-07
30.46	0.272966	1.60568E-07
30.56	0.224944	1.3232E-07
30.66	0.2667355	1.56903E-07
30.755	0.2603885	1.5317E-07
30.855	0.223761	1.31624E-07
30.955	0.2201545	1.29503E-07
31.055	0.282127	1.65957E-07
31.155	0.286082	1.68284E-07
31.255	0.3063935	1.80231E-07
31.355	0.2846055	1.67415E-07
31.455	0.282684	1.66285E-07
31.555	0.2669585	1.57034E-07



Depth	Mag Susc	Mag Susc
ft bgs	10e-3 SI units	m³/kg
31.655	0.276376	1.62574E-07
31.755	0.2960155	1.74127E-07
31.855	0.2533745	1.49044E-07
31.955	0.2455895	1.44464E-07
32.055	0.2427895	1.42817E-07
32.155	0.283364	1.66685E-07
32.255	0.258953	1.52325E-07
32.355	0.2981545	1.75385E-07
32.455	0.2156045	1.26826E-07
32.555	0.266842	1.56966E-07
32.65	0.2512115	1.47771E-07
32.75	0.233804	1.37532E-07
32.85	0.2496045	1.46826E-07
32.95	0.2776805	1.63341E-07
33.05	0.3065445	1.8032E-07
33.15	0.25075	1.475E-07
33.25	0.262473	1.54396E-07
33.35	0.246935	1.45256E-07
33.45	0.2153215	1.2666E-07
33.55	0.266699	1.56882E-07
33.65	0.298939	1.75846E-07
33.75	0.209965	1.23509E-07
33.85	0.269489	1.58523E-07
33.95	0.293948	1.72911E-07
34.045	0.2503865	1.47286E-07
34.145	0.218163	1.28331E-07
34.245	0.2650415	1.55907E-07
34.345	0.258747	1.52204E-07
34.445	0.2899835	1.70579E-07
34.545	0.2827925	1.66349E-07
34.645	0.264738	1.55728E-07
34.745	0.28702	1.68835E-07
34.845	0.307141	1.80671E-07
34.945	0.3233605	1.90212E-07
35.045	0.337236	1.98374E-07
35.145	0.275176	1.61868E-07
35.245	0.284355	1.67268E-07
35.345	0.2733275	1.60781E-07
35.445	0.322218	1.8954E-07
35.545	0.293047	1.72381E-07
35.645	0.3175735	1.86808E-07
35.745	0.31929	1.87818E-07
35.845	0.359404	2.11414E-07
35.94	0.2972425	1.74849E-07
36.04	0.3095445	1.82085E-07
36.14	0.335939	1.97611E-07
36.14 36.24	0.342204	2.01296E-07
00.24	0.042204	2.012302-07



Depth	Mag Susc	Mag Susc
ft bgs	10e-3 SI units	m <sup>3</sup> /kg
36.34	0.3275575	1.92681E-07
36.44	0.3407265	2.00427E-07
36.54	0.343403	2.02002E-07
36.64	0.353614	2.08008E-07
36.74	0.3296745	1.93926E-07
36.84	0.384416	2.26127E-07
36.94	0.324342	1.90789E-07
37.04	0.3239965	1.90586E-07
37.14	0.3144665	1.8498E-07
37.24	0.33769	1.98641E-07
37.335	0.3205715	1.88571E-07
37.435	0.3416095	2.00947E-07
37.535	0.340249	2.00146E-07
37.635	0.3088075	1.81651E-07
37.735	0.2739955	1.61174E-07
37.835	0.316225	1.86015E-07
37.935	0.3829525	2.25266E-07
38.035	0.3372875	1.98404E-07
38.135	0.3759425	2.21143E-07
38.235	0.3549475	2.08793E-07
38.335	0.291574	1.71514E-07
38.435	0.3522515	2.07207E-07
38.535	0.392149	2.30676E-07
38.635	0.4008645	2.35803E-07
38.735	0.36	2.11765E-07
38.835	0.3722505	2.18971E-07
38.935	0.334177	1.96575E-07
39.035	0.3498265	2.0578E-07
39.135	0.3599125	2.11713E-07
39.23	0.354996	2.08821E-07
39.33	0.3568275	2.09899E-07
39.43	0.349371	2.05512E-07
39.53	0.300241	1.76612E-07
39.63	0.3190605	1.87683E-07
39.73	0.324732	1.91019E-07
39.83	0.2964065	1.74357E-07
39.93	0.3090635	1.81802E-07
40.03	0.2444835	1.43814E-07
40.13	0.325648	1.91558E-07
40.23	0.3116165	1.83304E-07
40.33	0.307962	1.81154E-07
40.43	0.3054205	1.79659E-07
40.53	0.318734	1.87491E-07
40.63	0.2687945	1.58114E-07
40.725	0.263684	1.55108E-07
40.825	0.2752175	1.61893E-07
40.925	0.298448	1.75558E-07
10.020	0.200770	1.1 00002-01



Depth	Mag Susc	Mag Susc
ft bgs	10e-3 SI units	m <sup>3</sup> /kg
41.025	0.290412	1.70831E-07
41.125	0.2752865	1.61933E-07
41.225	0.3462435	2.03673E-07
41.325	0.2939245	1.72897E-07
41.425	0.3087205	1.816E-07
41.525	0.32238	1.89635E-07
41.625	0.299374	1.76102E-07
41.725	0.3066565	1.80386E-07
41.825	0.319521	1.87954E-07
41.925	0.3947665	2.32216E-07
42.025	0.3033325	1.78431E-07
42.125	0.304931	1.79371E-07
42.225	0.323157	1.90092E-07
42.325	0.3166115	1.86242E-07
42.425	0.293698	1.72764E-07
42.525	0.2783145	1.63714E-07
42.62	0.2573975	1.5141E-07
42.72	0.3034155	1.7848E-07
42.82	0.290978	1.71164E-07
42.92	0.3624555	2.13209E-07
43.02	0.358581	2.1093E-07
43.12	0.3467115	2.03948E-07
43.22	0.346128	2.03605E-07
43.32	0.3733095	2.19594E-07
43.42	0.373141	2.19495E-07
43.52	0.3338605	1.96389E-07
43.62	0.3332615	1.96036E-07
43.72	0.309044	1.81791E-07
43.82	0.353718	2.08069E-07
43.92	0.423136	2.48904E-07
44.015	0.424504	2.49708E-07
44.115	0.4045055	2.37944E-07
44.215	0.3964745	2.3322E-07
44.315	0.366134	2.15373E-07
44.415	0.367519	2.16188E-07
44.515	0.3244785	1.9087E-07
44.615	0.326501	1.92059E-07
44.715	0.332277	1.95457E-07
44.815	0.303699	1.78646E-07
44.915	0.321197	1.88939E-07
45.015	0.3707915	2.18113E-07
45.115	0.346539	2.03846E-07
45.215	0.3896315	2.29195E-07
45.315	0.3940625	2.31801E-07
45.415	0.3251295	1.91253E-07
45.515	0.387536	2.27962E-07
45.615	0.4725705	2.77983E-07



Depth	Mag Susc	Mag Susc
ft bgs	10e-3 SI units	m³/kg
45.715	0.3769535	2.21737E-07
45.815	0.435333	2.56078E-07
45.91	0.4344595	2.55564E-07
46.01	0.457011	2.6883E-07
46.11	0.3904885	2.29699E-07
46.21	0.3786275	2.22722E-07
46.31	0.494612	2.90948E-07
46.41	0.536664	3.15685E-07
46.51	0.5797885	3.41052E-07
46.61	0.595356	3.50209E-07
46.71	0.629452	3.70266E-07
46.81	0.58078	3.41635E-07
46.91	0.55903	3.28841E-07
47.01	0.567297	3.33704E-07
47.11	0.532653	3.13325E-07
47.21	0.4007815	2.35754E-07
47.305	0.3976025	2.33884E-07
47.405	0.441467	2.59686E-07
47.505	0.4660515	2.74148E-07
47.605	0.515719	3.03364E-07
47.705	0.426044	2.50614E-07
47.805	0.3578725	2.10513E-07
47.905	0.414495	2.43821E-07
48.005	0.453628	2.6684E-07
48.105	0.428247	2.5191E-07
48.205	0.406783	2.39284E-07
48.305	0.4497985	2.64587E-07
48.405	0.418546	2.46204E-07
48.505	0.438326	2.57839E-07
48.605	0.435894	2.56408E-07
48.705	0.4164235	2.44955E-07
48.805	0.3874965	2.27939E-07
48.905	0.3734005	2.19647E-07
49.005	0.335272	1.97219E-07
49.105	0.3721975	2.1894E-07
49.2	0.318547	1.87381E-07
49.3	0.3534595	2.07917E-07
49.4	0.409203	2.40708E-07
49.5	0.369827	2.17545E-07
49.6	0.343503	2.02061E-07
49.7	0.456818	2.68716E-07
49.8	0.4146235	2.43896E-07
49.9	0.4056755	2.38633E-07
	0.3035825	1.78578E-07
50.1	0.2997215	1.76307E-07
50.1 50.2	0.333067	1.95922E-07
50.2 50.3	0.356175	2.09515E-07
50.5	0.000170	2.000100-07



Depth	Mag Susc	Mag Susc
ft bgs	10e-3 SI units	m <sup>3</sup> /kg
50.4	0.3483675	2.04922E-07
50.5	0.341626	2.00956E-07
50.6	0.349736	2.05727E-07
50.695	0.33322	1.96012E-07
50.795	0.3980615	2.34154E-07
50.895	0.3399465	1.99969E-07
50.995	0.3844025	2.26119E-07
51.095	0.412965	2.42921E-07
51.195	0.4320355	2.54139E-07
51.295	0.4216305	2.48018E-07
51.395	0.4046875	2.38051E-07
51.495	0.433148	2.54793E-07
51.595	0.4324835	2.54402E-07
51.695	0.456132	2.68313E-07
51.795	0.462979	2.72341E-07
51.895	0.4845745	2.85044E-07
51.995	0.4198115	2.46948E-07
52.095	0.4700165	2.7648E-07
52.195	0.4076065	2.39769E-07
52.295	0.45797	2.69394E-07
52.395	0.4136455	2.43321E-07
52.495	0.4261235	2.50661E-07
52.59	0.4936355	2.90374E-07
52.69	0.478889	2.81699E-07
52.79	0.5035605	2.96212E-07
52.89	0.450261	2.64859E-07
52.99	0.4557445	2.68085E-07
53.09	0.4002385	2.35434E-07
53.19	0.2994895	1.7617E-07
53.29	0.3282535	1.9309E-07
53.39	0.262226	1.54251E-07
53.49	0.303073	1.78278E-07
53.59	0.20689	1.217E-07
53.69	0.2819625	1.6586E-07
53.79	0.289067	1.70039E-07
53.89	0.342586	2.01521E-07
53.985	0.471986	2.77639E-07
54.085	0.4516005	2.65647E-07
54.185	0.512605	3.01532E-07
54.285	0.552195	3.24821E-07
54.385	0.526153	3.09502E-07
54.485	0.523868	3.08158E-07
54.585	0.522869	3.0757E-07
54.685	0.5307715	3.12219E-07
54.785	0.38574	2.26906E-07
54.885	0.3509325	2.06431E-07
54.985	0.300757	1.76916E-07



Depth	Mag Susc	Mag Susc		
ft bgs	10e-3 SI units	m³/kg		
55.085	0.2526665	1.48627E-07		
55.185	0.2089425	1.22907E-07		
55.285	0.1865875 1.09757E-0			
55.385	0.248458 1.46152E-07			
55.485	0.2518925	1.48172E-07		
55.585	0.226915	1.33479E-07		
55.685	0.199759	1.17505E-07		
55.785	0.206361	1.21389E-07		
55.88	0.204251	1.20148E-07		
55.98	0.254694	1.4982E-07		
56.08	0.2077955	1.22233E-07		
56.18	0.224286	1.31933E-07		
56.28	0.2549685	1.49981E-07		
56.38	0.202451	1.19089E-07		
56.48	0.2068615	1.21683E-07		
56.58	0.2478725	1.45807E-07		
56.68	0.238387	1.40228E-07		
56.78	0.232473	1.36749E-07		
56.88	0.2185695	1.2857E-07		
56.98	0.2190385	1.28846E-07		
57.08	0.2554445	1.50261E-07		
57.18	0.260741	1.53377E-07		
57.275	0.2605895	1.53288E-07		
57.375	0.2143045	1.26061E-07		
57.475	0.194694	1.14526E-07		
57.575	0.2269005	1.33471E-07		
57.675	0.220087	1.29463E-07		
57.775	0.2307885	1.35758E-07		
57.875	0.2144875	1.26169E-07		
57.975	0.2099025	1.23472E-07		
58.075	0.2352915	1.38407E-07		
58.175	0.23249	1.36759E-07		
58.275	0.246225	1.44838E-07		
58.375	0.187206	1.10121E-07		
58.475	0.239136	1.40668E-07		
58.575	0.2438095	1.43417E-07		
58.675	0.2265205	1.33247E-07		
58.775	0.223692	1.31584E-07		
58.875	0.205593	1.20937E-07		
58.975	0.2370595	1.39447E-07		
59.075	0.19824	1.16612E-07		
59.17	0.277939	1.63494E-07		
59.27	0.230417	1.35539E-07		
59.37	0.23677	1.39276E-07		
59.47	0.270546	1.59145E-07		
59.57	0.291874	1.71691E-07		
59.67	0.197759	1.16329E-07		



Depth	Mag Susc	Mag Susc
ft bgs	10e-3 SI units	m <sup>3</sup> /kg
59.77	0.223827	1.31663E-07
59.87	0.2314095	1.36123E-07
59.97	0.2009335	1.18196E-07
60.07	0.2134085	1.25534E-07
60.17	0.244335	1.43726E-07
60.27	0.255067	1.50039E-07
60.37	0.2499205	1.47012E-07
60.47	0.2607995	1.53411E-07
60.57	0.26286	1.54624E-07
60.665	0.248222	1.46013E-07
60.765	0.2926445	1.72144E-07
60.865	0.267583	1.57402E-07
60.965	0.315314	1.85479E-07
61.065	0.2863555	1.68444E-07
61.165	0.303608	1.78593E-07
61.265	0.3376215	1.98601E-07
61.365	0.3471055	2.0418E-07
61.465	0.307772	1.81042E-07
61.565	0.37711	2.21829E-07
61.665	0.3842255	2.26015E-07
61.765	0.419468	2.46746E-07
61.865	0.4776325	2.8096E-07
61.965	0.428495	2.52056E-07
62.065	0.446117	2.62422E-07
62.165	0.433488	2.54993E-07
62.265	0.373502	2.19707E-07
62.365	0.3739455	2.19968E-07
62.465	0.461624	2.71544E-07
62.56	0.409549	2.40911E-07
62.66	0.3867835	2.2752E-07
62.76	0.407234	2.39549E-07
62.86	0.4059495	2.38794E-07
62.96	0.4128595	2.42859E-07
63.06	0.4849235	2.85249E-07
63.16	0.5119305	3.01136E-07
63.26	0.4097725	2.41043E-07
63.36	0.3779165	2.22304E-07
63.46	0.366654	2.15679E-07
63.56	0.303848	1.78734E-07
63.66	0.343178	2.01869E-07
63.76	0.3638055	2.14003E-07
63.86	0.381222	2.24248E-07
63.955	0.4366815	2.56871E-07
64.055	0.347488	2.04405E-07
64.155	0.324117	1.90657E-07
64.255	0.3431345	2.01844E-07
64.355	0.349367	2.0551E-07



Depth	Mag Susc	Mag Susc
ft bgs	10e-3 SI units	m³/kg
64.455	0.3440665	2.02392E-07
64.555	0.329488	1.93816E-07
64.655	0.2754985	1.62058E-07
64.755	0.286569	1.6857E-07
64.855	0.3697385	2.17493E-07
64.955	0.5380605	3.16506E-07
65.055	0.7964185	4.68481E-07
65.155	0.7333685	4.31393E-07
65.255	0.5832075	3.43063E-07
65.355	0.474028	2.7884E-07
65.455	0.4890575	2.87681E-07
65.555	0.6628825	3.89931E-07
65.655	0.672658	3.95681E-07
65.755	0.5566925	3.27466E-07
65.85	0.4106795	2.41576E-07
65.95	0.3436135	2.02126E-07
66.05	0.3307775	1.94575E-07
66.15	0.2780185	1.6354E-07
66.25	0.291217	1.71304E-07
66.35	0.2266585	1.33329E-07
66.45	0.280347	1.6491E-07
66.55	0.265972	1.56454E-07
66.65	0.287578	1.69164E-07
66.75	0.2212295	1.30135E-07
66.85	0.2518565	1.48151E-07
66.95	0.212215	1.24832E-07
67.05	0.2219855	1.3058E-07
67.15	0.2537845	1.49285E-07
67.245	0.2313825	1.36107E-07
67.345	0.300611	1.7683E-07
67.445	0.288328	1.69605E-07
67.545	0.214172	1.25984E-07
67.645	0.2767535	1.62796E-07
67.745	0.2890645	1.70038E-07
67.845	0.2357945	1.38703E-07
67.945	0.2973495	1.74911E-07
68.045	0.291741	1.71612E-07
68.145	0.302658	1.78034E-07
68.245	0.326179	1.9187E-07
68.345	0.335946	1.97615E-07
68.445	0.3660455	2.15321E-07
68.545	0.374503	2.20296E-07
68.645	0.4424955	2.60291E-07
68.745	0.399339	2.34905E-07
68.845	0.3835805	2.25636E-07
68.945	0.3799035	2.23473E-07
69.045	0.307075	1.80632E-07



Depth	Mag Susc	Mag Susc
ft bgs	10e-3 SI units	m³/kg
69.14	0.5124825	3.0146E-07
69.24	0.5614525	3.30266E-07
69.34	0.5588205	3.28718E-07
69.44	0.5983855	3.51991E-07
69.54	0.5962205	3.50718E-07
69.64	0.6619505	3.89383E-07
69.74	0.718509	4.22652E-07
69.84	0.6643795	3.90811E-07
69.94	0.513932	3.02313E-07
70.04	0.581996	3.42351E-07
70.14	0.549429	3.23194E-07
70.24	0.525723	3.09249E-07
70.34	0.4906315	2.88607E-07
70.44	0.4339655	2.55274E-07
70.54	0.465659	2.73917E-07
70.635	0.368162	2.16566E-07
70.735	0.336003	1.97649E-07
70.835	0.3111575	1.83034E-07
70.935	0.2869805	1.68812E-07
71.035	0.317124	1.86544E-07
71.135	0.29161	1.71535E-07
71.235	0.2725195	1.60306E-07
71.335	0.222315	1.30774E-07
71.435	0.2325365	1.36786E-07
71.535	0.2369945	1.39409E-07
71.635	0.2598875	1.52875E-07
71.735	0.2359805	1.38812E-07
71.835	0.2381795	1.40106E-07
71.935	0.2147185	1.26305E-07
72.035	0.1664375	9.79044E-08
72.135	0.1723885	1.01405E-07
72.235	0.2175405	1.27965E-07
72.335	0.215327	1.26663E-07
72.435	0.266256	1.56621E-07
72.53	0.3170495	1.865E-07
72.63	0.3893445	2.29026E-07
72.73	0.3959555	2.32915E-07
72.83	0.495881	2.91695E-07
72.93	0.445277	2.61928E-07
73.03	0.4669425	2.74672E-07
73.13	0.601525	3.53838E-07
73.23	0.775928	4.56428E-07
73.33	0.816988	4.80581E-07
73.43	0.796385	4.68462E-07
73.53	0.646552	3.80325E-07
73.63	0.7327525	4.31031E-07
73.73	0.779208	4.58358E-07
10.10	0.170200	



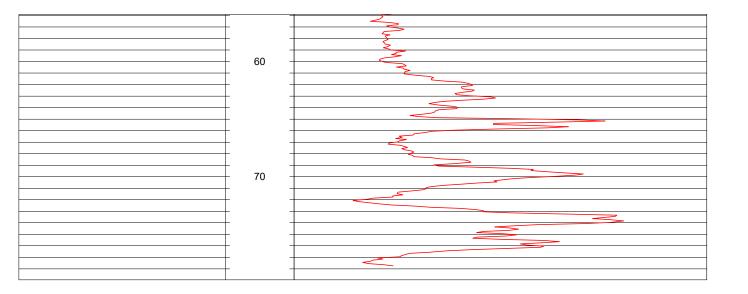
Depth	Mag Susc	Mag Susc
ft bgs	10e-3 SI units	m³/kg
73.83	0.764918	4.49952E-07
73.925	0.731292	4.30172E-07
74.025	0.598151	3.51854E-07
74.125	0.57523	3.38371E-07
74.225	0.478722	2.81601E-07
74.325	0.5078705	2.98747E-07
74.425	0.5637845	3.31638E-07
74.525	0.550171	3.2363E-07
74.625	0.493536	2.90315E-07
74.725	0.4330455	2.54733E-07
74.825	0.4703225	2.7666E-07
74.925	0.5624055	3.30827E-07
75.025	0.5846205	3.43894E-07
75.125	0.4396415	2.58613E-07
75.225	0.401451	2.36148E-07
75.325	0.463215	2.72479E-07
75.425	0.556859	3.27564E-07
75.525	0.713106	4.19474E-07
75.625	0.6917535	4.06914E-07
75.725	0.554234	3.2602E-07
75.82	0.571498	3.36175E-07
75.92	0.6142295	3.61311E-07
76.02	0.6412985	3.77234E-07
76.12	0.6213655	3.65509E-07
76.22	0.4889545	2.8762E-07
76.32	0.405896	2.38762E-07
76.42	0.3612215	2.12483E-07
76.52	0.355089	2.08876E-07
76.62	0.2730235	1.60602E-07
76.72	0.241892	1.42289E-07
76.82	0.2510315	1.47666E-07
76.92	0.2157155	1.26891E-07
77.02	0.242629	1.42723E-07
77.12	0.1812195	1.066E-07
77.215	0.1925315	1.13254E-07
77.315	0.164939	9.70229E-08
77.415	0.1905445	1.12085E-07
77.515	0.1884875	1.10875E-07
77.63	0.210123	1.23602E-07
77.73	0.254327	1.49604E-07

Average for Sonde =	2.8551E-07
Count =	51
Confidence Level(95.0%) =	3.11533E-08



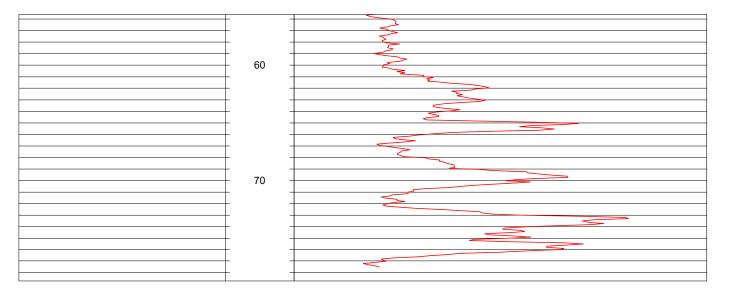
77	L	TOOL HMA-435-S
		CALIBRATION DATE/TIME 7/29/16 09:25
WIEDEMEIER		CALIBRATION STANDARDS 0 and 5E-3 SI Units
& ASSOC	CIATES	CALIBRATION RESULTS 0 =
PROJECT	ESTCP 201584	DEPTH TO WATER, TD 41.3 ft BTOC, 81.88 ft BTOC
LOCATION	Hill AFB Operable Unit 2	
WELL	U02-43 Down	CASING INNER DIAMETER 4"
LOGGER	T.H. Wiedemeier	REMARKS
DATE	7/29/16	

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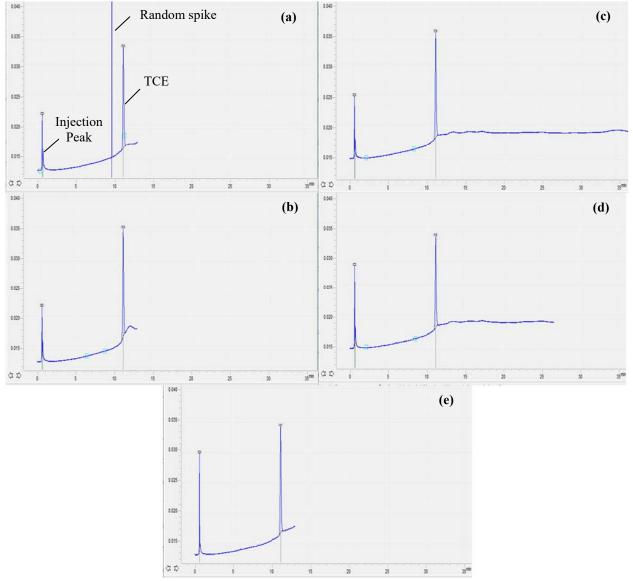
		TOOL HMA-453-S CALIBRATION DATE/TIME 7/29/16, 09:25 CALIBRATION STANDARDS 0 and 5E-3 CALIBRATION RESULTS 0 =
PROJECT	ESTCP 201584	DEPTH TO WATER, TD 41.30
	Hill AFB Operable Unit 2	CASING INNER DIAMETER 4"
WELL LOGGER	U02-43 T.H. Wiedemeier	REMARKS
DATE	7/29/16	

Depth	Mag Susc
1ft:100ft	0 10e-3 SI units 1
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# APPENDIX D SUPPLEMENTAL MATERIAL RELATED TO THE <sup>14</sup>C-TCE ASSAY



# D.1 Twin Cities Army Ammunition Plant

Figure D.1. GC chromatographs from TCAAP at Day 0 showing (a) 01U108, bottle 1; (b) 01U108, bottle 2; (c) 01U108, bottle 3; (d) 01U115, bottle 1; and (e) 01U115, bottle 3 using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min. These wells did not have significant VOCs in the initial headspace sampling, so the final chromatographs at Day 46 are not shown. The leftmost, smaller peak represents the injection peak and the rightmost, larger peak represents TCE as shown in panel (a) for an example.

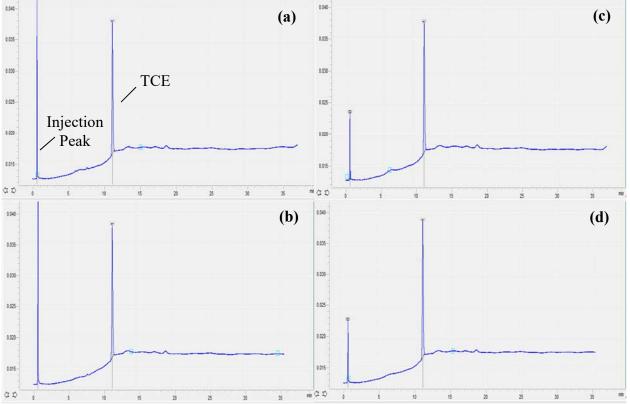


Figure D.2. GC chromatographs from TCAAP at Day 0 showing (a) 32PTLW12, bottle 2; (b) 32PTLW12, bottle 3; (c) 35PTLW13, bottle 1; and (d) 35PTLW13, bottle 2 using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min. These wells did not have significant VOCs in the initial headspace sampling, so the final chromatographs at Day 46 are not shown. The leftmost, smaller peak represents the injection peak and the rightmost, larger peak represents TCE as shown in panel (a) for an example.

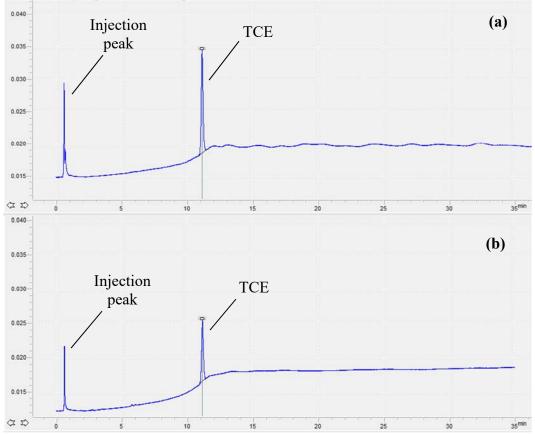


Figure D.3. GC chromatographs from TCAAP, well 01U115, bottle 2. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

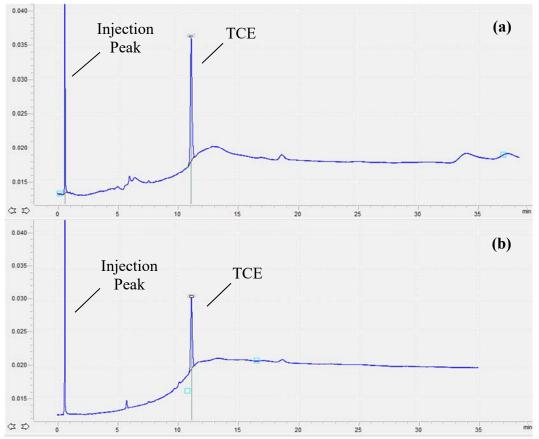


Figure D.4. GC chromatographs from TCAAP, well 01U117, bottle 1. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

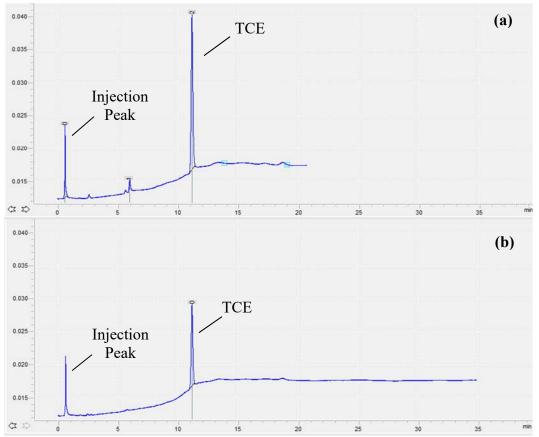
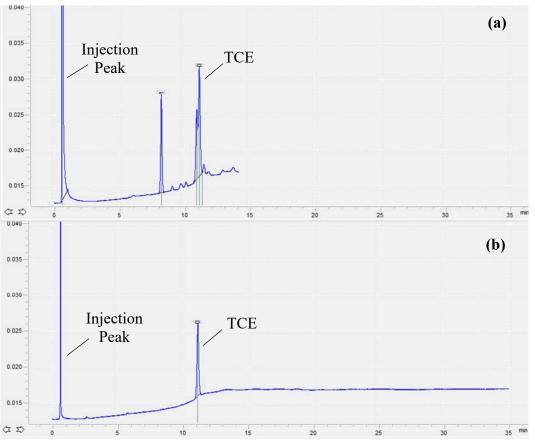


Figure D.5. GC chromatographs from TCAAP, well 01U119, bottle 3. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.



#### **D.2** Plattsburgh Air Force Base

Figure D.6. GC chromatographs from Plattsburgh, well MW-02-006, bottle 1. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

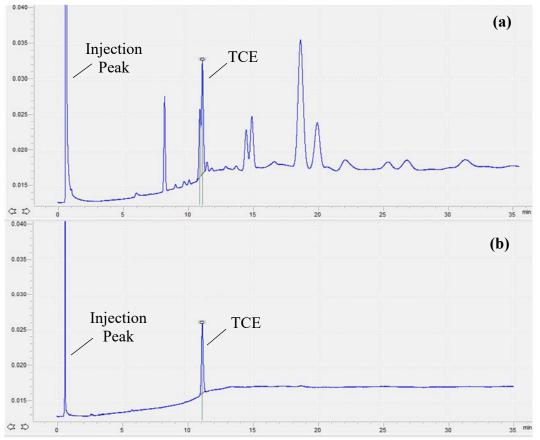


Figure D.7. GC chromatographs from Plattsburgh, well MW-02-006, bottle 2. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

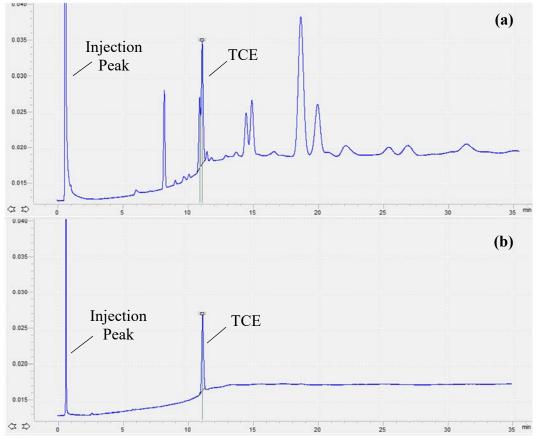


Figure D.8. GC chromatographs from Plattsburgh, well MW-02-006, bottle 3. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

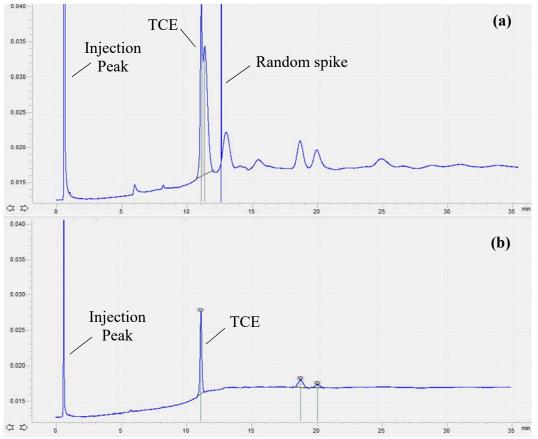


Figure D.9. GC chromatographs from Plattsburgh, well MW-02-019, bottle 1. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

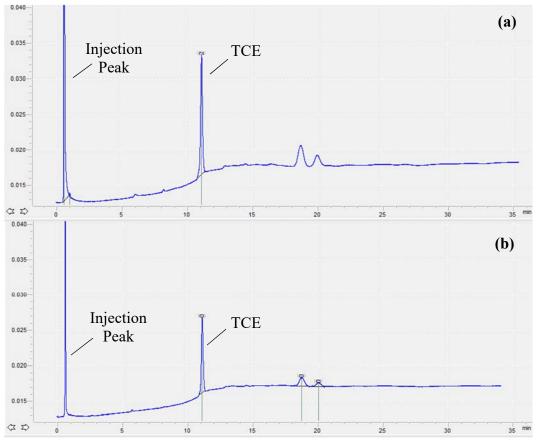


Figure D.10. GC chromatographs from Plattsburgh, well MW-02-019, bottle 2. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

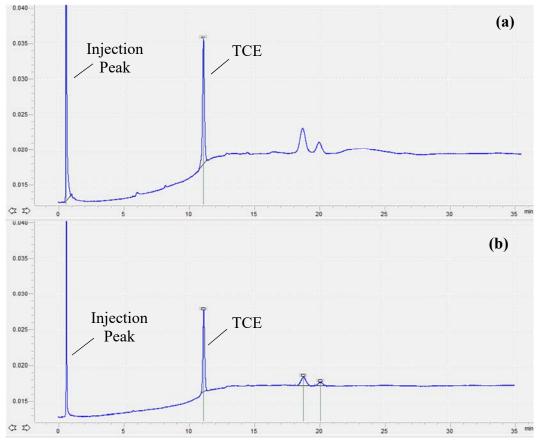


Figure D.11. GC chromatographs from Plattsburgh, well MW-02-019, bottle 3. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

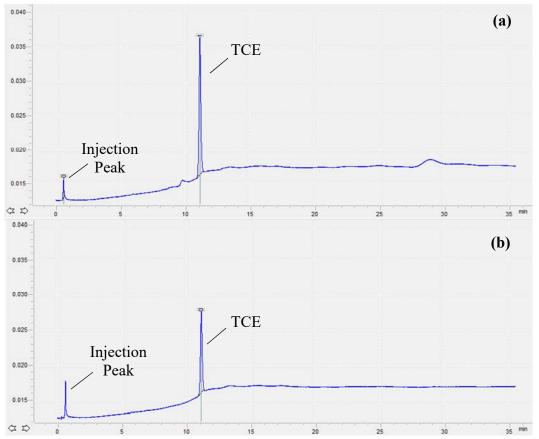


Figure D.12. GC chromatographs from Plattsburgh, well 32PTLW12, bottle 1. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

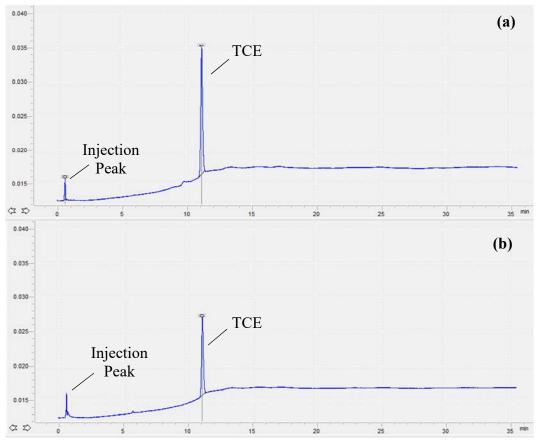


Figure D.13. GC chromatographs from Plattsburgh, well 32PTLW12, bottle 2. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

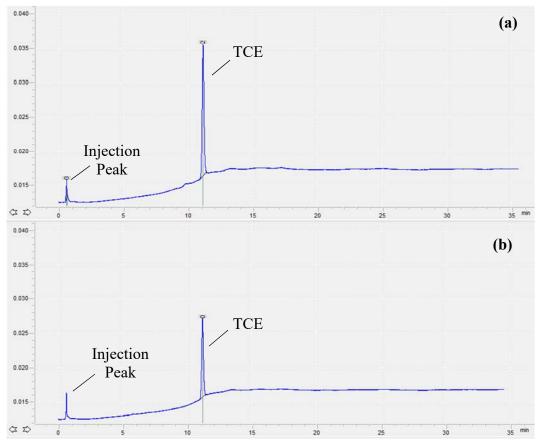


Figure D.14. GC chromatographs from Plattsburgh, well 32PTLW12, bottle 3. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

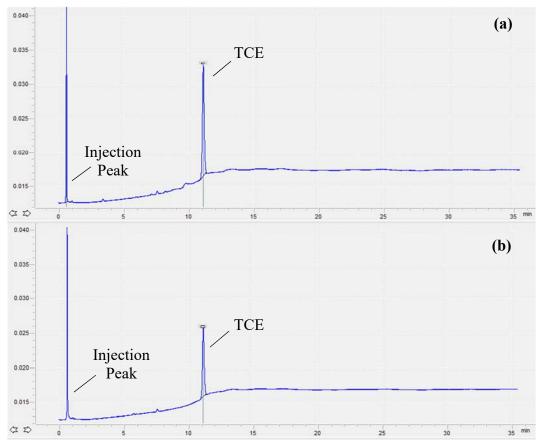


Figure D.15. GC chromatographs from Plattsburgh, well 35PTLW13, bottle 1. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

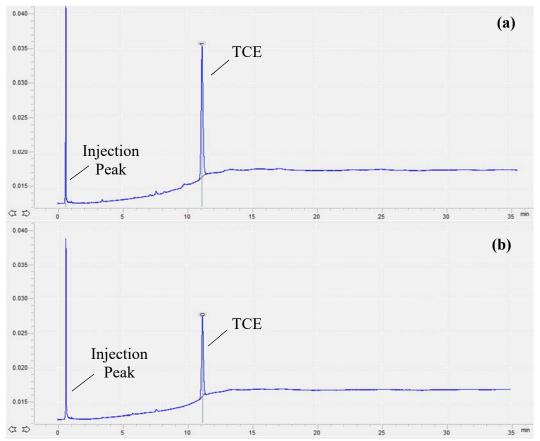


Figure D.16. GC chromatographs from Plattsburgh, well 35PTLW13, bottle 2. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

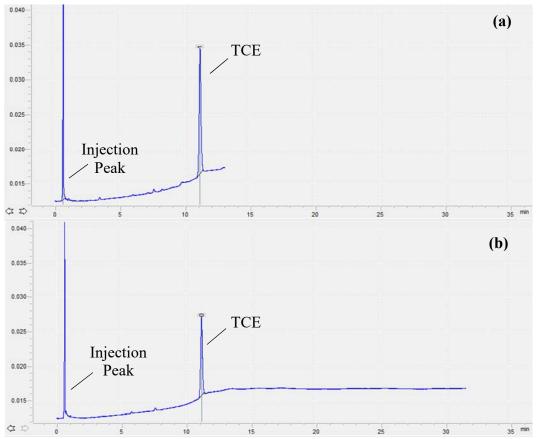
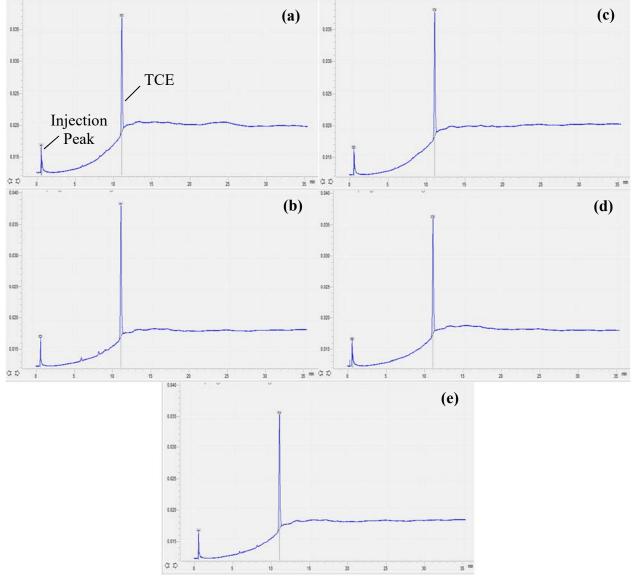


Figure D.17. GC chromatographs from Plattsburgh, well 35PTLW13, bottle 3. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.



### D.3 Hopewell Precision Superfund Site

Figure D.18. GC chromatographs from Hopewell at Day 0 showing (a) EPA-16S, bottle 2; (b) EPA-16S, bottle 3; (c) EPA-15D, bottle 1; (d) EPA-15D, bottle 2; and (e) EPA-15D, bottle 3 using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min. These wells did not have significant VOCs in the initial headspace sampling, so the final chromatographs at Day 46 are not shown. The leftmost, smaller peak represents the injection peak and the rightmost, larger peak represents TCE as shown in panel (a) for an example.

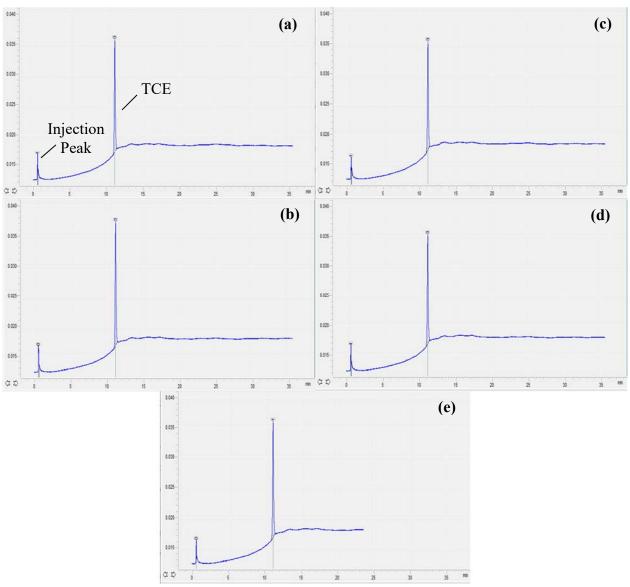


Figure D.19. GC chromatographs from Hopewell at Day 0 showing (a) EPA-12S, bottle 2; (b) EPA-12S, bottle 3; (c) EPA-10S, bottle 1; (d) EPA-10S, bottle 2; and (e) EPA-10S, bottle 3 using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min. These wells did not have significant VOCs in the initial headspace sampling, so the final chromatographs at Day 46 are not shown. The leftmost, smaller peak represents the injection peak and the rightmost, larger peak represents TCE as shown in panel (a) for an example.

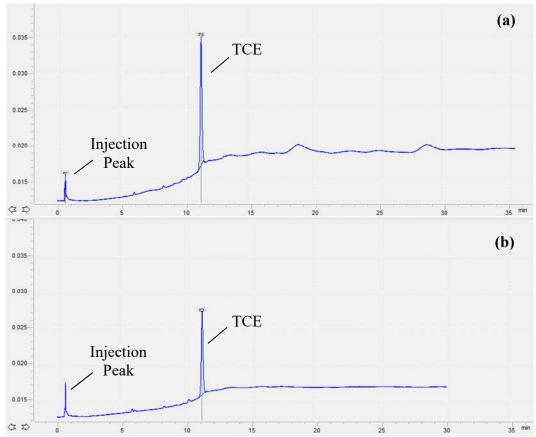


Figure D.20. GC chromatographs from Hopewell, well EPA-16S, bottle 1. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

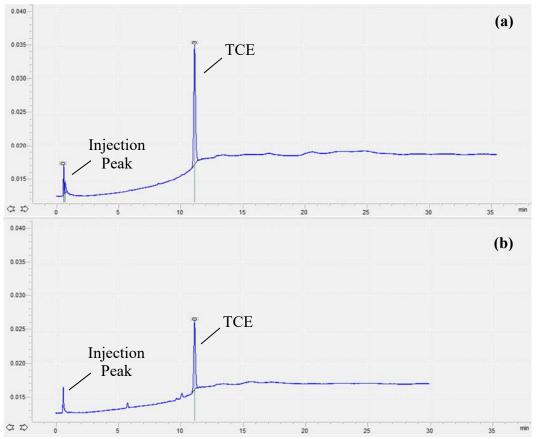
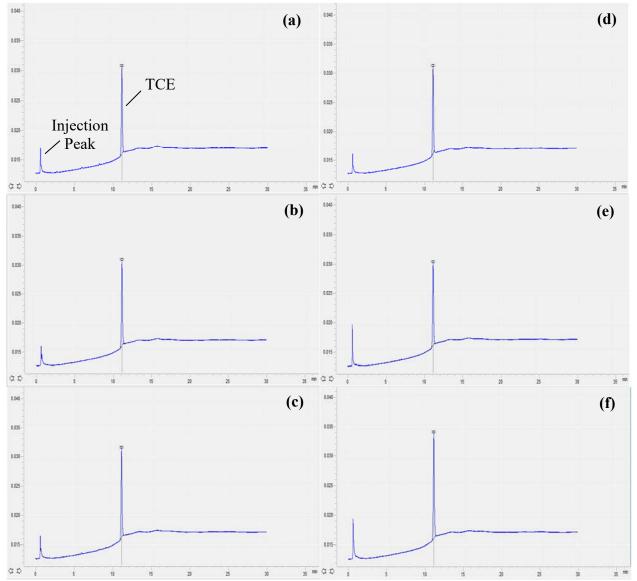


Figure D.21. GC chromatographs from Hopewell, well EPA-12S. Panel (a) shows Day 0 and (b) shows Day 40 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.



**D.4** Tooele Army Depot

Figure D.22. GC chromatographs from Tooele at Day 0 showing (a) D-20, bottle 1; (b) D-20, bottle 2; (c) D-20, bottle 3; (d) D-23, bottle 1; (e) D-23, bottle 2; and (f) D-23, bottle 3 using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min. These wells did not have significant VOCs in the initial headspace sampling, so the final chromatographs at Day 46 are not shown. The leftmost, smaller peak represents the injection peak and the rightmost, larger peak represents TCE as shown in panel (a) for an example.

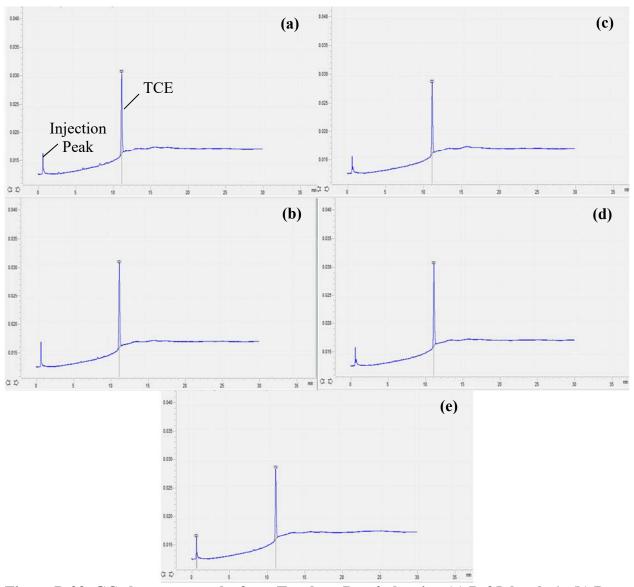


Figure D.23. GC chromatographs from Tooele at Day 0 showing (a) D-25, bottle 1; (b) D-25, bottle 2; (c) D-19, bottle 1; (d) D-19, bottle 2; and (e) D-19, bottle 3 using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min. These wells did not have significant VOCs in the initial headspace sampling, so the final chromatographs at Day 46 are not shown. The leftmost, smaller peak represents the injection peak and the rightmost, larger peak represents TCE as shown in panel (a) for an example

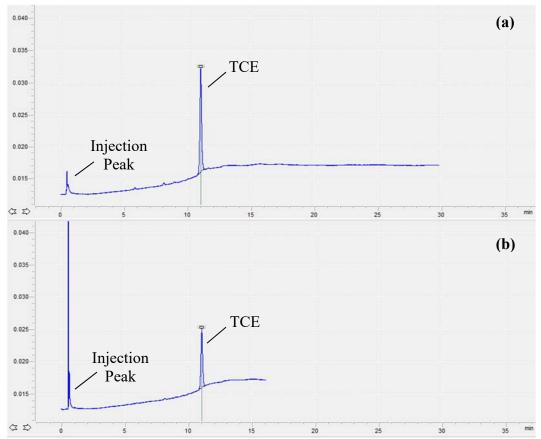
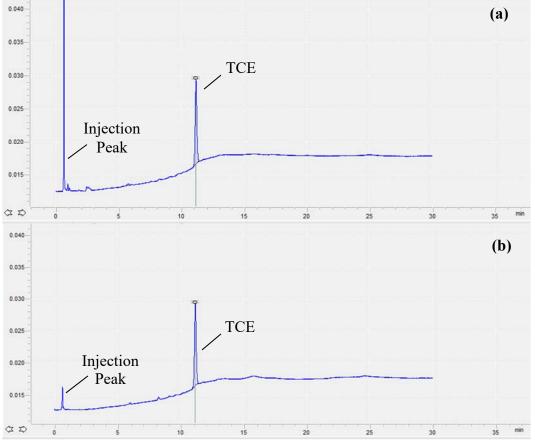


Figure D.24. GC chromatographs from Tooele, well D-25, bottle 3. Panel (a) shows Day 0 and (b) shows Day 46 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.



# D.5 Hill Air Force Base

Figure D.25. GC chromatographs from Hill at Day 0 showing (a) U10-019, bottle 3 and (b) U10-025, bottle 2 using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min. These wells did not have significant VOCs in the initial headspace sampling, so the final chromatographs at Day 46 are not shown.

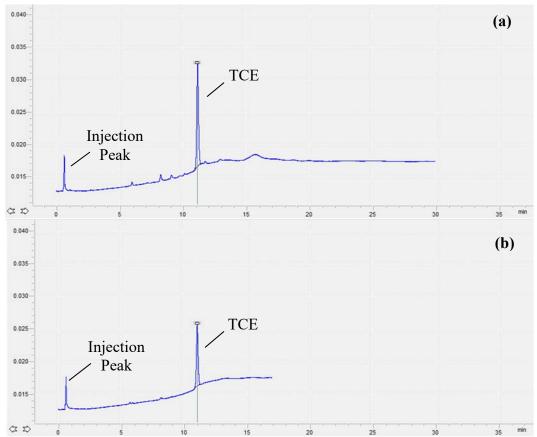


Figure D.26. GC chromatographs from Hill, well U10-043, bottle 1. Panel (a) shows Day 0 and (b) shows Day 46 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

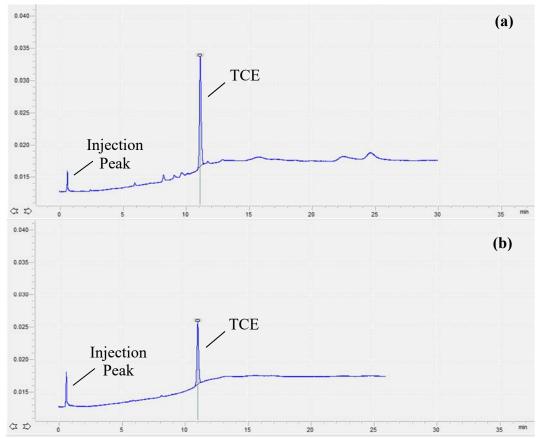


Figure D.27. GC chromatographs from Hill, well U10-043, bottle 2. Panel (a) shows Day 0 and (b) shows Day 46 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

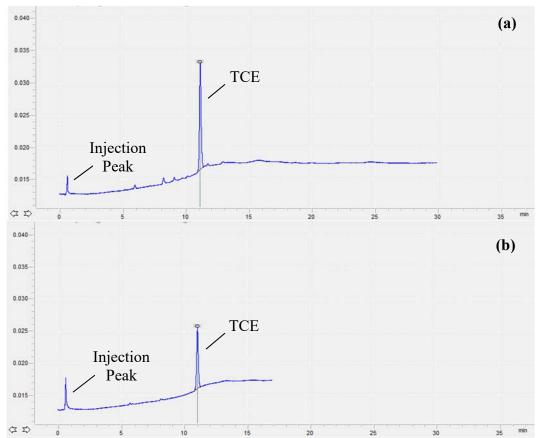


Figure D.28. GC chromatographs from Hill, well U10-043, bottle 3. Panel (a) shows Day 0 and (b) shows Day 46 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

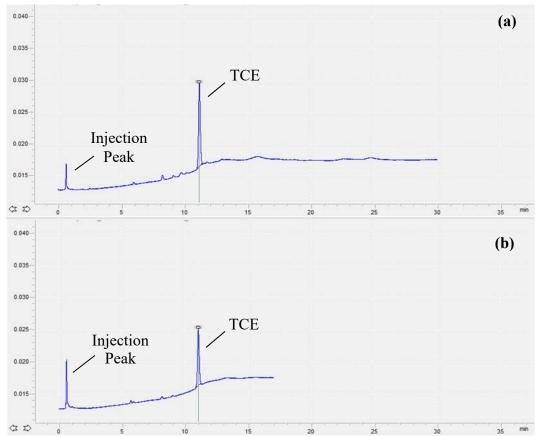


Figure D.29. GC chromatographs from Hill, well U10-025, bottle 1. Panel (a) shows Day 0 and (b) shows Day 46 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

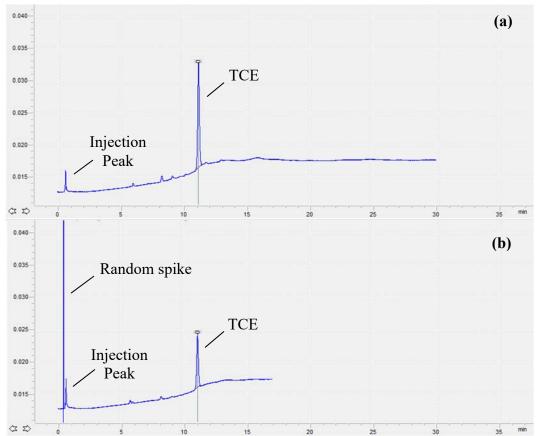


Figure D.30. GC chromatographs from Hill, well U10-025, bottle 3. Panel (a) shows Day 0 and (b) shows Day 46 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

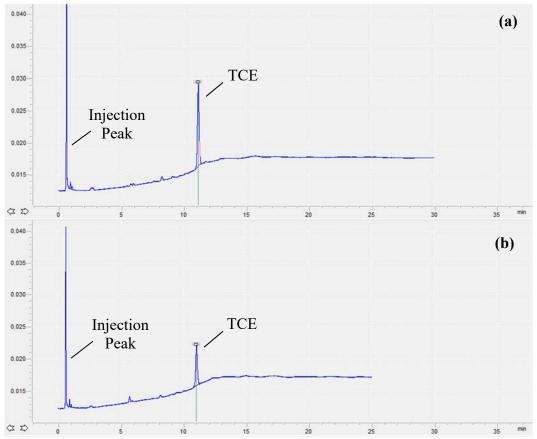


Figure D.31. GC chromatographs from Hill, well U10-019, bottle 1. Panel (a) shows Day 0 and (b) shows Day 46 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

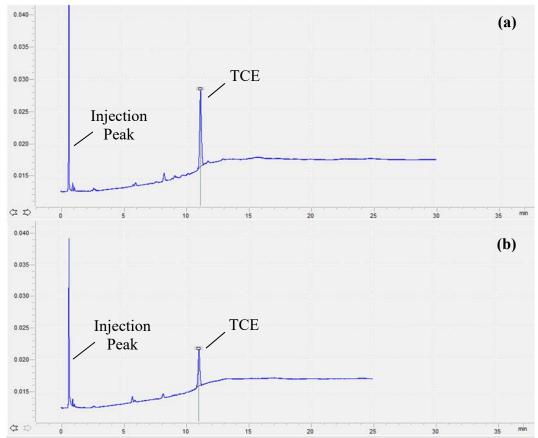


Figure D.32. GC chromatographs from Hill, well U10-019, bottle 2. Panel (a) shows Day 0 and (b) shows Day 46 measurements taken using 0.5 mL headspace injections onto a packed column connected to the GC FID. The residence time for TCE was determine using an external standard. Y-axis is measured in volts (V) and x-axis in min.

### **D.6 MATLAB Script for Model**

```
Original: 07/16/16
%
%
   Modified: 01/20/17
2
%
   Author: James Mills
%
%
   Purpose of script: This script will run a nonlinear regression
   model for experimental data that involves the cometabolism of TCE.
%
%
   The goal of the program is to solve for a first order rate constant
   using the least squares method. Additionally, confidence intervals and
%
   standard deviation for the rate constant will be included. This
%
   script will rely on multiple different functions in a stepwise manner
°
   because of the dynamic volume changes that occur during the experiment,
%
   which affect the concentration of TCE and its distribution between the
2
%
   aqueous and gaseous phases.
function experimentalModelReportEdit
%
  Dimensionaless Henry's Law constant for TCE
H_c = 0.349;
  Liquid removed with each sampling event (3.1 mL)
8
V_{lr} = 3.1;
  Gas removed with each sampling event (1.0 mL)
V_gr = 1.0;
%
  Total volume of serum bottle (160 mL)
V_{tot} = 160;
% Create on/off switchs so user can easily change sections of code
CSV = 'off';
Obtain folder and file paths
%
scriptPath = cd; % Current directory of MATLAB file
  Have user select Excel data file through dialogue box
[baseName,dirPath] = uigetfile({'*.xlsx';'*.xls'},'Select a file');
fileName = fullfile(dirPath, baseName); % Full file path of Excel WB
  Change to directory where Excel data files reside
cd(dirPath);
  Gather all sheet names from Excel data file
[~, sheets] = xlsfinfo(fileName);
```

\* For certain sheet names in selected file, list name and associated

```
numerical index value, separated by a tab.
fprintf('\n') % Add new line
for t = 1:length(sheets) % Iterate over all sheets
      If model is in sheetname, skip this sheet
    %
    if not(isempty(strfind(char(sheets(t)), 'Model')))
        continue
   end
       If sheet name contains certain identifier, then print to MATLAB
    %
    2
       command window with appropriate sheet index for user to select
   if not(isempty(strfind(char(sheets(t)),'well #'))) || ...
            not(isempty(strfind(char(sheets(t)), 'A WC'))) || ...
            not(isempty(strfind(char(sheets(t)), 'FS GW Hill'))) || ...
            not(isempty(strfind(char(sheets(t)), 'Propano'))) || ...
           not(isempty(strfind(char(sheets(t)), 'Room'))) || ...
           not(isempty(strfind(char(sheets(t)), 'Ice'))) || ...
            not(isempty(strfind(char(sheets(t)), 'WC Test'))) || ...
           not(isempty(strfind(char(sheets(t)), 'Twin Lakes'))) || ...
            not(isempty(strfind(char(sheets(t)), 'Tooele Rock Controls')))
        fprintf('%s \t %d',char(sheets(t)),t)
        fprintf(' \ n')
   end
end
  Prompt user for numerical input to select appropriate sheet and
8
  assign selected sheet to variable
fprintf('\n') % Add new line
prompt = 'Enter numerical value for sheet desired --> ';
sheetName = input(prompt);
  Read selected sheet from Excel data file to get raw data
[~,~,raw] = xlsread(fileName,sheetName);
   Determine size of raw data set from selected sheet
[row,col] = size(raw);
%
   Preallocate memory with zeros
sparInd = zeros(3,2);
dayInd = zeros(3,2);
    Iterate over selected data matrix to find certain data indices for
%
   dpm and day entries
countRow = 0; % Counter to be updated in loop
    % Iterate over columns in raw data
    for j = 1:col
        % Iterate over rows in raw data
        for m = 1:row
```

```
°
               Search sheet for exact string match, then get sparge
           %
               data indices and day indices using offsets from
           %
               location of exact string match
           if strcmp('Sparged alkaline liquid (3.0 mL)',raw(m,j))
               countRow = countRow + 1; % Update counter
               %
                   Sparge data start indices
               sparInd(countRow,1) = m+3; % +3 is offset for sparge rows
               sparInd(countRow,2) = j+4; % +4 is offset for sparge cols
                  Day data start indices
               2
               dayInd(countRow,1) = m+3; % +3 is offset for day rows
               dayInd(countRow,2) = j+1; % +1 is offset for day cols
           end
           8
             Find exact string in sheet and get measured
           2
              concentration data
           cMeasStr = ['Calculated total activity remaining '...
               'in bottle from direct counts'];
             Measured concentration data from offsets in sheets with 3
           2
              bottles
           if strcmp(cMeasStr,raw(m,j))
               C_ototm = cell2mat([raw(m+3,5), raw(m+3,12),raw(m+3,19)]);
           end
               Find exact match in sheet, then get initial volume
           %
               measurements using offsets in sheets with 3 bottles
           %
           if strncmp(raw(m,j),'Volume of Liquid',15)
               V_iL(1,:) = cell2mat([raw(m,2),raw(m,9),raw(m,16)]);
           end
       end
   end
   While data is numeric, update dpm and day data into matrices
for k = 1:length(sparInd)
   count2 = 0;
                 % Counter to be updated
   rowCount = 1; % Another counter to be updated
   while isnumeric(cell2mat(raw(sparInd(k,1)+count2,sparInd(k,2))))&& ...
           cell2mat(raw(sparInd(k,1)+count2,sparInd(k,2))) ~= 0 &&...
           not(isnan(cell2mat(raw(sparInd(k,1)+count2,sparInd(k,2)))))
       dpmData(rowCount,k) = cell2mat(raw(sparInd(k,1)+count2,sparInd(k,2)));
       dayData(rowCount,k) = cell2mat(raw(dayInd(k,1)+count2,dayInd(k,2)));
       count2 = count2 + 1; % Update counter
       rowCount = rowCount + 1; % Update counter
   end
end
```

```
*******
                           Initial case
   Print number of sparge samples in data set
2
fprintf('\n %s %d \n', 'n =',length(dpmData))
    Experimental data for days from time zero and dpm at each
2
   sampling event per bottle
%
8
   If IIA well #1 or VB well #1, then remove last data points
if strcmp(char(sheets(sheetName)),'IIA well #1')|| ...
        strcmp(char(sheets(sheetName)), 'VB well #1')
    fprintf(2,'\nsuccess IIA1 or VB1\n')
   dpm = dpmData(1:end-1,:); % x data
   days = dayData(1:end-1,:); % y data
   For storage test (Room Temp, Ice A ,Ice B) ask user to shorten data to
%
%
    4 days or leave all data
elseif strcmp(char(sheets(sheetName)), 'Room Temp')|| ...
        strcmp(char(sheets(sheetName)), 'Ice A')||...
        strcmp(char(sheets(sheetName)),'Ice B')
    fprintf(2, '\nsuccess storage\n')
   prompt2 = input('0-4 days (y/n) \rightarrow , s');
    if strcmp(prompt2,'y')
       dpm = dpmData(1:end-3,:); % x data
        days = dayData(1:end-3,:); % y data
   else
       dpm = dpmData(1:end,:); % x data
        days = dayData(1:end,:); % y data
    end
   Else include entire data set collected from worksheet
%
else
   dpm = dpmData(1:end,:);
                              % x data
    days = dayData(1:end,:); % y data
end
Ŷ
   Remove average dpm on initial reading from dpm data set for sorted
   Tooele Rock controls (well D-20) because some values lower than initial
%
8
   values
if strcmp(char(sheets(sheetName)), 'Tooele Rock Controls')
   fprintf(2, '\nsuccess TRC\n')
    sortDpm = sort(dpm, 'ascend');
   aveSortedDpm = mean(sortDpm(1,:));
    dpm = dpm - aveSortedDpm;
%
  Else remove average of initial data sparge sample data points
%
  from data set
else
   aveInitDpm = mean(dpm(1,:));
```

```
dpm = dpm - aveInitDpm;
end
dpm(dpm<0) = 0;
                    % if negative value, then update as zero in matrix
  Get values for gas volume using difference between total and liquid
V_{ig}(1,:) = V_{tot} - V_{iL}(1,:);
  Determine length of data set using time interval data
dataLength = length(days);
  Calculate liquid volume in bottles after each sampling event
2
for q = 1:3
   % Iterate over data of one bottle at a time
    for j = 2:dataLength
        % Update liquid volume between sampling events
        V_{iL}((j),q) = V_{iL}((j-1),q) - V_{lr};
    end
end
  Update dpm values to reflect all experimental products in bottle
8
dpm = (dpm)./3.*V_iL;
   Preallocate memory with zeros
C_ilb = zeros(1,length(C_ototm));
dpmLiq = zeros(1,length(C_ototm));
dpmGas = zeros(1,length(C_ototm));
totDpmRem = zeros(1,length(C_ototm));
C_itotp = zeros(1,length(C_ototm));
C_ila = zeros(1,length(C_ototm));
delta_ip = zeros(1,length(C_ototm));
sumDelta_ip = zeros(1,length(C_ototm));
    % Initial case in model, when t = 0
    for k = 1:length(C_ototm)
        % Multiply total 14C concentration by percent aqueous to
        % determine liquid concentration in bottles
        C_{ilb}(1,k) = C_{ototm}(k).*(V_{iL}(1,k)/(V_{iL}(1,k)+(V_{ig}(k).*H_c)));
        % Dpm removed from aqueous phase
        dpmLiq(1,k) = C_ilb(k).*(V_lr./V_iL(1,k));
          Dpm removed from gaseous phase. Remove only part for the
        %
        % controls because no O2 checks performed. Remove full for all
            experimental bottles because O2 checks performed.
        %
        % Controls
        if not(isempty(strfind(char(sheets(sheetName)), 'A WC'))) | ...
```

```
not(isempty(strfind(char(sheets(sheetName)), 'FS GW Hill'))) || ...
               not(isempty(strfind(char(sheets(sheetName)), 'Tooele Rock Controls')))
           dpmGas(1,k) = (C_ototm(k) - C_ilb(k)).*(((V_gr./2)./(V_ig(k))));
       % Experimental bottles
       else
           dpmGas(1,k) = (C_ototm(k)- C_ilb(k)).*(((V_gr./2)./(V_ig(k)))...
               + ((V_gr./2)./(V_ig(k)+ V_lr)));
       end
       % Total dpm removed
       totDpmRem(1,k) = dpmLiq(1,k) + dpmGas(1,k);
       % Final, predicted 14C total conc after sampling event
       C_itotp(1,k) = C_ototm(k) - totDpmRem(1,k);
          Final 14C liquid conc per bottle after sampling event
       C_{ila(1,k)} = C_{itotp(1,k)} * ((V_{iL(1,k)}-V_{lr})./...
           ((V_iL(1,k)-V_lr)+((V_tot-(V_iL(1,k)-V_lr)).*H_c)));
       % There are no initial products formed when t = 0
       delta_ip(1,k) = 0;
       sumDelta_ip(1,k) = 0;
   end
          %************************* Case II, when t >= 1 *********************************
  Create a function for Case II of the model, when t >= 1
   function yData = caseII(k,xData)
   yData = zeros(dataLength,3);
   % This loop allows the index to shift to data for next bottle
   for n = 1:3
       % Loop range iterates over data of one bottle at a time
       for i = 2:dataLength
             Change in time between sampling events
           deltaT = xData(i)-xData(i-1);
           % Update gas volume between sampling events
           V_{ig(i,n)} = V_{ig((i-1),n)} + V_{lr};
           % Determine products formed during incubation between
           %
              sampling events
           delta_ip(i,n) = C_ila(i-1,n).*(1-exp(-k.*deltaT));
           % Cumulative products formed during entire incubation since
```

```
\% 14C spiking or t = 0
           sumDelta_ip(i,n) = delta_ip(i,n) + sumDelta_ip(i-1,n);
           % Initial 14C liquid conc before sampling event
           C_{ilb(i,n)} = C_{ila((i-1),n)} - delta_{ip(i,n)};
             Dpm removed from aqueous phase
           %
           dpmLiq(i,n) = C_ilb(i,n).*(V_lr./V_iL(i,n));
              Dpm removed from gaseous phase. Remove only part for the
           %
             controls because no O2 checks performed. Remove full for all
           %
              experimental bottles because 02 checks performed.
           %
           % Controls
           if not(isempty(strfind(char(sheets(sheetName)), 'A WC'))) ||...
                   not(isempty(strfind(char(sheets(sheetName)), 'FS GW Hill'))) || ...
                   not(isempty(strfind(char(sheets(sheetName)), 'Tooele Rock
Controls')))
               dpmGas(i,n) = (C_itotp(i-1,n) - C_ilb(i,n)).*...
                   (((V_gr./2)./(V_ig(i,n))));
           % Experimental bottles
           else
               dpmGas(i,n) = (C_itotp(i-1,n) - C_ilb(i,n)).*...
                   (((V_gr./2)./(V_ig(i,n)))+((V_gr./2)./(V_ig(i,n)+ V_lr)));
           end
              Total dpm removed
           8
           totDpmRem(i,n) = dpmLiq(i,n) + dpmGas(i,n);
               Final, predicted 14C liquid concentration after sampling
           C_itotp(i,n) = C_itotp(i-1,n)-totDpmRem(i,n)-delta_ip(i,n);
              Percent aqueous
           8
           perAq = (V_iL(i,n)-V_lr)./...
               ((V_{iL}(i,n)-V_{lr})+((V_{tot}-(V_{iL}(i,n)-V_{lr})).*H_c));
             Final, 14C liquid conc after sampling
           %
           C_ila(i,n) = C_itotp(i,n).*perAq;
           yData(i,n) = sumDelta_ip(i,n);
       end
   end
   end
                           * * * * * * * * * *
First order rate constant based 20 year half life estimation
8
k = 9.489e-5; % d^-1
  Use nonlinear regression to determine value for first order
%
%
  rate constant, k
opts = optimset('Display','off');
```

```
[rateCons,~,resid,~,~,~,J] = lsqcurvefit(@caseII,k,days,dpm,[],[],opts);
  Determine confidence intervals and standard deviation on rate constant
[ciDays, se] = nlparciSE(rateCons, resid, 'Jacobian', J);
ciYears = ciDays*365;
rateConsYr = rateCons*365;
std = (se*(3*length(dpmData))^{(0.5)})*365;
fprintf('\n %s \%.5d \n', 'std =', std)
    Print values to command window with units
fprintf('\n %s \n', char(sheets(sheetName)))
fprintf('\n %s %.3d %s %.3d %s \n','k =', (rateConsYr),char(177),...
    ((rateConsYr)-ciYears(1)), 'y^-1');
fprintf('\n %s %.3f %s %s %.3f %s %.3f %s \n', 'half life =',...
    log(2)/(rateConsYr),char(177),'[',...
      (log(2)/(rateConsYr))-(log(2)./(ciYears(2))),',',...
      (log(2)./(ciYears(1)))-(log(2)/(rateConsYr)),'] yr');
   Create CSV file so output data easily to manipulate using copy and paste
%
   in MS Excel program
%
if strcmp(CSV, 'on')
    fName = char(sheets(sheetName));
                                       % filename
   restName = 'Model&AdjExpData';
                                       % rest of name
    % Includes model data (sumDelta_ip) and experimental data (dpm)
    % as single, reshaped matrices (1 col by x rows)
    totData = [reshape(sumDelta_ip,[],1),reshape(dpm,[],1)];
    % Create a CSV file and write in headers
    fid = fopen(strcat(fName,restName,'.csv'),'w');
    fprintf(fid, '%s \n %s \n', fName,...
        'DPM data per bottle from experimental and model data');
    fprintf(fid, '%s %s %s \n', 'Model DPM',',','Experimental DPM');
    fclose(fid);
    % Append rest of data below headers in file
    dlmwrite(strcat(fName,restName,'.csv'),totData,'-append')
end
%
   Change folder back to origin of MATLAB file, so script is callable
cd(scriptPath);
end
```

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# APPENDIX E APPLICATION OF MOLECULAR BIOLOGICAL TOOLS

# ACRONYMS

DO	dissolved oxygen			
EAP	enzyme activity probes			
HDPE	high density polyethylene			
L	liters			
m	time in minutes			
ORP	oxidation-reduction potential			

### PURPOSE

Successful application of enzyme activity probes requires that groundwater and sediments are sampled in a specific manner to minimize exposure to exogenous oxygen during shipment to the laboratory. This procedure describes the approach for collecting microbial samples for enzyme probe analysis.

### SCOPE

This procedure provides instruction for sampling personnel to collect groundwater for the enzyme probe analysis. Sample quantities, containers, preservatives, handling procedures, and shipping instructions are contained within this procedure. In addition, methods for staining bacterial cells with enzyme activity probes are included.

# GROUNDWATER SAMPLE COLLECTION FOR ENZYME ACTIVITY PROBE ANALYSIS

#### • Groundwater sampling procedure

A microbial groundwater sample for enzyme probes is collected in a sterile bottle as an unaltered groundwater sample. Requirements for microbial sample containers, preservation, and holding times are summarized in Table 2.

Sample Container	Preservation	Holding Time
Four separate -1L sterile HDPE bottles collected with zero headspace from each sampling location.	4°C Stored on ice (preferably blue ice or frozen gel packs).	Samples must be shipped on the same day as collection. Ship samples priority overnight express.

Table 2.	Sample co	ntainers, pres	ervation, l	holding tir	me, and shi	pping addre	sses.
----------	-----------	----------------	-------------	-------------	-------------	-------------	-------

This field method involves collecting four liters (1L) of groundwater at the well-head using sterile techniques. The lab will provide sterile bottles for sample collection. It is important to fill the bottles using low groundwater flow (1 to 4 L/min), in order to minimize turbulence and unnecessary exposure to the atmosphere during filling. Groundwater samples will be collected into the sterile one-liter (1L) bottles and filled to no-headspace. Use the following procedure to ensure no headspace:

- Fill the 1L bottles and form a meniscus at the top of the bottle.
- Fill the cap with groundwater, then screw on the bottle cap tightly, so as to fill the bottle with no headspace or bubbles. There may be a small amount of headspace that, if filled as requested, is minimal.
- Seal the bottle caps with parafilm and/or tape to minimize potential for exposure to air.
- Label each bottle with a unique sample number, the sample location, date and time of sample collection, sampling depth, groundwater temperature, client, and sampler.
- Place each bottle into a self-sealing plastic bag. Make sure the plastic bag is sealed shut (e.g. Ziploc bag)
- Pack the bottles UPRIGHT on ice (preferably blue ice or frozen gel packs) immediately following sampling and store/ship at 4°C. If samples have to be packed on cubed ice, PLEASE double or triple bag the ice separate from the samples. FedEx has refused to ship coolers in the past because they were "leaking".

### SAMPLE HANDLING AND SHIPPING

Use the following general guidance for sample packaging:

- Each sample container should be placed in a self-sealing plastic bag prior to placement in the cooler. Make sure each plastic bag is sealed shut.
- The bottles should be packed upright within the cooler with sufficient blue ice or frozen gel packs such that they maintain approximately 4°C during shipment.
- Pack the bottles tightly in the coolers so there is absolutely no movement. Add packaging materials to fill void space within the cooler. Include COC forms and other appropriate sample collection documentation in a self-sealing plastic bag.

Seal the cooler with strapping tape.

### STAINING PROCEDURES

### **Aromatic Oxygenase Activity**

Follow the procedures described in Lee et al. (2008). Process each of the four separate 1-liter samples from each well. Filter 100 mL from each sample through nine different 0.22  $\mu$ m, 25 mm diameter, black, polycarbonate filters. Incubate three of the nine filters in a solution containing 5 mM of phenylacetylene for 10 minutes. Incubate three of the nine filters in a solution containing 5 mM of *trans*-cinnamonitrile for 10 minutes. Incubate three of the nine filters in a solution containing 5 mM of 3-hydroxyphenylacetylene for 10 minutes. Mount the filters on a glass microscope slide with non-fluorescent immersion oil and a cover slip, and examined for fluorescent cells by epifluorescent microscopy. For each slide, count a minimum of 20 random fields, and calculate the average number of fluorescent cells per field. Then calculate the abundance of cells accumulating a fluorescent product. The abundance is the average

number of fluorescent cells in a field under the microscope, divided by the surface area of the field counted, then multiplied the surface area of the filter, and then divided the volume of sample passed through the filter. Filter and assay a culture of *Pseudomonas putida* F1 as a positive control to verify EAP signal.

### sMMO Enzyme Activity

Follow the procedures described in Wymore et al. (2007). Filter groundwater from each sample onto 25mm Supor filters, and placed into separate glass Petri plates. Pipet 1.0-mL of 5mM coumarin solution in phosphate buffer onto each filter, and incubate for 10 minutes at room temperature. Following the incubation, use phosphate buffer to wash the product from each filter. Determine relative fluorescence (excitation wavelength 338 nm, emission wavelength 450 nm) using a fluorescence spectrophotometer, with a quartz cuvette of 1 cm path length. Filter a culture of *Methylosinus trichosporium* OB3b as a positive control to verify the signal from coumarin.

### REFERENCES

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Wymore, R. A., M.H. Lee, W.K. Keener, A.R. Miller, F.S. Colwell, M.E. Watwood, K.S. Sorenson, Field Evidence for Intrinsic Aerobic Chlorinated Ethene Cometabolism by Methanotrophs Expressing Soluble Methane Monooxygenase, *Bioremediation J.*, 11 (2007) 125-139.

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# APPENDIX F PROTOCOL TO CONDUCT THE <sup>14</sup>C-TCE ASSAY

This appendix is summarized from: QUANTIFICATION OF TCE CO-OXIDATION IN GROUNDWATER USING A <sup>14</sup>C-ASSAY, which is a thesis presented to the Graduate School of Clemson University, in partial fulfillment of the requirements for the degree of Master of Science in Environmental Engineering and Earth Sciences, by James C. Mills IV, August 2017.

The procedures described in this appendix must only be carried out in a laboratory that is licensed to receive, store, and use radiolabeled substances.

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# ABBREVIATIONS & ACRONYMS

ACS	American Chemical Society
AFB	air force base
DDI	distilled deionized
dpm	disintegrations per minute
FID	flame ionization detector
FSGW	filter-sterilized groundwater
GC	gas chromatograph
LSC	liquid scintillation cocktail
PTFE	polytetrafluoroethylene
TCD	thermal conductivity detector
TCE	trichloroethylene
VOA	volatile organic analysis

## **Preparation of stock solutions**

Prepare a <sup>14</sup>C-TCE stock solution. Ionizing radiation from decay of <sup>14</sup>C causes radiolysis of water molecules to produce free radicals that degrade the <sup>14</sup>C- TCE to produce products that would be interpreted in the assay as biological cooxidation products (Schmidt et al., 1985; Field et al, 2004). To minimize abiotic degradation through radiolysis, create a stock solution that reduces the specific activity of the <sup>14</sup>C.

Among other potential suppliers, <sup>14</sup>C-TCE (1.0 mCi) is available through customsynthesis from Moravek Biochemicals, Inc. (Brea, CA, USA). It is shipped dissolved in acetonitrile. The <sup>14</sup>C-TCE sample should be shipped on dry-ice for over-night delivery. Add approximately 30 mL of Distilled Deionized (DDI) water that is saturated with TCE to an autoclaved 60- mL clear glass Volatile Organic Analysis (VOA) vial. Puncture the flame-seal on the shipment Pyrex distillation trap that contains the <sup>14</sup>C-TCE using a clean, blunt metal rod and hammer. Then immediately add the contents of the distillation trap container to the vial containing the Distilled Deionized (DDI) water that is saturated with TCE. Rinse the shipment container three times with TCE saturated DDI water, collecting the rinse in the VOA vial to a final volume of ~60 mL. Seal the VOA vial with a Mininert<sup>TM</sup> valve and store the <sup>14</sup>C-TCE **stock solution** at  $10 \pm 2$  °C.

To determine the concentration of TCE, prepare a **TCE stock solution** consisting of 25  $\mu$ L neat TCE dissolved in 125 mL methanol. Tare the container that will contain the TCE stock solution. Weight the container with the methanol and subtract the tare weight to determine the mass of the methanol. Transfer the TCE with a microliter syringe. Weight the syringe used to transfer the TCE with and without the TCE to determine the amount of TCE added to the methanol (± 0.0001 g). Express the concentration of TCE in the stock solution as the mass TCE per mass of **TCE stock solution**.

To evaluate the separation <sup>14</sup>C-TCE and acetonitrile during chromatography, prepare a **TCE/Acetonitrile stock solution** containing 1.0 mL acetonitrile, 1.0 mL saturated TCE (ACS grade), and 99 mL Distilled Deionized (DDI) water in a 160-mL glass serum bottle capped with a PTFE-faced gray butyl rubber septum and aluminum crimp cap. Prepare an **Acetonitrile alone stock solution** containing 1.0 mL acetonitrile, and 99 mL Distilled Deionized (DDI) water in a 160-mL glass serum bottle capped with a PTFE-faced gray butyl rubber septum and aluminum crimp cap. Prepare an **Acetonitrile alone stock solution** containing 1.0 mL acetonitrile, and 99 mL Distilled Deionized (DDI) water in a 160-mL glass serum bottle capped with a PTFE-faced gray butyl rubber septum and aluminum crimp cap. Place the solutions on an orbital shaker table (98  $\pm$  2 RPM) for 1 hour to equilibrate the aqueous and gaseous phases.

Use ScintiSafe<sup>TM</sup> Plus 50 % Cocktail (Fischer Scientific) or equivalent for Liquid Scintillation Counting. To minimize any losses of <sup>14</sup>C from volatilization, the Liquid Scintillation Cocktail is contained in a **specially prepared 20-mL Scintillation Vial**. The vial is prepared by drilling a hole (2.38 mm) in the polypropylene scintillation cap and placing a PTFE-faced gray butyl rubber septum inside the cap, with the PTFE facing the Scintillation Cocktail. The hole is used to accept the syringe needle that introduces the sample to the Cocktail through the septum.

#### Preparation of a gas chromatograph to measure $O_2$ in the headspace of serum bottles

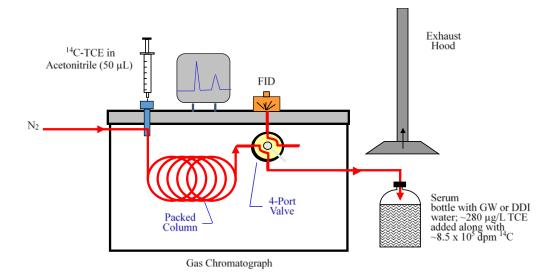
Pack a stainless-steel column with 100/120 Carbosieve S-II support (Supelco) and install on a gas chromatograph (GC) with a thermal conductivity detector (TCD). Supply N<sub>2</sub> at a flow rate of approximately  $50.5 \pm 0.2$  mL/min as the carrier and reference gas. Use an isothermal temperature program of 105 °C; O<sub>2</sub> should elute at 3.3 min. Inject 0.5 mL of room air to determine the response factor (% O<sub>2</sub> per GC peak area unit) of the GC TCD.

Other column packings and temperature programs may be adequate.

### Modification of a gas chromatograph to add <sup>14</sup>C-TCE to the serum bottles

Use gas chromatography to separate <sup>14</sup>C-TCE from impurities (including acetonitrile) in the <sup>14</sup>C-TCE stock solution following the approach of Darlington et al. (2008). Pack a stainless-steel gas chromatography column (44 m x 3.175 mm) with 1 % SP-1000 on 60/80 Carbopack-B (Supelco). Such a column is adequate to separate the <sup>14</sup>C-TCE from the impurities.

Connect the end of the column to a four-port valve in the gas chromatograph (GC) oven. Position the valve so that the valve can be used to direct the flow of carrier gas to either a flame ionization detector (FID) or to a stainless-steel tube that exits the oven and can be used to deliver the flow of carrier gas to the headspace of a serum bottle. The tubing should terminate with in a threaded Luer-Lok<sup>TM</sup> fitting for attachment of a sterile needle, through which the purified <sup>14</sup>C-TCE can be injected into the serum bottle. The configuration is depicted in Figure F1.



**Figure F1.** Experimental setup for use of a GC column to purify the 14C-TCE stock solution before addition to the serum bottles. Use of the 4-port valve allows for a quick transition between delivering the column effluent to the FID for measurements of analytes and delivering the effluent into the serum bottles, as illustrated.

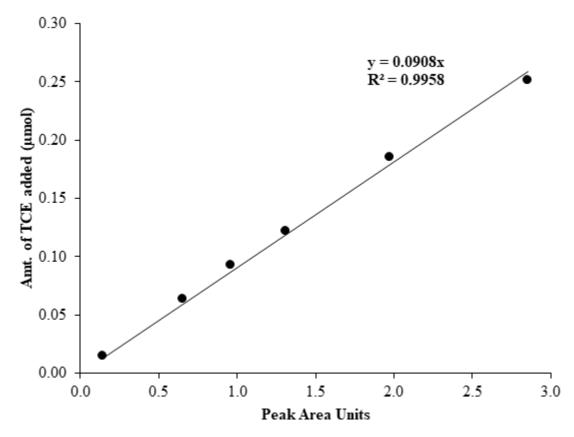
Use high purity N<sub>2</sub> as the carrier gas at a flow rate of  $33.5 \pm 0.5$  mL/min. The temperature program should be 60 °C for 2 min, increasing at 20 °C per min to 150 °C, then increasing at 10 °C to 200 °C and hold at 200 °C for 28.5 min. The extended hold time at 200 °C is designed to ensure that impurities did not accumulate on the column.

Under the conditions described above, the expected elution time for the purified TCE is 9.6 to 11.1 min. During this time window of 1.5 minutes, the four-port valve will be used to direct the flow of carrier gas into the headspace of a serum bottle.

Other column packings and temperature programs may be adequate. Confirm that the packing and program that are employed are adequate by comparing the chromatogram produced when 0.5 mL of headspace from the **TCE/Acetonitrile stock solution** or the **Acetonitrile alone stock solution** is injected into the GC. A comparison of the two chromatograms will distinguish the acetonitrile peak from the TCE peak. The time window used to deliver ~50 mL of carrier gas to the serum bottle should contain the TCE peak, and acetonitrile should not be present in the carrier gas in the time window when TCE is delivered to the headspace of the serum bottle.

#### Calibrate the gas chromatograph used to add <sup>14</sup>C-TCE to the serum bottles to TCE

Use microliter syringes to inject volumes of the **TCE stock solution** ranging from  $10 - 200 \ \mu$ L into 100 mL of DDI water in 160-mL glass serum bottles. Determine the masses of the **TCE stock solution** added to the DDI bottles by weighing the syringe before and after the TCE stock solution is added to the serum bottles ( $\pm 0.0001$  g). Calculate the mass of TCE added to each bottle by multiplying the mass of TCE stock solution added by the concentration of TCE in the stock solution. Place the bottles on an orbital shaker table ( $98 \pm 2$  RPM) for 1 hour to facilitate establishment of equilibrium between the headspace and liquid phases. Take 0.5 mL of headspace from each bottle with a 1.0 mL gas-tight syringe and inject into the GC. Create a calibration curve that compares area of the TCE peak to the amount of TCE added to the bottles. An example calibration curve is presented in Figure F2.



**Figure F2.** A calibration curve to determine the amount of TCE remaining the serum bottles based on analysis of 0.5 mL of headspace from the bottles. The y-intercept on the linear regression linear was set to 0  $\mu$ mol. The amount of TCE added to each bottle was determined through gravimetric analysis. Peak area units are units used in the GC computer software to identify the area under the peak.

#### Prepare a sparging apparatus

The central and critical measurement in the assay is the accumulation of <sup>14</sup>C-labelled transformation products of biological cooxidation. The initial transformation products are a series of organic acids including chloral, 2,2,2-trichloroethanol, trichloroacetic acid, dichloroacetic acid, glyoxylic acid, and formic acid (Wackett, 1995). These chemicals can be metabolized by bacteria to other polar compounds and ultimately to carbon dioxide. While TCE is a neutral compound and can be easily purged from water, the cooxidation degradation products and their further degradation products are polar compounds or anions at high pH. They do not purge from water with a high pH.

The assay measures the accumulation of <sup>14</sup>C from <sup>14</sup>C-TCE into material that does not purge from strongly alkaline solution. For the assay to be reproducible, the purging must be done under standard conditions.

To carry this out, construct a purging apparatus with following properties. Sparging is done from 20 mL scintillation vials. Create a custom holder that tilts the vials at a 30° angle from vertical. This can be conveniently done by drilling holes in a block of wood. Figure F3 shows a purging apparatus that was constructed at Clemson University and used by James Mills for his thesis research.

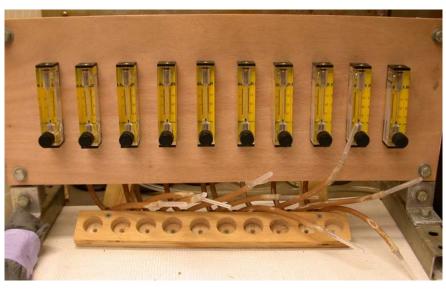


Figure F3. Custom sparging apparatus setup. The flow rate of  $N_2$  gas is controlled using air flow meters connected to thin-walled latex rubber tubing ending with sterilized, disposable needles. The flow meters were connected in parallel behind wooden panel, so that there is only one inlet for  $N_2$  gas. The sparge vials were tilted on a 30-degree angle using a custom wooden holder to ensure complete contact of  $N_2$  gas and liquid.

Construct a manifold so that  $N_2$  gas is passed through flow meters that are capable of regulating the flow to 550 ±50 mL a minute. There is one flow meter for each sample that is sparged. The flow passes through tubing to disposable syringe needles that are inserted in the deepest portion of the vial being sparged.

## Take field samples

In the laboratory, wash and clean 160 mL glass serum bottles, dry, and loosely fit PTFEfaced septa and aluminum crimp caps to the bottles. Autoclave the bottles with septa and caps in place at 121 °C for 20 minutes. Weigh the autoclaved bottles with their respective septa, cap, and labels ( $\pm$  0.01 g). Prepare four 160 mL serum bottles and one 1.0 L plastic bottle for each well. Prepare one bottle with 100 mL of water and cap the bottle with the respective PTFE-faced septa and seal with the aluminum crimp cap. This bottle will be used as a comparison bottle to judge the amount of water collected into the sample bottles in the field. Ship the bottles to the field site.

At the well head, replace any sample tubing used to pump ground water with fresh tubing. Decontaminate any down-hole pumps before use. If possible, remove at least three well volumes of groundwater to get a representative sample.

Using aseptic precautions, pump water from the well and directly add at least 100 mL of groundwater to four sterilized 160 mL glass serum bottles. Add water to the sample bottles until height of water collected matches or exceeds the height in the comparison bottle. Immediately cap the sample bottles with their respective PTFE-faced septa and seal with the aluminum crimp cap. Check to see the caps can be twisted on the serum bottles. If the camp can be twisted, crimp harder until it cannot be twisted. Then fill the 1.0 L plastic bottle with groundwater.

Store all the samples on ice. Ship the samples the same day as collected for next day arrival at the laboratory where the assay will be conducted. Ship the samples with enough ice to ensure that they will arrive at the laboratory at a temperature  $\leq 4$  °C.

## Adding <sup>14</sup>C-TCE to the Bottles

Immediately upon receipt at the laboratory, warm the bottles to room temperature ( $22 \pm 2$  °C), quiescently in the dark, for approximately 24 h before addition of the <sup>14</sup>C-TCE stock solution.

For water from a given well, prepare triplicate serum bottles. The fourth bottle collected in the field is a spare. Filter water from the 1.0 L bottle through a sterile 0.2  $\mu$  filter into a sterile

container. Using aseptic precautions, add 100 mL of the sterilized water to three 160 mL serum bottles and seal with a PTFE-faced septa and aluminum crimp cap as described above. These bottles are the filter sterilized groundwater controls (FSGW).

Record the mass of bottles  $(\pm 0.01 \text{ g})$  to determine the amount of water in each bottle. Subtract the filled weight from the tared weight. Assume 1.0 g of water has a volume of 1.0 mL. If the volume of water exceeds 101 mL, use aseptic precautions to remove enough water to bring the final volume within the range of 100 to 101 mL. Record the final mass of the filled bottle.

To determine amount of <sup>14</sup>C in the <sup>14</sup>C-T<sup>1</sup>CE stock solution, inject 25  $\mu$ L of the <sup>14</sup>C-TCE stock solution directly into 15 mL of Liquid Scintillation Cocktail in a 20-mL scintillation vial. Then count the vial in a Scintillation Counter.

Remove 50 mL headspace from each 160-mL serum bottle filled with ~100 mL water using a 100-mL gas-tight syringe. Inject an aliquot of the <sup>14</sup>C-TCE stock solution (50  $\mu$ L) onto the column of the GC prepared to add <sup>14</sup>C-TCE to the bottles and record the time (day, hour, minute, second). With the four-port valve in the position that supplies carrier gas to the FID, insert the syringe needle into the sample bottle or control bottle. Over the time interval from 9.6 to 11.1 minutes after injection of the <sup>14</sup>C-TCE stock solution into the GC, switch the position of the four-port valve to direct the flow of carrier gas to the sample bottle, then switch the valve to direct flow back to the FID detector and remove the sample bottle or control bottle from the syringe needle.

After the <sup>14</sup>C-TCE is added to bottles with groundwater samples and the FSGW immediately invert the bottles to reduce diffusional losses and place them on an orbital shaker table (98  $\pm$  2 RPM) for approximately 1 h to facilitate establishment of equilibrium between the headspace and liquid phases.

After 1 hr of equilibration, record the time (day, hour, minute), and then sample 0.5 mL of headspace from each bottle using a gas-tight syringe and inject directly into 15 mL of Liquid Scintillation Cocktail in a **specially prepared 20-mL scintillation vial** as described above. Flush the gas-tight syringe at least five times with air between sampling events.

Inject approximately 3 mL of room air into the serum bottle using a 5-mL syringe. This will compensate for the volume of the subsequent liquid samples. Record time (day, hour, minute), then sample 0.1 mL of water from each bottle using a liquid syringe and inject directly into 15 mL of Liquid Scintillation Cocktail in a **specially prepared 20-mL scintillation vial**. Then count the vial in a Scintillation Counter.

The decays per minute (dpm) in these samples are used to calculate the total amount of  $^{14}$ C added to each serum bottle.

Sample 0.5 mL of the headspace from each bottle and inject into the GC that was prepared to add <sup>14</sup>C-TCE to the bottles. Position the four-port valve to direct flow of carrier gas to the FID detector during the entire chromatogram. Record the area of the TCE peak and use the calibration curve (an example is depicted in Figure F2) to determine the amount of TCE in the serum bottle. Addition of <sup>14</sup>C-TCE should result in a TCE level of 0.2 to 0.3  $\mu$ mol per bottle, or an aqueous phase concentration of 214 to 322  $\mu$ g/L when taking into account partitioning between the headspace and liquid phases.

Using 5 mL liquid syringe, withdraw a 3- mL liquid sample from each serum bottle. Flush the syringe at least 5 times between sampling events. Record the time (day, hour, minute). This sample will be used to determine the amount of <sup>14</sup>C that cannot be spared from the water at high pH. Transfer the sample to a 20-mL scintillation vial, then add 12  $\mu$ L 8 M NaOH with a 100  $\mu$ L liquid syringe. Check the pH with a pH strip to make sure it is above pH 10.5. If it is not, add more NaOH solution. Place the vial in the sparging apparatus and sparge with N2 gas at 550 ± 50 mL per minute for 30 minutes. Then add 15 of Liquid Scintillation Cocktail and count the vial in a Scintillation Counter.

## Scintillation Counting

Count beta radiation using a scintillation counter with an ultra-low-level spectrometer and lead shielding to block external cosmic radiation. Prepare a quench correction curve and convert counts per minute to decays per minute.

The headspace and liquid samples from the serum bottles can be counted as soon as they are collected. Store the sparged alkaline liquid samples quiescently in the dark for approximately 24 h before counting to reduce chemilumenscence that is caused by mixing a sample with high pH with the Liquid Scintillation Cocktail.

#### Long Term Incubation

Incubate the serum bottles quiescently in the dark, at room temperature. In addition to the time zero sample described above, sample seven times over a period of 40 to 46 d. Recommended intervals are 3, 7, 14, 21, 28, 35, and 42 days after <sup>14</sup>C-TCE is added to the bottles.

At each sampling event, weigh the serum bottles after the water samples have been taken to calculate the reduction in volume of water, and corresponding increase in the volume of headspace in the bottle that was caused by the removal of the water sample.

At each sampling event, conduct the following sampling to determine the total <sup>14</sup>C remaining. Collect a 0.5 mL headspace sample and add the sample to 15 mL of Liquid Scintillation Cocktail in a **specially prepared 20-mL Scintillation Vial**, and then count beta decays on a Liquid Scintillation Counter. Collect a 0.1 mL liquid sample, add to 15 mL Liquid Scintillation Cocktail in a **specially prepared 20-mL Scintillation Vial**, and then count beta decays on a Liquid Scintillation Counter.

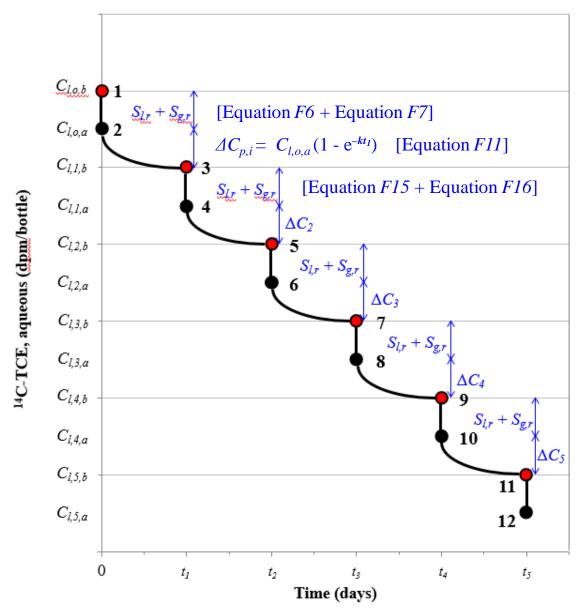
At each sampling event, collect a 3.0 mL aqueous phase sample and dispense to a 20 mL Scintillation Vial. Add NaOH to  $pH \ge 10.5$ , and sparge with N<sub>2</sub> at 550 ± 50 mL per minute for 30 minutes. Add 15 mL of Liquid Scintillation Cocktail, store at room temperature in the dark for 24 hours, then count beta decays on a Liquid Scintillation Counter.

At each sampling event, determine if the supply of oxygen is limiting to biological cooxidation of TCE. Collect a 0.5 mL of the headspace from the bottles containing groundwater, and analyze for  $O_2$  using the GC with a TCD.

If the concentration of oxygen is less than 5% (v/v), stop further incubation of the bottle, and do not use data from the current samples in calculations of the rate constant.

#### Calculations to extract a first order rate constant

Figure F4 provides an overview of the procedure used to extract the first order rate constants. The figure presents the quantity of <sup>14</sup>C-TCE in the water in the serum bottle as a function of time in the assay. Only the <sup>14</sup>C-TCE in the water is subject to co-oxidation by oxygenase enzymes. The first point is labeled  $C_{l,0,b}$ . This refers to the *original* concentration of <sup>14</sup>C in the *liquid* (water) in the bottle, *before* the samples are taken.



**Figure F4.** General overview of sampling events and respective equations used to generate firstorder rate constants. The red circles indicate the  ${}^{14}C$  in the aqueous phase before sampling and the black circles indicate the  ${}^{14}C$  in the aqueous phase after sampling.

## <sup>14</sup>C Calculations for Conditions at Time Zero

To begin the assay, the serum bottle is weighed to determine the mass of water in the bottle, and the volume of *liquid* (which is water) in the bottle ( $V_{l,b}$ ). The volume of the water is subtracted from the total volume (160 mL) to calculate the volume of *gas* in the headspace of the

*bottle* ( $V_{g,b}$ ). The following equation are used to calculate the total amount of <sup>14</sup>C present per bottle at the beginning of the assay ( $C_{tot,o}$ ), based on measurements taken before incubation began:

$$C_{tot,0} = \frac{S_l}{V_{l,s}} \cdot V_{l,b} + \frac{S_h}{V_{g,s}} \cdot V_{g,b}$$
(F1)

where  $C_{tot,0}$  = total dpm in a serum bottle;  $S_l$  = dpm in liquid sample;  $V_{l,s}$  = volume of liquid sample (0.1 mL); and  $V_{l,b}$  = volume of liquid in a serum bottle (~100 mL);  $S_h$  = dpm in a headspace sample;  $V_{g,s}$  = volume of headspace sample (0.5 mL);  $V_{g,b}$  = volume of headspace in a serum bottle (160mL -  $V_{l,b}$ ).

The *original* concentration of <sup>14</sup>C-TCE in *liquid* in the bottles *before* sampling ( $C_{l,o,b}$ ) are calculated based on the total <sup>14</sup>C-TCE present at the beginning of the assay ( $C_{tot,0}$ ) and Henry's Law. From Henry's Law:

$$H_c = \frac{C_{g,o,b}}{V_{g,b}} \Big/ \frac{C_{l,o,b}}{V_{l,b}} \tag{F2}$$

where  $C_{g,o,b}$  = total dpm in headspace *gas* in the serum bottle *before* sampling,  $C_{l,o,b}$  = total dpm in the *liquid* (water) in the serum bottle *before* sampling,  $V_{l,b}$  = the original volume of *liquid* in the bottle (~100 mL);  $V_{g,b}$  is the original volume of *gas* in the headspace of the bottle (~60 mL); and  $H_c$ is the dimensionless Henry's Law constant for TCE (0.349 at 23 °C, Gossett, J.M., 1987.

Due to the law of conservation of mass and the distribution of phases in the serum bottles:

$$C_{g,o,b} = C_{tot,o} - C_{l,o,b} \tag{F3}$$

where  $C_{tot,0}$  = total dpm in the bottle (determined using Equation *F1*).

Substituting equation F3 in equation F2, and solving for  $C_{l,o,b}$  produces equation F4.

$$C_{l,o,b} = C_{tot,o} \left( \frac{V_{l,b}}{V_{l,b} + V_{g,b}H_c} \right)$$
(F4)

#### <u>*C*<sub>*l,o,b*</sub> in equation *F4* corresponds to point 1 on Figure F4.</u>

The sampling removed some of the <sup>14</sup>C. The sampling also removed some of the water from the serum bottle, which changed the ratio of water to gas and thus the distribution of <sup>14</sup>C-TCE between the headspace and water in the serum bottle. Calculate the effect of removing the samples

on the concentration of <sup>14</sup>C in the water in the serum bottle before incubation. The dpm removed due to withdrawal of the liquid at time zero ( $S_{l,r}$ ) are calculated as follows:

$$S_{l,r} = C_{l,o,b} \left( \frac{V_{l,r}}{V_{l,b}} \right) \tag{F5}$$

where  $V_{l,r}$  = volume of liquid sample removed (3.1 mL = 3.0 mL for the sparging test + 0.1 mL for direct addition to the Liquid Scintillation Cocktail); and  $V_{l,b}$  = the initial volume of liquid in the bottle (~100 mL).

<sup>14</sup>C is also removed during gas sampling. For the groundwater bottles, gas samples were removed to determine the total <sup>14</sup>C in the headspace (0.5 mL) and to measure O<sub>2</sub> (0.5 mL). The amount of <sup>14</sup>C removed in these samples ( $S_{g,r}$ ) is calculated as follows:

$$S_{g,r} = \left(C_{tot,o} - C_{l,o,b}\right) \left(\frac{V_{g,r}(0.5)}{V_{g,b}} + \frac{V_{g,r}(0.5)}{V_{g,b} + V_{l,r}}\right)$$
(F6)

where  $V_{g,r}$  = total volume of gas removed at a sampling event (1.0 mL); and  $V_{g,b}$  = total volume of gas in the bottle before the samples were removed.

For the DDI water controls and FSGW controls, only one headspace sample is removed per sampling event. To determine the total <sup>14</sup>C in the headspace; it is not necessary to measure  $O_2$ in these bottles. Consequently, the amount of <sup>14</sup>C removed in the gas phase of the controls simplified to:

$$S_{g,r} = \left(C_{tot,o} - C_{l,o,b}\right) \left(\frac{V_{g,r}}{V_{g,b}}\right) \tag{F7}$$

where  $V_{g,r}$  = total volume of gas removed at a sampling event (0.5 mL).

The total <sup>14</sup>C removed during each sampling event ( $S_{tot,r}$ ) is:

$$S_{tot,r} = S_{l,r} + S_{g,r} \tag{F8}$$

#### Equation F8 is used to determine the vertical line from point 1 to 2 in Figure F4.

The calculated <sup>14</sup>C-TCE concentration in the bottle after the initial sampling event ( $C_{tot,o,a}$ ) is:

$$C_{tot,o,a} = (C_{tot,o}) - (S_{tot,r})$$
(F9)

Therefore, the <sup>14</sup>C-TCE liquid concentration in the bottle after the initial sampling event ( $C_{l,o,a}$ ) is the product of  $C_{tot,o,a}$  and the fraction of TCE in the aqueous phase. Correcting for the changes in the volume of liquid after sampling, and following the logic of equation *F4*:

$$C_{l,o,a} = C_{tot,o,a} \left( \frac{V_{l,b} - V_{l,r}}{(V_{l,b} - V_{l,r}) + (V_{tot} - (V_{l,b} - V_{l,r})) \times H_C} \right)$$
(F10)

where  $V_{tot}$  = total volume of the serum bottles (160 mL).

## <u>*C*<sub>*l,o,a*</sub> in equation *F8* is Point 2 in Figure F4.</u>

# Production of <sup>14</sup>C Degradation Products based on a First Order Rate Constant

The *predicted* increase in <sup>14</sup>C products formed during incubation between sampling points  $(\Delta C_{p,i})$  is calculated by evaluating first-order degradation reaction kinetics using the value for the previous <sup>14</sup>C-TCE concentration in the aqueous phase  $(C_{l,i-l,a})$  and the pseudo first-order rate constant (*k*):

$$\Delta C_{p,i} = C_{l,i-1,a} \left( 1 - e^{-k(t_i - t_{i-1})} \right) \tag{F11}$$

where  $t_i$  represents the time elapsed since <sup>14</sup>C-TCE is added to the serum bottles at each i*ndividual* sequential sampling time as depicted in the x-axis of Figure F4.

Equation *F11* represents the curved path from points 2 to 3, 4 to 5, 6 to 7, 8 to 9, and 10 to 11 in Figure F4. Values of  $(\Delta C_{p,i})$  are represented by  $\Delta_1$ ,  $\Delta_2$ ,  $\Delta_3$ ,  $\Delta_4$ , and  $\Delta_5$  for individual sampling times t<sub>1</sub>, t<sub>2</sub>, t<sub>3</sub>, t<sub>4</sub>, and t<sub>5</sub> in Figure F4.

Prediction of the accumulated <sup>14</sup>C degradation products in the serum bottle at particular sampling event ( $\Sigma \Delta C_{p,i}$ ) is calculated as the sum of ( $\Delta C_{p,i}$ ) and the previous summation of the products ( $\Sigma \Delta C_{p,i-1}$ ):

$$\Sigma \Delta C_{p,i} = \Delta C_{p,i} + \Sigma \Delta C_{p,i-1} \tag{F12}$$

where  $i \ge 1$ .

The calculation of the accumulation of degradation products  $(\Sigma\Delta C_{p,i})$  depends on the previous values for <sup>14</sup>C-TCE in the liquid phase in the serum bottles  $(C_{l,i,a})$ , and the values of  $(C_{l,i,a})$  are influenced by <sup>14</sup>C-TCE that is removed from the bottles during sampling. It is necessary to correct  $(C_{l,i,a})$  for sampling. In each time step, 3.1 mL of water is removed for analysis. As a result, the volume of liquid before sampling in each time step  $(V_{l,i})$  is calculated as follows;

$$V_{l,i} = V_{l,i-1} - 3.1 \, mL \tag{F13}$$

where  $i \ge 1$ , and  $V_{l,1-1} = V_{l,0} = V_{l,b}$ .

The volume of air in the headspace before sampling in each time step is calculated as follows:

$$V_{g,i} = V_{g,i-1} + 3.1 \, mL \tag{F14}$$

where  $i \ge 1$ , and  $V_{g,1-1} = V_{g,0} = V_{g,b}$ .

In each time step, The amount of <sup>14</sup>C removed due to withdrawal of the liquid  $(S_{l,r})$  is calculated as follows:

$$S_{l,r} = C_{l,i,b} \left( \frac{V_{l,r}}{V_{l,i}} \right) \tag{F15}$$

where  $V_{l,r}$  = volume of liquid sample removed (3.1 mL = 3.0 mL for the sparging test + 0.1 mL for direct addition to LSC).

The amount of <sup>14</sup>C removed from the gas in the experimental bottles is calculated as follows:

$$S_{g,r} = (C_{tot,i-1} - C_{l,i,b}) \left( \frac{V_{g,r}(0.5)}{V_{g,i}} + \frac{V_{g,r}(0.5)}{V_{g,i} + V_{l,r}} \right)$$
(F16)

where  $V_{g,r}$  = volume of gas sample removed (0.5 mL for Liquid Scintillation Counting plus 0.5 mL for O<sub>2</sub> determination). No oxygen sample is taken from the DDI water and FSGW control bottles, and  $S_{g,r}$  is calculated as follows:

$$S_{g,r} = (C_{tot,i-1} - C_{l,i,b}) \left(\frac{V_{g,r}}{V_{g,i}}\right)$$
(F17)

where  $V_{g,r} = 0.5$  mL.

The total removal due to sampling  $(S_{tot,r})$  corresponds to:

$$S_{tot,r} = S_{l,r} + S_{g,r} \tag{F18}$$

<u>The total removal due to sampling is represented by the vertical lines between points 3 to</u> 4, 5 to 6, 7 to 8, 9 to 10, and 11 to 12 in Figure F4.

The combined effect of sampling and biodegradation on the amount of <sup>14</sup>C in the liquid phase in the bottles at the end of a time period ( $C_{l,i,b}$ ) is calculated in two steps. First, the combined effect on the total amount of <sup>14</sup>C in the bottle ( $C_{tot,i}$ ) is calculated, and then Henry's Law is applied to calculate the effect on the <sup>14</sup>C in the liquid phase. The value of  $C_{tot,i}$  is calculated as follows:

$$C_{tot,i} = C_{tot,i-1} - S_{t,r} - \Delta C_{p,i} \tag{F19}$$

where  $i \ge 1$ , and  $C_{tot,1-1} = C_{tot,0} = C_{tot,0}$  as described in equation S1.

Following the logic in equation F3, the value of  $C_{l,i,a}$  is calculated from  $C_{tot,i}$  as follows:

$$C_{l,i,a} = C_{tot,i} \left( \frac{V_{l,i}}{V_{l,i} + V_{g,i} \times H_C} \right)$$
(F20)

where  $i \ge 1$ .

#### Equation F20 is used to determine points 4, 6, 8, 10, and 12 in Figure F4.

In addition,  $\Delta C_{p,i}$  (Equation 11) is used to determine the concentration of <sup>14</sup>C-TCE in the liquid phase ( $C_{l,i,b}$ ):

$$C_{l,i,b} = C_{l,i-1,a} - \Delta C_{p,i} \tag{F21}$$

where  $i \ge 1$ , and  $C_{l,1-1,a} = C_{l,0,a} = C_{l,o,a}$  as described in equation *F10*.

## Equation F21 corresponds to points 3, 5, 7, 9 and 11 in Figure F4.

# Direct Measurement of <sup>14</sup>C Degradation Products

Collate the data collected on the amount of <sup>14</sup>C in that could not be purged from a 3.0 mL sample of water from the serum bottles. The dpm that could not be purged is the quantity of transformation products in the sample ( $\Sigma\Delta C_p$ ) that accumulated in the water up to that individual sampling time. Subtract the dpm in the 3.0 mL sample at time zero ( $\Sigma\Delta C_o$ ) from the dpm at each individual sampling period ( $\Sigma\Delta C_p$ ) to produce a corrected value for the dpm that had accumulated in degradation products ( $\Sigma\Delta C_p$ ).

$$\Sigma \Delta C_{p,c} = \Sigma \Delta C_p - \Sigma \Delta C_o \tag{S22}$$

The *measured* dpm in transformation products that accumulated in the serum bottle  $(\Sigma \Delta C_{m,i})$  by the *i*<sup>th</sup> sampling period is calculated as follows:

$$\Sigma \Delta C_{m,i} = \Sigma \Delta C_{p,c} * V_{l,i} / V_{ps}$$
(S23)

Where  $V_{l,i}$  is the volume of liquid in the serum bottle before the *i*<sup>th</sup> sample is taken, and  $V_{ps}$  is the volume of the purged sample (3.0 mL), and  $i \ge 1$ .

## Extract a First Order Rate Constant

A spreadsheet titled **14C RESULTS example.xlsx** is provided as a separate file. The spreadsheet is a template that illustrates the calculations discussed above that can be used to

extract a first order rate constant from the data provided by the assay. The template applies the calculations to model data provided from the <sup>14</sup>C assay of groundwater and filter-sterilized groundwater from monitoring well MW-02-019 at the former Plattsburgh AFB.

Populate the tabs *data groundwater* and *data FSGW* with data from your assay. Then examine the tabs *Model, Groundwater* and *Model, FSGW*. Examine the data input to cells **E6** to **E9**, and correct if necessary. It may be necessary to adjust the number of rows corresponding to time steps, based on the time steps in your assay. Examine the data in column **U** and **V** of tab *Model, Groundwater* and column **T** of tab *Model, FSGW* to ensure that the summary data were copied over correctly from the *data groundwater* and *data FSGW* tabs.

To extract a first order rate constant for co-oxidation of TCE (*k*), enter an initial value of *k* in cell **E2** of Tab *Model, Groundwater* and in cell **E2** of tab *Model, FSGW*. This is a guess or estimate. Then use the Solver application in the Data Analysis menu of Excel to extract a value of *k* that minimizes the sum of the squares of the differences between the measured values of  ${}^{14}C$  in transformation products ( $\Sigma\Delta Cm$ ,i) and the predicted values for  ${}^{14}C$  in transformation products ( $\Sigma\Delta Cp$ ,i). The sum of squares is cell **Y68** of Tab *Model, Groundwater* and cell *W30* of Tab *Model, Groundwater* in the example spreadsheet.

The spreadsheet also provides a chart comparing the model provided by the best fit value of k to the actual data for groundwater and a second chart comparing the model provided by the best fit value of k to the actual data for the filter sterilized groundwater controls.

Following equation *S24*, the net rate constant for biological cooxidation ( $k_{net}$ ) is the rate constant for the water samples minus the rate constants for the filter sterilized controls.

$$k_{net} = k_{water \ samples} - k_{FSGW} = 0.159 - 0.029 \ per \ year = 0.13 \ per \ year$$
 (S24)

In the example, the rate constant for the water samples was 0.159 per year and the rate constant for the FSGW controls was 0.029 per year. The rate constant for biological cooxidation is 0.13 per year.

Use a Student's t-test to determine if the rate constant for the groundwater samples is statistically different from the FSGW control ( $\alpha = 0.05$ ). If it is different, calculate a confidence interval for the net rate by propagation of error using the standard deviations of the rate constants.

## REFERENCES

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- Gossett, J. M. Measurement of Henry's law constants for C1 and C2 chlorinated hydrocarbons. *Environ. Sci. Technol.* 1987, 21 (2), 202–208.